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OCEANOGRAPHIC DATA REPORT D'IBERVILLE FIORD, ELLESMERE ISLAND, N.W.T. March to April 1974 August 1974

by
Frozen Sea Research Group

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February, 1975

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PACIFIC MARINE SCIENCE REPORT 75-1

OCEANOGRAPHIC DATA REPORT
D'IBERVILLE FIORD, ELLESMERE ISLAND, N.W.T.
MARCH TO APRIL 1974

AUGUST 1974

by

FROZEN SEA RESEARCH GROUP

INSTITUTE OF OCEAN SCIENCES, PATRICIA BAY
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This is a manuscript which has received only limited circulation. On citing this report in a bibliography, the title should be followed by the words "UNPUBLISHED MANUSCRIPT" which is in accordance with accepted bibliographic custom.

INTRODUCTION

This report is the second in a series of oceanographic data reports listing information obtained from d'Iberville Fiord, Ellesmere Island, N.W.T. An earlier report (F.S.R.G., 1973) covers data collected in the period March to April 1973.

D'Iberville Fiord, an appendage to the Nansen Sound - Greely Fiord system of northwestern Ellesmere Island is located at 80°30' N, 79°00' W as shown in Figure 1. The fiord is about 35 km by 6 km with an area of 213 km^2. Data collected to date indicates a sill is located across the mouth of the fiord with a maximum depth near 200 m. The maximum depth inside the fiord is about 560 m. One outlet glacier from the large ice cap on the Victoria and Albert Mountains terminates in an ice shelf at the head of the fiord. The east end of d'Iberville Fiord and the ice shelf are illustrated in Figure 2.

During the period September to July, the fiord is completely covered with sea ice which remains landfast until shore leads develop in June. The sea ice cover normally consists of extensive young (annual) sea ice with some patches of second-year ice. Areas of rafted and hummocked ice may also occur. These latter areas cannot normally be traversed by a tracked vehicle train and hence must frequently be excluded as potential sites for the collection of oceanographic data during normal spring operations. One such area of interest is often the first few miles at the head of the fiord adjacent to the glacier where the profusion of icebergs calving off the glacial shelf leaves the sea ice in a chaotic state. In about fifty per cent of summers, the fiord remains largely covered with sea ice and icebergs from the glacier tend to be retained near the head of the fiord. In the remaining summers, the fiord clears of sea ice allowing icebergs to move out. Figure 2 is a good illustration of a relatively ice free August.

In d'Iberville Fiord, sea ice is normally evenly covered by 30 to 40 cm of snow. A layer of depth hoar usually exists next to the ice surface and is evidence of heat conduction from the ocean to the atmosphere. The inner two-thirds of the fiord is protected from wind by the surrounding mountains so that snow there is typically light and powdery. In contrast, the more exposed areas at the mouth of the fiord and in Greely Fiord are typically covered with dense wind packed snow (sastrugi). The sea ice thickness reflects this variation in the density of insulating snow cover.

The fiord had its normal winter ice cover in March and April 1974, and was partially ice free in August 1974. In spring data were collected from a tracked vehicle and oceanographic sleigh. The operation of this system is described by Lewis (1971). In summer data were collected with the use of a small vessel, the Mudhen . The tracked vehicle with sleigh and the vessel are shown in Figure 3 with typical ice cover being illustrated in each case. The in-situ CTD instrument and data recording equipment were similar in both cases and are described below.

The locations of each experiment are shown in Figure 1 and are identified by experiment number. The experiments numbered in the 900's were undertaken in March and April while those numbered in the 1000's were done in August.

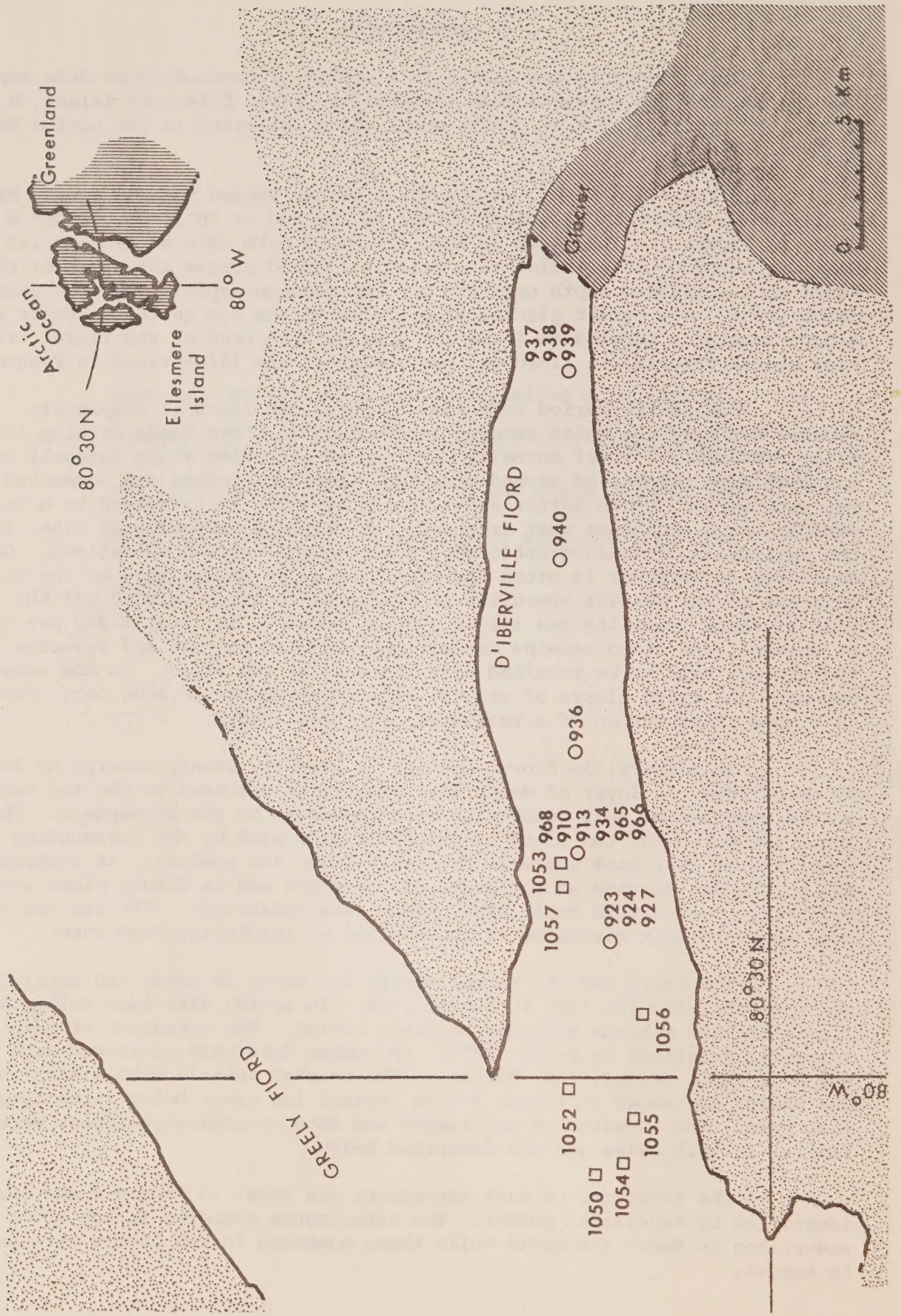

Greenland
Arctic Ocean
80° W
80° 30 N
Ellesmere Island
Glacier
0 5 Km
D'IBERVILLE FIORD
937
938
939
940
936
968
910
913
934
965
966
1053
1057
923
924
927
1056
GRELY FIORD
1052
1055
1050
1054
80° 30 N
80° W

FIGURE 1

Data included in this report are limited to conductivity, temperature, pressure and derived parameters such as salinity, sigma-T and sound velocity. Other data collected but not reported here are meteorological parameters, water levels (tides), current profiles and current time series measurements, and time lapse photography of ice movement, fresh water runoff and snow melt.

The physical oceanography of the area has been reported on by Ford and Hattersley-Smith (1965) and Hattersley-Smith and Serson (1966). The Frozen Sea Research Group has been working in d'Iberville Fiord since 1969 and results of their early oceanographic observations have been reviewed by Lake and Walker (1973).

Data Recording

Conductivity (C), temperature (T) and pressure or depth (D) measurements were taken with Guildline Model 8101A CTD units. To monitor the accuracy of the CTD measurements water samples were taken from time to time with oceanographic bottles. These water samples were run through a Hytech Model 6220 bench salinometer calibrated with Standard Sea Water. Thermistors used to check water temperatures were calibrated in a triple point cell. Values obtained from bench salinometer and thermistor were compared to the CTD values obtained coincidentally and temperature and salinity corrections were determined. A detailed discussion of our methods of in situ measurements of conductivity and temperature can be found in Lewis and Sudar (1972).

The principal recording system for output of the Guildline instrument was a Vidar 5400 data logger with printed and punched paper tape output.

Data Processing

Salinity values determined from CTD data occasionally indicated statically unstable water structure. Where these apparent instabilities could be attributed to insufficiently fast initial instrument lowering speeds or to sharp vertical gradients the conductivity values were discarded.

Data Processing - Equations

(a) Salinity

The Perkin-Walker equation (Perkin and Walker, 1972) was used to calculate salinity (S) from values of conductivity (C), temperature (T) and pressure (P). The equation is a numerical fit to the experimental data of Brown and Allentoft with a linear pressure correction. The temperature values used are with respect to the International Practical Temperature Scale of 1968 (Comite International des Poids et Mesures, 1969).

Where units are C(mmho/cm), T(°C), P(db), S(°/$_{oo}$) the equations used were:

$$C(S.T.O) = C(S.T.P)\left[1 + P\left\{49436+1567T+21.33T^2+554.43C(S.T.P)\right\}^{-1}\right]^{-1}$$

$$R_t = C(S.T.O)\left[29.03916\ (1+.0297175T+.00015551T^2-.000000789T^3)\right]^{-1}$$


ICE
SHELF
ICE CAP
1 KM
SEA ICE
ICEBERGS
N

FIGURE 2

East end of d'Iberville Fiord. About a third of the fiord is shown. The photo was taken from an aircraft in August 1959. (National Air Photo, A-16693-20)





FIGURE 3

(a) Tracked vehicle (Arctic Research Unit) pulling an oceanographic sleigh containing winch, electronic data logger and a variety of oceanographic instruments. A powered drill rig can be quickly assembled on the front of the vehicle to drill holes up to 12 inches in diameter through sea ice. The dome on the roof of the vehicle contains a radar antenna.

FIGURE 3

(b) The Mudhen is the covered vessel on the right and contains a winch, data logger and oceanographic instruments identical to those used in the sleigh in winter.

$$R_o = R_t - 10^{-5}\left[6.0 + 380\sin\pi\left\{\frac{R_t+.04}{1.03}\right\} + 15\sin 3\pi\left\{\frac{R_t+.04}{1.03}\right\}\right] \times \begin{bmatrix} .0777T-.000454T^2 \\ -.000018T^3 \end{bmatrix}$$

$$S = -.5933 + 32.4822R_o + 3.1106R_o^2 + .004\sin 2\pi\left[\frac{R_o-.64}{.57}\right] \quad \text{for } 0.4 \leq R_o \leq 1.2$$

$$S = -.2166 + 30.686R_o + 5.247R_o^2 \quad \text{for } 0.14 \leq R_o \leq 0.4$$

A correction must be added to salinities calculated from the above equations where temperatures fall below +1.0° C. The correction, based on Dauphinee's work, is

$$\Delta S = \delta[(-3.6 + 5.0T - 2.45T^2)10^{-3}]$$

where $\delta = 1$ for $-2° < T < 1°C$, $\delta = 0$ for $T \geq 1°C$

(b) Sigma τ

The sigma τ equation was taken from the work of Cox, McCartney and Culkin (1970).

$$\sigma_t = \Sigma_i \Sigma_j \; A_{ij} \; T^i S^j$$

i	j	A_{ij}
0	0	$8.00969062 \times 10^{-2}$
0	1	$7.97018644 \times 10^{-1}$
0	2	$1.31710842 \times 10^{-4}$
0	3	$-6.11831499 \times 10^{-8}$
1	0	$5.88194023 \times 10^{-2}$
1	1	$-3.25310441 \times 10^{-3}$
1	2	$2.87941530 \times 10^{-6}$
2	0	$-8.11465413 \times 10^{-3}$
2	1	$3.89187483 \times 10^{-5}$
3	0	$4.76600414 \times 10^{-5}$

(c) Sound Velocity

Sound speed (V) was calculated using Wilson's (1960) equation where salinity (S) is in °/₀₀, pressure (P) in db and V in $msec^{-1}$.

$$V = \Sigma_{ijk} \; V_{ijk} \; Q^i (S-35)^j \; T^k$$

where $Q = 1.00323 + 0.1019716P$

and where

$V_{ooo} = +1449.14$

$V_{001} = +4.5721$

$V_{002} = -4.4532 \times 10^{-2}$

$V_{003} = -2.6045 \times 10^{-4}$

$V_{004} = +7.9851 \times 10^{-6}$

$V_{010} = +1.39799$

$V_{011} = -1.1244 \times 10^{-2}$

$V_{012} = +7.7711 \times 10^{-7}$

$V_{020} = +1.69202 \times 10^{-3}$

$V_{100} = +1.60272 \times 10^{-1}$

$V_{101} = -1.8607 \times 10^{-4}$

$V_{102} = +7.4812 \times 10^{-6}$

$V_{103} = +4.5283 \times 10^{-8}$

$V_{110} = +7.7016 \times 10^{-5}$

$V_{111} = +3.1580 \times 10^{-8}$

$V_{112} = +1.5790 \times 10^{-9}$

$V_{200} = +1.0268 \times 10^{-5}$

$V_{201} = -2.5294 \times 10^{-7}$

$V_{202} = +1.8563 \times 10^{-9}$

$V_{210} = -1.2943 \times 10^{-7}$

$V_{300} = +3.5216 \times 10^{-9}$

$V_{301} = -1.9646 \times 10^{-10}$

$V_{400} = -3.3603 \times 10^{-12}$

Data Format

Cruise: Cruise number assigned by C.O.D.C.

Title: Location description

Experiment No.: Experiment Number. Each CTD drop was assigned a unique experiment number. Listing is chronological, not by experiment number.

Lat.: Latitude of experimental site

Long.: Longitude of experimental site

Water depth: In meters

Depth Incr.: Vertical increment in meters between sequential readings.

Date: DDMMYY

Local Time: HHMM

Depth: Corresponds to depth of the CTD transducers below water level as indicated by wire length. This is equivalent to depth as currents were negligible. The first depth is noted and the remaining depths are calculated.

Press: Pressure in decibars as read by the CTD pressure transducer.

Sal.: Salinity in parts per thousand ($^{\circ}/_{\circ\circ}$). The letter following the numerical value indicates the accuracy assigned to the value as discussed below.

Temp.: Temperature in degrees Centigrade (°C). The letter following the numerical value indicates the accuracy assigned to the value as discussed below.

Sigmat: Specific gravity anomaly, sigma-T

Sound: Speed of propagation of sound in water in $msec^{-1}$

Accuracy

The error estimate letter coding after temperature and salinity values is adapted from that used by C.O.D.C. Larger inaccuracies reflect the data processing discussed above and occur in regions of vertical gradients. Accuracies indicated in vertically homogeneous water should correspond to the best accuracy possible with the CTD system used. In this vertically homogeneous water accuracy is determined by comparison of CTD data and bottle and thermistor measurements as outlined above. In areas of vertical gradients the accuracy values assigned are subjective.

The numerical value indicated in the table below corresponds to the last (in this case the third) decimal place. Thus salinity accuracies of ±.005 and ±.05 appear as C and F respectively.

Possible Error	Code Letter
±0.005	C
±0.010	D
±0.020	E
±0.050	F

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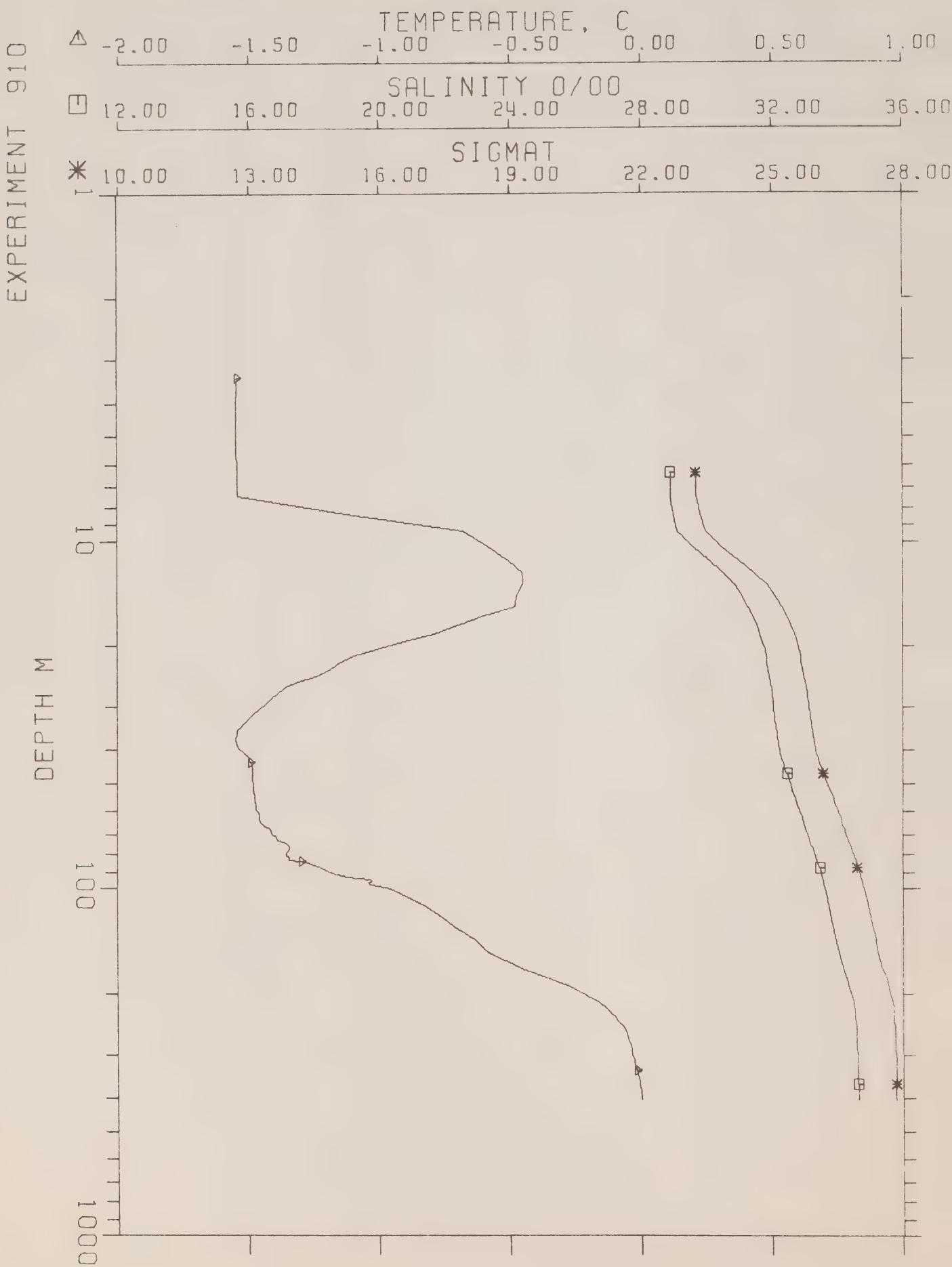
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OCEANOGRAPHIC DATA

MARCH - APRIL 1974


EXPERIMENT 910
TEMPERATURE, C
-2.00
-1.50
-1.00
-0.50
0.00
0.50
1.00
SALINITY 0/00
12.00
16.00
20.00
24.00
28.00
32.00
36.00
SIGMAT
10.00
13.00
16.00
19.00
22.00
25.00
28.00
DEPTH M
10
100
1000

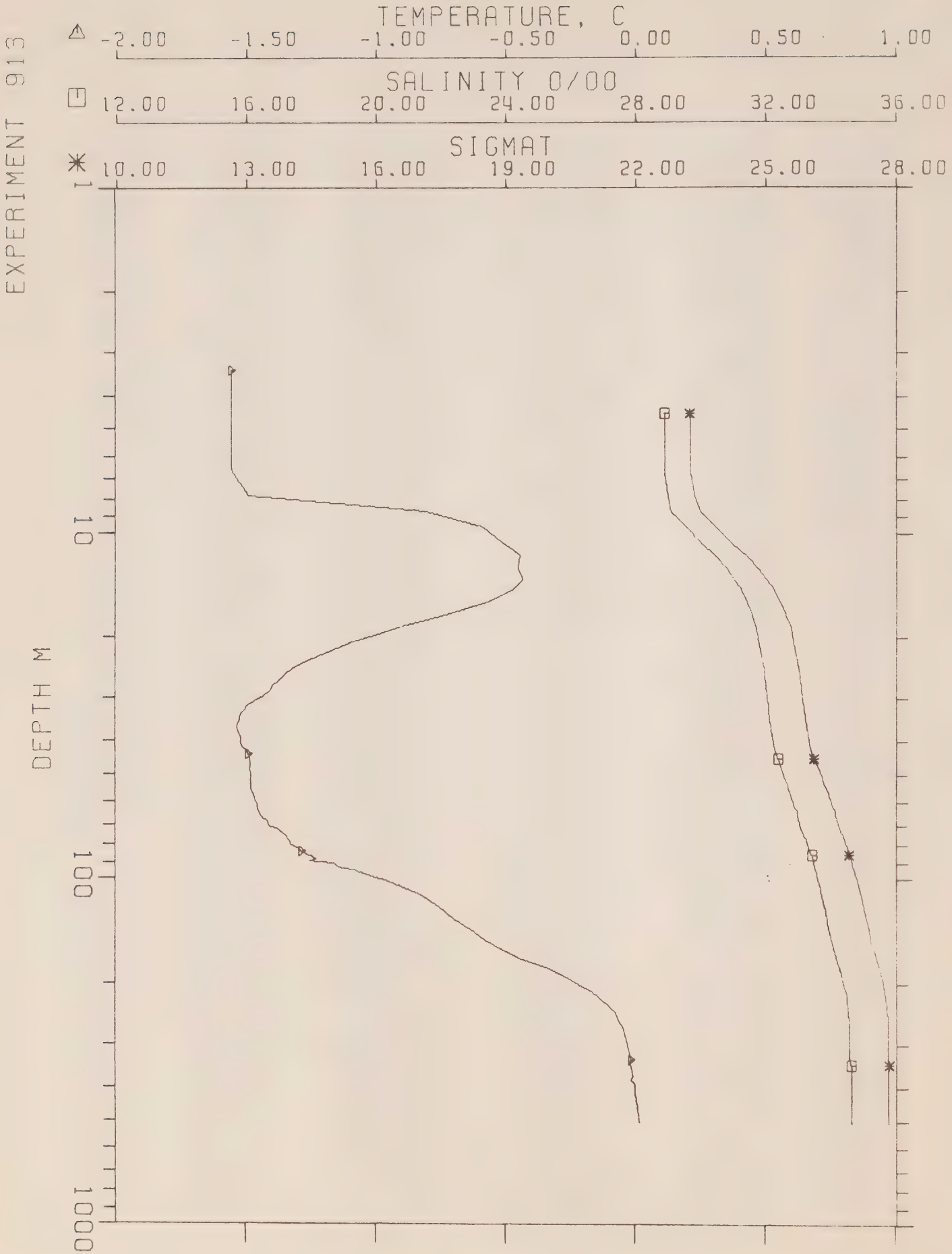
CRUISE 15-74-012 D'IBERVILLE FIORD-74 EXPER NO. 910

LAT N.80-34-45 LONG W.79-25-00 WATER DEPTH 519

DEPTH INCR. DATE 300374 LOCAL TIME 1615

DEPTH	PRES	SAL	TEMP	SIGMAT	SOUND
3.4	3.38		-1.547 E		
4.4	4.37		-1.548 E		
5.4	5.40		-1.548 E		
6.3	6.35	28.918 E	-1.547 E	23.271	1433.7
7.4	7.40	28.911 E	-1.547 E	23.265	1433.7
8.4	8.37		-1.131 E		
9.4	9.38	29.173 E	-0.682 E	23.462	1438.2
10.4	10.38	29.638 E	-0.587 E	23.834	1439.3
11.4	11.38	30.153 E	-0.502 E	24.247	1440.4
12.3	12.34	30.554 E	-0.449 E	24.569	1441.2
13.4	13.38	30.924 E	-0.445 E	24.867	1441.8
14.4	14.40	31.162 E	-0.469 E	25.060	1442.0
15.4	15.38	31.337 E	-0.475 E	25.202	1442.3
16.4	16.39	31.493 E	-0.593 E	25.331	1441.9
17.4	17.41	31.608 E	-0.690 E	25.427	1441.7
18.4	18.43	31.697 E	-0.787 E	25.502	1441.3
19.4	19.41	31.768 E	-0.898 E	25.563	1440.9
20.4	20.41	31.822 E	-0.992 E	25.609	1440.6
21.4	21.43	31.864 E	-1.088 E	25.645	1440.2
22.4	22.44	31.894 E	-1.145 E	25.671	1440.0
23.4	23.43	31.926 E	-1.182 E	25.698	1439.9
24.4	24.44	31.964 E	-1.224 E	25.730	1439.8
25.4	25.43	31.999 E	-1.304 E	25.760	1439.5
26.5	26.46	32.027 E	-1.357 E	25.784	1439.3
27.5	27.45	32.049 E	-1.387 E	25.803	1439.2
28.5	28.45	32.062 E	-1.410 E	25.813	1439.1
29.5	29.47	32.079 E	-1.429 E	25.828	1439.0
30.5	30.47	32.099 E	-1.456 E	25.845	1439.0
31.5	31.46	32.117 E	-1.477 E	25.860	1438.9
32.5	32.54	32.137 E	-1.496 E	25.876	1438.9
33.5	33.50	32.156 E	-1.517 E	25.893	1438.8
34.5	34.52	32.174 E	-1.528 E	25.907	1438.8
35.5	35.51	32.194 E	-1.543 E	25.924	1438.8
36.5	36.54	32.212 E	-1.547 E	25.938	1438.8
37.5	37.53	32.230 E	-1.553 E	25.953	1438.8
38.5	38.53	32.249 E	-1.548 E	25.968	1438.9
39.6	39.59	32.267 E	-1.544 E	25.983	1438.9
40.5	40.51	32.290 E	-1.523 E	26.001	1439.1
41.6	41.58	32.315 E	-1.512 E	26.021	1439.2
42.6	42.56	32.346 E	-1.505 E	26.046	1439.3
43.6	43.63	32.384 E	-1.496 E	26.076	1439.4
44.6	44.60	32.419 E	-1.492 E	26.105	1439.5
45.5	45.54	32.451 E	-1.490 E	26.130	1439.5
46.6	46.57	32.488 E	-1.484 E	26.160	1439.6
47.6	47.55	32.521 E	-1.484 E	26.187	1439.7
48.6	48.61	32.552 E	-1.491 E	26.212	1439.7
49.6	49.60	32.584 E	-1.490 E	26.239	1439.8
50.6	50.62	32.618 E	-1.483 E	26.266	1439.9
51.6	51.59	32.653 E	-1.483 E	26.294	1440.0
52.6	52.62	32.684 E	-1.485 E	26.319	1440.0
53.6	53.61	32.722 E	-1.485 E	26.350	1440.1
54.6	54.64	32.752 E	-1.482 E	26.374	1440.1
55.6	55.62	32.780 E	-1.481 E	26.396	1440.2
56.6	56.65	32.813 E	-1.482 E	26.424	1440.3
57.7	57.67	32.841 E	-1.476 E	26.446	1440.4
58.7	58.75	32.865 E	-1.475 E	26.466	1440.4
59.7	59.68	32.890 E	-1.474 E	26.486	1440.5
60.6	60.65	32.916 E	-1.471 E	26.507	1440.5
61.7	61.73	32.943 E	-1.462 E	26.529	1440.6
62.7	62.72	32.975 E	-1.461 E	26.554	1440.7
63.7	63.69	33.001 E	-1.464 E	26.575	1440.7
64.7	64.74	33.018 E	-1.459 E	26.589	1440.8

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
65.7	65.68	33.038 E	-1.449 E	26.605	1440.9
66.7	66.70	33.060 E	-1.438 E	26.623	1441.0
67.7	67.70	33.078 E	-1.426 E	26.637	1441.1
68.8	68.75	33.101 E	-1.418 E	26.655	1441.2
69.7	69.72	33.124 E	-1.413 E	26.674	1441.2
70.8	70.78	33.147 E	-1.406 E	26.692	1441.3
71.7	71.75	33.166 E	-1.402 E	26.708	1441.4
72.8	72.76	33.189 E	-1.393 E	26.726	1441.5
73.8	73.79	33.212 E	-1.370 E	26.744	1441.6
74.8	74.79	33.244 E	-1.356 E	26.770	1441.8
75.8	75.78	33.266 E	-1.351 E	26.787	1441.8
76.8	76.83	33.286 E	-1.346 E	26.803	1441.9
77.8	77.84	33.307 E	-1.343 E	26.820	1442.0
78.8	78.82	33.332 E	-1.354 E	26.841	1442.0
79.8	79.82	33.354 E	-1.360 E	26.859	1442.0
80.9	80.89	33.375 E	-1.358 E	26.876	1442.0
81.9	81.85	33.394 E	-1.347 E	26.891	1442.1
82.9	82.86	33.414 E	-1.348 E	26.907	1442.2
83.9	83.93	33.423 E	-1.301 E	26.913	1442.4
84.9	84.87	33.444 E	-1.273 E	26.929	1442.6
85.9	85.87	33.463 E	-1.254 E	26.944	1442.7
86.9	86.88	33.477 E	-1.241 E	26.955	1442.8
87.9	87.88	33.491 E	-1.225 E	26.965	1442.9
88.9	88.90	33.505 E	-1.210 E	26.976	1443.1
90.0	89.96	33.517 E	-1.189 E	26.986	1443.2
90.9	90.92	33.533 E	-1.188 E	26.999	1443.2
91.9	91.91	33.545 E	-1.144 E	27.007	1443.5
92.9	92.86	33.562 E	-1.128 E	27.020	1443.6
93.9	93.93	33.573 E	-1.084 E	27.028	1443.8
95.0	94.96	33.588 E	-1.041 E	27.039	1444.1
95.9	95.90	33.601 E	-1.030 E	27.048	1444.1
97.0	96.97	33.618 E	-1.044 E	27.062	1444.1
97.9	97.91	33.629 E	-1.037 E	27.071	1444.2
99.0	98.99	33.639 E	-1.012 E	27.079	1444.3
100.0	100.00	33.654 E	-0.983 E	27.090	1444.5
100.9	100.93	33.671 E	-0.960 E	27.103	1444.7
111.2	111.18	33.777 E	-0.840 E	27.184	1445.5
121.1	121.13	33.860 E	-0.763 E	27.248	1446.2
131.6	131.58	33.931 E	-0.707 E	27.304	1446.7
141.4	141.39	34.012 E	-0.642 E	27.367	1447.3
151.7	151.71	34.071 E	-0.594 E	27.412	1447.7
161.5	161.47	34.146 E	-0.526 E	27.470	1448.3
171.6	171.59	34.228 E	-0.452 E	27.533	1448.9
181.7	181.68	34.321 E	-0.364 E	27.604	1449.7
191.7	191.66	34.408 E	-0.276 E	27.670	1450.3
201.9	201.85	34.464 E	-0.217 E	27.713	1450.9
211.9	211.90	34.512 E	-0.169 E	27.749	1451.3
222.2	222.21	34.549 E	-0.135 E	27.778	1451.7
232.1	232.13	34.566 E	-0.108 E	27.790	1452.0
242.1	242.15	34.581 E	-0.088 E	27.801	1452.3
252.2	252.21	34.597 E	-0.072 E	27.813	1452.5
262.2	262.17	34.606 E	-0.061 E	27.820	1452.8
272.5	272.46	34.617 E	-0.056 E	27.829	1453.0
282.7	282.69	34.616 E	-0.046 E	27.827	1453.2
292.4	292.36	34.621 E	-0.040 E	27.831	1453.4
302.9	302.86	34.631 E	-0.041 E	27.839	1453.6
312.9	312.89	34.627 E	-0.030 E	27.835	1453.8
322.8	322.77	34.632 E	-0.029 E	27.839	1453.9
332.8	332.81	34.630 E	-0.021 E	27.837	1454.1
343.5	343.49	34.632 E	-0.018 E	27.839	1454.3
353.0	352.96	34.634 E	-0.016 E	27.841	1454.5
362.9	362.87	34.635 E	-0.012 E	27.841	1454.7
372.9	372.89	34.636 E	-0.009 E	27.841	1454.9
383.0	383.02	34.635 E	-0.007 E	27.841	1455.0
393.1	393.12	34.637 E	-0.005 E	27.842	1455.2
403.2	403.16	34.637 E	-0.004 E	27.842	1455.4


EXPERIMENT 913
TEMPERATURE, C
-2.00
-1.50
-1.00
-0.50
0.00
0.50
1.00
SALINITY 0/00
12.00
16.00
20.00
24.00
28.00
32.00
36.00
SIGMAT
10.00
13.00
16.00
19.00
22.00
25.00
28.00
DEPTH M
1
10
100
1000

CRUISE 15-74-012 D'IBERVILLE FIORD-74 EXPER NO. 913

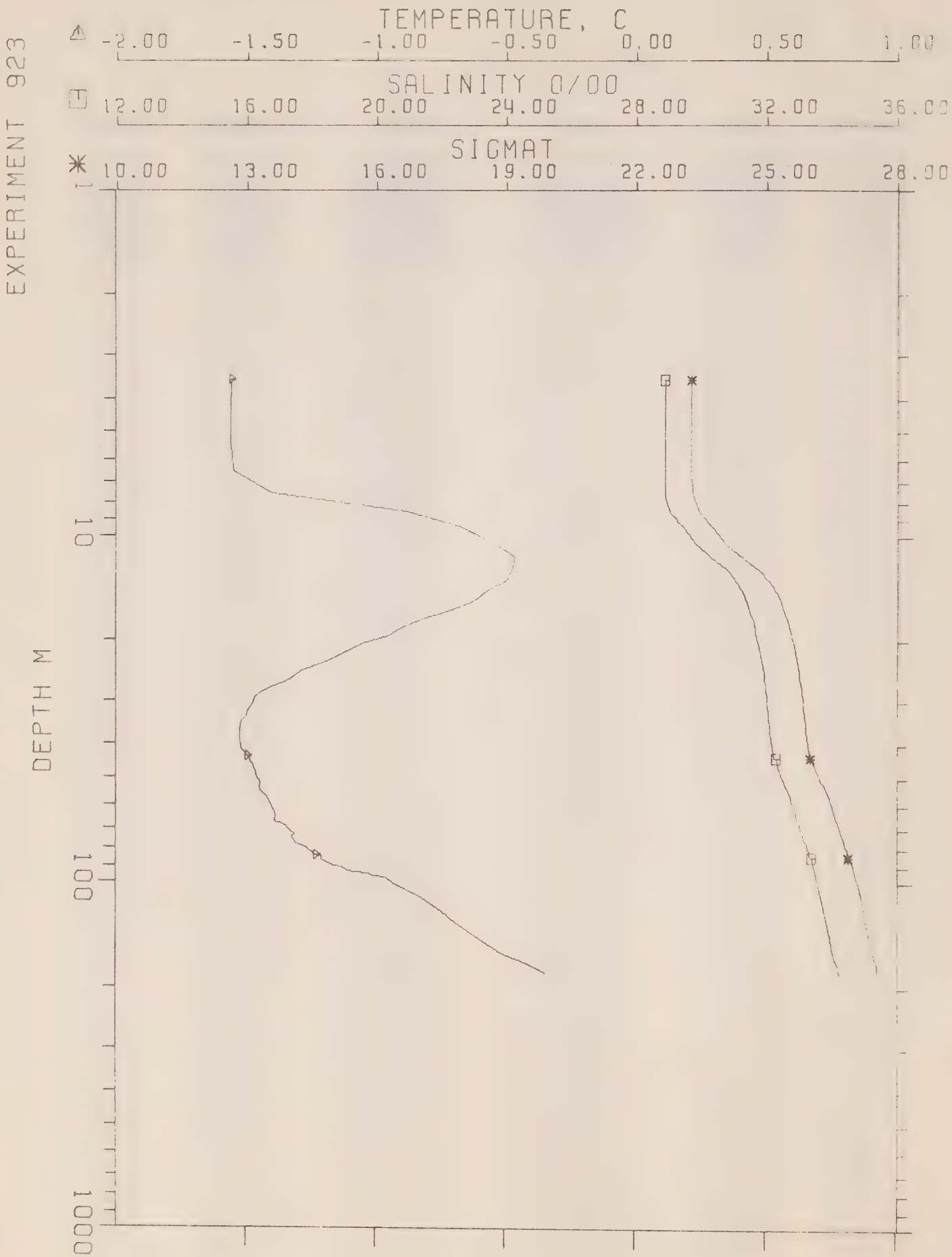
LAT N.80-34-45 LONG W.79-25-00 WATER DEPTH 519

DEPTH INCR. DATE 310374 LOCAL TIME 1000

DEPTH	PRES	SAL		TEMP		SIGMAT	SOUND
3.4	3.38			-1.561	E		
4.5	4.48	28.914	D	-1.562	E	23.268	1433.6
5.5	5.48	28.904	D	-1.561	E	23.260	1433.6
6.6	6.60	28.900	D	-1.561	E	23.257	1433.6
7.8	7.79			-1.496	E		
8.7	8.67	29.176	D	-0.808	E	23.467	1437.6
9.6	9.63	29.637	D	-0.591	E	23.834	1439.3
10.6	10.63	30.081	D	-0.515	E	24.190	1440.2
11.6	11.60	30.536	D	-0.440	E	24.555	1441.2
12.6	12.64	30.876	D	-0.449	E	24.829	1441.7
13.7	13.66	31.119	D	-0.429	E	25.024	1442.1
14.6	14.59	31.312	D	-0.466	E	25.181	1442.2
15.7	15.73	31.465	D	-0.552	E	25.307	1442.1
16.7	16.74	31.594	D	-0.660	E	25.415	1441.8
17.7	17.68	31.685	D	-0.781	E	25.492	1441.3
18.7	18.67	31.761	D	-0.896	E	25.557	1440.9
19.6	19.64	31.808	D	-0.985	E	25.597	1440.6
20.7	20.66	31.847	D	-1.085	E	25.631	1440.2
21.6	21.59	31.881	D	-1.147	E	25.661	1440.0
22.6	22.65	31.919	D	-1.205	E	25.693	1439.8
23.7	23.66	31.952	D	-1.263	E	25.721	1439.6
24.7	24.66	31.982	D	-1.313	E	25.746	1439.4
25.7	25.70	32.006	D	-1.346	E	25.767	1439.3
26.7	26.75	32.028	D	-1.371	E	25.785	1439.2
27.6	27.65	32.048	D	-1.389	E	25.802	1439.2
28.7	28.71	32.066	D	-1.407	E	25.817	1439.1
29.8	29.85	32.082	D	-1.428	E	25.830	1439.1
30.7	30.73	32.101	D	-1.467	E	25.846	1438.9
31.7	31.72	32.121	D	-1.491	E	25.863	1438.8
32.7	32.69	32.134	D	-1.504	E	25.874	1438.8
33.7	33.67	32.155	D	-1.520	E	25.892	1438.8
34.7	34.70	32.170	D	-1.525	E	25.904	1438.8
35.7	35.75	32.185	D	-1.531	E	25.916	1438.8
36.6	36.61	32.201	D	-1.538	E	25.929	1438.8
37.7	37.75	32.222	D	-1.535	E	25.946	1438.9
38.7	38.68	32.241	D	-1.531	E	25.961	1438.9
39.7	39.69	32.266	D	-1.519	E	25.982	1439.0
40.7	40.68	32.293	D	-1.524	E	26.003	1439.1
41.7	41.73	32.319	D	-1.520	E	26.025	1439.1
42.6	42.63	32.349	D	-1.502	E	26.049	1439.3
43.8	43.77	32.382	D	-1.494	E	26.075	1439.4
44.7	44.68	32.414	D	-1.492	E	26.101	1439.5
45.7	45.74	32.444	D	-1.489	E	26.125	1439.5
46.7	46.73	32.485	D	-1.485	E	26.158	1439.6
47.8	47.76	32.522	D	-1.484	E	26.188	1439.7
48.7	48.69	32.563	D	-1.491	E	26.221	1439.7
49.8	49.76	32.598	D	-1.483	E	26.249	1439.9
50.8	50.77	32.630	D	-1.484	E	26.275	1439.9
51.7	51.69	32.665	D	-1.483	E	26.304	1440.0
52.8	52.76	32.700	D	-1.486	E	26.332	1440.0
53.8	53.80	32.729	D	-1.485	E	26.356	1440.1
54.7	54.73	32.754	D	-1.485	E	26.376	1440.1
55.7	55.74	32.785	D	-1.486	E	26.401	1440.2
56.8	56.76	32.817	D	-1.481	E	26.427	1440.3
57.8	57.83	32.842	D	-1.477	E	26.447	1440.4
58.8	58.79	32.871	D	-1.472	E	26.471	1440.4
59.9	59.86	32.900	D	-1.468	E	26.493	1440.5
60.8	60.80	32.922	D	-1.462	E	26.511	1440.6
61.9	61.87	32.953	D	-1.459	E	26.537	1440.7
62.7	62.74	32.982	D	-1.458	E	26.560	1440.7
63.8	63.82	33.001	D	-1.460	E	26.575	1440.8
64.8	64.78	33.017	D	-1.455	E	26.588	1440.8

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
65.9	65.88	33.033 D	-1.448 E	26.601	1440.9
66.8	66.83	33.051 D	-1.439 E	26.615	1441.0
67.9	67.87	33.066 D	-1.428 E	26.627	1441.1
68.9	68.90	33.085 D	-1.421 E	26.642	1441.1
69.8	69.84	33.104 D	-1.418 E	26.657	1441.2
70.9	70.93	33.126 D	-1.409 E	26.676	1441.3
71.9	71.88	33.154 D	-1.387 E	26.697	1441.4
72.9	72.87	33.187 D	-1.376 E	26.724	1441.6
73.9	73.94	33.211 D	-1.365 E	26.743	1441.7
75.0	74.99	33.237 D	-1.354 E	26.764	1441.8
75.9	75.92	33.263 D	-1.346 E	26.785	1441.9
76.9	76.94	33.290 D	-1.343 E	26.806	1441.9
77.9	77.86	33.311 D	-1.339 E	26.823	1442.0
78.9	78.92	33.334 D	-1.329 E	26.842	1442.1
79.9	79.91	33.357 D	-1.335 E	26.860	1442.1
80.9	80.91	33.376 D	-1.321 E	26.875	1442.2
81.9	81.92	33.393 D	-1.303 E	26.888	1442.3
82.9	82.88	33.414 D	-1.293 E	26.905	1442.4
83.9	83.88	33.431 D	-1.290 E	26.919	1442.5
84.9	84.93	33.442 D	-1.280 E	26.927	1442.6
86.0	86.00	33.455 D	-1.262 E	26.938	1442.7
87.0	87.01	33.468 D	-1.247 E	26.948	1442.8
88.0	88.01	33.479 D	-1.223 E	26.956	1442.9
88.9	88.94	33.497 D	-1.260 E	26.972	1442.8
90.0	89.95	33.497 D	-1.222 E	26.970	1443.0
91.0	90.97	33.516 D	-1.167 E	26.984	1443.3
92.0	91.97	33.530 D	-1.155 E	26.995	1443.4
93.0	93.03	33.554 D	-1.152 E	27.014	1443.5
94.0	94.01	33.563 D	-1.119 E	27.021	1443.6
95.0	95.03	33.581 D	-1.088 E	27.034	1443.8
96.0	96.05	33.594 D	-1.064 E	27.044	1444.0
97.0	97.02	33.605 D	-1.051 E	27.052	1444.1
98.0	98.00	33.618 D	-1.028 E	27.062	1444.2
99.0	98.99	33.636 D	-1.019 E	27.076	1444.3
100.0	100.02	33.648 E	-1.006 E	27.086	1444.4
101.1	101.06	33.664 E	-0.968 E	27.097	1444.6
111.1	111.12	33.771 E	-0.836 E	27.179	1445.5
121.2	121.18	33.861 E	-0.758 E	27.249	1446.2
131.2	131.24	33.932 E	-0.705 E	27.304	1446.7
141.4	141.36	34.005 E	-0.642 E	27.361	1447.3
151.5	151.46	34.071 E	-0.584 E	27.412	1447.8
161.5	161.48	34.153 E	-0.514 E	27.475	1448.4
171.5	171.47	34.238 E	-0.439 E	27.541	1449.0
181.6	181.58	34.328 E	-0.351 E	27.609	1449.7
191.7	191.74	34.402 E	-0.276 E	27.665	1450.3
201.8	201.84	34.445 E	-0.227 E	27.698	1450.8
211.8	211.82	34.501 E	-0.176 E	27.741	1451.3
221.9	221.94	34.529 E	-0.138 E	27.762	1451.6
232.0	232.02	34.553 E	-0.108 E	27.779	1452.0
242.1	242.09	34.574 E	-0.085 E	27.795	1452.2
252.1	252.10	34.588 E	-0.074 E	27.806	1452.5
262.3	262.30	34.597 E	-0.063 E	27.813	1452.7
272.4	272.39	34.604 E	-0.052 E	27.818	1453.0
282.6	282.56	34.612 E	-0.046 E	27.824	1453.2
292.4	292.38	34.615 E	-0.038 E	27.826	1453.4
302.5	302.49	34.619 E	-0.034 E	27.829	1453.6
312.6	312.55	34.618 E	-0.030 E	27.828	1453.7
322.7	322.66	34.620 E	-0.025 E	27.829	1453.9
332.9	332.94	34.624 E	-0.021 E	27.832	1454.1
343.5	343.50	34.643 E	-0.026 E	27.848	1454.3
353.1	353.05	34.633 E	-0.021 E	27.840	1454.5
363.0	363.05	34.630 E	-0.012 E	27.837	1454.7
373.3	373.30	34.628 E	-0.010 E	27.835	1454.8
383.3	383.29	34.641 E	-0.018 E	27.846	1455.0
393.4	393.44	34.631 E	-0.005 E	27.837	1455.2
403.4	403.44	34.630 E	-0.004 E	27.837	1455.4
413.8	413.80	34.632 E	-0.003 E	27.838	1455.6
423.9	423.92	34.638 E	-0.003 E	27.843	1455.7
433.8	433.77	34.633 E	0.0 E	27.839	1455.9

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
444.0	444.04	34.634 E	0.002 E	27.840	1456.1
454.1	454.08		0.003 E		
463.9	463.89	34.634 E	0.004 E	27.839	1456.4
474.2	474.19	34.632 E	0.007 E	27.838	1456.6
484.2	484.16	34.635 E	0.008 E	27.840	1456.8
494.0	494.04	34.637 E	0.009 E	27.841	1456.9
504.1	504.12	34.640 E	0.011 E	27.844	1457.1


EXPERIMENT 923
TEMPERATURE, C
-2.00
-1.50
-1.00
-0.50
0.00
0.50
1.00
SALINITY 0/00
12.00
16.00
20.00
24.00
28.00
32.00
36.00
SIGMAT
10.00
13.00
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22.00
25.00
28.00
DEPTH M
10
100
1000

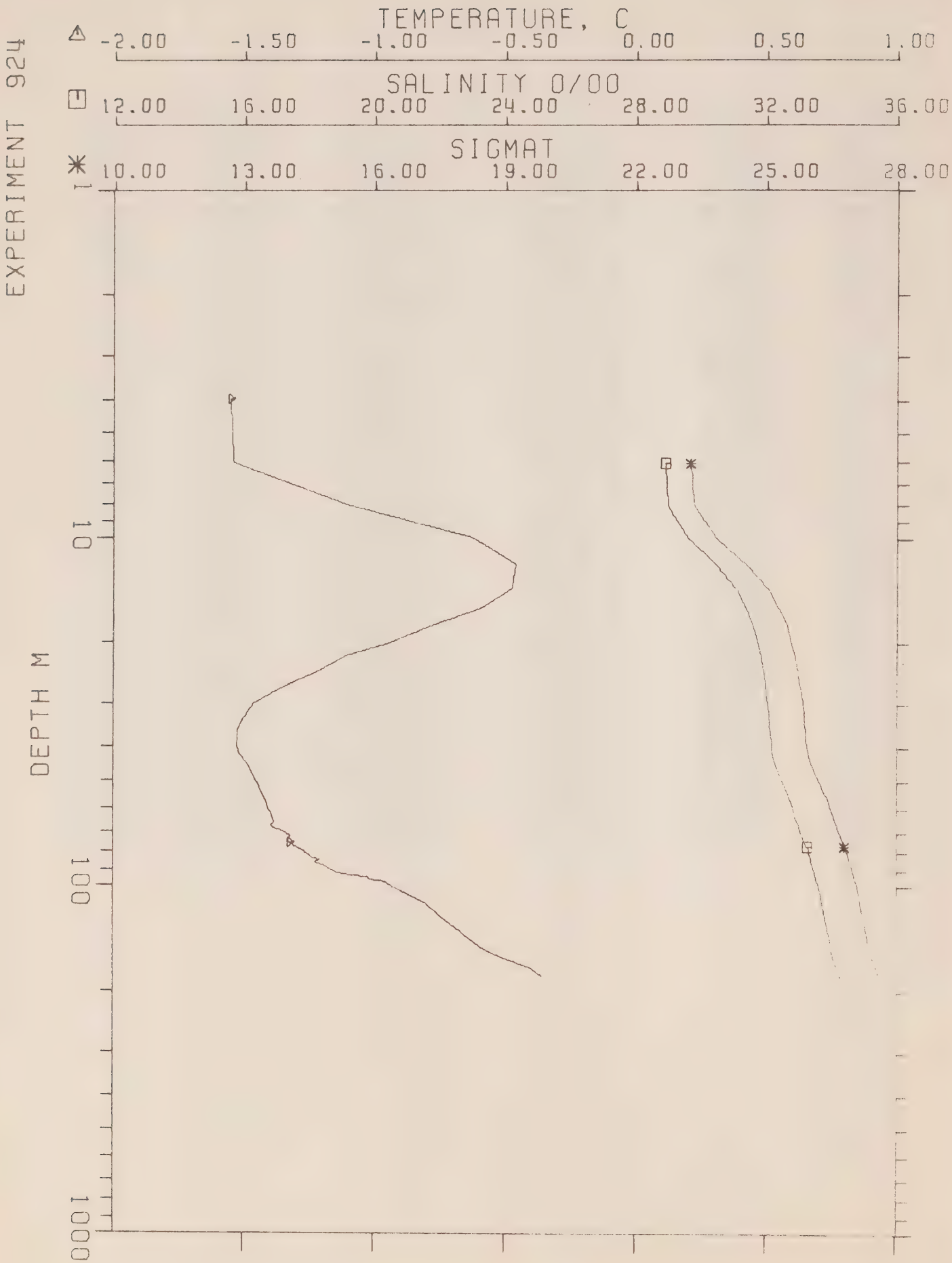
CRUISE 15-74-012 D'IBERVILLE FIORD-74 EXPER NO. 923

LAT N.80-34-23 LONG W.79-42-00 WATER DEPTH 203

DEPTH INCR. DATE 010474 LOCAL TIME 1410

DEPTH	PRES	SAL		TEMP		SIGMAT	SOUND
3.5	3.53	28.930	C	-1.562	D	23.281	1433.6
4.5	4.48	28.918	C	-1.565	D	23.271	1433.6
5.5	5.49	28.910	C	-1.563	D	23.264	1433.6
6.5	6.49	28.907	C	-1.554	D	23.262	1433.6
7.5	7.53	28.933	C	-1.410	D	23.282	1434.4
8.5	8.49	29.132	C	-0.885	D	23.433	1437.2
9.5	9.46	29.545	C	-0.667	D	23.761	1438.8
10.5	10.49	29.906	C	-0.548	D	24.050	1439.8
11.5	11.48	30.410	C	-0.462	D	24.454	1441.0
12.4	12.45	30.867	C	-0.465	D	24.822	1441.6
13.5	13.46	31.154	C	-0.491	D	25.054	1441.9
14.4	14.44	31.349	C	-0.565	D	25.214	1441.8
15.5	15.48	31.485	C	-0.615	D	25.326	1441.8
16.4	16.44	31.580	C	-0.707	D	25.405	1441.5
17.5	17.49	31.679	C	-0.815	D	25.488	1441.2
18.4	18.43	31.739	C	-0.901	D	25.539	1440.9
19.5	19.49	31.779	C	-0.947	D	25.573	1440.7
20.5	20.50	31.837	C	-1.052	D	25.622	1440.3
21.6	21.61	31.877	C	-1.110	D	25.657	1440.1
22.5	22.51	31.918	C	-1.155	D	25.691	1440.0
23.5	23.49	31.951	C	-1.217	D	25.719	1439.8
24.6	24.57	31.982	C	-1.287	D	25.746	1439.5
25.5	25.52	32.001	C	-1.310	D	25.762	1439.4
26.5	26.54	32.021	C	-1.348	D	25.779	1439.3
27.5	27.47	32.052	C	-1.405	D	25.805	1439.1
28.6	28.56	32.074	C	-1.443	D	25.824	1439.0
29.6	29.57	32.091	C	-1.464	D	25.838	1438.9
30.5	30.54	32.099	C	-1.471	D	25.845	1438.9
31.7	31.66	32.110	C	-1.483	D	25.855	1438.9
32.7	32.68	32.124	C	-1.494	D	25.866	1438.8
33.7	33.67	32.136	C	-1.507	D	25.875	1438.8
34.6	34.62	32.150	C	-1.520	D	25.888	1438.8
35.6	35.58	32.161	C	-1.523	D	25.897	1438.8
36.6	36.56	32.172	C	-1.528	D	25.906	1438.8
37.6	37.62	32.185	C	-1.531	D	25.916	1438.8
38.6	38.61	32.204	C	-1.531	D	25.932	1438.9
39.7	39.67	32.222	C	-1.530	D	25.946	1438.9
40.7	40.68	32.240	C	-1.523	D	25.961	1439.0
41.6	41.58	32.268	C	-1.524	D	25.983	1439.1
42.7	42.69	32.293	C	-1.509	D	26.003	1439.2
43.7	43.68	32.323	C	-1.500	D	26.027	1439.3
44.7	44.67	32.359	C	-1.494	D	26.056	1439.4
45.7	45.71	32.390	C	-1.483	D	26.081	1439.5
46.7	46.66	32.431	C	-1.480	D	26.114	1439.6
47.7	47.74	32.470	C	-1.473	D	26.145	1439.7
48.7	48.67	32.515	C	-1.466	D	26.182	1439.8
49.6	49.62	32.553	C	-1.468	D	26.213	1439.9
50.7	50.69	32.590	C	-1.460	D	26.243	1440.0
51.7	51.75	32.631	C	-1.450	D	26.275	1440.1
52.7	52.72	32.672	C	-1.448	D	26.309	1440.2
53.8	53.82	32.711	C	-1.456	D	26.340	1440.2
54.7	54.66	32.751	C	-1.457	D	26.372	1440.3
55.8	55.81	32.784	C	-1.438	D	26.399	1440.4
56.8	56.77	32.818	C	-1.430	D	26.427	1440.5
57.8	57.77	32.829	C	-1.426	D	26.435	1440.6
58.7	58.71	32.865	C	-1.422	D	26.464	1440.7
59.7	59.65	32.895	C	-1.415	D	26.488	1440.8
60.8	60.77	32.924	C	-1.409	D	26.511	1440.8
61.8	61.85	32.943	C	-1.403	D	26.527	1440.9
62.7	62.73	32.965	C	-1.401	D	26.544	1441.0
63.8	63.76	32.975	C	-1.394	D	26.553	1441.0
64.8	64.75	32.998	C	-1.392	D	26.571	1441.1

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
65.9	65.93	33.024 C	-1.388 D	26.592	1441.2
66.8	66.81	33.062 C	-1.400 D	26.623	1441.2
67.8	67.77	33.066 C	-1.381 D	26.626	1441.3
68.8	68.83	33.090 C	-1.357 D	26.644	1441.4
69.9	69.88	33.118 C	-1.351 D	26.667	1441.5
70.9	70.94	33.145 C	-1.338 D	26.688	1441.6
72.0	72.00	33.160 C	-1.329 D	26.701	1441.7
72.9	72.89	33.185 C	-1.313 D	26.721	1441.9
74.6	74.55	33.216 C	-1.328 D	26.746	1441.9
74.9	74.92	33.236 C	-1.331 D	26.762	1441.9
75.9	75.88	33.260 C	-1.324 D	26.782	1442.0
76.9	76.87	33.284 C	-1.322 D	26.801	1442.0
78.1	78.08	33.301 C	-1.302 D	26.814	1442.2
79.0	79.01	33.323 C	-1.284 D	26.831	1442.3
79.9	79.88	33.340 C	-1.277 D	26.845	1442.4
81.1	81.12	33.349 C	-1.266 D	26.852	1442.4
82.0	82.01	33.374 C	-1.255 D	26.872	1442.5
82.9	82.93	33.395 C	-1.248 D	26.888	1442.6
84.0	83.99	33.405 C	-1.233 D	26.896	1442.7
84.9	84.89	33.429 C	-1.210 D	26.915	1442.9
86.1	86.07	33.441 C	-1.222 D	26.925	1442.9
87.0	86.96	33.459 C	-1.212 D	26.939	1442.9
88.0	87.96	33.474 C	-1.201 D	26.951	1443.0
89.0	88.96	33.493 C	-1.186 D	26.966	1443.1
90.1	90.12	33.504 C	-1.164 D	26.974	1443.3
91.0	91.01	33.519 C	-1.142 D	26.986	1443.4
92.1	92.13	33.535 C	-1.127 D	26.998	1443.5
93.2	93.21	33.548 C	-1.113 D	27.009	1443.6
94.0	93.98	33.560 C	-1.086 D	27.017	1443.8
95.0	95.03	33.577 C	-1.041 D	27.030	1444.0
96.1	96.08	33.601 C	-1.013 D	27.048	1444.2
97.2	97.17	33.611 C	-0.972 D	27.054	1444.5
98.2	98.19	33.627 C	-0.965 D	27.067	1444.5
99.1	99.09	33.643 C	-0.953 D	27.080	1444.6
100.2	100.18	33.653 D	-0.946 E	27.088	1444.7
101.1	101.14	33.660 D	-0.934 E	27.093	1444.8
111.2	111.15	33.768 D	-0.829 F	27.177	1445.6
121.3	121.27	33.843 D	-0.756 E	27.234	1446.2
131.4	131.43	33.917 D	-0.702 E	27.292	1446.7
141.4	141.38	33.983 D	-0.642 E	27.343	1447.2
151.6	151.55	34.049 D	-0.579 E	27.394	1447.8
161.6	161.61	34.127 D	-0.517 E	27.454	1448.3
171.8	171.76	34.236 D	-0.418 E	27.538	1449.1
182.0	182.04	34.274 D	-0.354 E	27.566	1449.6


EXPERIMENT 924
TEMPERATURE, C
-2.00
-1.50
-1.00
-0.50
0.00
0.50
1.00
SALINITY O/OO
12.00
16.00
20.00
24.00
28.00
32.00
36.00
SIGMAT
10.00
13.00
16.00
19.00
22.00
25.00
28.00
DEPTH M
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100
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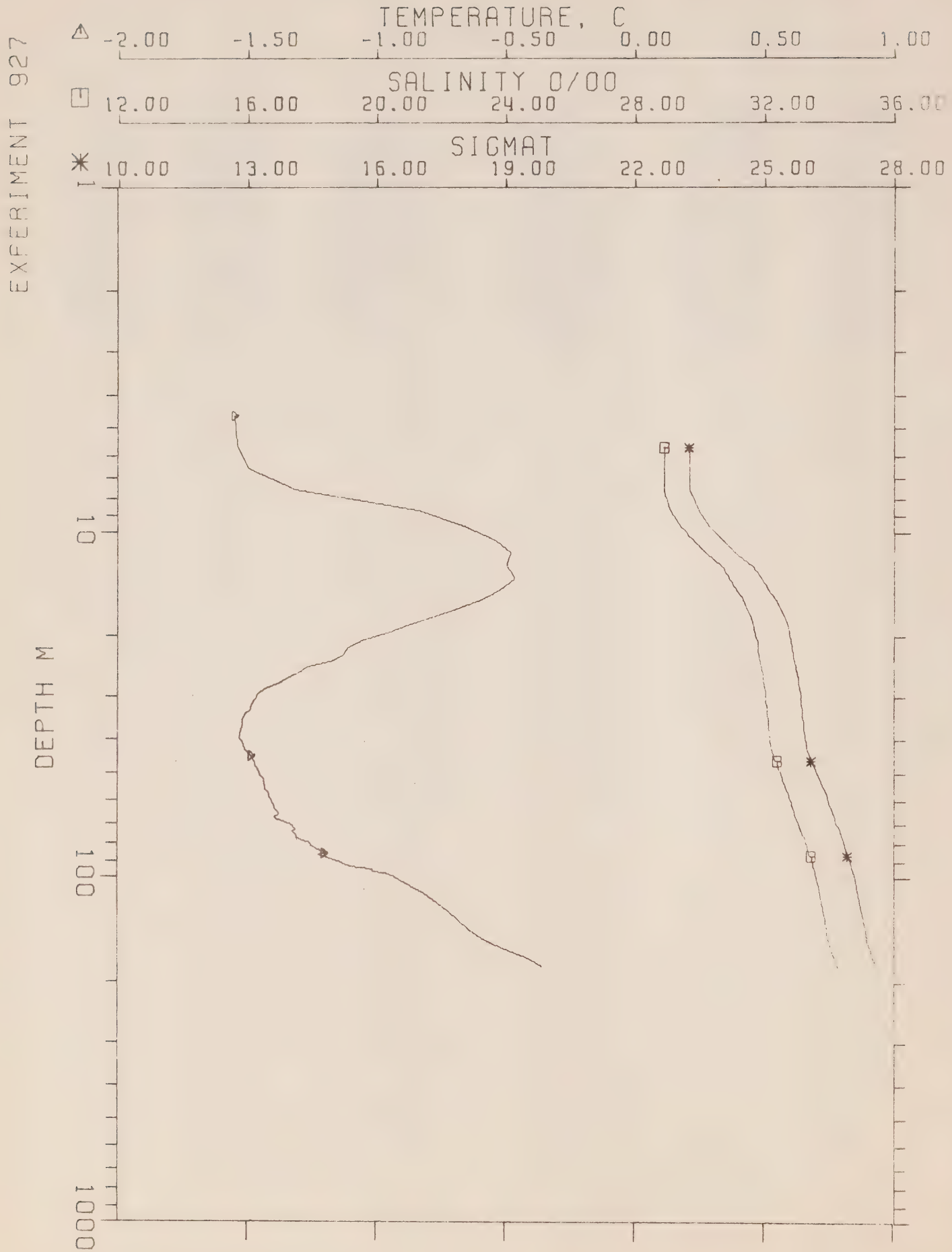
CRUISE 15-74-012 D'IBERVILLE FIORD-74 EXPER NO. 924

LAT N.80-34-23 LONG W.79-42-00 WATER DEPTH 203

DEPTH INCR. DATE 010474 LOCAL TIME 1503

DEPTH	PRES	SAL		TEMP		SIGMAT	SOUND
4.0	3.99			-1.557	D		
6.1	6.08	28.911	C	-1.545	D	23.265	1433.7
8.0	8.03	29.004	C	-1.110	D	23.334	1435.9
9.9	9.90	29.639	C	-0.631	D	23.836	1439.1
11.9	11.90	30.519	C	-0.455	D	24.541	1441.2
13.9	13.88	31.120	C	-0.470	D	25.026	1441.9
15.9	15.87	31.432	C	-0.583	D	25.281	1441.9
17.8	17.81	31.657	C	-0.778	D	25.469	1441.3
20.2	20.16	31.782	C	-0.951	D	25.576	1440.7
21.8	21.84	31.867	C	-1.103	D	25.649	1440.2
24.4	24.36	31.949	C	-1.220	D	25.718	1439.8
26.0	25.97	31.998	C	-1.307	D	25.760	1439.4
28.0	27.96	32.045	C	-1.390	D	25.799	1439.2
30.1	30.07	32.084	C	-1.459	D	25.832	1438.9
32.0	31.98	32.114	C	-1.485	D	25.858	1438.9
33.9	33.94	32.138	C	-1.509	D	25.878	1438.8
35.9	35.94	32.163	C	-1.525	D	25.898	1438.8
37.9	37.93	32.184	C	-1.526	D	25.915	1438.9
40.0	40.02	32.213	C	-1.529	D	25.939	1438.9
42.1	42.05	32.256	C	-1.519	D	25.973	1439.1
44.4	44.42	32.316	C	-1.494	D	26.022	1439.3
46.1	46.09	32.387	C	-1.478	D	26.078	1439.5
48.1	48.10	32.475	C	-1.471	D	26.150	1439.7
50.3	50.28	32.559	C	-1.455	D	26.217	1439.9
52.2	52.19	32.624	C	-1.445	D	26.270	1440.1
54.3	54.34	32.707	C	-1.437	D	26.337	1440.3
56.2	56.17	32.788	C	-1.423	D	26.402	1440.5
58.3	58.32	32.824	C	-1.416	D	26.431	1440.6
60.3	60.25	32.881	C	-1.408	D	26.477	1440.8
62.3	62.32	32.937	C	-1.397	D	26.522	1440.9
64.1	64.13	32.979	C	-1.392	D	26.556	1441.1
66.1	66.11	33.028	C	-1.387	D	26.595	1441.2
67.1	67.05	33.056	C	-1.398	D	26.618	1441.2
68.1	68.10	33.076	C	-1.390	D	26.634	1441.3
69.2	69.16	33.096	C	-1.354	D	26.650	1441.5
70.1	70.13	33.133	C	-1.344	D	26.679	1441.6
71.0	71.03	33.161	C	-1.335	D	26.701	1441.7
72.0	72.04	33.180	C	-1.321	D	26.716	1441.8
73.1	73.07	33.209	C	-1.326	D	26.740	1441.8
74.1	74.12	33.233	C	-1.335	D	26.760	1441.8
75.1	75.13	33.255	C	-1.323	D	26.777	1441.9
76.1	76.10	33.283	C	-1.317	D	26.800	1442.0
77.1	77.12	33.301	C	-1.304	D	26.814	1442.1
78.1	78.14	33.320	C	-1.283	D	26.829	1442.3
79.1	79.10	33.336	C	-1.273	D	26.842	1442.4
80.1	80.12	33.357	C	-1.270	D	26.859	1442.4
81.1	81.15	33.368	C	-1.257	D	26.867	1442.5
82.1	82.08	33.385	C	-1.248	D	26.881	1442.6
83.1	83.12	33.398	C	-1.242	D	26.891	1442.7
84.1	84.15	33.410	C	-1.205	D	26.899	1442.9
85.2	85.21	33.436	C	-1.228	D	26.921	1442.8
86.1	86.14	33.450	C	-1.219	D	26.933	1442.9
87.0	87.03	33.468	C	-1.201	D	26.946	1443.0
88.2	88.20	33.487	C	-1.185	D	26.961	1443.1
89.2	89.23	33.503	C	-1.173	D	26.974	1443.2
90.3	90.30	33.511	C	-1.160	D	26.979	1443.3
91.2	91.19	33.531	C	-1.143	D	26.995	1443.4
92.3	92.33	33.543	C	-1.117	D	27.004	1443.6
93.3	93.34	33.558	C	-1.095	D	27.016	1443.7
94.3	94.26	33.570	C	-1.029	D	27.023	1444.1
95.2	95.18	33.596	C	-1.026	D	27.044	1444.1
96.3	96.33	33.604	C	-0.986	D	27.049	1444.4

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
97.3	97.29	33.629 C	-0.960 D	27.069	1444.5
98.2	98.20	33.643 C	-0.953 D	27.080	1444.6
99.3	99.25	33.657 C	-0.945 D	27.091	1444.7
100.3	100.26	33.665 D	-0.934 E	27.097	1444.8
101.3	101.30	33.669 D	-0.921 E	27.100	1444.8
111.6	111.60	33.762 D	-0.811 E	27.171	1445.6
121.5	121.53	33.839 D	-0.753 E	27.231	1446.2
131.8	131.80	33.908 D	-0.696 E	27.285	1446.7
141.9	141.86	33.981 D	-0.640 E	27.342	1447.2
152.0	152.03	34.037 D	-0.584 E	27.384	1447.7
161.8	161.85	34.133 D	-0.507 E	27.458	1448.4
172.2	172.17	34.233 D	-0.406 E	27.535	1449.2
181.4	181.37	34.314 D	-0.364 E	27.599	1449.6


EXPERIMENT 927
TEMPERATURE, C
-2.00
-1.50
-1.00
-0.50
0.00
0.50
1.00
SALINITY 0/00
12.00
16.00
20.00
24.00
28.00
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SIGMAT
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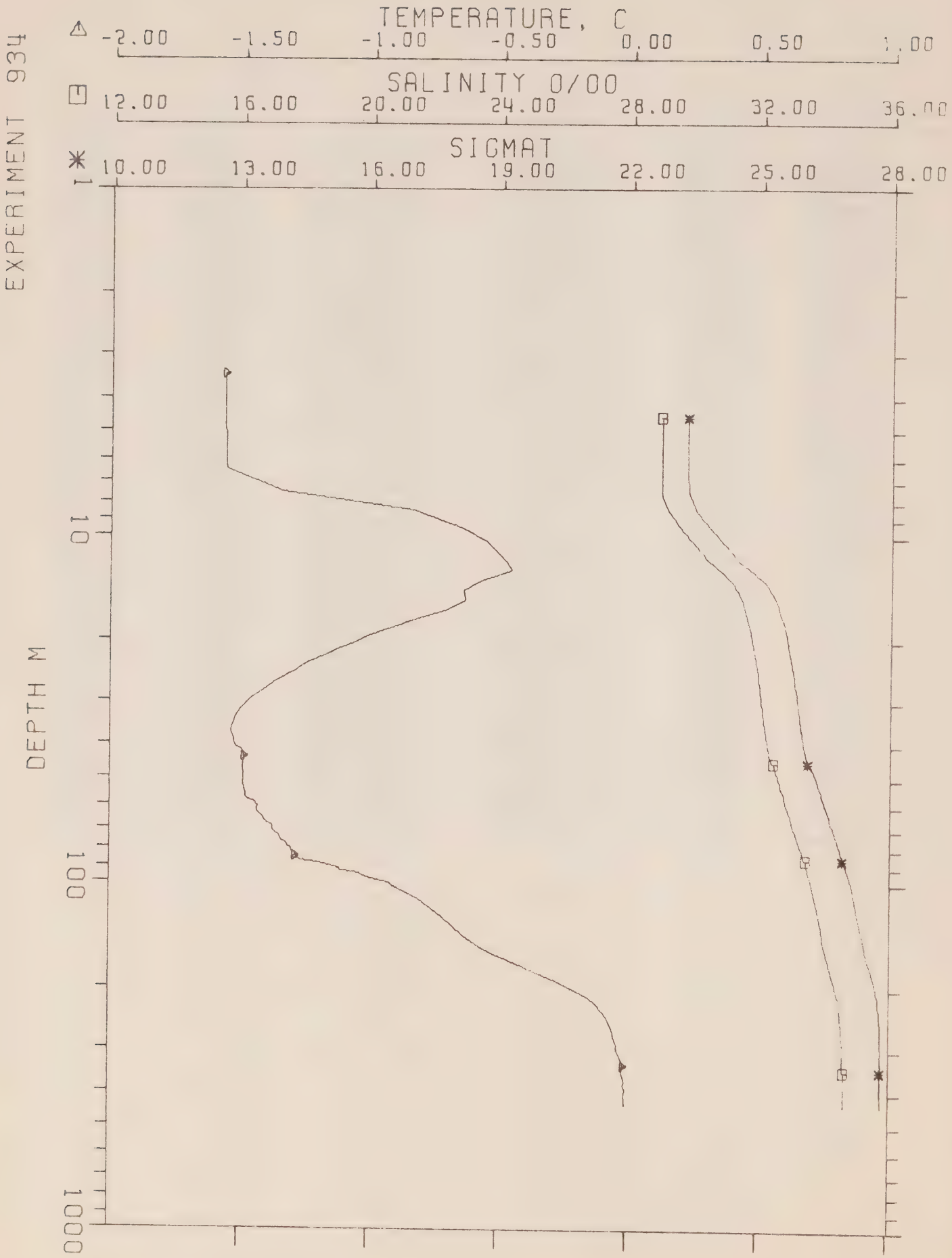
CRUISE 15-74-012 D'IBERVILLE FIORD-74 EXPER NO. 927

LAT N.80-34-23 LONG W.79-42-00 WATER DEPTH 203

DEPTH INCR. DATE 010474 LOCAL TIME 1518

DEPTH	PRES	SAL		TEMP		SIGMAT	SOUND
4.6	4.62			-1.553	D		
5.7	5.69	28.908	C	-1.543	D	23.262	1433.7
6.5	6.55	28.904	C	-1.502	D	23.259	1433.9
7.5	7.52	28.902	C	-1.321	D	23.255	1434.7
8.7	8.66	29.164	C	-0.842	D	23.458	1437.4
9.6	9.60	29.498	C	-0.666	D	23.724	1438.7
10.5	10.55	29.879	C	-0.540	D	24.028	1439.8
11.5	11.54	30.272	C	-0.473	D	24.343	1440.7
12.5	12.50	30.757	C	-0.496	D	24.734	1441.3
13.6	13.64	31.014	C	-0.458	D	24.940	1441.9
14.6	14.62	31.215	C	-0.513	D	25.104	1441.9
15.6	15.61	31.391	C	-0.572	D	25.248	1441.9
16.7	16.73	31.531	C	-0.682	D	25.365	1441.6
17.4	17.42	31.631	C	-0.756	D	25.448	1441.4
18.7	18.69	31.727	C	-0.876	D	25.529	1441.0
19.6	19.59	31.771	C	-0.955	D	25.567	1440.7
20.6	20.56	31.827	C	-1.040	D	25.614	1440.4
21.6	21.65	31.860	C	-1.105	D	25.642	1440.1
22.7	22.68	31.897	C	-1.123	D	25.673	1440.1
23.7	23.69	31.931	C	-1.177	D	25.702	1439.9
24.6	24.65	31.962	C	-1.264	D	25.729	1439.6
25.7	25.67	31.991	C	-1.302	D	25.754	1439.5
26.7	26.65	32.015	C	-1.344	D	25.774	1439.3
27.6	27.61	32.037	C	-1.374	D	25.792	1439.2
28.6	28.62	32.065	C	-1.429	D	25.817	1439.0
29.6	29.60	32.081	C	-1.453	D	25.830	1438.9
30.7	30.69	32.099	C	-1.470	D	25.845	1438.9
31.6	31.60	32.107	C	-1.479	D	25.851	1438.9
32.7	32.74	32.114	C	-1.485	D	25.858	1438.9
33.7	33.68	32.132	C	-1.504	D	25.873	1438.8
34.6	34.62	32.147	C	-1.516	D	25.885	1438.8
35.6	35.64	32.157	C	-1.519	D	25.893	1438.8
36.8	36.75	32.168	C	-1.522	D	25.902	1438.8
37.7	37.68	32.183	C	-1.527	D	25.914	1438.9
38.7	38.69	32.197	C	-1.530	D	25.926	1438.9
39.8	39.79	32.213	C	-1.534	D	25.938	1438.9
40.7	40.70	32.222	C	-1.527	D	25.946	1439.0
41.7	41.66	32.246	C	-1.520	D	25.965	1439.0
42.7	42.68	32.277	C	-1.517	D	25.990	1439.1
43.8	43.75	32.308	C	-1.498	D	26.015	1439.3
44.8	44.75	32.338	C	-1.488	D	26.039	1439.4
45.8	45.82	32.383	C	-1.484	D	26.075	1439.5
46.8	46.77	32.416	C	-1.477	D	26.102	1439.6
47.8	47.85	32.459	C	-1.476	D	26.137	1439.7
48.7	48.74	32.498	C	-1.463	D	26.168	1439.8
49.8	49.79	32.541	C	-1.462	D	26.203	1439.9
50.8	50.76	32.582	C	-1.453	D	26.236	1440.0
51.9	51.90	32.618	C	-1.446	D	26.265	1440.1
52.7	52.70	32.653	C	-1.442	D	26.293	1440.2
53.8	53.78	32.685	C	-1.439	D	26.319	1440.2
54.7	54.73	32.732	C	-1.436	D	26.357	1440.3
55.8	55.78	32.771	C	-1.437	D	26.388	1440.4
56.8	56.75	32.809	C	-1.423	D	26.419	1440.5
57.8	57.80	32.820	C	-1.420	D	26.427	1440.6
58.8	58.84	32.843	C	-1.419	D	26.447	1440.6
59.9	59.86	32.863	C	-1.412	D	26.462	1440.7
60.8	60.83	32.885	C	-1.409	D	26.480	1440.8
61.8	61.82	32.925	C	-1.399	D	26.512	1440.9
62.9	62.86	32.950	C	-1.398	D	26.532	1441.0
63.8	63.85	32.969	C	-1.393	D	26.547	1441.0
64.8	64.83	32.979	C	-1.383	D	26.556	1441.1
66.0	65.96	33.013	C	-1.382	D	26.583	1441.2

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
66.9	66.92	33.043 C	-1.398 D	26.608	1441.2
67.9	67.91	33.062 C	-1.392 D	26.623	1441.2
68.9	68.87	33.074 C	-1.367 D	26.632	1441.4
70.0	69.96	33.113 C	-1.347 D	26.663	1441.5
70.8	70.79	33.135 C	-1.330 D	26.681	1441.7
71.9	71.90	33.164 C	-1.323 D	26.704	1441.8
72.9	72.90	33.191 C	-1.317 D	26.725	1441.8
74.0	73.97	33.215 C	-1.330 D	26.746	1441.8
75.0	75.00	33.242 C	-1.322 D	26.767	1441.9
76.0	75.95	33.264 C	-1.314 D	26.784	1442.0
76.9	76.86	33.289 C	-1.313 D	26.805	1442.1
78.1	78.06	33.306 C	-1.292 D	26.817	1442.2
78.9	78.95	33.328 C	-1.270 D	26.835	1442.4
79.9	79.89	33.347 C	-1.265 D	26.850	1442.4
80.9	80.90	33.362 C	-1.260 D	26.862	1442.5
81.9	81.89	33.376 C	-1.247 D	26.873	1442.6
83.0	83.03	33.394 C	-1.237 D	26.887	1442.7
84.0	84.00	33.404 C	-1.211 D	26.895	1442.8
85.1	85.08	33.428 C	-1.206 D	26.914	1442.9
85.9	85.91	33.443 C	-1.230 D	26.927	1442.8
87.1	87.06	33.460 C	-1.208 D	26.940	1443.0
88.0	87.98	33.475 C	-1.184 D	26.951	1443.1
89.0	89.03	33.498 C	-1.167 D	26.969	1443.2
90.0	90.00	33.509 C	-1.153 D	26.978	1443.3
91.0	90.98	33.523 C	-1.139 D	26.989	1443.4
92.0	92.00	33.538 C	-1.119 D	27.000	1443.6
93.0	92.99	33.555 C	-1.104 D	27.013	1443.7
94.0	93.98	33.562 C	-1.071 D	27.018	1443.9
95.1	95.07	33.583 C	-1.021 D	27.034	1444.1
96.0	95.96	33.597 C	-1.018 D	27.044	1444.2
97.1	97.09	33.612 C	-0.972 D	27.055	1444.5
98.1	98.13	33.633 C	-0.959 D	27.072	1444.6
99.0	98.95	33.643 C	-0.941 D	27.080	1444.7
100.1	100.08	33.655 D	-0.935 E	27.089	1444.7
101.0	101.03	33.665 D	-0.920 E	27.096	1444.8
111.4	111.42	33.757 D	-0.819 E	27.167	1445.6
121.4	121.44	33.836 D	-0.748 E	27.229	1446.2
131.5	131.47	33.909 D	-0.696 E	27.285	1446.7
141.5	141.49	33.976 D	-0.647 E	27.338	1447.2
151.7	151.72	34.028 D	-0.584 E	27.377	1447.7
161.7	161.74	34.130 D	-0.505 E	27.456	1448.4
171.6	171.56	34.232 D	-0.413 E	27.535	1449.1
181.2	181.20	34.312 D	-0.363 E	27.597	1449.6


EXPERIMENT 934
TEMPERATURE, C
-2.00
-1.50
-1.00
-0.50
0.00
0.50
1.00
SALINITY 0/00
12.00
16.00
20.00
24.00
28.00
32.00
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SIGMAT
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DEPTH M
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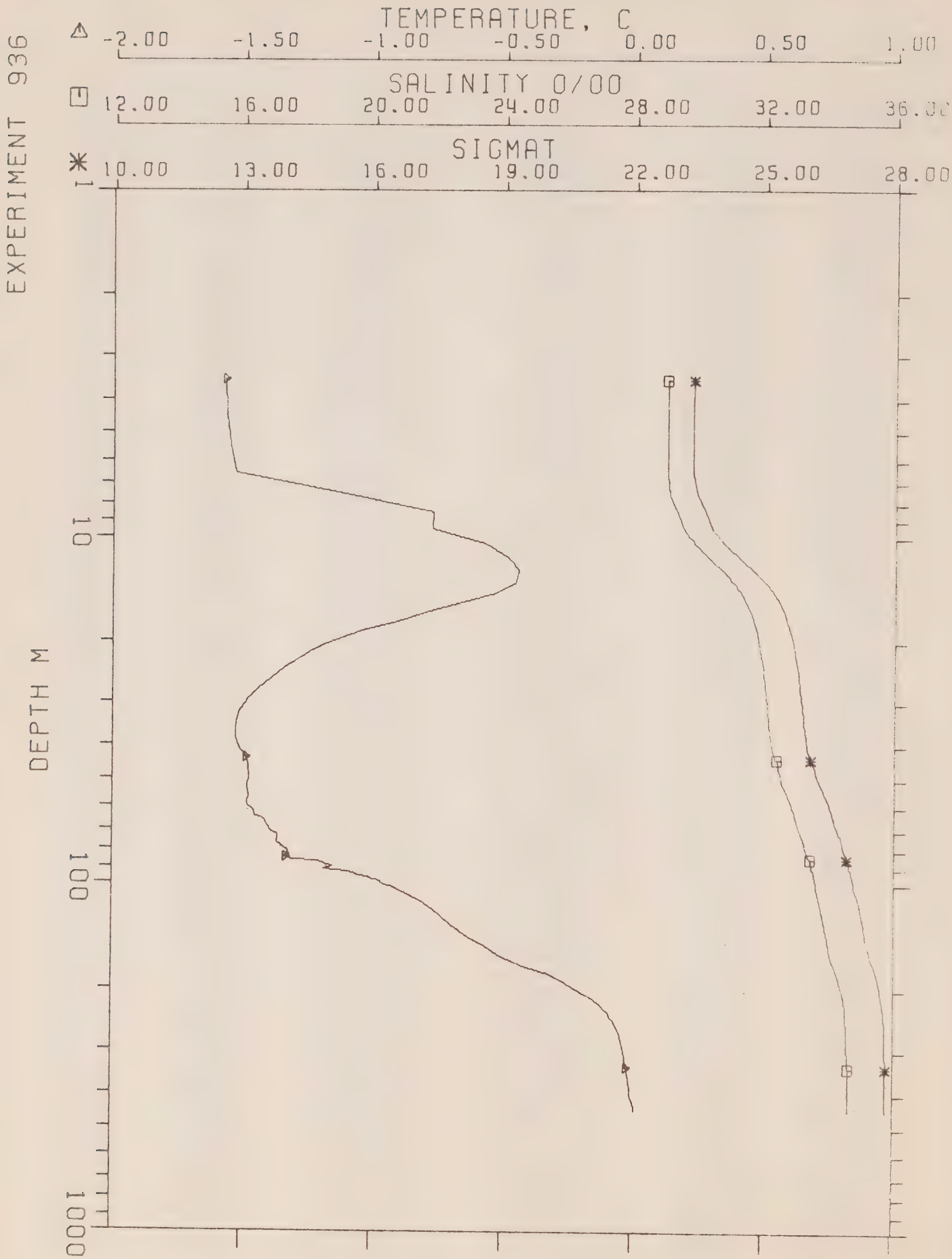
CRUISE 15-74-012 D'IBERVILLE FIORD-74 EXPER NO. 934

LAT N.80-34-45 LONG W.79-25-00 WATER DEPTH 519

DEPTH INCR. DATE 020474 LOCAL TIME 1100

DEPTH	PRES	SAL	TEMP	SIGMAT	SOUND
3.4	3.45		-1.568 F		
4.5	4.55	28.967 F	-1.568 F	23.311	1433.6
5.5	5.54	28.953 F	-1.566 F	23.300	1433.6
6.4	6.43	28.948 F	-1.566 F	23.295	1433.6
7.5	7.50	28.964 F	-1.350 F	23.305	1434.7
8.4	8.44	29.229 F	-0.842 F	23.511	1437.5
9.5	9.50	29.655 F	-0.645 F	23.849	1439.0
10.4	10.42	30.010 F	-0.553 F	24.133	1440.0
11.6	11.59	30.431 F	-0.488 F	24.471	1440.9
12.5	12.52	30.882 F	-0.451 F	24.833	1441.7
13.4	13.40	31.196 F	-0.569 F	25.091	1441.6
14.4	14.39	31.388 F	-0.640 F	25.248	1441.5
15.4	15.36	31.525 F	-0.631 F	25.358	1441.8
16.4	16.41	31.615 F	-0.711 F	25.434	1441.6
17.5	17.50	31.695 F	-0.825 F	25.502	1441.1
18.5	18.46	31.761 F	-0.923 F	25.557	1440.8
19.4	19.41	31.803 F	-1.012 F	25.594	1440.5
20.5	20.51	31.842 F	-1.072 F	25.627	1440.2
21.5	21.48	31.896 F	-1.134 F	25.672	1440.0
22.4	22.42	31.923 F	-1.184 F	25.696	1439.9
23.5	23.48	31.966 F	-1.254 F	25.732	1439.6
24.4	24.45	31.986 F	-1.279 F	25.749	1439.5
25.6	25.58	32.008 F	-1.326 F	25.768	1439.4
26.5	26.47	32.035 F	-1.366 F	25.791	1439.2
27.5	27.55	32.051 F	-1.394 F	25.804	1439.1
28.5	28.47	32.076 F	-1.426 F	25.825	1439.0
29.5	29.49	32.096 F	-1.453 F	25.842	1439.0
30.5	30.46	32.119 F	-1.477 F	25.861	1438.9
31.5	31.53	32.136 F	-1.496 F	25.876	1438.8
32.6	32.61	32.155 F	-1.509 F	25.892	1438.8
33.7	33.66	32.174 F	-1.520 F	25.907	1438.8
34.6	34.62	32.191 F	-1.526 F	25.921	1438.8
35.6	35.57	32.215 F	-1.536 F	25.940	1438.8
36.6	36.56	32.229 F	-1.541 F	25.952	1438.8
37.6	37.56	32.248 F	-1.541 F	25.967	1438.9
38.5	38.54	32.265 F	-1.531 F	25.981	1439.0
39.7	39.69	32.287 F	-1.531 F	25.998	1439.0
40.6	40.61	32.312 F	-1.523 F	26.019	1439.1
41.6	41.57	32.335 F	-1.500 F	26.037	1439.3
42.6	42.59	32.369 F	-1.496 F	26.064	1439.3
43.7	43.69	32.403 F	-1.488 F	26.091	1439.4
44.6	44.64	32.438 F	-1.486 F	26.120	1439.5
45.6	45.64	32.476 F	-1.489 F	26.151	1439.6
46.6	46.56	32.520 F	-1.493 F	26.186	1439.6
47.6	47.56	32.560 F	-1.496 F	26.219	1439.7
48.6	48.59	32.600 F	-1.490 F	26.251	1439.8
49.7	49.70	32.639 F	-1.490 F	26.283	1439.9
50.6	50.63	32.669 F	-1.489 F	26.307	1439.9
51.6	51.64	32.698 F	-1.491 F	26.331	1440.0
52.6	52.60	32.729 F	-1.493 F	26.355	1440.0
53.7	53.66	32.756 F	-1.488 F	26.377	1440.1
54.6	54.63	32.781 F	-1.491 F	26.398	1440.1
55.8	55.76	32.803 F	-1.482 F	26.415	1440.2
56.7	56.70	32.833 F	-1.486 F	26.440	1440.3
57.7	57.68	32.858 F	-1.474 F	26.460	1440.4
58.8	58.82	32.886 F	-1.446 F	26.481	1440.6
59.8	59.82	32.910 F	-1.444 F	26.501	1440.6
60.7	60.68	32.937 F	-1.428 F	26.523	1440.8
61.7	61.72	32.955 F	-1.441 F	26.538	1440.7
62.7	62.74	32.983 F	-1.442 F	26.560	1440.8
63.8	63.80	33.007 F	-1.429 F	26.580	1440.9
64.7	64.71	33.034 F	-1.419 F	26.601	1441.0

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
65.8	65.79	33.053 F	-1.414 F	26.616	1441.1
66.8	66.77	33.074 F	-1.405 F	26.633	1441.2
67.8	67.83	33.097 F	-1.395 F	26.652	1441.3
68.8	68.81	33.126 F	-1.380 F	26.674	1441.4
69.8	69.81	33.150 F	-1.376 F	26.694	1441.5
70.9	70.87	33.167 F	-1.379 F	26.707	1441.5
71.8	71.76	33.180 F	-1.372 F	26.718	1441.6
72.8	72.80	33.207 F	-1.355 F	26.739	1441.7
73.8	73.79	33.233 F	-1.355 F	26.760	1441.7
74.9	74.88	33.253 F	-1.349 F	26.777	1441.8
75.9	75.85	33.276 F	-1.344 F	26.795	1441.9
76.8	76.81	33.298 F	-1.331 F	26.813	1442.0
77.8	77.84	33.317 F	-1.323 F	26.827	1442.1
78.9	78.88	33.342 F	-1.320 F	26.848	1442.1
79.9	79.91	33.356 F	-1.307 F	26.858	1442.2
80.9	80.92	33.375 F	-1.305 F	26.874	1442.3
81.9	81.92	33.398 F	-1.296 F	26.892	1442.4
82.9	82.88	33.414 F	-1.283 F	26.905	1442.5
83.9	83.90	33.429 F	-1.289 F	26.918	1442.5
84.9	84.90	33.444 F	-1.304 F	26.930	1442.5
86.0	85.98	33.454 F	-1.268 F	26.937	1442.7
86.9	86.94	33.469 F	-1.240 F	26.949	1442.8
88.0	87.97	33.485 F	-1.200 F	26.960	1443.1
89.0	88.98	33.510 F	-1.164 F	26.980	1443.3
89.9	89.91	33.528 F	-1.140 F	26.993	1443.4
91.0	91.00	33.538 F	-1.121 F	27.000	1443.5
92.0	91.98	33.555 F	-1.121 F	27.014	1443.6
93.0	92.99	33.576 F	-1.062 F	27.029	1443.9
94.1	94.10	33.594 F	-1.052 F	27.044	1444.0
95.0	94.97	33.612 F	-1.035 F	27.058	1444.1
96.1	96.06	33.623 F	-1.017 F	27.066	1444.2
97.1	97.07	33.637 F	-0.998 F	27.077	1444.4
98.0	97.97	33.650 F	-0.974 F	27.086	1444.5
99.1	99.08	33.665 F	-0.955 F	27.097	1444.6
100.0	100.04	33.677 F	-0.928 F	27.107	1444.8
101.1	101.06	33.689 F	-0.920 F	27.116	1444.9
111.3	111.26	33.792 F	-0.813 F	27.195	1445.7
121.3	121.28	33.876 F	-0.746 F	27.261	1446.3
131.3	131.32	33.943 F	-0.691 F	27.312	1446.8
141.5	141.51	34.004 F	-0.642 F	27.360	1447.3
151.6	151.59	34.077 F	-0.579 F	27.416	1447.8
161.6	161.60	34.152 F	-0.508 F	27.474	1448.4
171.7	171.74	34.244 F	-0.422 F	27.545	1449.1
181.9	181.86	34.333 F	-0.343 F	27.613	1449.8
191.9	191.89	34.402 F	-0.270 F	27.665	1450.4
202.2	202.17	34.452 F	-0.213 F	27.703	1450.9
212.0	212.05	34.511 F	-0.160 F	27.748	1451.4
222.3	222.33	34.540 F	-0.125 F	27.770	1451.7
232.4	232.38	34.561 F	-0.105 F	27.786	1452.0
242.3	242.28	34.575 F	-0.086 F	27.796	1452.3
252.8	252.78	34.590 F	-0.074 F	27.808	1452.5
262.5	262.54	34.602 F	-0.064 F	27.817	1452.7
272.5	272.53	34.612 F	-0.058 F	27.825	1453.0
282.8	282.76	34.621 F	-0.054 F	27.831	1453.2
293.0	292.95	34.623 F	-0.046 F	27.833	1453.4
303.1	303.14	34.635 F	-0.046 F	27.842	1453.5
313.1	313.13	34.625 F	-0.036 F	27.834	1453.7
323.3	323.32	34.619 F	-0.023 F	27.829	1454.0
333.4	333.41	34.628 F	-0.020 F	27.836	1454.1
343.4	343.44	34.626 F	-0.018 F	27.834	1454.3
353.9	353.86	34.634 F	-0.023 F	27.841	1454.5
363.8	363.76	34.631 F	-0.017 F	27.838	1454.7
373.8	373.78	34.629 F	-0.012 F	27.836	1454.9
383.8	383.85	34.640 F	-0.018 F	27.845	1455.0
394.0	393.97	34.624 F	-0.006 F	27.832	1455.2
403.8	403.80	34.642 F	-0.014 F	27.847	1455.4
414.1	414.09	34.635 F	-0.013 F	27.841	1455.5
424.1	424.07	34.643 F	-0.013 F	27.847	1455.7
434.1	434.07	34.646 F	-0.012 F	27.849	1455.8


EXPERIMENT 936
TEMPERATURE, C
-2.00
-1.50
-1.00
-0.50
0.00
0.50
1.00
SALINITY 0/00
12.00
16.00
20.00
24.00
28.00
32.00
36.00
SIGMAT
10.00
13.00
16.00
19.00
22.00
25.00
28.00
DEPTH M
10
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1000

CRUISE 15-74-012 D'IBERVILLE FIORD-74 EXPER NO. 235

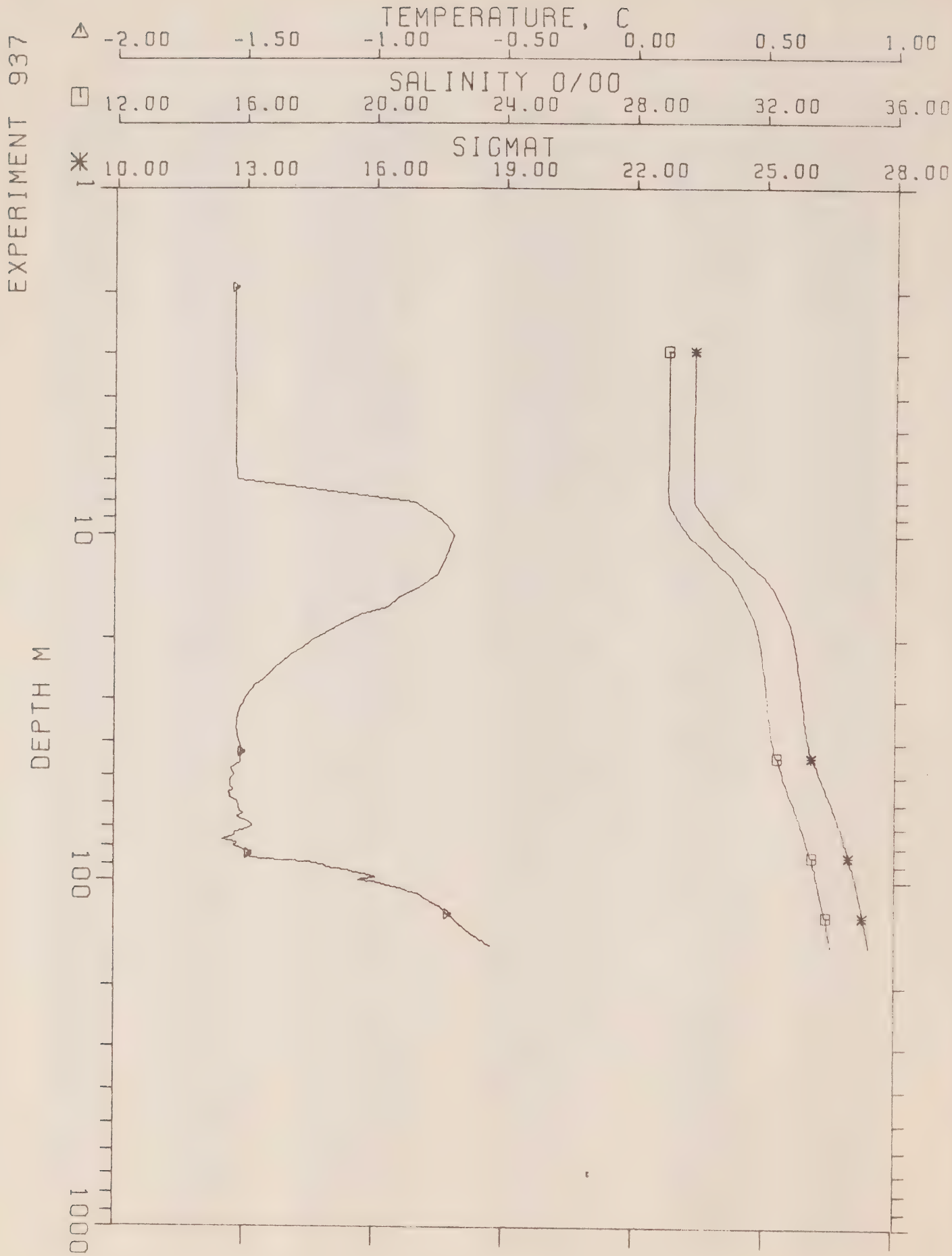
LAT N.80-34-38 LONG W.79-12-30 WATER DEPTH 492

DEPTH INCR. DATE 020474 LOCAL TIME 1425

DEPTH	PRES	SAL		TEMP		SIGMAT	SOUND
3.5	3.52	29.007	D	-1.576	E	23.344	1433.0
4.5	4.49	28.996	D	-1.571	E	23.334	1433.6
5.5	5.53	28.991	D	-1.557	E	23.330	1433.7
6.6	6.57	28.991	D	-1.536	E	23.330	1433.8
7.5	7.49	29.097	D	-1.138	E	23.410	1435.9
8.5	8.51	29.357	D	-0.770	E	23.612	1438.0
9.5	9.51	29.564	D	-0.775	E	23.780	1438.3
10.5	10.51	29.934	D	-0.575	E	24.073	1439.8
11.5	11.51	30.366	D	-0.487	E	24.419	1440.8
12.5	12.53	30.796	D	-0.442	E	24.764	1441.6
13.5	13.53	31.134	D	-0.451	E	25.037	1442.0
14.5	14.52	31.359	D	-0.525	E	25.221	1442.0
15.6	15.59	31.521	D	-0.671	E	25.356	1441.6
16.5	16.53	31.627	D	-0.795	E	25.445	1441.2
17.6	17.58	31.707	D	-0.901	E	25.513	1440.8
18.5	18.53	31.790	D	-1.020	E	25.584	1440.4
19.5	19.54	31.845	D	-1.105	E	25.630	1440.1
20.5	20.55	31.892	D	-1.186	E	25.671	1439.8
21.6	21.61	31.931	D	-1.240	E	25.704	1439.6
22.6	22.61	31.958	D	-1.278	E	25.726	1439.5
23.5	23.54	31.990	D	-1.322	E	25.754	1439.3
24.6	24.64	32.016	D	-1.357	E	25.775	1439.2
25.6	25.60	32.035	D	-1.383	E	25.791	1439.1
26.6	26.57	32.054	D	-1.409	E	25.807	1439.1
27.6	27.56	32.073	D	-1.433	E	25.823	1439.0
28.6	28.63	32.095	D	-1.458	E	25.841	1438.9
29.6	29.62	32.111	D	-1.477	E	25.855	1438.9
30.6	30.62	32.127	D	-1.492	E	25.868	1438.8
31.7	31.67	32.139	D	-1.506	E	25.878	1438.8
32.6	32.60	32.151	D	-1.514	E	25.888	1438.8
33.6	33.59	32.163	D	-1.522	E	25.898	1438.8
34.6	34.63	32.173	D	-1.524	E	25.906	1438.8
35.6	35.62	32.186	D	-1.528	E	25.917	1438.8
36.9	36.88	32.205	D	-1.532	E	25.932	1438.9
37.6	37.63	32.224	D	-1.531	E	25.947	1438.9
38.7	38.67	32.241	D	-1.528	E	25.961	1438.9
39.8	39.75	32.261	D	-1.523	E	25.977	1439.0
40.7	40.65	32.283	D	-1.518	E	25.995	1439.1
41.7	41.65	32.307	D	-1.509	E	26.014	1439.2
42.8	42.75	32.348	D	-1.496	E	26.048	1439.3
43.7	43.68	32.393	D	-1.491	E	26.083	1439.4
44.7	44.68	32.430	D	-1.485	E	26.113	1439.5
45.8	45.79	32.458	D	-1.482	E	26.136	1439.6
46.7	46.72	32.483	D	-1.480	E	26.156	1439.7
47.8	47.83	32.509	D	-1.480	E	26.177	1439.7
48.7	48.68	32.537	D	-1.477	E	26.200	1439.8
49.8	49.76	32.565	D	-1.474	E	26.223	1439.8
50.7	50.70	32.600	D	-1.476	E	26.251	1439.9
51.7	51.69	32.639	D	-1.482	E	26.282	1439.9
52.8	52.80	32.684	D	-1.484	E	26.319	1440.0
53.7	53.69	32.720	D	-1.484	E	26.349	1440.1
54.9	54.92	32.754	D	-1.480	E	26.376	1440.2
55.8	55.80	32.787	D	-1.480	E	26.403	1440.2
57.0	56.97	32.822	D	-1.476	E	26.431	1440.3
57.8	57.82	32.865	D	-1.485	E	26.466	1440.3
58.9	58.90	32.892	D	-1.483	E	26.488	1440.4
59.9	59.93	32.921	D	-1.483	E	26.511	1440.5
60.8	60.83	32.947	D	-1.471	E	26.532	1440.5
61.8	61.77	32.966	D	-1.462	E	26.547	1440.7
63.0	63.01	32.988	D	-1.461	E	26.565	1440.7
64.0	64.01	33.012	D	-1.453	E	26.584	1440.8
64.8	64.79	33.023	D	-1.431	E	26.593	1440.9

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
66.1	66.09	33.047 D	-1.422 E	26.612	1441.0
67.1	67.13	33.072 D	-1.416 E	26.632	1441.1
68.0	68.02	33.098 D	-1.412 E	26.653	1441.2
68.9	68.94	33.119 D	-1.398 E	26.669	1441.3
69.9	69.89	33.150 D	-1.401 E	26.694	1441.3
71.0	71.01	33.176 D	-1.390 E	26.715	1441.4
72.1	72.07	33.193 D	-1.370 E	26.729	1441.6
73.3	73.25	33.230 D	-1.367 E	26.758	1441.7
74.2	74.16	33.242 D	-1.364 E	26.768	1441.7
74.9	74.94	33.267 D	-1.365 E	26.788	1441.8
76.1	76.06	33.287 D	-1.371 E	26.805	1441.8
77.2	77.24	33.298 D	-1.359 E	26.813	1441.9
78.0	78.00	33.325 D	-1.356 E	26.835	1441.9
79.1	79.11	33.335 D	-1.339 E	26.842	1442.0
80.3	80.31	33.353 D	-1.318 E	26.856	1442.2
81.5	81.50	33.376 D	-1.326 E	26.875	1442.2
82.2	82.17	33.395 D	-1.313 E	26.891	1442.3
83.0	83.04	33.420 D	-1.339 E	26.912	1442.2
84.2	84.24	33.434 D	-1.335 E	26.922	1442.3
85.3	85.25	33.444 D	-1.312 E	26.930	1442.4
86.2	86.17	33.451 D	-1.215 E	26.933	1442.9
87.2	87.21	33.473 D	-1.197 E	26.950	1443.0
88.6	88.59	33.495 D	-1.177 E	26.968	1443.2
89.1	89.11	33.492 D	-1.148 E	26.964	1443.3
90.4	90.39	33.543 D	-1.190 E	27.006	1443.2
91.1	91.09	33.539 D	-1.141 E	27.002	1443.5
92.2	92.18	33.548 D	-1.101 E	27.008	1443.7
93.3	93.32	33.559 D	-1.073 E	27.016	1443.8
94.5	94.46	33.585 D	-1.055 E	27.037	1444.0
95.3	95.29	33.593 D	-1.017 E	27.042	1444.2
96.6	96.61	33.607 D	-1.014 E	27.053	1444.2
97.2	97.19	33.624 D	-0.994 E	27.066	1444.4
98.2	98.17	33.630 D	-0.972 E	27.070	1444.5
99.5	99.53	33.644 D	-0.968 E	27.081	1444.6
100.2	100.21	33.654 E	-0.957 E	27.089	1444.6
101.2	101.22	33.648 E	-0.937 E	27.083	1444.7
111.2	111.22	33.776 E	-0.818 E	27.183	1445.6
121.3	121.33	33.854 E	-0.751 E	27.243	1446.2
131.4	131.38	33.933 E	-0.700 E	27.305	1446.7
141.6	141.55	33.990 E	-0.636 E	27.349	1447.3
151.5	151.54	34.058 E	-0.572 E	27.401	1447.8
161.7	161.69	34.134 E	-0.511 E	27.460	1448.4
171.8	171.80	34.236 E	-0.426 E	27.538	1449.1
181.7	181.70	34.333 E	-0.325 E	27.612	1449.8
192.1	192.15	34.417 E	-0.260 E	27.677	1450.4
202.0	201.95	34.466 E	-0.209 E	27.714	1450.9
211.9	211.89	34.507 E	-0.160 E	27.745	1451.3
222.1	222.08	34.540 E	-0.127 E	27.770	1451.7
232.2	232.15	34.559 E	-0.101 E	27.784	1452.0
242.2	242.21	34.579 E	-0.085 E	27.799	1452.3
252.3	252.25	34.595 E	-0.072 E	27.811	1452.5
262.3	262.31	34.602 E	-0.062 E	27.817	1452.8
272.4	272.35	34.607 E	-0.052 E	27.821	1453.0
282.4	282.41	34.618 E	-0.046 E	27.829	1453.2
292.5	292.47	34.617 E	-0.038 E	27.828	1453.4
302.7	302.66	34.622 E	-0.035 E	27.832	1453.6
312.7	312.65	34.624 E	-0.029 E	27.833	1453.8
322.8	322.79	34.631 E	-0.030 E	27.839	1453.9
332.8	332.84	34.631 E	-0.025 E	27.839	1454.1
342.9	342.92	34.629 E	-0.018 E	27.836	1454.3
353.0	352.98	34.636 E	-0.021 E	27.842	1454.5
362.8	362.85	34.634 E	-0.013 E	27.840	1454.7
373.1	373.14	34.640 E	-0.016 E	27.845	1454.8
383.1	383.06	34.637 E	-0.010 E	27.843	1455.0
393.3	393.33	34.641 E	-0.011 E	27.846	1455.2
403.4	403.39	34.642 E	-0.008 E	27.846	1455.4
413.5	413.45	34.637 E	-0.003 E	27.842	1455.6
423.5	423.48	34.636 E	-0.002 E	27.841	1455.7
433.4	433.44	34.636 E	0.003 E	27.841	1455.9

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
443.6	443.59	34.636 E	0.004 E	27.841	1456.1


EXPERIMENT 937
TEMPERATURE, C
-2.00
-1.50
-1.00
-0.50
0.00
0.50
1.00
SALINITY 0/00
12.00
16.00
20.00
24.00
28.00
32.00
36.00
SIGMAT
10.00
13.00
16.00
19.00
22.00
25.00
28.00
DEPTH M
10
100
1000

CRUISE 15-74-012 D'IBERVILLE FIORD-74 EXPER NO. 937

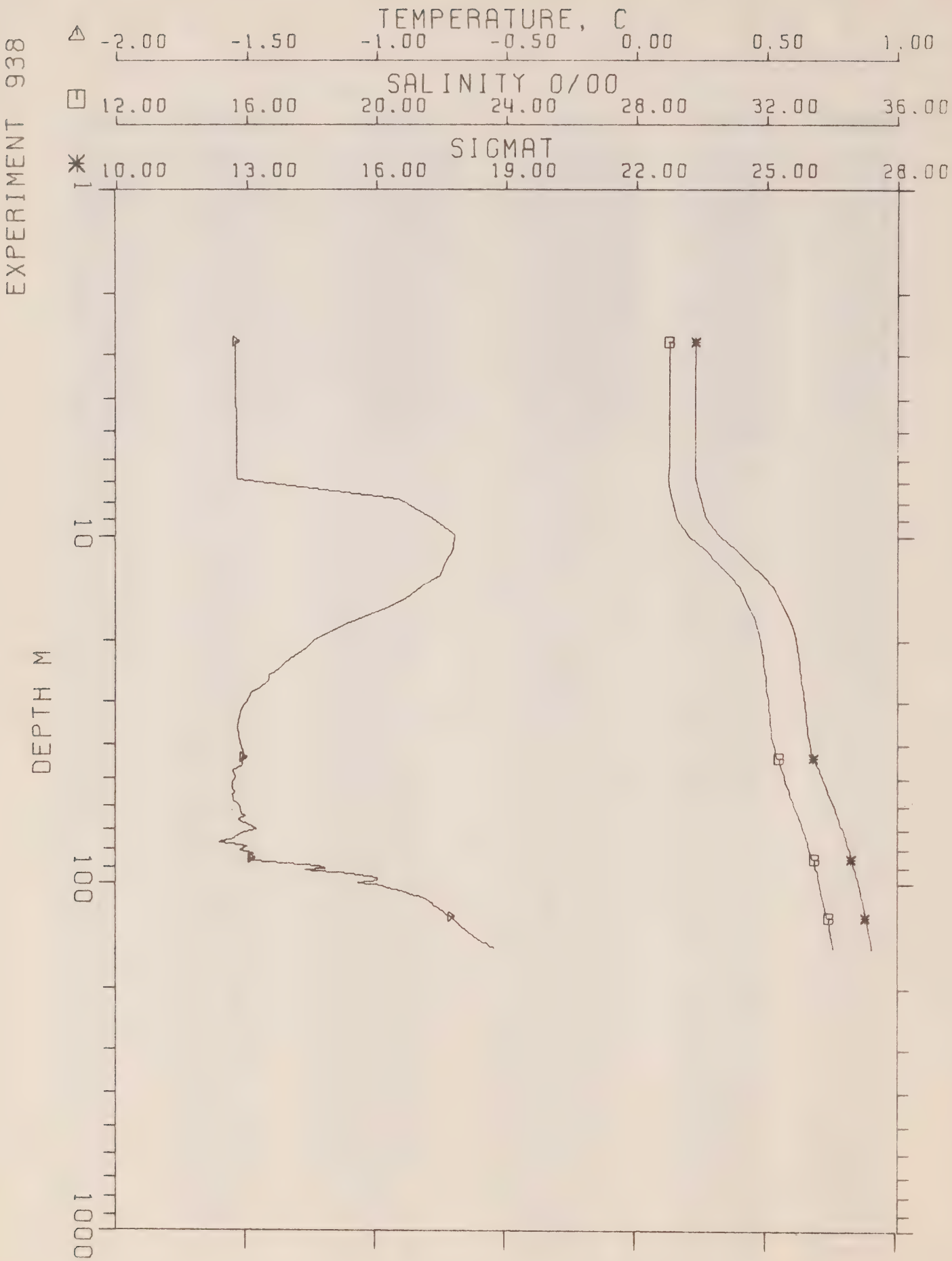
LAT N.80-34-52 LONG W.78-19-10 WATER DEPTH 199

DEPTH INCR. DATE 040474 LOCAL TIME 2000

DEPTH	PRES	SAL		TEMP		SIGMAT	SOUND
1.9	1.95			-1.543	D		
2.9	2.95	29.052	C	-1.543	D	23.379	1433.8
4.0	4.00	29.042	C	-1.542	D	23.371	1433.8
5.0	5.05	29.029	C	-1.542	D	23.361	1433.8
6.0	6.05	29.026	C	-1.542	D	23.358	1433.8
7.0	7.00	29.016	C	-1.535	D	23.350	1433.9
8.0	8.05	29.048	C	-0.849	D	23.365	1437.2
9.0	9.05	29.357	C	-0.752	D	23.612	1438.1
10.1	10.10	29.735	C	-0.690	D	23.915	1438.9
11.1	11.15	30.229	C	-0.709	D	24.315	1439.5
12.1	12.15	30.607	C	-0.731	D	24.620	1440.0
13.1	13.15	30.999	C	-0.753	D	24.938	1440.4
14.2	14.20	31.245	C	-0.820	D	25.138	1440.5
15.2	15.20	31.411	C	-0.898	D	25.274	1440.4
16.2	16.20	31.546	C	-0.947	D	25.385	1440.3
17.2	17.20	31.678	C	-1.055	D	25.494	1440.0
18.2	18.25	31.760	C	-1.123	D	25.562	1439.9
19.2	19.25	31.824	C	-1.184	D	25.615	1439.7
20.3	20.30	31.878	C	-1.241	D	25.661	1439.5
21.3	21.30	31.910	C	-1.269	D	25.687	1439.4
22.3	22.30	31.956	C	-1.320	D	25.726	1439.3
23.3	23.30	31.977	C	-1.351	D	25.744	1439.2
24.3	24.35	31.999	C	-1.380	D	25.762	1439.1
25.4	25.45	32.027	C	-1.406	D	25.785	1439.0
26.4	26.45	32.046	C	-1.423	D	25.801	1439.0
27.4	27.40	32.074	C	-1.455	D	25.825	1438.9
28.4	28.40	32.094	C	-1.474	D	25.841	1438.8
29.4	29.45	32.110	C	-1.489	D	25.855	1438.8
30.5	30.55	32.126	C	-1.502	D	25.867	1438.8
31.4	31.45	32.140	C	-1.511	D	25.879	1438.8
32.5	32.55	32.153	C	-1.519	D	25.890	1438.8
33.5	33.55	32.169	C	-1.526	D	25.903	1438.8
34.6	34.60	32.182	C	-1.531	D	25.914	1438.8
35.6	35.60	32.191	C	-1.532	D	25.921	1438.8
36.5	36.55	32.207	C	-1.533	D	25.934	1438.8
37.6	37.60	32.230	C	-1.530	D	25.953	1438.9
38.7	38.70	32.258	C	-1.529	D	25.975	1439.0
39.6	39.65	32.280	C	-1.523	D	25.993	1439.0
40.7	40.70	32.308	C	-1.518	D	26.015	1439.1
41.6	41.65	32.332	C	-1.514	D	26.034	1439.2
42.7	42.75	32.360	C	-1.514	D	26.057	1439.3
43.7	43.75	32.392	C	-1.513	D	26.083	1439.3
44.7	44.75	32.429	C	-1.514	D	26.114	1439.4
45.8	45.80	32.474	C	-1.516	D	26.149	1439.5
46.8	46.80	32.525	C	-1.533	D	26.192	1439.5
47.8	47.80	32.553	C	-1.553	D	26.214	1439.4
48.8	48.85	32.583	C	-1.550	D	26.238	1439.5
49.8	49.85	32.610	C	-1.538	D	26.261	1439.6
50.9	50.90	32.658	C	-1.549	D	26.299	1439.6
51.9	51.90	32.700	C	-1.557	D	26.334	1439.7
52.9	52.95	32.722	C	-1.557	D	26.352	1439.7
53.9	53.95	32.744	C	-1.554	D	26.369	1439.8
55.0	55.00	32.776	C	-1.545	D	26.395	1439.9
55.9	55.95	32.809	C	-1.563	D	26.422	1439.9
57.0	57.00	32.851	C	-1.555	D	26.456	1440.0
58.0	58.00	32.886	C	-1.558	D	26.485	1440.0
59.0	59.00	32.907	C	-1.535	D	26.501	1440.2
60.1	60.10	32.940	C	-1.529	D	26.528	1440.3
61.1	61.10	32.970	C	-1.522	D	26.552	1440.4
62.1	62.10	32.998	C	-1.524	D	26.574	1440.4
63.1	63.10	33.027	C	-1.522	D	26.598	1440.5
64.1	64.15	33.049	C	-1.499	D	26.615	1440.6

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
65.1	65.15	33.096	C	-1.525	D	26.654	1440.6
66.1	66.15	33.101	C	-1.530	D	26.658	1440.6
67.2	67.20	33.114	C	-1.503	D	26.668	1440.8
68.2	68.20	33.143	C	-1.481	D	26.691	1440.9
69.2	69.25	33.172	C	-1.472	D	26.714	1441.0
70.2	70.25	33.200	C	-1.465	D	26.737	1441.1
71.2	71.25	33.242	C	-1.489	D	26.771	1441.1
72.3	72.30	33.240	C	-1.531	D	26.771	1440.9
73.3	73.30	33.270	C	-1.535	D	26.795	1440.9
74.4	74.40	33.289	C	-1.537	D	26.811	1441.0
75.4	75.40	33.323	C	-1.567	D	26.839	1440.9
76.4	76.45	33.332	C	-1.592	D	26.847	1440.8
77.4	77.45	33.329	C	-1.534	D	26.843	1441.1
78.4	78.45	33.377	C	-1.530	D	26.881	1441.2
79.5	79.55	33.394	C	-1.545	D	26.896	1441.2
80.5	80.55	33.403	C	-1.532	D	26.903	1441.3
81.5	81.50	33.421	C	-1.507	D	26.917	1441.4
82.5	82.55	33.437	C	-1.469	D	26.929	1441.6
83.6	83.60	33.458	C	-1.492	D	26.947	1441.6
84.6	94.60	33.469	C	-1.472	D	26.955	1441.7
85.6	85.60	33.492	C	-1.502	D	26.975	1441.6
86.6	86.60	33.479	C	-1.437	D	26.962	1441.9
87.7	87.70	33.494	C	-1.340	D	26.971	1442.4
88.7	88.70	33.502	C	-1.259	D	26.976	1442.8
89.7	89.70	33.527	C	-1.211	D	26.994	1443.1
90.6	90.65	33.545	C	-1.184	D	27.008	1443.3
91.7	91.70	33.587	C	-1.191	D	27.043	1443.3
92.7	92.70	33.579	C	-1.116	D	27.034	1443.7
93.8	93.75	33.592	C	-1.092	D	27.043	1443.8
94.8	94.80	33.607	C	-1.078	D	27.055	1443.9
95.8	95.85	33.615	C	-1.038	D	27.060	1444.1
96.9	96.90	33.631	C	-1.001	D	27.072	1444.3
97.9	97.95	33.652	C	-0.992	D	27.089	1444.4
98.9	98.90	33.691	C	-1.044	D	27.122	1444.3
99.9	99.90	33.672	C	-1.066	D	27.107	1444.1
100.9	100.90	33.672	D	-1.004	E	27.105	1444.4
101.9	101.90	33.695	D	-0.972	E	27.123	1444.6
103.0	103.00	33.702	D	-0.956	E	27.127	1444.7
104.0	104.00	33.708	D	-0.926	E	27.131	1444.9
105.0	105.00	33.726	D	-0.907	E	27.145	1445.0
106.0	106.00	33.730	D	-0.887	E	27.148	1445.2
107.0	107.05	33.737	D	-0.875	E	27.153	1445.2
108.1	108.10	33.741	D	-0.865	F	27.156	1445.3
109.1	109.15	33.759	D	-0.842	E	27.170	1445.5
110.1	110.10	33.774	D	-0.824	F	27.182	1445.6
111.1	111.10	33.790	D	-0.814	E	27.193	1445.7
112.2	112.20	33.798	D	-0.803	E	27.199	1445.7
113.1	113.15	33.807	D	-0.796	E	27.207	1445.8
114.1	114.15	33.813	D	-0.790	E	27.212	1445.9
115.2	115.25	33.824	D	-0.779	E	27.220	1445.9
116.2	116.25	33.838	D	-0.769	E	27.231	1446.0
117.2	117.25	33.847	D	-0.760	E	27.238	1446.1
118.3	118.30	33.859	D	-0.752	E	27.248	1446.2
119.3	119.35	33.868	D	-0.746	E	27.254	1446.2
120.4	120.40	33.876	D	-0.739	E	27.261	1446.3
121.3	121.30	33.881	D	-0.734	E	27.264	1446.3
122.4	122.40	33.886	D	-0.729	E	27.268	1446.4
123.4	123.40	33.897	D	-0.725	E	27.277	1446.4
124.4	124.45	33.903	D	-0.721	E	27.282	1446.5
125.4	125.40	33.911	D	-0.713	E	27.287	1446.5
126.4	126.45	33.918	D	-0.709	E	27.293	1446.6
127.5	127.50	33.922	D	-0.704	E	27.297	1446.6
128.5	128.55	33.928	D	-0.699	E	27.301	1446.7
129.5	129.55	33.933	D	-0.694	E	27.305	1446.7
130.6	130.60	33.939	D	-0.690	E	27.310	1446.8
131.6	131.60	33.946	D	-0.685	E	27.315	1446.8
132.6	132.65	33.951	D	-0.678	E	27.319	1446.9
133.6	133.60	33.962	D	-0.673	E	27.328	1446.9
134.6	134.65	33.968	D	-0.667	E	27.332	1447.0

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
135.7	135.70	33.976	D	-0.661	E	27.338	1447.0
136.7	136.70	33.981	D	-0.657	E	27.342	1447.1
137.6	137.65	33.984	D	-0.655	E	27.345	1447.1
138.7	138.70	33.991	D	-0.649	E	27.350	1447.2
139.8	139.80	34.000	D	-0.641	E	27.357	1447.2
140.7	140.75	34.008	D	-0.634	E	27.363	1447.3
141.8	141.85	34.013	D	-0.629	E	27.367	1447.3
142.8	142.85	34.020	D	-0.626	E	27.373	1447.4
143.8	143.85	34.025	D	-0.619	E	27.376	1447.4
144.8	144.80	34.038	D	-0.612	E	27.386	1447.5
145.9	145.90	34.046	D	-0.607	E	27.392	1447.6
146.9	146.95	34.054	D	-0.599	E	27.399	1447.6
147.9	147.95	34.061	D	-0.591	E	27.404	1447.7
148.9	148.95	34.068	D	-0.584	E	27.409	1447.7
149.9	149.95	34.075	D	-0.578	E	27.415	1447.8
151.0	151.00	34.083	D	-0.574	E	27.421	1447.8
152.0	152.05	34.090	D	-0.565	E	27.427	1447.9
153.1	153.10	34.099	D	-0.556	E	27.433	1448.0


EXPERIMENT 938
TEMPERATURE, C
-2.00
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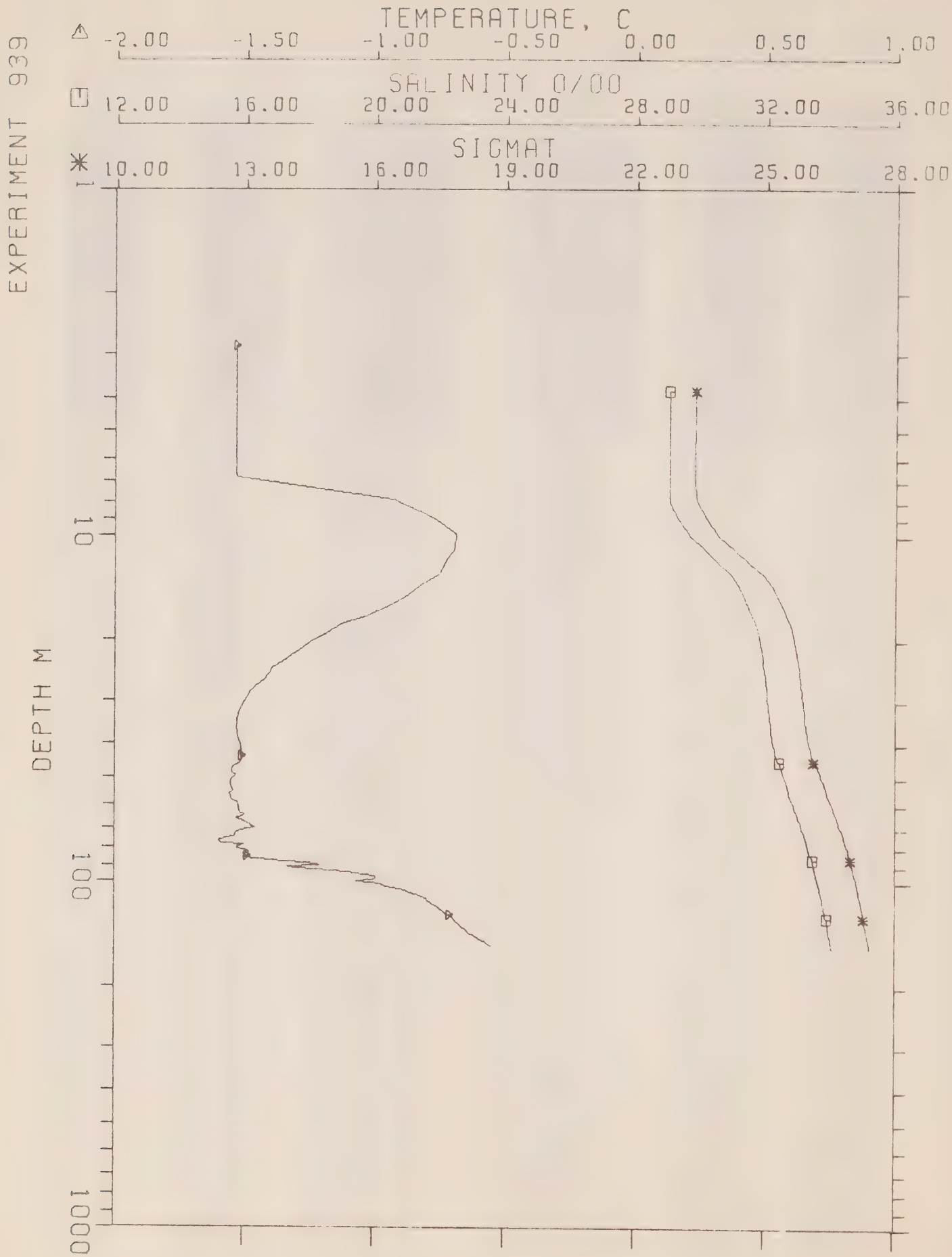
LAT N.80-34-52 LONG W.78-19-10 WATER DEPTH 199

DEPTH INCR. DATE 040474 LOCAL TIME 2026

DEPTH	PRES	SAL		TEMP		SIGMAT	SOUND
2.7	2.75	29.039	C	-1.543	D	23.369	1433.8
3.8	3.80	29.033	C	-1.544	D	23.364	1433.8
4.8	4.80	29.026	C	-1.542	D	23.358	1433.8
5.8	5.85	29.021	C	-1.542	D	23.354	1433.8
6.8	6.85	29.020	C	-1.542	D	23.353	1433.9
7.8	7.80			-0.913	D		
8.9	8.90	29.312	C	-0.783	D	23.576	1437.9
9.9	9.90	29.692	C	-0.689	D	23.880	1438.9
10.9	10.95	30.197	C	-0.697	D	24.289	1439.6
11.9	11.95	30.544	C	-0.725	D	24.569	1439.9
12.9	12.95	30.976	C	-0.743	D	24.918	1440.5
13.9	13.95	31.239	C	-0.815	D	25.133	1440.5
15.0	15.00	31.393	C	-0.874	D	25.259	1440.5
15.9	15.95	31.532	C	-0.942	D	25.373	1440.3
16.9	16.95	31.667	C	-1.031	D	25.485	1440.1
18.0	18.00	31.765	C	-1.122	D	25.566	1439.9
19.0	19.05	31.825	C	-1.182	D	25.616	1439.7
20.0	20.05	31.878	C	-1.233	D	25.660	1439.5
21.1	21.10	31.909	C	-1.266	D	25.687	1439.4
22.1	22.15	31.946	C	-1.310	D	25.717	1439.3
23.2	23.20	31.968	C	-1.344	D	25.736	1439.2
24.2	24.20	31.991	C	-1.371	D	25.755	1439.1
25.2	25.20	32.021	C	-1.409	D	25.780	1439.0
26.2	26.20	32.034	C	-1.411	D	25.791	1439.0
27.2	27.20	32.060	C	-1.442	D	25.813	1438.9
28.2	28.20	32.093	C	-1.477	D	25.840	1438.8
29.2	29.20	32.103	C	-1.485	D	25.848	1438.8
30.2	30.20	32.124	C	-1.502	D	25.866	1438.8
31.3	31.25	32.139	C	-1.514	D	25.878	1438.8
32.3	32.30	32.151	C	-1.518	D	25.888	1438.8
33.3	33.35	32.165	C	-1.525	D	25.899	1438.8
34.3	34.35	32.179	C	-1.531	D	25.911	1438.8
35.3	35.30	32.190	C	-1.534	D	25.920	1438.8
36.3	36.35	32.205	C	-1.534	D	25.932	1438.8
37.4	37.45	32.220	C	-1.531	D	25.944	1438.9
38.4	38.40	32.251	C	-1.530	D	25.969	1439.0
39.5	39.50	32.278	C	-1.526	D	25.991	1439.0
40.5	40.55	32.305	C	-1.519	D	26.012	1439.1
41.5	41.55	32.326	C	-1.515	D	26.030	1439.2
42.6	42.60	32.350	C	-1.511	D	26.050	1439.3
43.5	43.55	32.381	C	-1.513	D	26.074	1439.3
44.6	44.60	32.422	C	-1.514	D	26.108	1439.4
45.6	45.65	32.472	C	-1.515	D	26.148	1439.5
46.6	46.60	32.526	C	-1.534	D	26.193	1439.5
47.6	47.65	32.553	C	-1.555	D	26.214	1439.4
48.6	48.65	32.582	C	-1.550	D	26.238	1439.5
49.6	49.65	32.607	C	-1.539	D	26.258	1439.6
50.7	50.70	32.656	C	-1.549	D	26.298	1439.6
51.7	51.70	32.695	C	-1.555	D	26.330	1439.7
52.7	52.75	32.718	C	-1.556	D	26.348	1439.7
53.8	53.80	32.743	C	-1.554	D	26.369	1439.8
54.8	54.80	32.775	C	-1.545	D	26.394	1439.9
55.8	55.85	32.806	C	-1.559	D	26.419	1439.9
56.8	56.85	32.835	C	-1.551	D	26.443	1440.0
57.8	57.85	32.876	C	-1.555	D	26.477	1440.0
58.9	58.90	32.894	C	-1.538	D	26.490	1440.2
59.9	59.90	32.932	C	-1.531	D	26.522	1440.3
60.9	60.90	32.962	C	-1.523	D	26.545	1440.4
61.8	61.85	32.993	C	-1.524	D	26.571	1440.4
62.8	62.85	33.023	C	-1.520	D	26.595	1440.5
63.9	63.95	33.041	C	-1.501	D	26.609	1440.6
65.0	65.00	33.094	C	-1.520	D	26.652	1440.6

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
66.0	66.00	33.104	C	-1.535	D	26.661	1440.6
67.0	67.05	33.115	C	-1.508	D	26.669	1440.7
68.0	68.00	33.140	C	-1.483	D	26.689	1440.9
69.0	69.00	33.166	C	-1.473	D	26.710	1441.0
70.0	70.05	33.193	C	-1.457	D	26.731	1441.1
71.1	71.15	33.244	C	-1.502	D	26.773	1441.0
72.1	72.15	33.244	C	-1.526	D	26.774	1440.9
73.1	73.10	33.273	C	-1.537	D	26.797	1440.9
74.2	74.20	33.290	C	-1.538	D	26.812	1441.0
75.2	75.25	33.320	C	-1.566	D	26.837	1440.9
76.2	76.25	33.325	C	-1.612	D	26.842	1440.7
77.2	77.20	33.325	C	-1.567	D	26.841	1440.9
78.3	78.30	33.361	C	-1.495	D	26.868	1441.3
79.3	79.30	33.374	C	-1.508	D	26.879	1441.3
80.2	80.25	33.407	C	-1.530	D	26.906	1441.3
81.3	81.35	33.411	C	-1.502	D	26.909	1441.4
82.3	82.30	33.424	C	-1.470	D	26.918	1441.6
83.3	83.35	33.454	C	-1.497	D	26.943	1441.5
84.4	84.40	33.473	C	-1.483	D	26.958	1441.6
85.4	85.40	33.487	C	-1.500	D	26.970	1441.6
86.4	86.45	33.483	C	-1.473	D	26.966	1441.7
87.4	87.45	33.494	C	-1.359	D	26.972	1442.3
88.4	88.45	33.503	C	-1.285	D	26.977	1442.7
89.5	89.50	33.527	C	-1.223	D	26.995	1443.0
90.4	90.45	33.546	C	-1.190	D	27.009	1443.2
91.5	91.55	33.589	C	-1.282	D	27.047	1442.9
92.5	92.55			-1.229	D		
93.6	93.60	33.584	C	-1.097	D	27.037	1443.8
94.6	94.60	33.601	C	-1.075	D	27.050	1443.9
95.6	95.65	33.615	C	-1.032	D	27.060	1444.2
96.6	96.65	33.637	C	-0.993	D	27.076	1444.4
97.6	97.65	33.655	C	-0.989	D	27.091	1444.4
98.6	98.60	33.677	C	-1.014	D	27.110	1444.4
99.7	99.75	33.676	C	-1.074	D	27.110	1444.1
100.7	100.75	33.681	D	-1.015	E	27.112	1444.4
101.7	101.75	33.697	D	-0.980	E	27.125	1444.6
102.8	102.80	33.706	D	-0.960	E	27.131	1444.7
103.8	103.80	33.715	D	-0.928	E	27.138	1444.9
104.8	104.80	33.729	D	-0.909	E	27.148	1445.0
105.8	105.80	33.737	D	-0.891	E	27.153	1445.1
106.9	106.90	33.739	D	-0.879	E	27.155	1445.2
107.8	107.85	33.754	D	-0.877	E	27.167	1445.3
108.9	108.90	33.760	D	-0.844	E	27.170	1445.4
109.9	109.90	33.779	D	-0.829	E	27.185	1445.6
110.9	110.90	33.794	D	-0.817	E	27.197	1445.7
111.9	111.95	33.803	D	-0.805	E	27.204	1445.7
112.9	112.95	33.814	D	-0.799	E	27.213	1445.8
113.9	113.95	33.818	D	-0.792	E	27.215	1445.9
115.0	115.05	33.827	D	-0.784	E	27.223	1445.9
116.0	116.00	33.838	D	-0.775	E	27.231	1446.0
117.1	117.10	33.847	D	-0.767	E	27.238	1446.1
118.1	118.10	33.856	D	-0.759	E	27.245	1446.1
119.1	119.10	33.863	D	-0.751	E	27.251	1446.2
120.1	120.10	33.873	D	-0.745	E	27.258	1446.3
121.1	121.15	33.881	D	-0.739	E	27.265	1446.3
122.2	122.20	33.887	D	-0.734	E	27.269	1446.4
123.2	123.25	33.894	D	-0.728	E	27.275	1446.4
124.2	124.20	33.900	D	-0.722	E	27.279	1446.5
125.2	125.25	33.907	D	-0.717	E	27.285	1446.5
126.2	126.25	33.919	D	-0.711	E	27.294	1446.6
127.3	127.30	33.924	D	-0.705	E	27.298	1446.6
128.3	128.30	33.934	D	-0.701	E	27.306	1446.7
129.3	129.35	33.939	D	-0.695	E	27.310	1446.7
130.4	130.40	33.945	D	-0.690	E	27.315	1446.8
131.3	131.35	33.951	D	-0.686	E	27.319	1446.8
132.3	132.35	33.957	D	-0.680	E	27.324	1446.9
133.4	133.45	33.965	D	-0.673	E	27.330	1446.9
134.4	134.45	33.970	D	-0.667	E	27.333	1447.0
135.5	135.50	33.977	D	-0.662	E	27.339	1447.0

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
136.5	136.50	33.984 D	-0.659 E	27.345	1447.1
137.5	137.50	33.988 D	-0.656 E	27.347	1447.1
138.5	138.50	33.993 D	-0.652 E	27.352	1447.2
139.5	139.50	34.000 D	-0.642 E	27.357	1447.2
140.5	140.55	34.011 D	-0.636 E	27.366	1447.3
141.5	141.55	34.018 D	-0.631 E	27.371	1447.3
142.6	142.60	34.023 D	-0.628 E	27.375	1447.4
143.6	143.60	34.026 D	-0.621 E	27.377	1447.4
144.6	144.65	34.037 D	-0.613 E	27.386	1447.5
145.7	145.70	34.045 D	-0.606 E	27.391	1447.6
146.6	146.65	34.055 D	-0.598 E	27.400	1447.6
147.7	147.70	34.062 D	-0.589 E	27.405	1447.7
148.7	148.70	34.071 D	-0.582 E	27.412	1447.8
149.8	149.80	34.078 D	-0.577 E	27.417	1447.8
150.8	150.80	34.085 D	-0.571 E	27.423	1447.9
151.8	151.80	34.092 D	-0.565 E	27.428	1447.9
152.8	152.85	34.098 D	-0.557 E	27.432	1448.0
153.8	153.80	34.092 D	-0.551 E	27.428	1448.0


EXPERIMENT 939
TEMPERATURE, C
-2.00
-1.50
-1.00
-0.50
0.00
0.50
1.00
SALINITY 0/00
12.00
16.00
20.00
24.00
28.00
32.00
36.00
SIGMAT
10.00
13.00
16.00
19.00
22.00
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DEPTH M
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100
1000

CRUISE 15-74-012 D'IBERVILLE FIORD-74 EXPER NO. 939

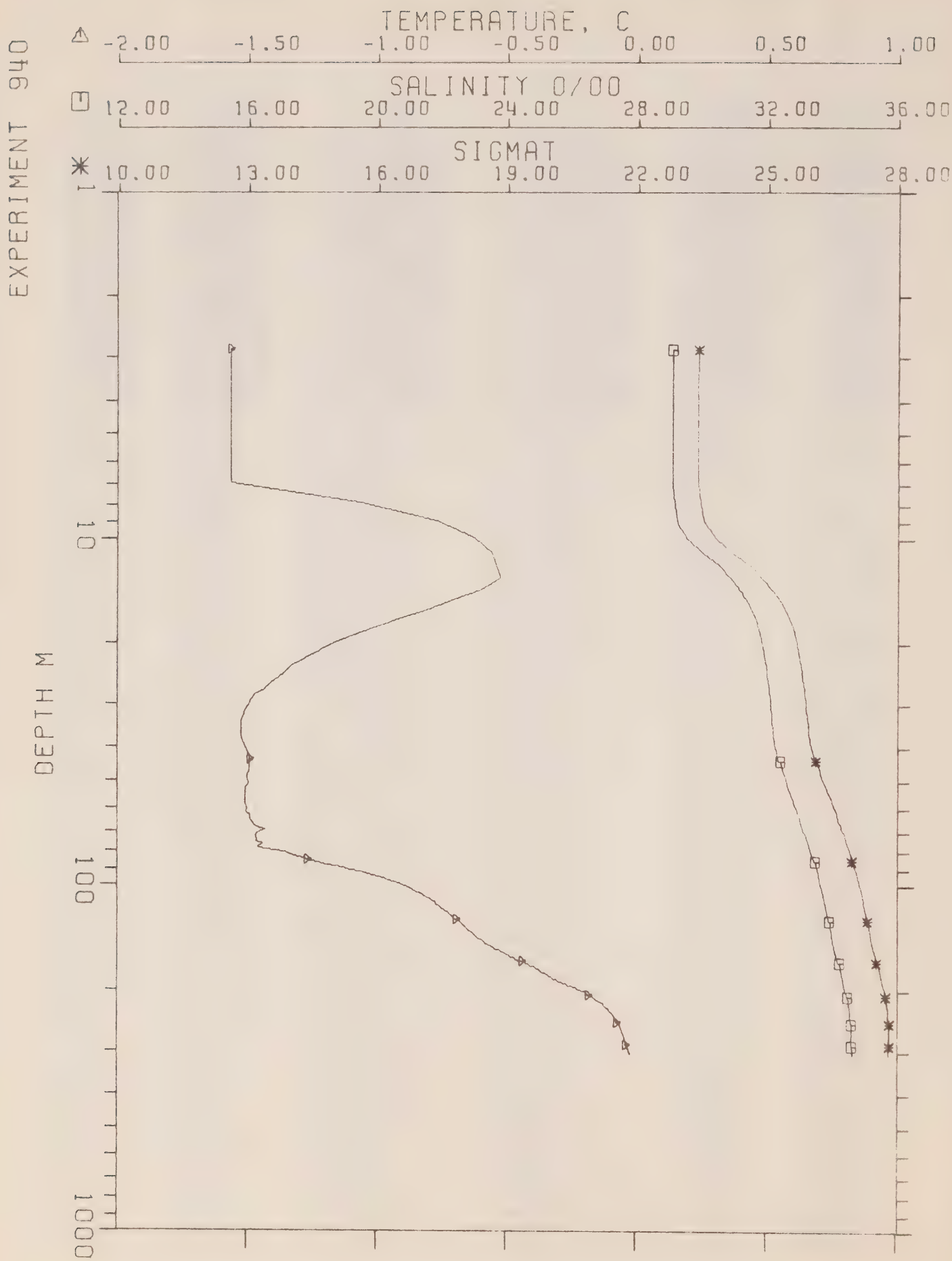
LAT N.80-34-52 LONG W.78-19-10 WATER DEPTH 199

DEPTH INCR. DATE 040474 LOCAL TIME 2045

DEPTH	PRES	SAL		TEMP		SIGMAT	SOUND
2.8	2.85			-1.542	D		
3.8	3.80	29.050	C	-1.542	D	23.377	1433.8
4.8	4.85	29.036	C	-1.542	D	23.366	1433.8
5.8	5.80	29.030	C	-1.540	D	23.361	1433.9
6.8	6.80	29.028	C	-1.539	D	23.360	1433.9
7.9	7.90	29.055	C	-0.937	D	23.372	1436.8
8.8	8.85	29.359	C	-0.780	D	23.614	1438.0
9.9	9.90	29.704	C	-0.683	D	23.890	1438.9
10.9	10.95	30.202	C	-0.691	D	24.292	1439.6
11.9	11.95	30.594	C	-0.725	D	24.610	1440.0
12.9	12.90	30.985	C	-0.745	D	24.926	1440.5
13.9	13.95	31.260	C	-0.818	D	25.150	1440.5
15.0	15.00	31.411	C	-0.881	D	25.274	1440.5
16.0	16.00	31.539	C	-0.940	D	25.379	1440.4
17.1	17.10	31.670	C	-1.028	D	25.487	1440.2
18.1	18.10	31.775	C	-1.124	D	25.574	1439.9
19.1	19.10	31.827	C	-1.179	D	25.618	1439.7
20.1	20.15	31.884	C	-1.239	D	25.666	1439.5
21.1	21.10	31.913	C	-1.268	D	25.690	1439.4
22.2	22.20	31.950	C	-1.314	D	25.721	1439.3
23.1	23.15	31.979	C	-1.349	D	25.745	1439.2
24.2	24.20	32.009	C	-1.392	D	25.770	1439.0
25.2	25.20	32.023	C	-1.404	D	25.782	1439.0
26.2	26.25	32.043	C	-1.422	D	25.799	1439.0
27.2	27.25	32.071	C	-1.454	D	25.822	1438.9
28.3	28.30	32.091	C	-1.475	D	25.839	1438.8
29.2	29.25	32.099	C	-1.484	D	25.846	1438.8
30.2	30.25	32.122	C	-1.499	D	25.864	1438.8
31.3	31.30	32.138	C	-1.512	D	25.878	1438.8
32.3	32.30	32.154	C	-1.519	D	25.891	1438.8
33.3	33.35	32.169	C	-1.526	D	25.903	1438.8
34.3	34.35	32.183	C	-1.532	D	25.914	1438.8
35.4	35.45	32.192	C	-1.532	D	25.922	1438.8
36.4	36.45	32.208	C	-1.533	D	25.934	1438.8
37.4	37.45	32.226	C	-1.530	D	25.949	1438.9
38.4	38.40	32.256	C	-1.530	D	25.973	1439.0
39.5	39.50	32.282	C	-1.524	D	25.994	1439.0
40.5	40.50	32.311	C	-1.517	D	26.018	1439.1
41.5	41.55	32.333	C	-1.514	D	26.036	1439.2
42.5	42.55	32.363	C	-1.514	D	26.060	1439.3
43.5	43.55	32.393	C	-1.517	D	26.085	1439.3
44.5	44.55	32.437	C	-1.512	D	26.119	1439.4
45.6	45.60	32.487	C	-1.517	D	26.160	1439.5
46.6	46.65	32.535	C	-1.543	D	26.200	1439.4
47.7	47.70	32.563	C	-1.551	D	26.222	1439.4
48.6	48.65	32.592	C	-1.548	D	26.246	1439.5
49.7	49.70	32.622	C	-1.537	D	26.270	1439.6
50.7	50.70	32.667	C	-1.550	D	26.306	1439.6
51.6	51.65	32.702	C	-1.556	D	26.335	1439.7
52.7	52.75	32.722	C	-1.557	D	26.352	1439.7
53.7	53.75	32.746	C	-1.554	D	26.371	1439.8
54.8	54.80	32.777	C	-1.545	D	26.396	1439.9
55.8	55.80	32.808	C	-1.563	D	26.422	1439.9
56.8	56.85	32.847	C	-1.554	D	26.453	1440.0
57.9	57.90	32.881	C	-1.557	D	26.481	1440.0
58.9	58.90	32.902	C	-1.537	D	26.497	1440.2
59.9	59.95	32.939	C	-1.530	D	26.527	1440.3
60.9	60.95	32.966	C	-1.523	D	26.549	1440.4
62.0	62.00	32.995	C	-1.523	D	26.572	1440.4
63.0	63.00	33.021	C	-1.518	D	26.593	1440.5
64.0	64.05	33.044	C	-1.501	D	26.611	1440.6
65.0	65.05	33.092	C	-1.520	D	26.651	1440.6

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
66.0	66.05	33.104	C	-1.534	D	26.661	1440.6
67.1	67.10	33.115	C	-1.507	D	26.669	1440.7
68.0	68.05	33.140	C	-1.483	D	26.689	1440.9
69.1	69.10	33.171	C	-1.473	D	26.713	1441.0
70.1	70.10	33.195	C	-1.455	D	26.732	1441.2
71.1	71.15	33.255	C	-1.509	D	26.782	1441.0
72.1	72.10	33.249	C	-1.523	D	26.778	1440.9
73.1	73.15	33.277	C	-1.536	D	26.801	1440.9
74.1	74.15	33.291	C	-1.537	D	26.812	1441.0
75.2	75.25	33.323	C	-1.568	D	26.839	1440.9
76.2	76.25	33.323	C	-1.603	D	26.839	1440.7
77.3	77.30	33.341	C	-1.596	D	26.854	1440.8
78.3	78.30	33.351	C	-1.499	D	26.860	1441.3
79.3	79.30	33.376	C	-1.525	D	26.881	1441.2
80.3	80.30	33.407	C	-1.537	D	26.906	1441.2
81.3	81.35	33.414	C	-1.505	D	26.911	1441.4
82.4	82.40	33.418	C	-1.479	D	26.913	1441.6
83.4	83.40	33.463	C	-1.511	D	26.951	1441.5
84.4	84.45	33.472	C	-1.495	D	26.958	1441.6
85.4	85.45	33.485	C	-1.510	D	26.969	1441.6
86.4	86.45	33.484	C	-1.451	D	26.966	1441.8
87.4	87.45	33.501	C	-1.349	D	26.977	1442.4
88.5	88.50	33.506	C	-1.261	D	26.979	1442.8
89.5	89.55	33.537	C	-1.203	D	27.002	1443.1
90.5	90.50	33.575	C	-1.339	D	27.037	1442.6
91.5	91.55	33.569	C	-1.302	D	27.031	1442.8
92.5	92.55	33.563	C	-1.237	D	27.024	1443.1
93.6	93.65	33.582	C	-1.104	D	27.035	1443.7
94.6	94.65	33.600	C	-1.078	D	27.049	1443.9
95.6	95.65	33.619	C	-1.042	D	27.064	1444.1
96.6	96.65	33.634	C	-1.000	D	27.074	1444.3
97.7	97.75	33.656	C	-0.988	D	27.091	1444.4
98.7	98.70	33.675	C	-1.007	D	27.108	1444.4
99.7	99.70	33.681	C	-1.077	D	27.115	1444.1
100.8	100.80	33.682	D	-1.013	E	27.113	1444.4
101.8	101.80	33.700	D	-0.984	E	27.127	1444.6
102.8	102.80	33.707	D	-0.959	E	27.132	1444.7
103.8	103.80	33.718	D	-0.928	E	27.140	1444.9
104.8	104.80	33.732	D	-0.909	E	27.150	1445.0
105.8	105.85	33.741	D	-0.886	E	27.156	1445.2
106.9	106.90	33.747	D	-0.875	E	27.161	1445.3
107.9	107.95	33.755	D	-0.868	E	27.167	1445.3
108.9	108.95	33.765	D	-0.845	E	27.175	1445.5
109.9	109.95	33.783	D	-0.830	E	27.189	1445.6
110.9	110.95	33.792	D	-0.818	E	27.196	1445.6
112.0	112.00	33.804	D	-0.806	E	27.205	1445.7
113.1	113.10	33.814	D	-0.798	E	27.212	1445.8
114.0	114.05	33.821	D	-0.791	E	27.218	1445.9
115.0	115.00	33.831	D	-0.783	E	27.226	1445.9
116.1	116.10	33.839	D	-0.775	E	27.232	1446.0
117.1	117.10	33.847	D	-0.767	E	27.238	1446.1
118.1	118.10	33.858	D	-0.759	E	27.247	1446.1
119.1	119.15	33.866	D	-0.753	E	27.253	1446.2
120.2	120.20	33.873	D	-0.745	E	27.259	1446.3
121.1	121.15	33.882	D	-0.738	E	27.265	1446.3
122.2	122.20	33.888	D	-0.734	E	27.270	1446.4
123.2	123.25	33.898	D	-0.728	E	27.278	1446.4
124.3	124.30	33.906	D	-0.722	E	27.284	1446.5
125.3	125.30	33.912	D	-0.715	E	27.288	1446.5
126.2	126.25	33.918	D	-0.709	E	27.294	1446.6
127.3	127.30	33.927	D	-0.705	E	27.300	1446.6
128.3	128.35	33.933	D	-0.701	E	27.305	1446.7
129.4	129.40	33.938	D	-0.695	E	27.309	1446.7
130.4	130.40	33.945	D	-0.691	E	27.314	1446.8
131.4	131.40	33.950	D	-0.685	E	27.318	1446.8
132.5	132.50	33.957	D	-0.680	E	27.323	1446.9
133.4	133.45	33.962	D	-0.673	E	27.328	1446.9
134.5	134.50	33.972	D	-0.669	E	27.335	1447.0
135.5	135.55	33.977	D	-0.664	E	27.339	1447.0

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
136.5	136.50	33.984	D	-0.660	E	27.344	1447.1
137.6	137.60	33.986	D	-0.655	E	27.346	1447.1
138.6	138.60	33.992	D	-0.652	E	27.351	1447.2
139.5	139.55	34.000	D	-0.644	E	27.357	1447.2
140.6	140.60	34.009	D	-0.638	E	27.364	1447.3
141.6	141.60	34.019	D	-0.632	E	27.372	1447.3
142.6	142.65	34.022	D	-0.627	E	27.374	1447.4
143.6	143.65	34.029	D	-0.622	E	27.379	1447.4
144.7	144.75	34.038	D	-0.612	E	27.386	1447.5
145.7	145.70	34.046	D	-0.605	E	27.393	1447.6
146.7	146.70	34.057	D	-0.597	E	27.401	1447.6
147.7	147.70	34.066	D	-0.589	E	27.408	1447.7
148.7	148.70	34.075	D	-0.580	E	27.415	1447.8
149.7	149.75	34.082	D	-0.574	E	27.420	1447.8
150.8	150.80	34.090	D	-0.568	E	27.426	1447.9
151.8	151.85	34.096	D	-0.563	E	27.431	1447.9
152.9	152.90	34.100	D	-0.556	E	27.434	1448.0


EXPERIMENT 940
TEMPERATURE, C
-2.00
-1.50
-1.00
-0.50
0.00
0.50
1.00
SALINITY 0/00
12.00
16.00
20.00
24.00
28.00
32.00
36.00
SIGMAT
10.00
13.00
16.00
19.00
22.00
25.00
28.00
DEPTH M
1
10
100
1000

CRUISE 15-74-012 D'IBERVILLE FIORD-74 EXPER NO. 940

LAT N. 80-35-30 LONG W. 78-43-00 WATER DEPTH 0

DEPTH INCR. DATE 050474 LOCAL TIME 1625

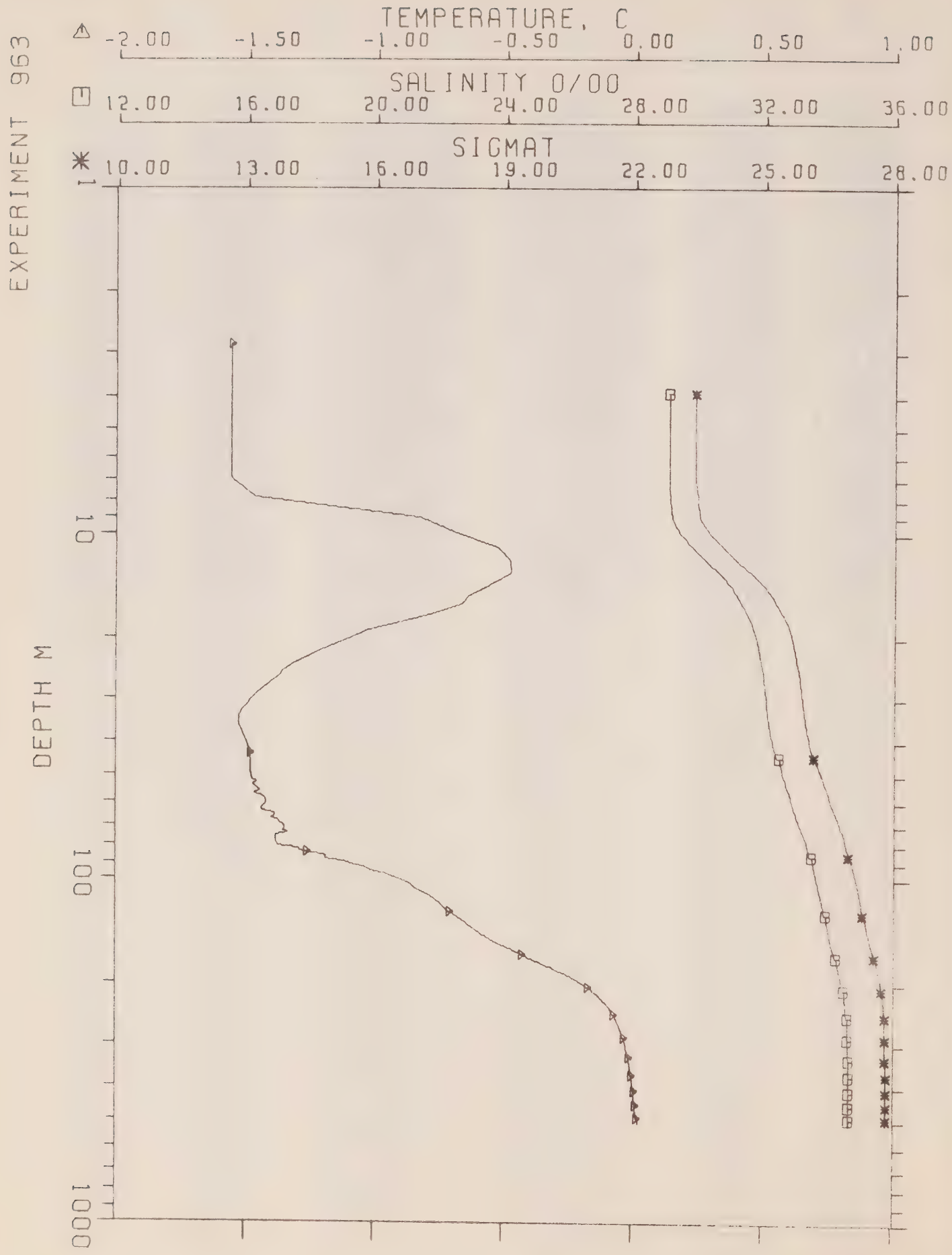
DEPTH	PRES	SAL	TEMP	SIGMAT	SOUND
2.8	2.85	29.073 C	-1.568 D	23.396	1433.7
3.8	3.85	29.069 C	-1.568 D	23.394	1433.7
4.8	4.85	29.064 C	-1.568 D	23.389	1433.8
5.8	5.85	29.064 C	-1.569 D	23.390	1433.8
6.9	6.90	29.063 C	-1.568 D	23.389	1433.8
7.8	7.85		-1.072 D		
8.9	8.90	29.225 C	-0.775 D	23.506	1437.8
9.9	9.95	29.545 C	-0.629 D	23.760	1439.0
11.0	11.00	30.083 C	-0.561 D	24.193	1440.0
11.9	11.95	30.548 C	-0.543 D	24.567	1440.8
12.9	12.95	30.916 C	-0.526 D	24.863	1441.4
14.0	14.00	31.207 C	-0.594 D	25.100	1441.5
15.0	15.05	31.407 C	-0.704 D	25.265	1441.3
16.0	16.05	31.559 C	-0.794 D	25.391	1441.1
17.0	17.05	31.675 C	-0.904 D	25.487	1440.7
18.0	18.05	31.766 C	-1.004 D	25.564	1440.4
19.1	19.15	31.836 C	-1.102 D	25.623	1440.1
20.1	20.10	31.885 C	-1.175 D	25.664	1439.8
21.1	21.10	31.913 C	-1.220 D	25.689	1439.7
22.1	22.15	31.954 C	-1.274 D	25.723	1439.5
23.2	23.20	31.989 C	-1.324 D	25.752	1439.3
24.2	24.25	32.008 C	-1.352 D	25.768	1439.2
25.3	25.30	32.034 C	-1.378 D	25.790	1439.2
26.2	26.25	32.061 C	-1.412 D	25.813	1439.0
27.3	27.30	32.077 C	-1.436 D	25.827	1439.0
28.2	28.25	32.101 C	-1.468 D	25.847	1438.9
29.2	29.25	32.118 C	-1.484 D	25.861	1438.8
30.3	30.30	32.133 C	-1.497 D	25.873	1438.8
31.3	31.35	32.147 C	-1.508 D	25.884	1438.8
32.4	32.40	32.159 C	-1.517 D	25.895	1438.8
33.4	33.40	32.175 C	-1.526 D	25.908	1438.8
34.4	34.40	32.189 C	-1.530 D	25.919	1438.8
35.5	35.50	32.201 C	-1.532 D	25.929	1438.8
36.5	36.50	32.217 C	-1.532 D	25.942	1438.9
37.5	37.50	32.236 C	-1.529 D	25.958	1438.9
38.5	38.50	32.254 C	-1.524 D	25.972	1439.0
39.5	39.50	32.277 C	-1.519 D	25.990	1439.1
40.5	40.55	32.302 C	-1.512 D	26.011	1439.1
41.5	41.55	32.338 C	-1.504 D	26.039	1439.2
42.6	42.60	32.374 C	-1.497 D	26.068	1439.3
43.6	43.60	32.420 C	-1.494 D	26.105	1439.4
44.6	44.65	32.456 C	-1.494 D	26.135	1439.5
45.6	45.65	32.486 C	-1.496 D	26.159	1439.6
46.6	46.65	32.519 C	-1.496 D	26.186	1439.6
47.6	47.65	32.551 C	-1.496 D	26.211	1439.7
48.7	48.75	32.591 C	-1.503 D	26.245	1439.7
49.8	49.80	32.627 C	-1.503 D	26.273	1439.8
50.8	50.80	32.656 C	-1.498 D	26.297	1439.9
51.8	51.85	32.695 C	-1.502 D	26.328	1439.9
52.8	52.80	32.736 C	-1.508 D	26.362	1440.0
53.8	53.85	32.764 C	-1.510 D	26.384	1440.0
54.9	54.90	32.803 C	-1.510 D	26.416	1440.1
55.9	55.90	32.830 C	-1.514 D	26.438	1440.1
56.8	56.85	32.854 C	-1.509 D	26.458	1440.2
57.9	57.90	32.884 C	-1.513 D	26.482	1440.2
58.9	58.90	32.914 C	-1.513 D	26.506	1440.3
59.9	59.90	32.952 C	-1.510 D	26.537	1440.4
60.9	60.90	32.972 C	-1.505 D	26.553	1440.5
61.9	61.95	33.011 C	-1.509 D	26.584	1440.5
63.0	63.00	33.025 C	-1.494 D	26.596	1440.6
64.0	64.05	33.056 C	-1.497 D	26.621	1440.7
65.0	65.05	33.072 C	-1.494 D	26.634	1440.7

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
66.0	66.05	33.094	C	-1.489	D	26.652	1440.8
67.1	67.10	33.114	C	-1.485	D	26.668	1440.8
68.1	68.10	33.139	C	-1.471	D	26.687	1441.0
69.1	69.15	33.165	C	-1.431	D	26.708	1441.2
70.1	70.15	33.204	C	-1.452	D	26.740	1441.2
71.2	71.20	33.240	C	-1.467	D	26.769	1441.2
72.2	72.20	33.257	C	-1.469	D	26.783	1441.2
73.2	73.25	33.273	C	-1.475	D	26.796	1441.2
74.2	74.25	33.291	C	-1.466	D	26.810	1441.3
75.2	75.25	33.302	C	-1.475	D	26.820	1441.3
76.2	76.25	33.333	C	-1.442	D	26.843	1441.5
77.3	77.30	33.361	C	-1.467	D	26.868	1441.4
78.3	78.35	33.376	C	-1.464	D	26.880	1441.5
79.4	79.40	33.389	C	-1.399	D	26.888	1441.8
80.4	80.40	33.414	C	-1.361	D	26.907	1442.1
81.4	81.45	33.430	C	-1.338	D	26.920	1442.2
82.5	82.50	33.451	C	-1.325	D	26.936	1442.3
83.4	83.40	33.467	C	-1.305	D	26.948	1442.5
84.5	84.55	33.485	C	-1.277	D	26.962	1442.6
85.5	85.55	33.505	C	-1.255	D	26.978	1442.8
86.4	86.45	33.517	C	-1.235	D	26.987	1442.9
87.5	87.55	33.527	C	-1.205	D	26.994	1443.1
88.5	88.55	33.541	C	-1.162	D	27.004	1443.3
89.6	89.65	33.557	C	-1.120	D	27.016	1443.6
90.6	90.60	33.582	C	-1.111	D	27.036	1443.7
91.6	91.65	33.588	C	-1.071	D	27.040	1443.9
92.6	92.60	33.607	C	-1.057	D	27.054	1444.0
93.7	93.70	33.613	C	-1.026	D	27.058	1444.1
94.7	94.70	33.629	C	-0.999	D	27.070	1444.3
95.7	95.70	33.646	C	-0.986	D	27.084	1444.4
96.7	96.75	33.659	C	-0.958	D	27.093	1444.6
97.7	97.75	33.672	C	-0.947	D	27.103	1444.7
98.8	98.80	33.687	C	-0.921	D	27.114	1444.8
99.8	99.85	33.696	C	-0.908	D	27.121	1444.9
100.8	100.85	33.707	D	-0.898	E	27.130	1445.0
101.8	101.85	33.721	D	-0.883	E	27.141	1445.1
102.9	102.95	33.731	D	-0.871	E	27.148	1445.2
103.8	103.85	33.745	D	-0.858	E	27.159	1445.3
104.9	104.95	33.755	D	-0.848	E	27.167	1445.4
105.9	105.95	33.767	D	-0.837	E	27.176	1445.4
106.9	106.95	33.778	D	-0.828	E	27.184	1445.5
108.0	108.05	33.786	D	-0.819	E	27.191	1445.6
109.0	109.00	33.796	D	-0.809	E	27.198	1445.7
110.1	110.10	33.806	D	-0.800	E	27.206	1445.7
111.1	111.10	33.817	D	-0.792	E	27.215	1445.8
112.0	112.00	33.825	D	-0.786	E	27.221	1445.9
113.1	113.10	33.833	D	-0.778	E	27.227	1445.9
114.1	114.15	33.843	D	-0.771	E	27.235	1446.0
115.1	115.15	33.851	D	-0.764	E	27.241	1446.1
116.1	116.15	33.858	D	-0.758	E	27.247	1446.1
117.2	117.20	33.867	D	-0.751	E	27.254	1446.2
118.2	118.25	33.877	D	-0.744	E	27.262	1446.2
119.2	119.25	33.883	D	-0.735	E	27.266	1446.3
120.2	120.25	33.895	D	-0.729	E	27.275	1446.4
121.2	121.25	33.902	D	-0.724	E	27.281	1446.4
122.2	122.25	33.909	D	-0.718	E	27.286	1446.5
123.3	123.30	33.915	D	-0.713	E	27.291	1446.5
124.3	124.30	33.921	D	-0.709	E	27.295	1446.6
125.4	125.40	33.926	D	-0.702	E	27.300	1446.6
126.4	126.40	33.937	D	-0.697	E	27.308	1446.7
127.4	127.40	33.945	D	-0.690	E	27.314	1446.7
128.4	128.40	33.951	D	-0.685	E	27.319	1446.8
129.4	129.45	33.957	D	-0.680	E	27.323	1446.8
130.5	130.50	33.963	D	-0.676	E	27.328	1446.9
131.5	131.55	33.971	D	-0.671	E	27.335	1446.9
132.5	132.55	33.974	D	-0.666	E	27.337	1447.0
133.6	133.65	33.981	D	-0.662	E	27.342	1447.0
134.6	134.60	33.987	D	-0.657	E	27.347	1447.1
135.6	135.65	33.993	D	-0.652	E	27.352	1447.1

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
136.6	136.65	33.998 D	-0.647 E	27.356	1447.2
137.6	137.65	34.006 D	-0.642 E	27.362	1447.2
138.6	138.65	34.011 D	-0.636 E	27.365	1447.3
139.6	139.65	34.018 D	-0.631 E	27.371	1447.3
140.7	140.70	34.024 D	-0.625 E	27.375	1447.4
141.8	141.80	34.031 D	-0.620 E	27.381	1447.4
142.7	142.75	34.037 D	-0.615 E	27.386	1447.5
143.7	143.75	34.044 D	-0.607 E	27.391	1447.5
144.8	144.80	34.053 D	-0.602 E	27.398	1447.6
145.8	145.85	34.058 D	-0.596 E	27.402	1447.6
146.8	146.85	34.065 D	-0.591 E	27.407	1447.7
147.8	147.85	34.072 D	-0.583 E	27.413	1447.7
148.9	148.95	34.080 D	-0.579 E	27.419	1447.8
149.9	149.90	34.088 D	-0.570 E	27.425	1447.9
150.9	150.95	34.097 D	-0.562 E	27.432	1447.9
152.0	152.00	34.106 D	-0.555 E	27.439	1448.0
152.9	152.95	34.117 D	-0.546 E	27.448	1448.1
154.0	154.05	34.127 D	-0.536 E	27.455	1448.1
155.0	155.00	34.136 D	-0.528 E	27.462	1448.2
156.1	156.10	34.145 D	-0.521 E	27.469	1448.3
157.0	157.05	34.157 D	-0.515 E	27.478	1448.3
158.2	158.20	34.161 D	-0.508 E	27.482	1448.4
159.1	159.15	34.169 D	-0.501 E	27.488	1448.4
160.1	160.15	34.177 D	-0.494 E	27.493	1448.5
161.2	161.25	34.185 D	-0.487 E	27.500	1448.5
162.1	162.15	34.194 D	-0.479 E	27.507	1448.6
163.2	163.25	34.203 D	-0.473 E	27.513	1448.7
164.3	164.30	34.212 D	-0.463 E	27.521	1448.8
165.3	165.30	34.221 D	-0.454 E	27.528	1448.8
166.3	166.30	34.230 D	-0.445 E	27.535	1448.9
167.3	167.30	34.241 D	-0.437 E	27.543	1449.0
168.3	168.35	34.249 D	-0.430 E	27.549	1449.0
169.3	169.35	34.254 D	-0.425 E	27.553	1449.1
170.4	170.40	34.261 D	-0.418 E	27.559	1449.1
171.4	171.40	34.272 D	-0.410 E	27.567	1449.2
172.4	172.45	34.279 D	-0.402 E	27.572	1449.3
173.4	173.45	34.285 D	-0.396 E	27.577	1449.3
174.5	174.55	34.292 D	-0.391 E	27.582	1449.4
175.4	175.45	34.297 D	-0.385 E	27.586	1449.4
176.5	176.50	34.307 D	-0.378 E	27.594	1449.5
177.6	177.60	34.311 D	-0.374 E	27.597	1449.5
178.6	178.60	34.317 D	-0.367 E	27.601	1449.6
179.6	179.60	34.323 D	-0.362 E	27.606	1449.6
180.6	180.60	34.329 D	-0.355 E	27.611	1449.7
181.7	181.70	34.336 D	-0.350 E	27.616	1449.7
182.7	182.70	34.341 D	-0.345 E	27.619	1449.8
183.6	183.65	34.347 D	-0.339 E	27.624	1449.8
184.6	184.65	34.350 D	-0.334 E	27.627	1449.9
185.7	185.75	34.354 D	-0.329 E	27.630	1449.9
186.8	186.80	34.361 D	-0.324 E	27.635	1450.0
187.8	187.85	34.366 D	-0.317 E	27.638	1450.0
188.8	188.85	34.370 D	-0.312 E	27.642	1450.1
189.8	189.85	34.376 D	-0.305 E	27.646	1450.1
190.9	190.90	34.384 D	-0.297 E	27.652	1450.2
191.8	191.85	34.391 D	-0.291 E	27.657	1450.3
192.8	192.85	34.399 D	-0.281 E	27.663	1450.3
193.8	193.85	34.407 D	-0.274 E	27.669	1450.4
194.9	194.90	34.415 D	-0.265 E	27.676	1450.5
195.9	195.90	34.423 D	-0.257 E	27.682	1450.5
196.9	196.95	34.431 D	-0.248 E	27.688	1450.6
198.0	198.00	34.440 D	-0.239 E	27.695	1450.7
199.0	199.05	34.446 D	-0.233 E	27.699	1450.7
200.0	200.05	34.454 D	-0.224 E	27.705	1450.8
201.1	201.10	34.461 D	-0.218 E	27.710	1450.8
202.1	202.15	34.464 D	-0.211 E	27.713	1450.9
203.2	203.20	34.471 D	-0.206 E	27.718	1450.9
204.2	204.20	34.475 D	-0.201 E	27.721	1451.0
205.2	205.20	34.478 D	-0.198 E	27.724	1451.0
206.2	206.20	34.482 D	-0.197 E	27.726	1451.0

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
207.2	207.25	34.481	D	-0.191	E	27.726	1451.1
208.3	208.30	34.488	D	-0.188	E	27.731	1451.1
209.3	209.30	34.493	D	-0.183	E	27.734	1451.2
210.3	210.35	34.496	D	-0.177	E	27.737	1451.2
211.4	211.40	34.502	D	-0.171	E	27.741	1451.3
212.4	212.40	34.506	D	-0.167	E	27.744	1451.3
213.3	213.35	34.509	D	-0.164	E	27.747	1451.4
214.4	214.40	34.514	D	-0.159	E	27.751	1451.4
215.4	215.40	34.518	D	-0.155	E	27.753	1451.4
216.4	216.45	34.521	D	-0.151	E	27.756	1451.5
217.4	217.45	34.525	D	-0.146	E	27.759	1451.5
218.5	218.55	34.529	D	-0.142	E	27.762	1451.6
219.5	219.55	34.531	D	-0.137	E	27.764	1451.6
220.5	220.50	34.536	D	-0.135	E	27.767	1451.6
221.5	221.55	34.539	D	-0.132	E	27.769	1451.7
222.5	222.55	34.541	D	-0.129	E	27.771	1451.7
223.6	223.60	34.542	D	-0.126	E	27.772	1451.7
224.6	224.65	34.546	D	-0.124	E	27.775	1451.8
225.6	225.65	34.551	D	-0.121	E	27.778	1451.8
226.6	226.60	34.553	D	-0.117	E	27.780	1451.8
227.7	227.70	34.556	D	-0.114	E	27.782	1451.9
228.7	228.70	34.557	D	-0.112	E	27.783	1451.9
229.7	229.70	34.560	D	-0.110	E	27.786	1451.9
230.7	230.75	34.562	D	-0.108	E	27.787	1452.0
231.8	231.80	34.562	D	-0.105	E	27.786	1452.0
232.8	232.80	34.563	D	-0.103	E	27.787	1452.0
233.8	233.85	34.568	D	-0.102	E	27.791	1452.1
234.8	234.80	34.569	D	-0.099	E	27.792	1452.1
235.9	235.90	34.569	D	-0.096	E	27.792	1452.1
237.0	237.00	34.572	D	-0.095	E	27.794	1452.1
237.9	237.90	34.575	D	-0.093	E	27.796	1452.2
238.9	238.95	34.576	D	-0.092	E	27.797	1452.2
240.0	240.05	34.578	D	-0.090	E	27.799	1452.2
241.0	241.05	34.579	D	-0.088	E	27.800	1452.3
242.0	242.05	34.581	D	-0.086	E	27.801	1452.3
243.0	243.05	34.583	D	-0.085	E	27.802	1452.3
244.1	244.10	34.584	D	-0.084	E	27.803	1452.3
245.1	245.10	34.584	D	-0.081	E	27.803	1452.4
246.1	246.15	34.585	D	-0.080	E	27.804	1452.4
247.2	247.20	34.587	D	-0.080	E	27.806	1452.4
248.2	248.20	34.587	D	-0.078	E	27.806	1452.4
249.1	249.15	34.589	D	-0.076	E	27.807	1452.5
250.2	250.20	34.591	D	-0.074	E	27.809	1452.5
251.2	251.25	34.591	D	-0.073	E	27.809	1452.5
252.2	252.25	34.594	D	-0.072	E	27.811	1452.5
253.2	253.25	34.595	D	-0.070	E	27.812	1452.6
254.3	254.30	34.595	D	-0.068	E	27.812	1452.6
255.3	255.35	34.598	D	-0.067	E	27.814	1452.6
256.3	256.30	34.600	D	-0.066	E	27.815	1452.6
257.4	257.40	34.600	D	-0.065	E	27.815	1452.7
258.4	258.45	34.600	D	-0.063	E	27.815	1452.7
259.3	259.35	34.601	D	-0.064	E	27.816	1452.7
260.4	260.40	34.602	D	-0.062	E	27.817	1452.7
261.4	261.45	34.603	D	-0.061	E	27.818	1452.7
262.5	262.55	34.606	D	-0.062	E	27.820	1452.8
263.5	263.50	34.606	D	-0.062	E	27.820	1452.8
264.5	264.50	34.605	D	-0.060	E	27.819	1452.8
265.5	265.55	34.607	D	-0.060	E	27.821	1452.8
266.5	266.65	34.606	D	-0.058	E	27.820	1452.8
267.6	267.65	34.607	D	-0.057	E	27.821	1452.9
268.6	268.60	34.609	D	-0.057	E	27.822	1452.9
269.6	269.60	34.610	D	-0.056	E	27.823	1452.9
270.7	270.70	34.611	D	-0.055	E	27.824	1452.9
271.7	271.75	34.609	D	-0.053	E	27.822	1453.0
272.8	272.80	34.612	D	-0.052	E	27.824	1453.0
273.7	273.75	34.612	D	-0.052	E	27.825	1453.0
274.7	274.75	34.612	D	-0.050	E	27.824	1453.0
275.8	275.80	34.612	D	-0.050	E	27.824	1453.0
276.8	276.85	34.614	D	-0.050	E	27.826	1453.1

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
277.8	277.85	34.614	D	-0.049	E	27.826	1453.1
278.8	278.85	34.615	D	-0.049	E	27.827	1453.1
279.9	279.90	34.614	D	-0.048	E	27.826	1453.1
280.9	280.95	34.615	D	-0.047	E	27.826	1453.1
281.9	281.95	34.615	D	-0.047	E	27.827	1453.2
282.8	282.85	34.615	D	-0.045	E	27.826	1453.2
284.0	284.00	34.616	D	-0.045	E	27.828	1453.2
285.0	285.00	34.616	D	-0.044	E	27.827	1453.2
286.0	286.00	34.618	D	-0.044	E	27.829	1453.2
287.0	287.00	34.616	D	-0.042	E	27.827	1453.3
288.1	288.10	34.618	D	-0.042	E	27.828	1453.3
289.0	289.05	34.620	D	-0.043	E	27.830	1453.3
290.1	290.10	34.621	D	-0.043	E	27.831	1453.3
291.1	291.15	34.619	D	-0.041	E	27.830	1453.3
292.1	292.10	34.621	D	-0.041	E	27.831	1453.4
293.2	293.20	34.620	D	-0.040	E	27.830	1453.4
294.2	294.25	34.621	D	-0.039	E	27.831	1453.4
295.2	295.25	34.621	D	-0.038	E	27.831	1453.4
296.2	296.25	34.622	D	-0.037	E	27.831	1453.5
297.3	297.30	34.622	D	-0.037	E	27.831	1453.5
298.3	298.30	34.621	D	-0.035	E	27.831	1453.5
299.4	299.40	34.621	D	-0.035	E	27.831	1453.5
300.4	300.40	34.623	D	-0.035	E	27.832	1453.5
301.4	301.40	34.623	D	-0.034	E	27.832	1453.6
302.4	302.40	34.624	D	-0.034	E	27.833	1453.6
303.4	303.45	34.623	D	-0.033	E	27.832	1453.6
304.4	304.45	34.622	D	-0.032	E	27.831	1453.6
305.5	305.50	34.623	D	-0.032	E	27.833	1453.6
306.5	306.50	34.624	D	-0.031	E	27.833	1453.7


EXPERIMENT 963
TEMPERATURE, C
-2.00
-1.50
-1.00
-0.50
0.00
0.50
1.00
SALINITY 0/00
12.00
16.00
20.00
24.00
28.00
32.00
36.00
SIGMAT
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DEPTH M
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CRUISE 15-74-012 D'IBERVILLE FIORD-74 EXPER NO. 963

LAT N.80-34-45 LONG W.79-25-00 WATER DEPTH 519

DEPTH INCR. DATE 090474 LOCAL TIME 1345

DEPTH	PRES	SAL		TEMP		SIGMAT	SOUND
2.8	2.85			-1.565	D		
3.9	3.90	29.080	C	-1.567	D	23.402	1433.3
4.9	4.90	29.071	C	-1.567	D	23.395	1433.3
5.9	5.90	29.069	C	-1.567	D	23.393	1433.3
6.9	6.95	29.065	C	-1.566	D	23.390	1433.3
7.8	7.85			-1.475	D		
8.9	8.95	29.190	C	-0.836	D	23.479	1437.5
9.9	9.95	29.489	C	-0.692	D	23.717	1438.6
10.9	10.95	29.887	C	-0.530	D	24.034	1439.9
12.0	12.00	30.322	C	-0.473	D	24.382	1440.8
13.0	13.00	30.706	C	-0.469	D	24.692	1441.4
14.0	14.05	31.054	C	-0.549	D	24.975	1441.5
15.0	15.05	31.258	C	-0.629	D	25.143	1441.4
16.0	16.05	31.400	C	-0.658	D	25.258	1441.5
17.0	17.05	31.553	C	-0.764	D	25.385	1441.2
18.0	18.05	31.685	C	-0.895	D	25.495	1440.8
19.0	19.05	31.776	C	-1.019	D	25.572	1440.4
20.1	20.15	31.836	C	-1.100	D	25.623	1440.1
21.1	21.10	31.888	C	-1.162	D	25.667	1439.9
22.0	22.05	31.923	C	-1.218	D	25.697	1439.7
23.1	23.10	31.968	C	-1.279	D	25.734	1439.5
24.1	24.10	32.000	C	-1.324	D	25.762	1439.3
25.1	25.15	32.022	C	-1.355	D	25.780	1439.2
26.2	26.25	32.041	C	-1.377	D	25.796	1439.2
27.1	27.15	32.062	C	-1.405	D	25.813	1439.1
28.2	28.25	32.085	C	-1.436	D	25.833	1439.0
29.2	29.25	32.104	C	-1.460	D	25.849	1438.9
30.2	30.20	32.123	C	-1.481	D	25.864	1438.9
31.3	31.25	32.138	C	-1.495	D	25.877	1438.8
32.3	32.30	32.158	C	-1.512	D	25.894	1438.8
33.2	33.25	32.178	C	-1.523	D	25.910	1438.8
34.3	34.35	32.197	C	-1.529	D	25.926	1438.8
35.3	35.35	32.218	C	-1.537	D	25.943	1438.8
36.3	36.35	32.240	C	-1.537	D	25.960	1438.9
37.3	37.30	32.256	C	-1.527	D	25.973	1439.0
38.3	38.35	32.279	C	-1.521	D	25.992	1439.0
39.3	39.35	32.303	C	-1.514	D	26.011	1439.1
40.4	40.40	32.332	C	-1.506	D	26.034	1439.2
41.3	41.35	32.361	C	-1.502	D	26.058	1439.3
42.4	42.40	32.395	C	-1.494	D	26.085	1439.4
43.4	43.45	32.427	C	-1.492	D	26.111	1439.5
44.4	44.45	32.464	C	-1.493	D	26.141	1439.5
45.4	45.45	32.507	C	-1.487	D	26.176	1439.6
46.4	46.45	32.547	C	-1.483	D	26.208	1439.7
47.5	47.55	32.581	C	-1.483	D	26.235	1439.8
48.5	48.50	32.617	C	-1.487	D	26.265	1439.8
49.6	49.60	32.648	C	-1.490	D	26.290	1439.9
50.5	50.50	32.683	C	-1.487	D	26.318	1440.0
51.6	51.60	32.707	C	-1.486	D	26.338	1440.0
52.5	52.55	32.725	C	-1.461	D	26.352	1440.2
53.6	53.60	32.772	C	-1.478	D	26.391	1440.2
54.6	54.65	32.803	C	-1.465	D	26.415	1440.3
55.7	55.70	32.831	C	-1.447	D	26.437	1440.4
56.7	56.75	32.861	C	-1.475	D	26.462	1440.4
57.7	57.75	32.877	C	-1.442	D	26.474	1440.6
58.7	58.70	32.905	C	-1.428	D	26.496	1440.7
59.7	59.70	32.924	C	-1.424	D	26.512	1440.7
60.8	60.80	32.958	C	-1.423	D	26.540	1440.8
61.7	61.75	32.972	C	-1.436	D	26.551	1440.8
62.8	62.80	33.006	C	-1.444	D	26.579	1440.8
63.8	63.80	33.033	C	-1.445	D	26.601	1440.9
64.8	64.80	33.059	C	-1.396	D	26.621	1441.2

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
65.9	65.90	33.089	C	-1.392	D	26.645	1441.2
66.9	66.90	33.120	C	-1.411	D	26.671	1441.2
67.9	67.90	33.128	C	-1.384	D	26.676	1441.4
68.8	68.85	33.166	C	-1.374	D	26.707	1441.5
69.9	69.90	33.189	C	-1.362	D	26.725	1441.6
71.0	71.00	33.217	C	-1.354	D	26.748	1441.7
71.9	71.95	33.254	C	-1.351	D	26.777	1441.8
73.0	73.00	33.274	C	-1.358	D	26.794	1441.8
74.0	74.00	33.300	C	-1.333	D	26.814	1441.9
75.0	75.05	33.329	C	-1.387	D	26.839	1441.7
76.0	76.05	33.345	C	-1.392	D	26.852	1441.8
77.1	77.10	33.358	C	-1.392	D	26.863	1441.8
78.0	78.00	33.370	C	-1.392	D	26.873	1441.8
79.1	79.10	33.382	C	-1.392	D	26.882	1441.9
80.0	80.05	33.390	C	-1.383	D	26.888	1441.9
81.2	81.20	33.395	C	-1.343	D	26.892	1442.1
82.1	82.10	33.424	C	-1.303	D	26.914	1442.4
83.1	83.15	33.455	C	-1.299	D	26.939	1442.5
84.2	84.20	33.452	C	-1.272	D	26.935	1442.6
85.1	85.15	33.473	C	-1.209	D	26.951	1442.9
86.1	86.15	33.503	C	-1.188	D	26.974	1443.1
87.2	87.25	33.523	C	-1.198	D	26.990	1443.1
88.2	88.25	33.530	C	-1.171	D	26.995	1443.3
89.3	89.30	33.544	C	-1.131	D	27.006	1443.5
90.3	90.30	33.562	C	-1.101	D	27.019	1443.7
91.3	91.30	33.579	C	-1.081	D	27.032	1443.8
92.4	92.40	33.592	C	-1.056	D	27.042	1444.0
93.3	93.35	33.606	C	-1.041	D	27.053	1444.1
94.3	94.35	33.614	C	-1.021	D	27.059	1444.2
95.4	95.40	33.630	C	-1.005	D	27.071	1444.3
96.4	96.40	33.641	C	-0.978	D	27.079	1444.5
97.4	97.40	33.657	C	-0.953	D	27.091	1444.6
98.5	98.50	33.670	C	-0.934	D	27.101	1444.7
99.4	99.45	33.681	C	-0.920	D	27.110	1444.8
100.5	100.50	33.695	D	-0.906	E	27.120	1444.9
101.4	101.45	33.708	D	-0.893	E	27.130	1445.0
102.5	102.50	33.717	D	-0.881	E	27.137	1445.1
103.6	103.60	33.726	D	-0.871	E	27.144	1445.2
104.5	104.50	33.737	D	-0.863	E	27.153	1445.3
105.6	105.60	33.748	D	-0.855	E	27.162	1445.3
106.6	106.60	33.755	D	-0.846	E	27.167	1445.4
107.6	107.65	33.766	D	-0.835	E	27.175	1445.5
108.6	108.65	33.776	D	-0.823	E	27.183	1445.6
109.6	109.60	33.786	D	-0.814	E	27.191	1445.6
110.7	110.70	33.796	D	-0.805	E	27.199	1445.7
111.7	111.70	33.806	D	-0.797	E	27.206	1445.8
112.7	112.70	33.814	D	-0.789	E	27.212	1445.8
113.7	113.75	33.824	D	-0.782	E	27.220	1445.9
114.7	114.75	33.833	D	-0.775	E	27.227	1446.0
115.7	115.75	33.840	D	-0.768	E	27.233	1446.0
116.7	116.75	33.852	D	-0.762	E	27.242	1446.1
117.7	117.75	33.857	D	-0.755	E	27.245	1446.1
118.8	118.85	33.863	D	-0.751	E	27.251	1446.2
119.8	119.85	33.871	D	-0.745	E	27.256	1446.2
120.8	120.85	33.878	D	-0.740	E	27.262	1446.3
121.8	121.80	33.882	D	-0.736	E	27.265	1446.3
122.9	122.90	33.889	D	-0.732	E	27.270	1446.4
123.9	123.90	33.893	D	-0.723	E	27.274	1446.4
124.9	124.90	33.906	D	-0.714	E	27.284	1446.5
125.9	125.95	33.918	D	-0.706	E	27.293	1446.6
127.0	127.00	33.927	D	-0.698	E	27.300	1446.7
128.0	128.00	33.938	D	-0.690	E	27.309	1446.7
129.0	129.00	33.947	D	-0.685	E	27.316	1446.8
129.9	129.95	33.953	D	-0.677	E	27.320	1446.8
131.0	131.00	33.964	D	-0.670	E	27.329	1446.9
132.0	132.05	33.969	D	-0.666	E	27.333	1446.9
133.0	133.05	33.978	D	-0.662	E	27.340	1447.0
134.1	134.10	33.985	D	-0.655	E	27.345	1447.1
135.1	135.10	33.994	D	-0.649	E	27.352	1447.1

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
136.1	136.15	33.999 D	-0.645 E	27.356	1447.2
137.1	137.15	34.006 D	-0.637 E	27.361	1447.2
138.2	138.20	34.014 D	-0.631 E	27.368	1447.3
139.2	139.20	34.021 D	-0.624 E	27.373	1447.3
140.2	140.20	34.030 D	-0.619 E	27.380	1447.4
141.1	141.15	34.036 D	-0.613 E	27.385	1447.4
142.2	142.25	34.043 D	-0.607 E	27.391	1447.5
143.3	143.30	34.053 D	-0.601 E	27.398	1447.6
144.3	144.30	34.061 D	-0.593 E	27.404	1447.6
145.3	145.35	34.072 D	-0.585 E	27.413	1447.7
146.3	146.35	34.078 D	-0.582 E	27.417	1447.7
147.3	147.35	34.084 D	-0.577 E	27.422	1447.8
148.3	148.35	34.094 D	-0.566 E	27.429	1447.9
149.4	149.45	34.100 D	-0.562 E	27.435	1447.9
150.4	150.40	34.109 D	-0.554 E	27.441	1448.0
151.4	151.45	34.116 D	-0.548 E	27.447	1448.0
152.5	152.50	34.123 D	-0.541 E	27.452	1448.1
153.5	153.50	34.135 D	-0.530 E	27.461	1448.2
154.4	154.45	34.144 D	-0.526 E	27.469	1448.2
155.5	155.50	34.148 D	-0.519 E	27.471	1448.3
156.5	156.50	34.160 D	-0.508 E	27.480	1448.3
157.5	157.50	34.172 D	-0.497 E	27.490	1448.4
158.5	158.55	34.181 D	-0.489 E	27.497	1448.5
159.5	159.55	34.191 D	-0.481 E	27.505	1448.6
160.6	160.60	34.200 D	-0.474 E	27.511	1448.6
161.6	161.60	34.211 D	-0.464 E	27.520	1448.7
162.6	162.60	34.219 D	-0.454 E	27.526	1448.8
163.6	163.65	34.230 D	-0.445 E	27.534	1448.9
164.6	164.65	34.239 D	-0.439 E	27.542	1448.9
165.7	165.70	34.245 D	-0.433 E	27.546	1449.0
166.7	166.75	34.251 D	-0.426 E	27.550	1449.0
167.7	167.75	34.258 D	-0.420 E	27.556	1449.1
168.7	168.70	34.264 D	-0.414 E	27.560	1449.1
169.7	169.75	34.271 D	-0.407 E	27.566	1449.2
170.8	170.80	34.279 D	-0.398 E	27.572	1449.3
171.8	171.85	34.290 D	-0.388 E	27.580	1449.3
172.8	172.80	34.298 D	-0.381 E	27.587	1449.4
173.8	173.85	34.306 D	-0.374 E	27.593	1449.5
174.9	174.90	34.313 D	-0.367 E	27.598	1449.5
175.9	175.90	34.320 D	-0.361 E	27.603	1449.6
176.9	176.90	34.326 D	-0.357 E	27.608	1449.6
177.8	177.85	34.332 D	-0.350 E	27.612	1449.7
178.8	178.85	34.342 D	-0.334 E	27.620	1449.8
179.9	179.95	34.355 D	-0.324 E	27.630	1449.9
181.0	181.00	34.361 D	-0.319 E	27.635	1449.9
182.0	182.00	34.367 D	-0.314 E	27.639	1450.0
183.0	183.05	34.370 D	-0.310 E	27.642	1450.0
184.0	184.00	34.377 D	-0.301 E	27.647	1450.1
185.0	185.05	34.384 D	-0.293 E	27.652	1450.1
186.0	186.05	34.393 D	-0.284 E	27.659	1450.2
187.0	187.05	34.397 D	-0.279 E	27.662	1450.2
188.0	188.05	34.406 D	-0.269 E	27.668	1450.3
189.1	189.15	34.412 D	-0.265 E	27.673	1450.4
190.2	190.20	34.417 D	-0.258 E	27.677	1450.4
191.1	191.10	34.423 D	-0.251 E	27.682	1450.5
192.2	192.20	34.426 D	-0.246 E	27.684	1450.5
193.2	193.20	34.431 D	-0.242 E	27.688	1450.6
194.1	194.15	34.436 D	-0.236 E	27.691	1450.6
195.2	195.25	34.442 D	-0.230 E	27.696	1450.7
196.2	196.25	34.446 D	-0.224 E	27.699	1450.7
197.2	197.25	34.452 D	-0.221 E	27.704	1450.7
198.3	198.35	34.452 D	-0.216 E	27.704	1450.8
199.2	199.25	34.459 D	-0.208 E	27.708	1450.9
200.3	200.35	34.466 D	-0.204 E	27.714	1450.9
201.3	201.35	34.472 D	-0.200 E	27.719	1450.9
202.4	202.40	34.475 D	-0.194 E	27.721	1451.0
203.3	203.30	34.478 D	-0.191 E	27.723	1451.0
204.3	204.35	34.485 D	-0.189 E	27.729	1451.1
205.5	205.50	34.488 D	-0.184 E	27.731	1451.1

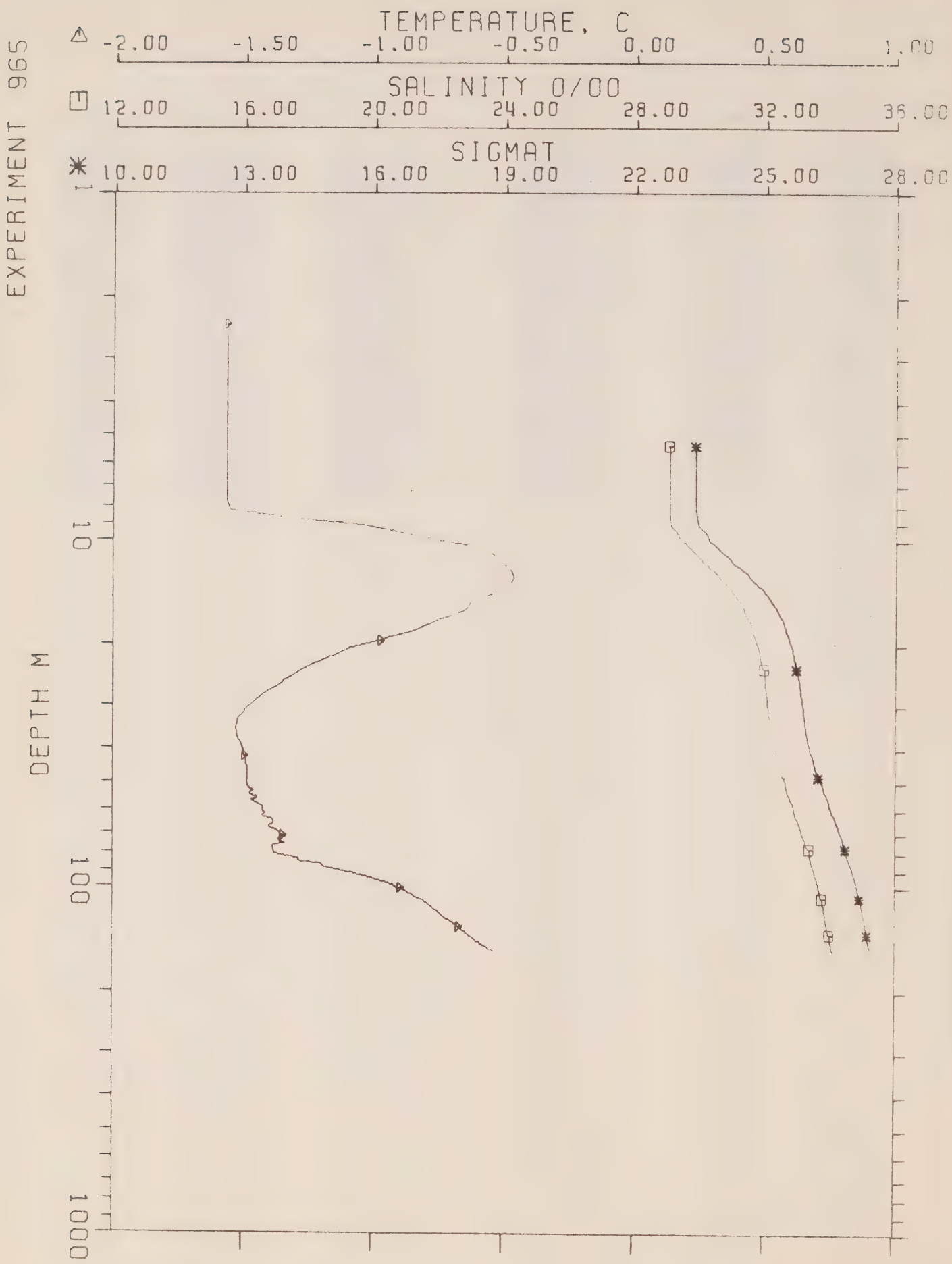
DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
206.4	206.40	34.493	D	-0.181	E	27.734	1451.1
207.4	207.45	34.497	D	-0.176	E	27.737	1451.2
208.4	208.45	34.500	D	-0.171	E	27.740	1451.2
209.4	209.45	34.502	D	-0.167	E	27.742	1451.3
210.5	210.55	34.504	D	-0.163	E	27.742	1451.3
211.6	211.60	34.508	D	-0.161	E	27.746	1451.3
212.5	212.55	34.509	D	-0.158	E	27.746	1451.4
213.5	213.50	34.513	D	-0.156	E	27.750	1451.4
214.5	214.55	34.516	D	-0.151	E	27.752	1451.4
215.6	215.60	34.520	D	-0.147	E	27.754	1451.5
216.6	216.65	34.523	D	-0.144	E	27.757	1451.5
217.7	217.70	34.525	D	-0.141	E	27.759	1451.6
218.7	218.70	34.528	D	-0.139	E	27.761	1451.6
219.7	219.70	34.530	D	-0.136	E	27.762	1451.6
220.6	220.65	34.534	D	-0.133	E	27.765	1451.7
221.7	221.70	34.537	D	-0.130	E	27.768	1451.7
222.7	222.70	34.538	D	-0.126	E	27.768	1451.7
223.7	223.75	34.542	D	-0.125	E	27.772	1451.8
224.7	224.75	34.544	D	-0.123	E	27.773	1451.8
225.7	225.75	34.546	D	-0.120	E	27.775	1451.8
226.7	226.75	34.549	D	-0.117	E	27.777	1451.8
227.8	227.80	34.552	D	-0.115	E	27.779	1451.9
228.8	228.85	34.555	D	-0.111	E	27.781	1451.9
229.9	229.90	34.557	D	-0.109	E	27.782	1451.9
230.9	230.90	34.558	D	-0.107	E	27.784	1452.0
231.8	231.85	34.561	D	-0.106	E	27.786	1452.0
232.9	232.95	34.561	D	-0.103	E	27.786	1452.0
234.0	234.00	34.563	D	-0.102	E	27.788	1452.1
234.9	234.90	34.566	D	-0.100	E	27.790	1452.1
236.0	236.05	34.567	D	-0.097	E	27.790	1452.1
237.0	237.00	34.568	D	-0.095	E	27.791	1452.1
238.0	238.00	34.571	D	-0.095	E	27.794	1452.2
239.1	239.10	34.573	D	-0.092	E	27.795	1452.2
240.1	240.10	34.574	D	-0.090	E	27.796	1452.2
241.1	241.15	34.577	D	-0.089	E	27.798	1452.2
242.2	242.20	34.576	D	-0.087	E	27.797	1452.3
243.1	243.15	34.579	D	-0.086	E	27.800	1452.3
244.1	244.10	34.581	D	-0.084	E	27.801	1452.3
245.2	245.20	34.583	D	-0.083	E	27.802	1452.4
246.1	246.15	34.585	D	-0.082	E	27.804	1452.4
247.2	247.20	34.586	D	-0.081	E	27.805	1452.4
248.2	248.20	34.586	D	-0.078	E	27.805	1452.4
249.2	249.25	34.589	D	-0.077	E	27.807	1452.5
250.3	250.30	34.590	D	-0.077	E	27.808	1452.5
251.3	251.30	34.590	D	-0.075	E	27.807	1452.5
252.3	252.30	34.590	D	-0.073	E	27.808	1452.5
253.3	253.30	34.593	D	-0.073	E	27.810	1452.5
254.3	254.35	34.592	D	-0.071	E	27.809	1452.6
255.3	255.30	34.594	D	-0.070	E	27.811	1452.6
256.4	256.40	34.596	D	-0.070	E	27.812	1452.6
257.4	257.40	34.596	D	-0.068	E	27.812	1452.6
258.4	258.45	34.597	D	-0.067	E	27.813	1452.7
259.4	259.45	34.599	D	-0.067	E	27.815	1452.7
260.5	260.50	34.599	D	-0.066	E	27.815	1452.7
261.5	261.50	34.600	D	-0.064	E	27.815	1452.7
262.5	262.55	34.601	D	-0.064	E	27.816	1452.7
263.5	263.50	34.601	D	-0.062	E	27.816	1452.8
264.5	264.55	34.603	D	-0.062	E	27.817	1452.8
265.5	265.50	34.603	D	-0.061	E	27.818	1452.8
266.6	266.60	34.604	D	-0.060	E	27.818	1452.8
267.6	267.60	34.605	D	-0.059	E	27.819	1452.9
268.6	268.60	34.605	D	-0.057	E	27.819	1452.9
269.7	269.70	34.606	D	-0.056	E	27.820	1452.9
270.7	270.70	34.608	D	-0.056	E	27.821	1452.9
271.7	271.70	34.608	D	-0.055	E	27.821	1452.9
272.7	272.70	34.609	D	-0.054	E	27.822	1453.0
273.7	273.70	34.608	D	-0.052	E	27.821	1453.0
274.8	274.80	34.609	D	-0.052	E	27.822	1453.0
275.7	275.75	34.610	D	-0.051	E	27.823	1453.0

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
276.8	276.85	34.611	D	-0.050	E	27.823	1453.1
277.8	277.85	34.612	D	-0.049	E	27.824	1453.1
278.9	278.90	34.614	D	-0.049	E	27.826	1453.1
279.8	279.85	34.613	D	-0.047	E	27.825	1453.1
280.9	280.95	34.615	D	-0.048	E	27.827	1453.1
281.9	281.95	34.614	D	-0.046	E	27.825	1453.2
282.9	282.95	34.616	D	-0.046	E	27.827	1453.2
283.9	283.95	34.615	D	-0.045	E	27.827	1453.2
284.9	284.90	34.615	D	-0.044	E	27.827	1453.2
285.9	285.95	34.615	D	-0.044	E	27.827	1453.2
286.9	286.95	34.616	D	-0.043	E	27.827	1453.3
288.0	288.05	34.616	D	-0.042	E	27.827	1453.3
289.0	289.00	34.617	D	-0.041	E	27.828	1453.3
290.0	290.00	34.617	D	-0.041	E	27.828	1453.3
291.0	291.00	34.618	D	-0.041	E	27.829	1453.3
292.0	292.05	34.618	D	-0.040	E	27.829	1453.4
293.1	293.15	34.618	D	-0.039	E	27.829	1453.4
294.1	294.10	34.619	D	-0.038	E	27.829	1453.4
295.1	295.15	34.619	D	-0.037	E	27.829	1453.4
296.1	296.15	34.620	D	-0.037	E	27.830	1453.4
297.2	297.20	34.620	D	-0.036	E	27.830	1453.5
298.2	298.25	34.621	D	-0.036	E	27.831	1453.5
299.3	299.30	34.620	D	-0.034	E	27.830	1453.5
300.3	300.30	34.621	D	-0.034	E	27.831	1453.5
301.3	301.30	34.621	D	-0.032	E	27.830	1453.5
302.2	302.25	34.622	D	-0.032	E	27.831	1453.5
303.3	303.30	34.623	D	-0.032	E	27.832	1453.6
304.3	304.35	34.622	D	-0.031	E	27.831	1453.6
305.3	305.35	34.624	D	-0.032	E	27.833	1453.6
306.3	306.35	34.623	D	-0.031	E	27.832	1453.6
307.4	307.40	34.623	D	-0.031	E	27.832	1453.7
308.4	308.45	34.623	D	-0.030	E	27.832	1453.7
309.4	309.45	34.622	D	-0.030	E	27.831	1453.7
310.4	310.45	34.623	D	-0.030	E	27.832	1453.7
311.4	311.45	34.624	D	-0.030	E	27.833	1453.7
312.4	312.45	34.623	D	-0.028	E	27.832	1453.8
313.5	313.50	34.625	D	-0.028	E	27.833	1453.8
314.4	314.45	34.625	D	-0.027	E	27.833	1453.8
315.4	315.45	34.623	D	-0.025	E	27.832	1453.8
316.5	316.55	34.626	D	-0.026	E	27.834	1453.8
317.5	317.55	34.627	D	-0.026	E	27.835	1453.9
318.6	318.60	34.626	D	-0.025	E	27.834	1453.9
319.6	319.65	34.626	D	-0.025	E	27.834	1453.9
320.6	320.65	34.626	D	-0.025	E	27.834	1453.9
321.7	321.70	34.626	D	-0.025	E	27.834	1453.9
322.7	322.75	34.626	D	-0.024	E	27.834	1454.0
323.7	323.70	34.626	D	-0.024	E	27.835	1454.0
324.6	324.65	34.627	D	-0.023	E	27.835	1454.0
325.7	325.75	34.627	D	-0.023	E	27.835	1454.0
326.7	326.75	34.627	D	-0.022	E	27.835	1454.0
327.8	327.80	34.627	D	-0.022	E	27.835	1454.0
328.8	328.80	34.628	D	-0.022	E	27.835	1454.1
329.8	329.80	34.626	D	-0.021	E	27.834	1454.1
330.8	330.80	34.627	D	-0.021	E	27.835	1454.1
331.8	331.80	34.627	D	-0.021	E	27.835	1454.1
332.8	332.85	34.627	D	-0.020	E	27.835	1454.1
333.9	333.95	34.629	D	-0.020	E	27.836	1454.2
334.9	334.90	34.628	D	-0.019	E	27.836	1454.2
335.9	335.95	34.628	D	-0.019	E	27.836	1454.2
336.9	336.95	34.628	D	-0.019	E	27.836	1454.2
338.0	338.05	34.628	D	-0.019	E	27.836	1454.2
339.0	339.00	34.629	D	-0.018	E	27.836	1454.3
340.0	340.05	34.629	D	-0.018	E	27.837	1454.3
341.0	341.05	34.629	D	-0.017	E	27.836	1454.3
342.1	342.10	34.629	D	-0.016	E	27.836	1454.3
343.1	343.10	34.629	D	-0.016	E	27.836	1454.3
344.1	344.15	34.628	D	-0.015	E	27.835	1454.3
345.1	345.10	34.628	D	-0.014	E	27.836	1454.4
346.1	346.10	34.629	D	-0.014	E	27.836	1454.4

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
347.1	347.15	34.630	D	-0.014	E	27.837	1454.4
348.1	348.10	34.629	D	-0.013	E	27.836	1454.4
349.2	349.20	34.630	D	-0.013	E	27.837	1454.4
350.2	350.25	34.630	D	-0.013	E	27.837	1454.5
351.3	351.30	34.630	D	-0.013	E	27.837	1454.5
352.2	352.25	34.631	D	-0.013	E	27.838	1454.5
353.3	353.30	34.630	D	-0.012	E	27.837	1454.5
354.2	354.25	34.631	D	-0.012	E	27.837	1454.5
355.3	355.35	34.631	D	-0.012	E	27.837	1454.5
356.3	356.35	34.631	D	-0.012	E	27.837	1454.6
357.4	357.40	34.631	D	-0.012	E	27.837	1454.6
358.4	358.40	34.629	D	-0.010	E	27.836	1454.6
359.4	359.45	34.631	D	-0.011	E	27.838	1454.6
360.4	360.45	34.631	D	-0.011	E	27.838	1454.6
361.4	361.45	34.632	D	-0.011	E	27.838	1454.7
362.4	362.45	34.632	D	-0.011	E	27.838	1454.7
363.5	363.50	34.631	D	-0.010	E	27.838	1454.7
364.4	364.45	34.630	D	-0.009	E	27.837	1454.7
365.4	365.45	34.632	D	-0.010	E	27.838	1454.7
366.5	366.50	34.631	D	-0.009	E	27.837	1454.7
367.5	367.55	34.632	D	-0.009	E	27.838	1454.8
368.6	368.60	34.632	D	-0.010	E	27.839	1454.8
369.6	369.65	34.633	D	-0.010	E	27.839	1454.8
370.6	370.65	34.631	D	-0.008	E	27.837	1454.8
371.6	371.60	34.633	D	-0.010	E	27.839	1454.8
372.7	372.70	34.631	D	-0.008	E	27.837	1454.9
373.6	373.65	34.631	D	-0.008	E	27.837	1454.9
374.7	374.70	34.632	D	-0.008	E	27.838	1454.9
375.8	375.80	34.632	D	-0.008	E	27.839	1454.9
376.8	376.80	34.632	D	-0.008	E	27.839	1454.9
377.8	377.80	34.632	D	-0.008	E	27.839	1454.9
378.8	378.80	34.632	D	-0.008	E	27.839	1455.0
379.8	379.85	34.632	D	-0.008	E	27.839	1455.0
380.8	380.85	34.632	D	-0.007	E	27.838	1455.0
381.8	381.80	34.633	D	-0.007	E	27.839	1455.0
382.8	382.85	34.632	D	-0.006	E	27.838	1455.0
383.8	383.80	34.633	D	-0.007	E	27.839	1455.0
384.9	384.90	34.632	D	-0.006	E	27.839	1455.1
385.9	385.90	34.633	D	-0.006	E	27.839	1455.1
386.9	386.90	34.632	D	-0.005	E	27.838	1455.1
387.9	387.90	34.632	D	-0.005	E	27.838	1455.1
389.0	389.00	34.633	D	-0.005	E	27.839	1455.1
390.0	390.05	34.633	D	-0.005	E	27.839	1455.2
391.0	391.00	34.634	D	-0.005	E	27.839	1455.2
392.0	392.05	34.632	D	-0.004	E	27.838	1455.2
393.1	393.10	34.633	D	-0.004	E	27.838	1455.2
394.0	394.05	34.633	D	-0.004	E	27.839	1455.2
395.0	395.05	34.633	D	-0.004	E	27.839	1455.2
396.1	396.15	34.633	D	-0.004	E	27.839	1455.3
397.1	397.15	34.633	D	-0.004	E	27.839	1455.3
398.2	398.20	34.633	D	-0.004	E	27.839	1455.3
399.1	399.15	34.634	D	-0.004	E	27.840	1455.3
400.2	400.25	34.634	D	-0.004	E	27.839	1455.3
401.2	401.20	34.634	D	-0.003	E	27.839	1455.3
402.2	402.20	34.634	D	-0.003	E	27.840	1455.4
403.2	403.20	34.634	D	-0.003	E	27.840	1455.4
404.3	404.30	34.634	D	-0.003	E	27.840	1455.4
405.2	405.25	34.634	D	-0.003	E	27.840	1455.4
406.3	406.30	34.635	D	-0.003	E	27.840	1455.4
407.3	407.35	34.635	D	-0.003	E	27.840	1455.5
408.3	408.35	34.634	D	-0.002	E	27.839	1455.5
409.4	409.40	34.634	D	-0.002	E	27.840	1455.5
410.4	410.40	34.633	D	-0.001	E	27.839	1455.5
411.4	411.45	34.634	D	0.0	E	27.839	1455.5
412.4	412.45	34.634	D	-0.001	E	27.840	1455.5
413.5	413.55	34.633	D	0.0	E	27.839	1455.6
414.5	414.55	34.635	D	-0.001	E	27.840	1455.6
415.5	415.50	34.635	D	-0.001	E	27.840	1455.6
416.5	416.55	34.634	D	0.0	E	27.840	1455.6

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
417.6	417.60	34.634	D	0.0	E	27.840	1455.6
418.5	418.55	34.635	D	0.0	E	27.840	1455.6
419.6	419.60	34.635	D	0.0	E	27.840	1455.7
420.5	420.50	34.634	D	0.001	E	27.840	1455.7
421.6	421.60	34.635	D	0.001	E	27.840	1455.7
422.6	422.65	34.635	D	0.001	E	27.840	1455.7
423.6	423.65	34.636	D	0.001	E	27.841	1455.7
424.6	424.60	34.635	D	0.002	E	27.840	1455.8
425.7	425.70	34.634	D	0.002	E	27.839	1455.8
426.7	426.70	34.635	D	0.002	E	27.840	1455.8
427.7	427.75	34.634	D	0.003	E	27.839	1455.8
428.7	428.75	34.634	D	0.003	E	27.839	1455.8
429.8	429.80	34.634	D	0.003	E	27.840	1455.8
430.8	430.85	34.634	D	0.003	E	27.840	1455.9
431.8	431.80	34.636	D	0.002	E	27.841	1455.9
432.8	432.85	34.634	D	0.003	E	27.839	1455.9
433.8	433.85	34.635	D	0.002	E	27.840	1455.9
434.9	434.95	34.636	D	0.002	E	27.841	1455.9
435.9	435.90	34.635	D	0.003	E	27.840	1455.9
436.9	436.90	34.635	D	0.003	E	27.840	1456.0
437.9	437.95	34.635	D	0.003	E	27.841	1456.0
438.9	438.95	34.634	D	0.004	E	27.840	1456.0
440.0	440.00	34.635	D	0.004	E	27.840	1456.0
441.0	441.05	34.636	D	0.004	E	27.841	1456.0
442.0	442.00	34.635	D	0.004	E	27.840	1456.1
443.0	443.00	34.636	D	0.004	E	27.841	1456.1
444.0	444.05	34.636	D	0.004	E	27.841	1456.1
445.0	445.05	34.636	D	0.004	E	27.841	1456.1
446.1	446.10	34.635	D	0.005	E	27.840	1456.1
447.1	447.10	34.635	D	0.005	E	27.840	1456.1
448.1	448.15	34.636	D	0.004	E	27.841	1456.2
449.2	449.20	34.637	D	0.003	E	27.842	1456.2
450.2	450.20	34.637	D	0.003	E	27.842	1456.2
451.3	451.30	34.636	D	0.004	E	27.841	1456.2
452.3	452.30	34.636	D	0.004	E	27.841	1456.2
453.3	453.30	34.636	D	0.004	E	27.841	1456.2
454.3	454.30	34.637	D	0.003	E	27.842	1456.3
455.3	455.35	34.636	D	0.003	E	27.841	1456.3
456.3	456.35	34.637	D	0.004	E	27.841	1456.3
457.3	457.30	34.636	D	0.004	E	27.841	1456.3
458.3	458.30	34.637	D	0.004	E	27.842	1456.3
459.3	459.35	34.637	D	0.004	E	27.842	1456.3
460.3	460.35	34.637	D	0.005	E	27.842	1456.4
461.4	461.45	34.636	D	0.006	E	27.841	1456.4
462.4	462.40	34.636	D	0.006	E	27.841	1456.4
463.4	463.40	34.638	D	0.005	E	27.842	1456.4
464.5	464.50	34.637	D	0.005	E	27.842	1456.4
465.4	465.45	34.636	D	0.006	E	27.841	1456.4
466.5	466.50	34.637	D	0.005	E	27.842	1456.5
467.5	467.55	34.636	D	0.006	E	27.841	1456.5
468.5	468.55	34.637	D	0.005	E	27.842	1456.5
469.6	469.60	34.638	D	0.005	E	27.842	1456.5
470.7	470.70	34.635	D	0.007	E	27.840	1456.5
471.6	471.60	34.637	D	0.006	E	27.842	1456.6
472.6	472.65	34.636	D	0.008	E	27.841	1456.6
473.7	473.75	34.637	D	0.008	E	27.841	1456.6
474.7	474.75	34.637	D	0.009	E	27.842	1456.6
475.7	475.75	34.638	D	0.009	E	27.842	1456.6
476.7	476.75	34.637	D	0.010	E	27.842	1456.7
477.7	477.75	34.639	D	0.009	E	27.843	1456.7
478.7	478.70	34.639	D	0.009	E	27.843	1456.7
479.8	479.80	34.638	D	0.009	E	27.842	1456.7
480.8	480.80	34.638	D	0.009	E	27.842	1456.7
481.8	481.80	34.639	D	0.007	E	27.843	1456.7
482.8	482.85	34.639	D	0.007	E	27.843	1456.7
483.8	483.80	34.638	D	0.008	E	27.842	1456.8
484.8	484.85	34.638	D	0.008	E	27.842	1456.8
485.9	485.95	34.638	D	0.008	E	27.842	1456.8
486.9	486.95	34.638	D	0.008	E	27.843	1456.8

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
488.0	488.00	34.637 D	0.009 E	27.842	1456.8
489.0	489.00	34.638 D	0.008 E	27.843	1456.8
490.0	490.00	34.636 D	0.010 E	27.841	1456.9
490.9	490.95	34.637 D	0.009 E	27.842	1456.9
492.0	492.05	34.638 D	0.010 E	27.842	1456.9
493.1	493.10	34.638 D	0.010 E	27.842	1456.9
494.0	494.05	34.638 D	0.011 E	27.842	1456.9
495.1	495.10	34.639 D	0.010 E	27.843	1457.0
496.1	496.15	34.638 D	0.011 E	27.842	1457.0
497.1	497.10	34.638 D	0.011 E	27.842	1457.0
498.1	498.15	34.638 D	0.011 E	27.842	1457.0
499.1	499.15	34.638 D	0.011 E	27.842	1457.0
500.1	500.10	34.638 D	0.014 E	27.842	1457.1
501.1	501.15	34.638 D	0.014 E	27.842	1457.1
502.2	502.25	34.638 D	0.014 E	27.842	1457.1
503.2	503.25	34.638 D	0.014 E	27.842	1457.1
504.2	504.20	34.638 D	0.014 E	27.842	1457.1
505.2	505.20	34.639 D	0.014 E	27.842	1457.1
506.3	506.30	34.639 D	0.014 E	27.842	1457.2
507.4	507.40	34.639 D	0.014 E	27.843	1457.2
508.3	508.35	34.637 D	0.015 E	27.841	1457.2
509.4	509.40	34.639 D	0.014 E	27.843	1457.2


EXPERIMENT 965
TEMPERATURE, C
-2.00
-1.50
-1.00
-0.50
0.00
0.50
1.00
SALINITY 0/00
12.00
16.00
20.00
24.00
28.00
32.00
36.00
SIGMAT
10.00
13.00
16.00
19.00
22.00
25.00
28.00
DEPTH M
1
10
100
1000

CRUISE 15-74-012 D'IBERVILLE FIORD-74 EXPER NO. 965

LAT N.80-34-45 LONG W.79-25-00 WATER DEPTH 519

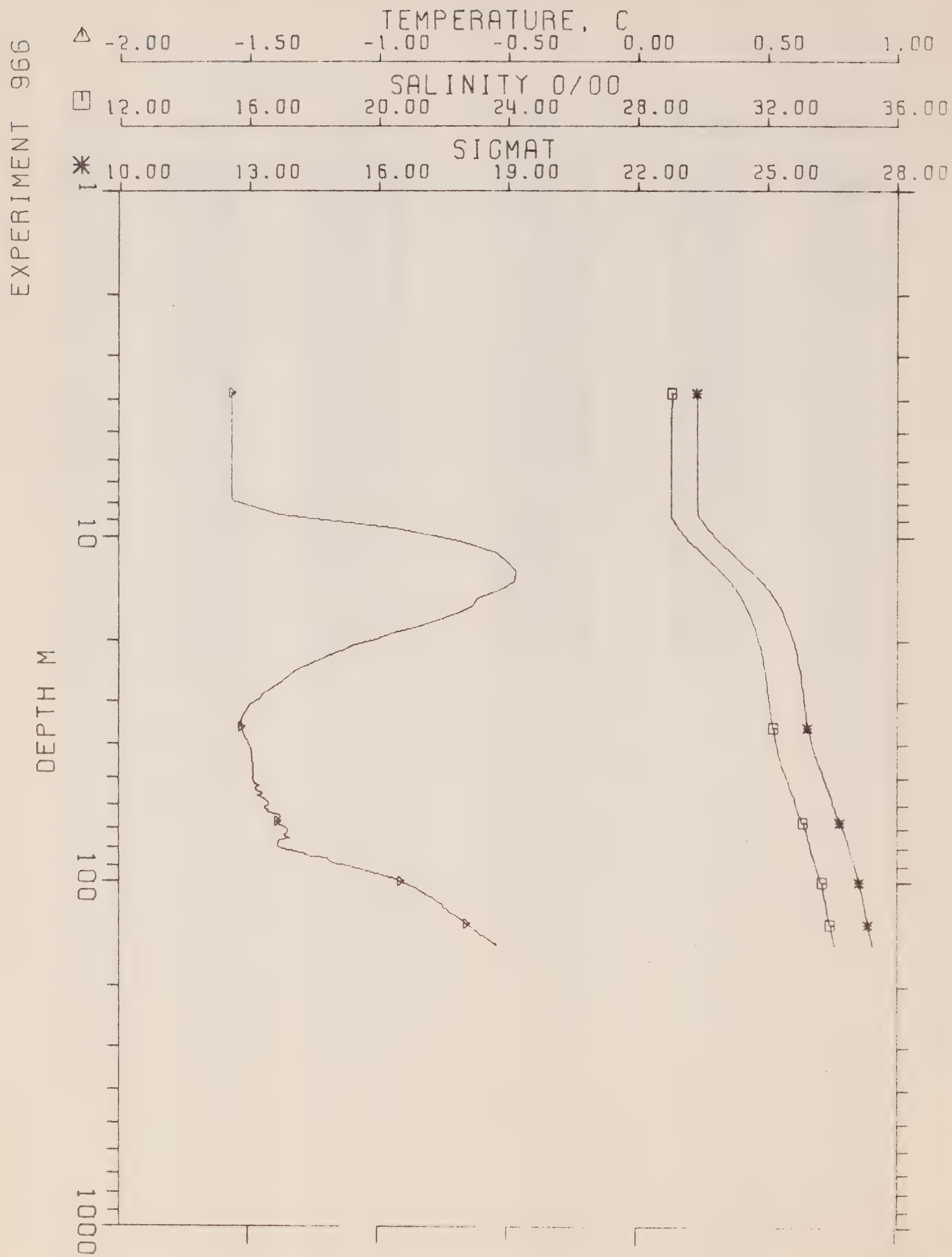
DEPTH INCR. DATE 090474 LOCAL TIME 1615

DEPTH	PRES	SAL	TEMP	SIGMAT	SOUND
2.4	2.40		-1.569 D		
2.7	2.75		-1.569 D		
3.1	3.10		-1.569 D		
3.4	3.40		-1.569 D		
3.7	3.75		-1.570 D		
4.2	4.20		-1.569 D		
4.5	4.50		-1.569 D		
4.9	4.90		-1.569 D		
5.3	5.35	29.059 C	-1.568 D	23.385	1433.8
5.7	5.70	29.059 C	-1.568 D	23.385	1433.8
6.1	6.10	29.058 C	-1.568 D	23.384	1433.8
6.5	6.55	29.057 C	-1.569 D	23.384	1433.8
7.0	7.00	29.054 C	-1.568 D	23.381	1433.8
7.4	7.40	29.054 C	-1.569 D	23.382	1433.8
7.8	7.80	29.054 C	-1.569 D	23.381	1433.8
8.2	8.25	29.047 C	-1.559 D	23.376	1433.8
8.6	8.65		-1.315 D		
9.0	9.05	29.131 C	-1.047 D	23.436	1436.4
9.4	9.40	29.311 C	-0.914 D	23.578	1437.3
9.9	9.90	29.452 C	-0.779 D	23.689	1438.1
10.3	10.30	29.637 C	-0.650 D	23.835	1439.0
10.7	10.70	29.829 C	-0.564 D	23.988	1439.7
11.1	11.10	30.003 C	-0.533 D	24.128	1440.1
11.6	11.60	30.168 C	-0.509 D	24.259	1440.4
11.9	11.95	30.338 C	-0.488 D	24.396	1440.7
12.3	12.35	30.539 C	-0.468 D	24.558	1441.1
12.9	12.90	30.676 C	-0.458 D	24.668	1441.4
13.3	13.30	30.826 C	-0.468 D	24.789	1441.5
13.6	13.65	30.969 C	-0.503 D	24.905	1441.6
14.1	14.15	31.086 C	-0.534 D	25.001	1441.6
14.6	14.65	31.189 C	-0.580 D	25.086	1441.5
15.0	15.05	31.273 C	-0.623 D	25.155	1441.5
15.5	15.50	31.345 C	-0.629 D	25.213	1441.5
16.0	16.05	31.418 C	-0.650 D	25.272	1441.6
16.5	16.50	31.494 C	-0.694 D	25.335	1441.5
16.9	16.90	31.548 C	-0.739 D	25.380	1441.3
17.4	17.45	31.599 C	-0.784 D	25.422	1441.2
18.0	18.00	31.637 C	-0.832 D	25.455	1441.0
18.4	18.45	31.678 C	-0.871 D	25.489	1440.9
18.9	18.95	31.722 C	-0.934 D	25.526	1440.7
19.5	19.50	31.747 C	-0.974 D	25.548	1440.6
19.9	19.90	31.786 C	-1.021 D	25.580	1440.4
20.3	20.35	31.827 C	-1.078 D	25.615	1440.2
20.9	20.90	31.855 C	-1.116 D	25.639	1440.1
21.4	21.40	31.869 C	-1.141 D	25.651	1440.0
21.8	21.80	31.896 C	-1.174 D	25.673	1439.9
22.3	22.35	31.912 C	-1.202 D	25.687	1439.8
22.8	22.85	31.932 C	-1.230 D	25.704	1439.7
23.3	23.30	31.952 C	-1.256 D	25.721	1439.6
23.7	23.75	31.970 C	-1.281 D	25.736	1439.5
24.3	24.35	31.982 C	-1.302 D	25.746	1439.4
24.8	24.80	31.994 C	-1.320 D	25.757	1439.4
25.3	25.30	32.006 C	-1.338 D	25.767	1439.3
25.8	25.85	32.014 C	-1.352 D	25.773	1439.3
26.4	26.40	32.025 C	-1.366 D	25.783	1439.2
26.8	26.80	32.040 C	-1.382 D	25.795	1439.2
27.4	27.40	32.056 C	-1.404 D	25.808	1439.1
27.9	27.95	32.067 C	-1.423 D	25.818	1439.0
28.5	28.50	32.079 C	-1.437 D	25.828	1439.0
29.0	29.05	32.089 C	-1.450 D	25.836	1438.9
29.6	29.65	32.099 C	-1.463 D	25.845	1438.9
30.1	30.15	32.112 C	-1.476 D	25.856	1438.9

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
30.7	30.70	32.123 C	-1.488 D	25.865	1438.8
31.3	31.30	32.130 C	-1.496 D	25.870	1438.8
31.9	31.90	32.142 C	-1.507 D	25.880	1438.8
32.4	32.40	32.153 C	-1.515 D	25.890	1438.9
33.0	33.00	32.163 C	-1.521 D	25.898	1438.8
33.6	33.65	32.172 C	-1.526 D	25.905	1438.8
34.2	34.20	32.179 C	-1.527 D	25.911	1438.8
34.7	34.70	32.191 C	-1.531 D	25.921	1438.8
35.4	35.40	32.204 C	-1.533 D	25.931	1438.8
35.9	35.90	32.212 C	-1.532 D	25.938	1438.8
36.4	36.45	32.225 C	-1.531 D	25.949	1438.9
37.1	37.10	32.239 C	-1.529 D	25.960	1438.9
37.7	37.75	32.254 C	-1.526 D	25.972	1439.0
38.4	38.40	32.268 C	-1.522 D	25.983	1439.0
39.0	39.00	32.284 C	-1.517 D	25.996	1439.1
39.8	39.80	32.303 C	-1.512 D	26.011	1439.1
40.4	40.45	32.324 C	-1.507 D	26.028	1439.2
41.1	41.10	32.348 C	-1.503 D	26.047	1439.3
41.9	41.90	32.371 C	-1.499 D	26.066	1439.3
42.5	42.55	32.392 C	-1.496 D	26.083	1439.4
43.2	43.25	32.412 C	-1.494 D	26.099	1439.4
44.0	44.00	32.437 C	-1.495 D	26.119	1439.5
44.7	44.70	32.462 C	-1.493 D	26.140	1439.5
45.4	45.40	32.481 C	-1.489 D	26.155	1439.6
46.1	46.15	32.511 C	-1.487 D	26.179	1439.6
46.9	46.95	32.540 C	-1.485 D	26.203	1439.7
47.7	47.70	32.575 C	-1.487 D	26.231	1439.8
48.3	48.35	32.598 C	-1.486 D	26.250	1439.8
49.1	49.15	32.620 C	-1.486 D	26.267	1439.9
49.9	49.95	32.646 C	-1.488 D	26.289	1439.9
50.6	50.65	32.667 C	-1.492 D	26.305	1439.9
51.4	51.40	32.687 C	-1.489 D	26.322	1440.0
52.2	52.25	32.712 C	-1.487 D	26.342	1440.0
52.9	52.95	32.732 C	-1.462 D	26.357	1440.2
53.6	53.65	32.763 C	-1.474 D	26.383	1440.2
54.3	54.35	32.787 C	-1.479 D	26.403	1440.2
55.1	55.15	32.810 C	-1.456 D	26.421	1440.4
55.9	55.90	32.833 C	-1.446 D	26.439	1440.5
56.6	56.60	32.860 C	-1.475 D	26.462	1440.4
57.3	57.35	32.867 C	-1.453 D	26.467	1440.5
58.1	58.15	32.889 C	-1.437 D	26.484	1440.6
58.9	58.90	32.908 C	-1.430 D	26.499	1440.7
59.6	59.60	32.920 C	-1.425 D	26.509	1440.7
60.4	60.45	32.944 C	-1.423 D	26.529	1440.8
61.1	61.10	32.956 C	-1.432 D	26.538	1440.8
61.6	61.65	32.980 C	-1.417 D	26.557	1440.9
62.4	62.45	33.003 C	-1.430 D	26.576	1440.9
63.2	63.20	33.028 C	-1.424 D	26.596	1441.0
63.9	63.90	33.057 C	-1.393 D	26.619	1441.2
64.6	64.60	33.073 C	-1.383 D	26.632	1441.2
65.4	65.45	33.093 C	-1.386 D	26.648	1441.3
66.1	66.10	33.109 C	-1.387 D	26.661	1441.3
66.8	66.80	33.130 C	-1.398 D	26.679	1441.3
67.6	67.60	33.145 C	-1.403 D	26.691	1441.3
68.3	68.35	33.156 C	-1.387 D	26.699	1441.4
69.1	69.10	33.172 C	-1.368 D	26.712	1441.5
69.8	69.80	33.199 C	-1.365 D	26.733	1441.6
70.6	70.60	33.215 C	-1.358 D	26.746	1441.6
71.3	71.30	33.228 C	-1.351 D	26.757	1441.7
71.9	71.95	33.244 C	-1.343 D	26.769	1441.8
72.7	72.75	33.270 C	-1.361 D	26.791	1441.7
73.4	73.45	33.281 C	-1.367 D	26.800	1441.7
74.1	74.15	33.297 C	-1.358 D	26.812	1441.8
74.9	74.90	33.310 C	-1.333 D	26.822	1442.0
75.7	75.70	33.340 C	-1.378 D	26.847	1441.8
76.3	76.35	33.346 C	-1.388 D	26.853	1441.8
77.0	77.05	33.355 C	-1.391 D	26.861	1441.8
77.9	77.90	33.364 C	-1.392 D	26.867	1441.8
78.6	78.60	33.373 C	-1.392 D	26.875	1441.8

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
79.2	79.25	33.385	C	-1.392	D	26.884	1441.9
80.0	80.05	33.392	C	-1.387	D	26.890	1441.9
80.8	80.80	33.396	C	-1.362	D	26.893	1442.1
81.5	81.50	33.407	C	-1.337	D	26.901	1442.2
82.2	82.25	33.426	C	-1.300	D	26.915	1442.4
83.0	83.00	33.434	C	-1.285	D	26.921	1442.5
83.7	83.70	33.459	C	-1.295	D	26.942	1442.5
84.4	84.45	33.464	C	-1.275	D	26.946	1442.6
85.2	85.20	33.475	C	-1.215	D	26.953	1442.9
85.8	85.85	33.503	C	-1.198	D	26.974	1443.1
86.5	86.55	33.519	C	-1.198	D	26.987	1443.1
87.3	87.35	33.529	C	-1.190	D	26.995	1443.2
88.1	88.10	33.542	C	-1.171	D	27.005	1443.3
88.8	88.80	33.549	C	-1.146	D	27.010	1443.4
89.5	89.55	33.561	C	-1.122	D	27.019	1443.6
90.4	90.45	33.574	C	-1.106	D	27.029	1443.7
91.0	91.00	33.584	C	-1.088	D	27.036	1443.8
91.7	91.75	33.595	C	-1.073	D	27.045	1443.9
92.6	92.60	33.606	C	-1.053	D	27.054	1444.0
93.3	93.35	33.618	C	-1.034	D	27.062	1444.1
94.1	94.10	33.630	C	-1.016	D	27.071	1444.2
94.9	94.90	33.646	C	-0.999	D	27.083	1444.3
95.8	95.80	33.654	C	-0.989	D	27.090	1444.4
96.5	96.55	33.663	C	-0.965	D	27.097	1444.5
97.3	97.30	33.672	C	-0.949	D	27.103	1444.6
98.0	98.05	33.680	C	-0.931	D	27.109	1444.8
98.7	98.75	33.689	C	-0.927	D	27.116	1444.8
99.4	99.40	33.696	C	-0.919	D	27.121	1444.9
100.1	100.15	33.704	C	-0.910	E	27.128	1444.9
100.9	100.90	33.710	C	-0.900	E	27.132	1445.0
101.6	101.60	33.721	C	-0.890	E	27.141	1445.1
102.3	102.35	33.730	C	-0.881	E	27.148	1445.1
103.1	103.10	33.738	C	-0.874	E	27.154	1445.2
103.8	103.80	33.743	C	-0.867	E	27.158	1445.2
104.5	104.50	33.752	C	-0.861	E	27.164	1445.3
105.2	105.25	33.757	C	-0.855	E	27.168	1445.3
105.9	105.95	33.762	C	-0.848	E	27.173	1445.4
106.6	106.60	33.769	C	-0.841	E	27.178	1445.4
107.4	107.40	33.776	C	-0.833	E	27.184	1445.5
108.1	108.15	33.784	C	-0.825	E	27.189	1445.6
108.8	108.80	33.791	C	-0.817	E	27.195	1445.6
109.5	109.50	33.800	C	-0.811	E	27.201	1445.7
110.2	110.25	33.806	C	-0.806	E	27.207	1445.7
110.9	110.95	33.812	C	-0.800	E	27.211	1445.8
111.6	111.65	33.820	C	-0.795	E	27.217	1445.8
112.4	112.45	33.825	C	-0.789	E	27.221	1445.9
113.1	113.15	33.830	C	-0.784	E	27.225	1445.9
113.8	113.85	33.838	C	-0.778	E	27.231	1445.9
114.5	114.55	33.845	C	-0.773	E	27.237	1446.0
115.3	115.35	33.850	C	-0.768	E	27.241	1446.0
116.0	116.00	33.856	C	-0.764	E	27.245	1446.1
116.7	116.70	33.861	C	-0.760	E	27.249	1446.1
117.5	117.50	33.864	C	-0.756	E	27.251	1446.1
118.2	118.20	33.871	C	-0.753	E	27.257	1446.2
118.9	118.90	33.873	C	-0.749	E	27.259	1446.2
119.6	119.65	33.879	C	-0.744	E	27.263	1446.3
120.4	120.40	33.886	C	-0.741	E	27.268	1446.3
121.1	121.10	33.889	C	-0.736	E	27.271	1446.3
121.8	121.80	33.895	C	-0.734	E	27.276	1446.4
122.5	122.55	33.897	C	-0.732	E	27.277	1446.4
123.2	123.25	33.902	C	-0.725	E	27.281	1446.4
123.9	123.95	33.912	C	-0.716	E	27.289	1446.5
124.7	124.75	33.918	C	-0.711	E	27.293	1446.5
125.4	125.45	33.926	C	-0.705	E	27.300	1446.6
126.1	126.15	33.934	C	-0.700	E	27.306	1446.6
126.9	126.90	33.938	C	-0.696	E	27.309	1446.7
127.6	127.65	33.943	C	-0.693	E	27.313	1446.7
128.3	128.35	33.948	C	-0.687	E	27.317	1446.8
129.1	129.10	33.956	C	-0.681	E	27.323	1446.8

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
129.8	129.85	33.960 C	-0.677 E	27.326	1446.8
130.5	130.55	33.965 C	-0.674 E	27.329	1446.9
131.2	131.25	33.972 C	-0.671 E	27.335	1446.9
132.0	132.05	33.976 C	-0.667 E	27.339	1447.0
132.7	132.75	33.980 C	-0.665 E	27.342	1447.0
133.4	133.45	33.983 C	-0.661 E	27.344	1447.0
134.2	134.20	33.987 C	-0.656 E	27.347	1447.1
135.0	135.00	33.993 C	-0.652 E	27.352	1447.1
135.7	135.70	33.997 C	-0.648 E	27.355	1447.1
136.4	136.45	34.003 C	-0.644 E	27.360	1447.2
137.2	137.25	34.009 C	-0.640 E	27.364	1447.2
137.9	137.90	34.012 C	-0.637 E	27.366	1447.2
138.6	138.60	34.019 C	-0.632 E	27.372	1447.3
139.3	139.35	34.023 C	-0.626 E	27.375	1447.3
140.1	140.15	34.029 C	-0.623 E	27.380	1447.4
140.8	140.80	34.033 C	-0.618 E	27.382	1447.4
141.5	141.55	34.039 C	-0.616 E	27.387	1447.4
142.3	142.30	34.044 C	-0.612 E	27.391	1447.5
143.0	143.05	34.050 C	-0.608 E	27.396	1447.5
143.7	143.75	34.055 C	-0.600 E	27.400	1447.6
144.5	144.55	34.062 C	-0.597 E	27.405	1447.6
145.2	145.25	34.068 C	-0.593 E	27.409	1447.6
145.9	145.95	34.070 C	-0.588 E	27.411	1447.7
146.7	146.70	34.076 C	-0.584 E	27.416	1447.7
147.5	147.50	34.083 C	-0.578 E	27.421	1447.8
148.2	148.20	34.088 C	-0.571 E	27.425	1447.8
148.8	148.85	34.094 C	-0.568 E	27.430	1447.9
149.7	149.75	34.095 C	-0.565 E	27.430	1447.9
150.4	150.40	34.100 C	-0.561 E	27.435	1447.9
151.0	151.05	34.107 C	-0.557 E	27.440	1448.0
151.9	151.90	34.113 C	-0.552 E	27.444	1448.0
152.7	152.70	34.118 C	-0.547 E	27.448	1448.0


EXPERIMENT 966
TEMPERATURE, C
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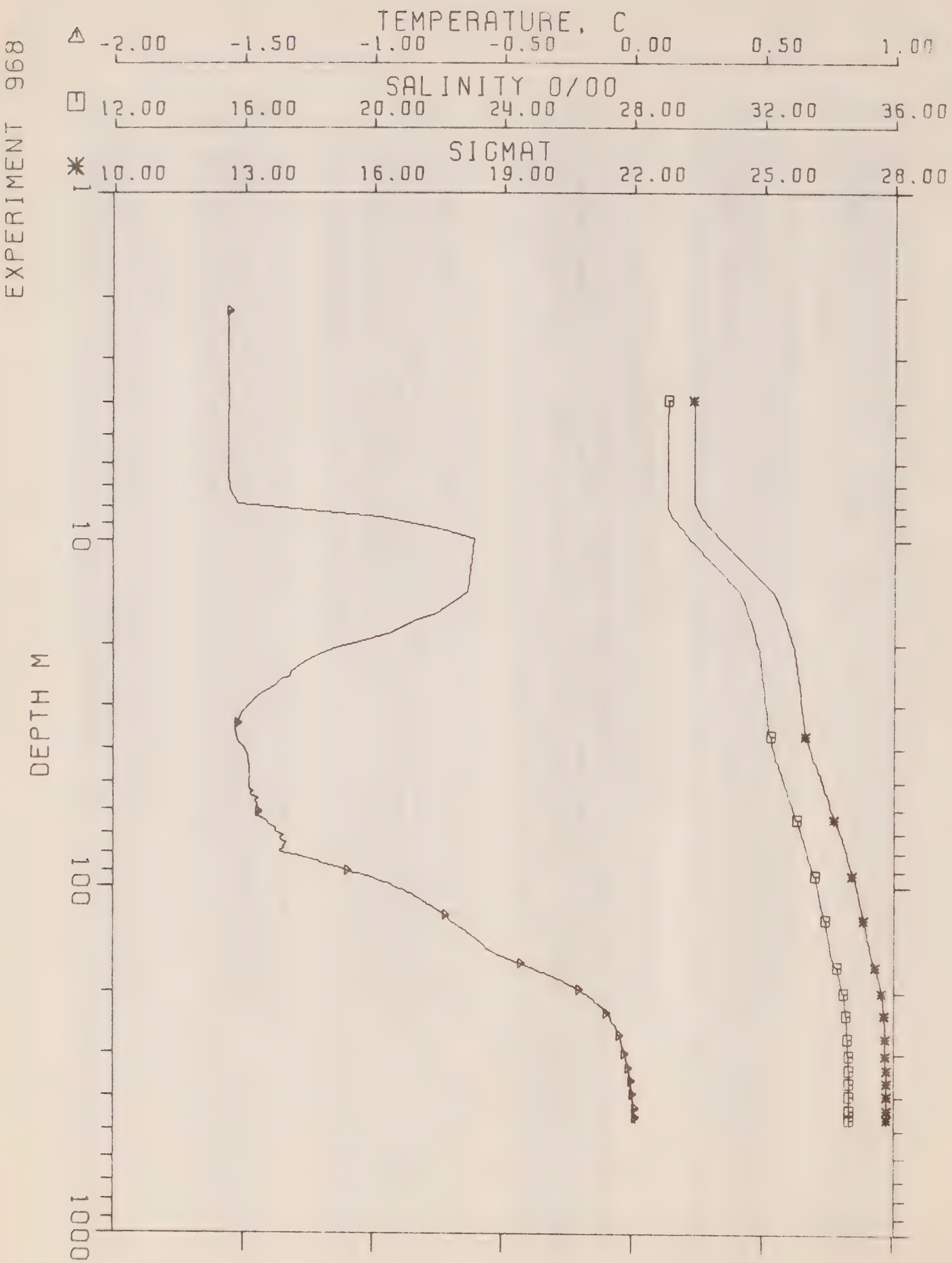
LAT N.80-34-45 LONG W.79-25-00 WATER DEPTH 519

DEPTH INCR. DATE 090474 LOCAL TIME 1625

DEPTH	PRES	SAL		TEMP		SIGMAT	SOUND
3.8	3.85	29.063	C	-1.568	D	23.388	1433.7
4.6	4.60	29.055	C	-1.568	D	23.382	1433.7
5.5	5.50	29.054	C	-1.569	D	23.381	1433.8
6.3	6.35	29.053	C	-1.569	D	23.380	1433.8
7.1	7.10	29.052	C	-1.569	D	23.380	1433.8
7.9	7.90	29.052	C	-1.569	D	23.380	1433.8
8.6	8.65	29.042	C	-1.385	D	23.369	1434.7
9.4	9.45	29.324	C	-0.947	D	23.589	1437.1
10.3	10.30	29.659	C	-0.692	D	23.854	1438.8
11.1	11.15	30.042	C	-0.543	D	24.159	1440.1
11.9	11.90	30.340	C	-0.500	D	24.398	1440.7
12.6	12.65	30.638	C	-0.465	D	24.637	1441.3
13.4	13.45	30.900	C	-0.472	D	24.849	1441.6
14.3	14.30	31.111	C	-0.528	D	25.020	1441.7
15.1	15.10	31.284	C	-0.614	D	25.163	1441.5
15.9	15.90	31.407	C	-0.636	D	25.263	1441.6
16.7	16.75	31.518	C	-0.697	D	25.354	1441.5
17.5	17.55	31.606	C	-0.779	D	25.428	1441.2
18.3	18.30	31.668	C	-0.857	D	25.481	1441.0
19.0	19.05	31.728	C	-0.939	D	25.531	1440.7
19.8	19.85	31.775	C	-1.004	D	25.572	1440.5
20.6	20.60	31.834	C	-1.084	D	25.621	1440.2
21.3	21.35	31.868	C	-1.138	D	25.650	1440.0
22.2	22.25	31.905	C	-1.193	D	25.681	1439.8
23.0	23.00	31.933	C	-1.233	D	25.705	1439.7
23.8	23.80	31.964	C	-1.278	D	25.731	1439.5
24.5	24.50	31.986	C	-1.313	D	25.750	1439.4
25.3	25.35	32.004	C	-1.340	D	25.765	1439.3
26.0	26.05	32.021	C	-1.363	D	25.780	1439.2
26.9	26.95	32.038	C	-1.384	D	25.793	1439.2
27.7	27.75	32.060	C	-1.416	D	25.812	1439.0
28.4	28.45	32.077	C	-1.438	D	25.826	1439.0
29.4	29.40	32.092	C	-1.457	D	25.839	1438.9
30.1	30.15	32.109	C	-1.477	D	25.854	1438.9
30.9	30.90	32.126	C	-1.494	D	25.867	1438.8
31.7	31.70	32.137	C	-1.505	D	25.876	1438.8
32.5	32.55	32.151	C	-1.515	D	25.888	1438.8
33.3	33.35	32.166	C	-1.523	D	25.901	1438.8
34.0	34.05	32.180	C	-1.528	D	25.912	1438.8
34.9	34.95	32.196	C	-1.533	D	25.925	1438.8
35.7	35.70	32.212	C	-1.534	D	25.938	1438.8
36.4	36.45	32.229	C	-1.532	D	25.951	1438.9
37.3	37.30	32.246	C	-1.529	D	25.965	1438.9
38.0	38.05	32.263	C	-1.523	D	25.979	1439.0
38.8	38.80	32.281	C	-1.517	D	25.994	1439.1
39.6	39.60	32.306	C	-1.512	D	26.014	1439.1
40.4	40.45	32.329	C	-1.506	D	26.032	1439.2
41.1	41.15	32.352	C	-1.501	D	26.050	1439.3
41.9	41.95	32.376	C	-1.496	D	26.070	1439.3
42.7	42.75	32.404	C	-1.495	D	26.093	1439.4
43.5	43.50	32.428	C	-1.493	D	26.112	1439.5
44.2	44.25	32.454	C	-1.491	D	26.133	1439.5
45.0	45.05	32.477	C	-1.493	D	26.151	1439.6
45.9	45.90	32.500	C	-1.487	D	26.170	1439.6
46.6	46.60	32.529	C	-1.488	D	26.194	1439.7
47.3	47.35	32.562	C	-1.485	D	26.221	1439.7
48.2	48.20	32.593	C	-1.488	D	26.246	1439.8
48.9	48.95	32.613	C	-1.485	D	26.262	1439.8
49.7	49.70	32.639	C	-1.487	D	26.283	1439.9
50.5	50.55	32.664	C	-1.491	D	26.303	1439.9
51.3	51.35	32.687	C	-1.489	D	26.322	1440.0
52.0	52.05	32.714	C	-1.487	D	26.343	1440.0

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
52.7	52.75	32.729	C	-1.462	D	26.355	1440.2
53.5	53.55	32.762	C	-1.473	D	26.382	1440.2
54.4	54.40	32.788	C	-1.480	D	26.404	1440.2
55.1	55.10	32.814	C	-1.458	D	26.424	1440.4
55.8	55.85	32.838	C	-1.447	D	26.443	1440.5
56.5	56.55	32.861	C	-1.475	D	26.463	1440.4
57.4	57.40	32.871	C	-1.452	D	26.469	1440.5
58.2	58.20	32.893	C	-1.436	D	26.487	1440.6
58.9	58.95	32.908	C	-1.429	D	26.499	1440.7
59.7	59.75	32.921	C	-1.424	D	26.510	1440.7
60.6	60.60	32.952	C	-1.435	D	26.535	1440.8
61.3	61.30	32.968	C	-1.443	D	26.548	1440.7
62.1	62.10	32.986	C	-1.423	D	26.563	1440.9
62.9	62.95	33.010	C	-1.433	D	26.582	1440.9
63.7	63.70	33.038	C	-1.401	D	26.604	1441.1
64.4	64.45	33.065	C	-1.384	D	26.625	1441.2
65.3	65.30	33.079	C	-1.379	D	26.637	1441.3
66.1	66.10	33.098	C	-1.385	D	26.652	1441.3
66.8	66.80	33.129	C	-1.396	D	26.678	1441.3
67.6	67.65	33.146	C	-1.402	D	26.691	1441.3
68.5	68.50	33.158	C	-1.385	D	26.701	1441.4
69.2	69.25	33.181	C	-1.367	D	26.719	1441.5
70.0	70.00	33.204	C	-1.362	D	26.737	1441.6
70.8	70.85	33.222	C	-1.357	D	26.752	1441.7
71.6	71.65	33.240	C	-1.348	D	26.766	1441.7
72.4	72.40	33.267	C	-1.352	D	26.788	1441.8
73.2	73.25	33.282	C	-1.368	D	26.800	1441.7
74.1	74.10	33.298	C	-1.361	D	26.813	1441.8
74.8	74.85	33.315	C	-1.334	D	26.826	1442.0
75.6	75.65	33.339	C	-1.380	D	26.847	1441.8
76.5	76.55	33.347	C	-1.388	D	26.854	1441.8
77.3	77.30	33.357	C	-1.391	D	26.862	1441.8
78.0	78.05	33.366	C	-1.392	D	26.869	1441.8
78.9	78.95	33.378	C	-1.393	D	26.879	1441.8
79.8	79.80	33.388	C	-1.390	D	26.887	1441.9
80.5	80.55	33.395	C	-1.377	D	26.892	1442.0
81.4	81.40	33.407	C	-1.345	D	26.901	1442.2
82.3	82.30	33.425	C	-1.303	D	26.915	1442.4
83.0	83.05	33.446	C	-1.282	D	26.931	1442.5
83.8	83.85	33.463	C	-1.289	D	26.945	1442.5
84.7	84.75	33.471	C	-1.249	D	26.950	1442.8
85.5	85.55	33.494	C	-1.201	D	26.968	1443.0
86.3	86.35	33.515	C	-1.198	D	26.984	1443.1
87.2	87.20	33.525	C	-1.193	D	26.992	1443.1
88.0	88.05	33.533	C	-1.180	D	26.998	1443.2
88.8	88.80	33.554	C	-1.154	D	27.015	1443.4
89.6	89.60	33.564	C	-1.122	D	27.021	1443.6
90.3	90.35	33.579	C	-1.106	D	27.033	1443.7
91.2	91.25	33.589	C	-1.083	D	27.040	1443.8
92.0	92.05	33.600	C	-1.066	D	27.049	1443.9
92.8	92.80	33.609	C	-1.047	D	27.055	1444.0
93.8	93.75	33.621	C	-1.029	D	27.065	1444.1
94.5	94.55	33.635	C	-1.011	D	27.075	1444.3
95.3	95.35	33.650	C	-0.992	D	27.087	1444.4
96.1	96.15	33.655	C	-0.980	D	27.090	1444.5
97.1	97.10	33.671	C	-0.957	D	27.102	1444.6
97.8	97.85	33.677	C	-0.940	D	27.107	1444.7
98.6	98.65	33.689	C	-0.930	D	27.117	1444.8
99.5	99.50	33.700	C	-0.921	D	27.125	1444.9
100.4	100.40	33.706	C	-0.909	E	27.129	1444.9
101.1	101.15	33.717	C	-0.899	E	27.138	1445.0
102.0	102.00	33.726	C	-0.887	E	27.145	1445.1
102.8	102.85	33.734	C	-0.877	E	27.151	1445.2
103.6	103.60	33.740	C	-0.870	E	27.155	1445.2
104.4	104.45	33.749	C	-0.862	E	27.162	1445.3
105.3	105.30	33.758	C	-0.855	E	27.169	1445.3
106.1	106.10	33.762	C	-0.847	E	27.172	1445.4
106.8	106.85	33.771	C	-0.839	E	27.179	1445.5
107.7	107.70	33.778	C	-0.830	E	27.185	1445.5

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
108.5	108.55	33.789 C	-0.823 E	27.193	1445.6
109.3	109.30	33.797 C	-0.814 E	27.199	1445.6
110.1	110.15	33.806 C	-0.808 E	27.207	1445.7
111.0	111.05	33.813 C	-0.800 E	27.212	1445.8
111.8	111.80	33.821 C	-0.794 E	27.218	1445.8
112.5	112.55	33.828 C	-0.788 E	27.223	1445.9
113.4	113.45	33.834 C	-0.783 E	27.229	1445.9
114.2	114.25	33.841 C	-0.776 E	27.233	1446.0
115.0	115.00	33.848 C	-0.771 E	27.239	1446.0
115.9	115.90	33.854 C	-0.767 E	27.243	1446.1
116.7	116.70	33.858 C	-0.761 E	27.247	1446.1
117.5	117.50	33.864 C	-0.757 E	27.252	1446.1
118.3	118.30	33.871 C	-0.754 E	27.257	1446.2
119.1	119.15	33.875 C	-0.749 E	27.260	1446.2
119.9	119.95	33.882 C	-0.744 E	27.265	1446.3
120.7	120.70	33.886 C	-0.741 E	27.269	1446.3
121.4	121.45	33.892 C	-0.736 E	27.273	1446.3
122.3	122.35	33.897 C	-0.733 E	27.277	1446.4
123.1	123.15	33.900 C	-0.728 E	27.280	1446.4
123.9	123.95	33.912 C	-0.718 E	27.289	1446.5
124.7	124.75	33.920 C	-0.712 E	27.295	1446.5
125.6	125.65	33.930 C	-0.704 E	27.303	1446.6
126.4	126.45	33.937 C	-0.700 E	27.308	1446.7
127.2	127.20	33.943 C	-0.696 E	27.313	1446.7
128.1	128.10	33.947 C	-0.691 E	27.316	1446.7
128.9	128.90	33.954 C	-0.685 E	27.322	1446.8
129.7	129.70	33.960 C	-0.680 E	27.326	1446.8
130.5	130.50	33.966 C	-0.677 E	27.331	1446.9
131.4	131.40	33.972 C	-0.671 E	27.336	1446.9
132.1	132.15	33.978 C	-0.667 E	27.340	1447.0
132.9	132.95	33.982 C	-0.665 E	27.343	1447.0
133.8	133.85	33.986 C	-0.660 E	27.347	1447.0
134.6	134.65	33.994 C	-0.655 E	27.352	1447.1
135.4	135.40	33.996 C	-0.650 E	27.354	1447.1
136.3	136.30	34.004 C	-0.644 E	27.360	1447.2
137.1	137.10	34.009 C	-0.641 E	27.365	1447.2
137.9	137.90	34.015 C	-0.636 E	27.369	1447.2
138.7	138.75	34.023 C	-0.630 E	27.375	1447.3
139.6	139.65	34.029 C	-0.625 E	27.380	1447.3
140.4	140.40	34.034 C	-0.621 E	27.383	1447.4
141.2	141.25	34.040 C	-0.619 E	27.388	1447.4
142.1	142.10	34.043 C	-0.613 E	27.390	1447.5
142.9	142.95	34.050 C	-0.606 E	27.396	1447.5
143.7	143.70	34.057 C	-0.601 E	27.401	1447.6
144.6	144.60	34.062 C	-0.596 E	27.405	1447.6
145.4	145.40	34.070 C	-0.591 E	27.411	1447.7
146.2	146.20	34.074 C	-0.586 E	27.414	1447.7
147.0	147.05	34.081 C	-0.581 E	27.420	1447.7
147.9	147.90	34.089 C	-0.573 E	27.426	1447.8
148.7	148.70	34.095 C	-0.570 E	27.431	1447.8
149.4	149.45	34.097 C	-0.567 E	27.432	1447.9
150.3	150.35	34.104 C	-0.562 E	27.438	1447.9
151.2	151.25	34.112 C	-0.555 E	27.444	1448.0
152.0	152.00	34.118 C	-0.551 E	27.448	1448.0


EXPERIMENT 968
TEMPERATURE, C
-2.00
-1.50
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-0.50
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SALINITY 0/00
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16.00
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SIGMAT
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CRUISE 15-74-012 D'IBERVILLE FIORD-74 EXPER NO. 968

LAT N.80-34-45 LONG W.79-25-00 WATER DEPTH 519

DEPTH INCR. DATE 100474 LOCAL TIME 0955

DEPTH	PRES	SAL		TEMP		SIGMAT	SOUND
2.2	2.20			-1.562	D		
2.3	2.30			-1.563	D		
2.7	2.75			-1.567	D		
3.3	3.35			-1.566	D		
3.9	3.95	29.063	C	-1.562	D	23.389	1433.8
4.6	4.60	29.060	C	-1.563	D	23.386	1433.8
5.3	5.30	29.061	C	-1.565	D	23.387	1433.8
5.8	5.85	29.060	C	-1.565	D	23.386	1433.8
6.5	6.50	29.063	C	-1.567	D	23.388	1433.8
7.2	7.25	29.061	C	-1.562	D	23.387	1433.8
7.8	7.85	29.055	C	-1.530	D	23.381	1434.0
8.5	8.55	29.244	C	-0.978	D	23.526	1436.9
9.2	9.25	29.549	C	-0.746	D	23.767	1438.4
9.9	9.90	29.800	C	-0.605	D	23.966	1439.4
14.1	14.10	31.320	C	-0.632	D	25.192	1441.5
14.8	14.80	31.421	C	-0.669	D	25.276	1441.5
15.5	15.55	31.524	C	-0.714	D	25.360	1441.4
16.2	16.25	31.567	C	-0.749	D	25.395	1441.3
16.9	16.95	31.667	C	-0.827	D	25.478	1441.1
17.6	17.60	31.713	C	-0.871	D	25.517	1441.0
18.4	18.45	31.782	C	-0.927	D	25.575	1440.8
19.1	19.10	31.813	C	-0.993	D	25.601	1440.6
19.7	19.75	31.857	C	-1.051	D	25.638	1440.4
20.5	20.50	31.906	C	-1.144	D	25.681	1440.0
21.2	21.25	31.923	C	-1.193	D	25.696	1439.8
21.9	21.90	31.943	C	-1.228	D	25.713	1439.7
22.6	22.60	31.969	C	-1.263	D	25.734	1439.6
23.4	23.40	31.984	C	-1.296	D	25.748	1439.4
24.0	24.00	31.996	C	-1.317	D	25.758	1439.4
24.7	24.75	32.016	C	-1.321	D	25.774	1439.4
25.3	25.35	32.036	C	-1.353	D	25.791	1439.3
26.1	26.10	32.047	C	-1.377	D	25.800	1439.2
26.8	26.85	32.060	C	-1.395	D	25.812	1439.1
27.5	27.55	32.078	C	-1.425	D	25.827	1439.0
28.2	28.20	32.090	C	-1.445	D	25.837	1439.0
28.7	28.75	32.098	C	-1.456	D	25.844	1438.9
31.4	31.40	32.140	C	-1.503	D	25.879	1438.8
32.0	32.00	32.153	C	-1.512	D	25.889	1438.8
32.5	32.50	32.160	C	-1.517	D	25.895	1438.8
33.3	33.30	32.173	C	-1.525	D	25.906	1438.8
33.9	33.95	32.187	C	-1.531	D	25.917	1438.8
34.6	34.65	32.200	C	-1.537	D	25.928	1438.8
35.3	35.35	32.211	C	-1.541	D	25.937	1438.8
36.1	36.10	32.225	C	-1.539	D	25.948	1438.8
36.7	36.75	32.237	C	-1.537	D	25.958	1438.9
37.4	37.40	32.256	C	-1.534	D	25.974	1438.9
38.2	38.20	32.277	C	-1.530	D	25.991	1439.0
38.8	38.85	32.298	C	-1.519	D	26.007	1439.1
39.5	39.50	32.327	C	-1.511	D	26.031	1439.2
40.2	40.25	32.350	C	-1.503	D	26.049	1439.2
40.9	40.95	32.372	C	-1.502	D	26.067	1439.3
41.6	41.65	32.391	C	-1.496	D	26.082	1439.4
42.3	42.35	32.417	C	-1.492	D	26.103	1439.4
43.1	43.10	32.442	C	-1.488	D	26.123	1439.5
43.7	43.70	32.475	C	-1.489	D	26.150	1439.5
44.4	44.40	32.508	C	-1.488	D	26.177	1439.6
45.0	45.05	32.531	C	-1.487	D	26.195	1439.7
45.8	45.85	32.558	C	-1.485	D	26.217	1439.7
46.5	46.50	32.582	C	-1.484	D	26.236	1439.8
47.2	47.20	32.607	C	-1.485	D	26.256	1439.8
47.9	47.90	32.630	C	-1.485	D	26.275	1439.9
48.6	48.65	32.647	C	-1.482	D	26.289	1439.9

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
49.3	49.30	32.672	C	-1.485	D	26.309	1439.9
50.0	50.00	32.694	C	-1.487	D	26.327	1440.0
50.7	50.75	32.712	C	-1.486	D	26.342	1440.0
51.3	51.30	32.726	C	-1.486	D	26.353	1440.0
51.9	51.95	32.742	C	-1.486	D	26.366	1440.1
52.6	52.60	32.757	C	-1.485	D	26.379	1440.1
53.2	53.25	32.774	C	-1.465	D	26.391	1440.2
53.7	53.75	32.792	C	-1.474	D	26.406	1440.2
54.3	54.30	32.817	C	-1.480	D	26.426	1440.2
54.9	54.95	32.835	C	-1.476	D	26.441	1440.3
55.7	55.70	32.856	C	-1.447	D	26.457	1440.5
56.3	56.30	32.871	C	-1.458	D	26.470	1440.5
57.0	57.05	32.896	C	-1.464	D	26.490	1440.5
57.5	57.55	32.905	C	-1.457	D	26.497	1440.5
58.3	58.35	32.922	C	-1.453	D	26.511	1440.6
59.0	59.00	32.941	C	-1.451	D	26.527	1440.6
59.7	59.70	32.959	C	-1.451	D	26.541	1440.7
60.3	60.35	32.983	C	-1.440	D	26.560	1440.8
61.0	61.05	33.004	C	-1.451	D	26.577	1440.8
61.8	61.80	33.019	C	-1.459	D	26.590	1440.8
62.4	62.45	33.032	C	-1.454	D	26.600	1440.8
62.9	62.95	33.041	C	-1.451	D	26.608	1440.8
63.6	63.60	33.049	C	-1.436	D	26.614	1440.9
64.2	64.25	33.070	C	-1.426	D	26.631	1441.0
64.9	64.90	33.086	C	-1.422	D	26.643	1441.1
65.6	65.60	33.101	C	-1.413	D	26.655	1441.1
66.3	66.35	33.116	C	-1.405	D	26.667	1441.2
66.7	66.75	33.131	C	-1.400	D	26.679	1441.3
67.2	67.20	33.143	C	-1.397	D	26.688	1441.3
67.9	67.90	33.156	C	-1.387	D	26.699	1441.4
68.6	68.60	33.182	C	-1.381	D	26.720	1441.5
69.2	69.20	33.198	C	-1.386	D	26.733	1441.5
69.9	69.90	33.212	C	-1.377	D	26.744	1441.5
70.6	70.65	33.229	C	-1.364	D	26.758	1441.6
71.3	71.35	33.240	C	-1.346	D	26.766	1441.8
72.0	72.00	33.264	C	-1.361	D	26.786	1441.7
72.8	72.80	33.281	C	-1.363	D	26.799	1441.8
73.5	73.55	33.295	C	-1.355	D	26.811	1441.8
74.1	74.10	33.306	C	-1.347	D	26.819	1441.9
74.6	74.65	33.315	C	-1.337	D	26.827	1442.0
75.3	75.35	33.336	C	-1.343	D	26.843	1442.0
76.0	76.00	33.349	C	-1.344	D	26.854	1442.0
76.6	76.65	33.360	C	-1.353	D	26.863	1442.0
77.4	77.45	33.364	C	-1.344	D	26.867	1442.0
78.1	78.15	33.386	C	-1.359	D	26.884	1442.0
78.8	78.80	33.389	C	-1.371	D	26.887	1442.0
79.5	79.55	33.396	C	-1.362	D	26.892	1442.0
80.3	80.30	33.402	C	-1.343	D	26.897	1442.1
80.9	80.95	33.416	C	-1.304	D	26.907	1442.4
83.2	83.20	33.451	C	-1.257	D	26.935	1442.7
83.9	83.95	33.469	C	-1.231	D	26.948	1442.8
84.6	84.65	33.481	C	-1.217	D	26.958	1442.9
85.3	85.35	33.495	C	-1.213	D	26.969	1443.0
86.1	86.10	33.502	C	-1.192	D	26.973	1443.1
86.8	86.80	33.513	C	-1.169	D	26.981	1443.2
87.5	87.50	33.529	C	-1.152	D	26.994	1443.3
88.2	88.25	33.543	C	-1.133	D	27.005	1443.5
88.9	88.95	33.556	C	-1.119	D	27.015	1443.5
89.6	89.65	33.567	C	-1.103	D	27.023	1443.7
90.4	90.40	33.583	C	-1.095	D	27.036	1443.7
91.1	91.15	33.584	C	-1.082	D	27.037	1443.8
91.8	91.85	33.596	C	-1.064	D	27.046	1443.9
92.5	92.55	33.608	C	-1.049	D	27.055	1444.0
93.3	93.30	33.618	C	-1.031	D	27.063	1444.1
94.0	94.05	33.628	C	-1.016	D	27.070	1444.2
94.6	94.65	33.638	C	-1.002	D	27.078	1444.3
95.3	95.35	33.650	C	-0.989	D	27.087	1444.4
96.1	96.10	33.658	C	-0.980	D	27.093	1444.5
96.9	96.90	33.664	C	-0.961	D	27.097	1444.6

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
97.5	97.50	33.674 C	-0.949 D	27.105	1444.7
98.2	98.25	33.681 C	-0.941 D	27.110	1444.7
98.9	98.90	33.688 C	-0.933 D	27.116	1444.8
99.5	99.55	33.695 C	-0.923 D	27.121	1444.8
100.2	100.20	33.704 D	-0.913 E	27.128	1444.9
101.0	101.05	33.712 D	-0.903 E	27.134	1445.0
101.7	101.75	33.719 D	-0.893 E	27.139	1445.0
102.4	102.45	33.730 D	-0.884 E	27.147	1445.1
103.1	103.15	33.735 D	-0.878 E	27.152	1445.2
103.9	103.90	33.740 D	-0.869 E	27.155	1445.2
104.5	104.55	33.748 D	-0.862 E	27.162	1445.3
105.2	105.20	33.754 D	-0.856 E	27.167	1445.3
105.9	105.90	33.761 D	-0.848 E	27.172	1445.4
106.5	106.55	33.769 D	-0.841 E	27.178	1445.4
108.8	108.85	33.792 D	-0.819 E	27.196	1445.6
109.5	109.55	33.799 D	-0.814 E	27.201	1445.7
110.3	110.35	33.805 D	-0.809 E	27.206	1445.7
110.9	110.95	33.810 D	-0.805 E	27.210	1445.7
111.6	111.65	33.814 D	-0.801 E	27.212	1445.8
112.3	112.35	33.818 D	-0.798 E	27.216	1445.8
113.0	113.00	33.823 D	-0.789 E	27.220	1445.9
113.6	113.65	33.836 D	-0.782 E	27.229	1445.9
114.3	114.30	33.844 D	-0.775 E	27.236	1446.0
115.0	115.00	33.849 D	-0.769 E	27.240	1446.0
115.7	115.70	33.857 D	-0.765 E	27.246	1446.1
116.5	116.50	33.863 D	-0.759 E	27.251	1446.1
118.8	118.85	33.887 D	-0.741 E	27.270	1446.3
119.5	119.50	33.893 D	-0.736 E	27.274	1446.3
120.2	120.20	33.899 D	-0.732 E	27.279	1446.3
120.9	120.95	33.904 D	-0.727 E	27.283	1446.4
121.7	121.70	33.910 D	-0.723 E	27.287	1446.4
122.3	122.35	33.916 D	-0.719 E	27.292	1446.5
122.9	122.95	33.918 D	-0.715 E	27.293	1446.5
123.6	123.65	33.923 D	-0.713 E	27.297	1446.5
124.4	124.40	33.925 D	-0.710 E	27.299	1446.6
125.1	125.15	33.929 D	-0.708 E	27.302	1446.6
125.8	125.85	33.935 D	-0.703 E	27.307	1446.6
126.5	126.55	33.940 D	-0.697 E	27.311	1446.7
127.3	127.30	33.947 D	-0.692 E	27.316	1446.7
127.9	127.95	33.954 D	-0.688 E	27.321	1446.8
128.6	128.65	33.959 D	-0.681 E	27.325	1446.8
129.3	129.35	33.966 D	-0.678 E	27.331	1446.8
130.3	130.35	33.971 D	-0.674 E	27.335	1446.9
131.6	131.65	33.978 D	-0.667 E	27.340	1446.9
144.6	144.65	34.069 D	-0.592 E	27.410	1447.6
146.2	146.20	34.076 D	-0.585 E	27.416	1447.7
148.1	148.15	34.088 D	-0.577 E	27.426	1447.8
148.9	148.90	34.091 D	-0.575 E	27.428	1447.8
149.6	149.60	34.094 D	-0.572 E	27.430	1447.8
150.4	150.40	34.097 D	-0.568 E	27.432	1447.9
151.1	151.10	34.102 D	-0.564 E	27.436	1447.9
151.7	151.70	34.105 D	-0.560 E	27.439	1448.0
152.4	152.45	34.111 D	-0.555 E	27.443	1448.0
155.0	155.05	34.133 D	-0.537 E	27.460	1448.2
155.8	155.80	34.137 D	-0.532 E	27.463	1448.2
156.5	156.55	34.145 D	-0.529 E	27.469	1448.2
157.2	157.25	34.148 D	-0.521 E	27.472	1448.3
157.9	157.90	34.157 D	-0.515 E	27.479	1448.3
158.7	158.70	34.165 D	-0.508 E	27.485	1448.4
159.4	159.45	34.172 D	-0.502 E	27.490	1448.4
160.2	160.20	34.179 D	-0.497 E	27.496	1448.5
160.9	160.90	34.186 D	-0.490 E	27.501	1448.5
161.7	161.70	34.194 D	-0.485 E	27.507	1448.6
162.4	162.40	34.201 D	-0.477 E	27.512	1448.6
163.1	163.10	34.209 D	-0.469 E	27.519	1448.7
163.7	163.75	34.216 D	-0.464 E	27.524	1448.8
164.3	164.35	34.221 D	-0.457 E	27.528	1448.8
165.0	165.00	34.228 D	-0.451 E	27.533	1448.8
165.8	165.80	34.235 D	-0.444 E	27.538	1448.9

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
166.5	166.50	34.245 D	-0.437 E	27.546	1449.0
167.2	167.25	34.255 D	-0.430 E	27.554	1449.0
168.0	168.00	34.262 D	-0.423 E	27.559	1449.1
168.7	168.70	34.266 D	-0.416 E	27.563	1449.1
169.3	169.35	34.273 D	-0.410 E	27.568	1449.2
170.1	170.10	34.280 D	-0.403 E	27.573	1449.2
170.7	170.75	34.286 D	-0.396 E	27.577	1449.3
171.5	171.50	34.293 D	-0.390 E	27.583	1449.3
172.2	172.25	34.298 D	-0.384 E	27.587	1449.4
172.9	172.90	34.305 D	-0.379 E	27.592	1449.4
173.6	173.60	34.311 D	-0.374 E	27.596	1449.5
174.3	174.30	34.315 D	-0.369 E	27.600	1449.5
176.2	176.20	34.331 D	-0.352 E	27.612	1449.6
176.7	176.75	34.338 D	-0.347 E	27.618	1449.7
177.6	177.60	34.345 D	-0.341 E	27.623	1449.7
179.8	179.80	34.365 D	-0.318 E	27.638	1449.9
180.6	180.60	34.372 D	-0.314 E	27.644	1449.9
181.2	181.25	34.375 D	-0.309 E	27.646	1450.0
181.9	181.90	34.381 D	-0.304 E	27.650	1450.0
184.1	184.15	34.394 D	-0.289 E	27.660	1450.1
184.8	184.80	34.398 D	-0.284 E	27.663	1450.2
185.5	185.55	34.404 D	-0.281 E	27.668	1450.2
186.3	186.30	34.407 D	-0.276 E	27.670	1450.3
186.9	186.95	34.413 D	-0.272 E	27.674	1450.3
187.6	187.65	34.415 D	-0.268 E	27.676	1450.3
188.3	188.30	34.417 D	-0.266 E	27.677	1450.3
188.8	188.80	34.418 D	-0.263 E	27.678	1450.4
189.3	189.30	34.422 D	-0.260 E	27.681	1450.4
190.0	190.05	34.428 D	-0.256 E	27.686	1450.4
190.8	190.80	34.431 D	-0.250 E	27.688	1450.5
191.5	191.50	34.434 D	-0.246 E	27.691	1450.5
192.2	192.20	34.440 D	-0.242 E	27.695	1450.6
192.9	192.95	34.443 D	-0.237 E	27.697	1450.6
193.6	193.65	34.447 D	-0.232 E	27.700	1450.6
194.3	194.35	34.451 D	-0.229 E	27.703	1450.7
195.0	195.05	34.454 D	-0.225 E	27.706	1450.7
195.5	195.55	34.456 D	-0.223 E	27.707	1450.7
196.0	196.00	34.459 D	-0.220 E	27.709	1450.7
196.6	196.60	34.460 D	-0.217 E	27.710	1450.8
197.3	197.35	34.465 D	-0.214 E	27.714	1450.8
198.0	198.05	34.466 D	-0.209 E	27.714	1450.8
198.7	198.70	34.472 D	-0.207 E	27.719	1450.9
199.5	199.50	34.474 D	-0.203 E	27.720	1450.9
200.2	200.25	34.478 D	-0.201 E	27.724	1450.9
200.9	200.95	34.481 D	-0.198 E	27.726	1451.0
201.6	201.65	34.486 D	-0.195 E	27.729	1451.0
202.5	202.50	34.487 D	-0.190 E	27.730	1451.0
203.1	203.15	34.491 D	-0.185 E	27.734	1451.1
203.8	203.85	34.493 D	-0.181 E	27.735	1451.1
204.6	204.60	34.497 D	-0.178 E	27.738	1451.1
205.3	205.35	34.500 D	-0.176 E	27.740	1451.2
206.0	206.00	34.502 D	-0.173 E	27.741	1451.2
206.7	206.70	34.503 D	-0.170 E	27.742	1451.2
207.4	207.40	34.505 D	-0.168 E	27.744	1451.2
208.1	208.10	34.509 D	-0.165 E	27.747	1451.3
208.8	208.85	34.511 D	-0.162 E	27.748	1451.3
209.6	209.60	34.513 D	-0.159 E	27.750	1451.3
210.2	210.25	34.517 D	-0.157 E	27.753	1451.3
210.9	210.90	34.518 D	-0.156 E	27.754	1451.4
211.5	211.55	34.521 D	-0.154 E	27.756	1451.4
212.0	212.05	34.521 D	-0.152 E	27.756	1451.4
212.6	212.65	34.523 D	-0.151 E	27.758	1451.4
213.4	213.45	34.524 D	-0.149 E	27.758	1451.4
214.1	214.15	34.525 D	-0.148 E	27.759	1451.5
214.7	214.75	34.527 D	-0.146 E	27.761	1451.5
215.4	215.45	34.529 D	-0.143 E	27.762	1451.5
216.1	216.15	34.532 D	-0.141 E	27.764	1451.5
216.8	216.85	34.532 D	-0.138 E	27.764	1451.6
217.6	217.60	34.534 D	-0.136 E	27.766	1451.6

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
218.3	218.35	34.537 D	-0.133 E	27.768	1451.6
219.0	219.05	34.539 D	-0.131 E	27.769	1451.6
219.8	219.80	34.540 D	-0.128 E	27.770	1451.7
220.6	220.60	34.544 D	-0.127 E	27.773	1451.7
221.2	221.25	34.546 D	-0.124 E	27.775	1451.7
221.9	221.95	34.546 D	-0.122 E	27.774	1451.7
222.6	222.65	34.546 D	-0.119 E	27.775	1451.8
225.0	225.05	34.553 D	-0.114 E	27.780	1451.8
227.6	227.60	34.557 D	-0.108 E	27.783	1451.9
228.4	228.40	34.560 D	-0.107 E	27.785	1451.9
229.1	229.15	34.561 D	-0.105 E	27.786	1452.0
229.8	229.85	34.562 D	-0.104 E	27.786	1452.0
230.5	230.50	34.564 D	-0.103 E	27.788	1452.0
231.3	231.35	34.565 D	-0.101 E	27.789	1452.0
232.1	232.10	34.568 D	-0.100 E	27.791	1452.0
232.7	232.75	34.569 D	-0.097 E	27.792	1452.1
233.5	233.55	34.570 D	-0.096 E	27.792	1452.1
234.2	234.25	34.570 D	-0.094 E	27.792	1452.1
234.9	234.95	34.572 D	-0.093 E	27.794	1452.1
235.7	235.75	34.572 D	-0.092 E	27.794	1452.1
236.5	236.50	34.574 D	-0.092 E	27.796	1452.2
237.2	237.20	34.574 D	-0.091 E	27.796	1452.2
237.9	237.90	34.576 D	-0.091 E	27.797	1452.2
238.7	238.75	34.577 D	-0.090 E	27.798	1452.2
239.4	239.40	34.577 D	-0.089 E	27.798	1452.2
240.1	240.10	34.579 D	-0.089 E	27.799	1452.2
240.9	240.90	34.580 D	-0.088 E	27.800	1452.3
241.6	241.60	34.579 D	-0.087 E	27.800	1452.3
242.2	242.25	34.580 D	-0.086 E	27.800	1452.3
243.0	243.00	34.581 D	-0.086 E	27.801	1452.3
243.7	243.75	34.580 D	-0.085 E	27.800	1452.3
244.4	244.45	34.582 D	-0.083 E	27.802	1452.3
245.1	245.15	34.584 D	-0.083 E	27.803	1452.4
245.9	245.90	34.585 D	-0.082 E	27.804	1452.4
246.6	246.60	34.587 D	-0.081 E	27.806	1452.4
249.1	249.10	34.590 D	-0.076 E	27.808	1452.5
249.7	249.75	34.591 D	-0.075 E	27.808	1452.5
255.8	255.80	34.597 D	-0.067 E	27.813	1452.6
256.4	256.45	34.598 D	-0.066 E	27.813	1452.6
257.2	257.20	34.600 D	-0.066 E	27.815	1452.6
257.6	257.60	34.599 D	-0.065 E	27.815	1452.7
258.3	258.30	34.600 D	-0.065 E	27.815	1452.7
259.0	259.00	34.600 D	-0.064 E	27.815	1452.7
260.7	260.70	34.601 D	-0.063 E	27.816	1452.7
261.3	261.35	34.601 D	-0.061 E	27.816	1452.7
262.0	262.05	34.603 D	-0.061 E	27.817	1452.8
262.7	262.75	34.602 D	-0.060 E	27.817	1452.8
263.5	263.55	34.603 D	-0.060 E	27.818	1452.8
264.2	264.25	34.604 D	-0.059 E	27.818	1452.8
266.4	266.40	34.606 D	-0.058 E	27.820	1452.8
267.1	267.15	34.607 D	-0.058 E	27.820	1452.9
267.9	267.95	34.607 D	-0.057 E	27.821	1452.9
268.6	268.65	34.606 D	-0.055 E	27.819	1452.9
269.2	269.25	34.606 D	-0.055 E	27.820	1452.9
269.9	269.95	34.607 D	-0.054 E	27.820	1452.9
270.6	270.65	34.607 D	-0.054 E	27.821	1452.9
273.2	273.20	34.608 D	-0.051 E	27.821	1453.0
273.9	273.90	34.608 D	-0.051 E	27.821	1453.0
274.7	274.70	34.609 D	-0.051 E	27.822	1453.0
275.3	275.35	34.610 D	-0.051 E	27.823	1453.0
276.0	276.05	34.612 D	-0.051 E	27.824	1453.0
276.8	276.85	34.611 D	-0.050 E	27.823	1453.1
277.6	277.60	34.610 D	-0.049 E	27.822	1453.1
278.3	278.30	34.612 D	-0.049 E	27.824	1453.1
279.0	279.05	34.613 D	-0.049 E	27.825	1453.1
279.8	279.80	34.611 D	-0.047 E	27.823	1453.1
280.5	280.50	34.612 D	-0.047 E	27.824	1453.1
281.2	281.20	34.613 D	-0.046 E	27.825	1453.2
282.0	282.00	34.612 D	-0.045 E	27.824	1453.2

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
282.6	282.65	34.614	D	-0.046	E	27.826	1453.2
283.3	283.35	34.612	D	-0.044	E	27.824	1453.2
284.0	284.05	34.613	D	-0.045	E	27.825	1453.2
284.8	284.80	34.615	D	-0.045	E	27.826	1453.2
285.5	285.55	34.614	D	-0.044	E	27.826	1453.2
286.2	286.25	34.615	D	-0.044	E	27.827	1453.2
286.9	286.95	34.615	D	-0.043	E	27.826	1453.3
287.7	287.75	34.616	D	-0.043	E	27.827	1453.3
288.5	288.50	34.615	D	-0.042	E	27.826	1453.3
289.1	289.10	34.617	D	-0.042	E	27.827	1453.3
289.9	289.95	34.616	D	-0.041	E	27.827	1453.3
290.6	290.65	34.616	D	-0.040	E	27.827	1453.3
291.3	291.35	34.617	D	-0.040	E	27.828	1453.4
293.8	293.80	34.618	D	-0.038	E	27.829	1453.4
294.6	294.60	34.619	D	-0.038	E	27.829	1453.4
295.2	295.25	34.619	D	-0.037	E	27.829	1453.4
296.0	296.00	34.620	D	-0.038	E	27.830	1453.4
296.8	296.80	34.619	D	-0.037	E	27.829	1453.5
297.3	297.30	34.620	D	-0.037	E	27.830	1453.5
298.1	298.15	34.619	D	-0.036	E	27.829	1453.5
298.8	298.85	34.618	D	-0.035	E	27.829	1453.5
299.5	299.50	34.619	D	-0.035	E	27.829	1453.5
300.3	300.30	34.620	D	-0.034	E	27.830	1453.5
301.1	301.10	34.619	D	-0.033	E	27.829	1453.5
301.8	301.80	34.621	D	-0.034	E	27.830	1453.6
302.3	302.30	34.620	D	-0.034	E	27.830	1453.6
302.9	302.95	34.620	D	-0.033	E	27.830	1453.6
303.7	303.70	34.621	D	-0.033	E	27.831	1453.6
304.5	304.50	34.622	D	-0.033	E	27.832	1453.6
305.2	305.25	34.620	D	-0.031	E	27.830	1453.6
305.9	305.90	34.621	D	-0.031	E	27.830	1453.6
306.4	306.40	34.621	D	-0.031	E	27.831	1453.6
307.0	307.05	34.621	D	-0.030	E	27.830	1453.7
307.8	307.80	34.622	D	-0.031	E	27.832	1453.7
312.1	312.10	34.624	D	-0.028	E	27.833	1453.8
312.8	312.80	34.624	D	-0.027	E	27.833	1453.8
313.4	313.45	34.623	D	-0.027	E	27.832	1453.8
314.1	314.15	34.625	D	-0.028	E	27.833	1453.8
314.9	314.95	34.625	D	-0.028	E	27.834	1453.8
315.6	315.60	34.625	D	-0.028	E	27.834	1453.8
316.3	316.30	34.624	D	-0.027	E	27.833	1453.8
317.1	317.15	34.625	D	-0.027	E	27.834	1453.8
317.8	317.80	34.624	D	-0.026	E	27.833	1453.9
318.4	318.45	34.625	D	-0.026	E	27.833	1453.9
319.2	319.25	34.625	D	-0.026	E	27.834	1453.9
319.9	319.95	34.624	D	-0.025	E	27.833	1453.9
320.6	320.65	34.625	D	-0.025	E	27.833	1453.9
321.3	321.35	34.627	D	-0.026	E	27.835	1453.9
322.1	322.15	34.624	D	-0.024	E	27.833	1453.9
322.8	322.85	34.626	D	-0.025	E	27.834	1453.9
323.5	323.55	34.625	D	-0.024	E	27.834	1454.0
324.3	324.30	34.626	D	-0.024	E	27.834	1454.0
325.0	325.05	34.625	D	-0.023	E	27.833	1454.0
325.7	325.70	34.627	D	-0.024	E	27.835	1454.0
326.5	326.50	34.626	D	-0.023	E	27.834	1454.0
327.2	327.20	34.626	D	-0.023	E	27.834	1454.0
327.9	327.90	34.626	D	-0.022	E	27.834	1454.0
328.6	328.60	34.628	D	-0.023	E	27.835	1454.1
329.4	329.40	34.627	D	-0.022	E	27.835	1454.1
330.1	330.15	34.627	D	-0.022	E	27.835	1454.1
330.8	330.80	34.627	D	-0.021	E	27.835	1454.1
331.6	331.60	34.627	D	-0.021	E	27.835	1454.1
332.2	332.25	34.627	D	-0.021	E	27.835	1454.1
333.0	333.00	34.627	D	-0.020	E	27.835	1454.1
333.7	333.70	34.626	D	-0.020	E	27.834	1454.2
334.4	334.45	34.627	D	-0.020	E	27.835	1454.2
335.2	335.20	34.628	D	-0.020	E	27.836	1454.2
335.9	335.90	34.627	D	-0.019	E	27.835	1454.2
336.6	336.60	34.629	D	-0.020	E	27.836	1454.2

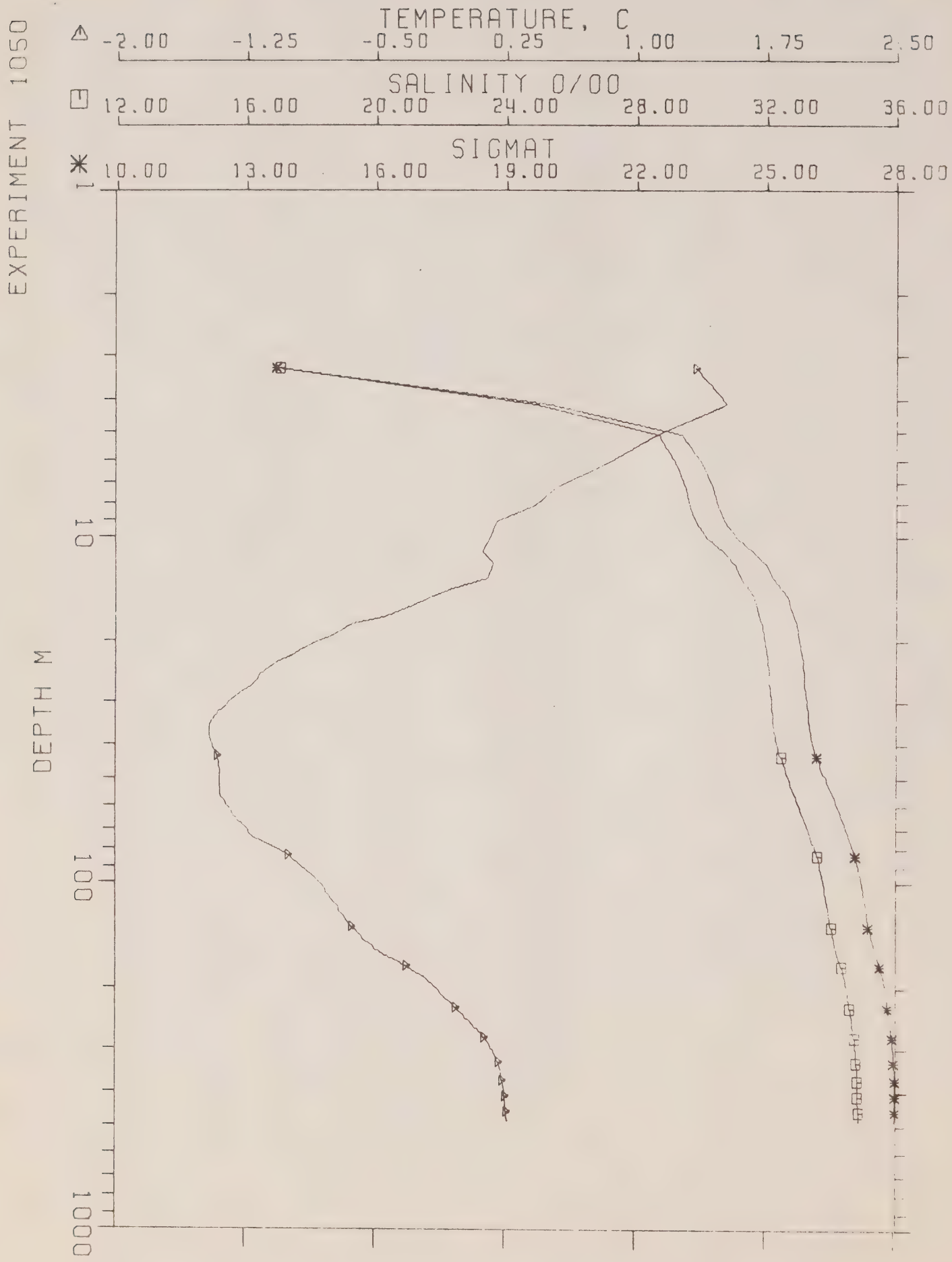
DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
337.4	337.40	34.627 D	-0.018 E	27.835	1454.2
338.1	338.10	34.627 D	-0.018 E	27.835	1454.2
338.8	338.80	34.629 D	-0.019 E	27.837	1454.2
339.5	339.55	34.628 D	-0.018 E	27.835	1454.3
340.3	340.30	34.629 D	-0.018 E	27.836	1454.3
341.0	341.00	34.628 D	-0.017 E	27.835	1454.3
341.7	341.75	34.629 D	-0.017 E	27.836	1454.3
342.5	342.55	34.628 D	-0.016 E	27.836	1454.3
343.2	343.20	34.628 D	-0.016 E	27.835	1454.3
343.9	343.90	34.628 D	-0.016 E	27.836	1454.3
344.7	344.70	34.629 D	-0.016 E	27.836	1454.4
345.4	345.40	34.629 D	-0.015 E	27.836	1454.4
346.1	346.10	34.628 D	-0.014 E	27.835	1454.4
346.9	346.90	34.630 D	-0.015 E	27.837	1454.4
347.6	347.65	34.629 D	-0.015 E	27.836	1454.4
348.3	348.30	34.629 D	-0.014 E	27.836	1454.4
349.0	349.05	34.629 D	-0.014 E	27.836	1454.4
349.9	349.90	34.628 D	-0.013 E	27.836	1454.5
350.5	350.55	34.629 D	-0.013 E	27.836	1454.5
351.2	351.25	34.630 D	-0.014 E	27.837	1454.5
351.9	351.95	34.630 D	-0.014 E	27.837	1454.5
352.7	352.75	34.629 D	-0.013 E	27.836	1454.5
353.4	353.40	34.630 D	-0.013 E	27.837	1454.5
354.1	354.15	34.630 D	-0.013 E	27.837	1454.5
354.7	354.75	34.630 D	-0.013 E	27.837	1454.5
355.2	355.25	34.630 D	-0.013 E	27.837	1454.5
356.0	356.00	34.630 D	-0.013 E	27.837	1454.6
356.7	356.70	34.629 D	-0.012 E	27.836	1454.6
357.3	357.35	34.629 D	-0.012 E	27.836	1454.6
358.1	358.15	34.630 D	-0.012 E	27.837	1454.6
358.8	358.85	34.629 D	-0.011 E	27.836	1454.6
359.5	359.55	34.629 D	-0.012 E	27.836	1454.6
360.2	360.25	34.630 D	-0.012 E	27.837	1454.6
361.0	361.00	34.630 D	-0.012 E	27.837	1454.6
361.8	361.80	34.630 D	-0.011 E	27.836	1454.7
362.5	362.50	34.629 D	-0.010 E	27.836	1454.7
363.2	363.20	34.630 D	-0.010 E	27.836	1454.7
364.0	364.00	34.630 D	-0.010 E	27.837	1454.7
364.6	364.65	34.629 D	-0.010 E	27.836	1454.7
365.4	365.40	34.631 D	-0.011 E	27.838	1454.7
366.1	366.15	34.630 D	-0.010 E	27.837	1454.7
366.9	366.90	34.632 D	-0.011 E	27.838	1454.7
367.6	367.60	34.631 D	-0.010 E	27.837	1454.8
368.4	368.40	34.631 D	-0.009 E	27.837	1454.8
369.0	369.05	34.631 D	-0.010 E	27.838	1454.8
369.8	369.85	34.631 D	-0.010 E	27.838	1454.8
370.5	370.50	34.629 D	-0.008 E	27.836	1454.8
371.2	371.20	34.632 D	-0.010 E	27.838	1454.8
371.9	371.90	34.631 D	-0.009 E	27.838	1454.8
372.5	372.55	34.632 D	-0.010 E	27.839	1454.8
373.2	373.25	34.632 D	-0.009 E	27.838	1454.9
374.0	374.05	34.631 D	-0.008 E	27.838	1454.9
374.7	374.70	34.632 D	-0.009 E	27.838	1454.9
375.4	375.40	34.632 D	-0.009 E	27.839	1454.9
376.2	376.20	34.631 D	-0.008 E	27.838	1454.9
376.9	376.90	34.633 D	-0.009 E	27.839	1454.9
377.6	377.60	34.631 D	-0.007 E	27.837	1454.9
378.3	378.30	34.634 D	-0.009 E	27.840	1454.9
379.0	379.05	34.633 D	-0.008 E	27.839	1455.0
379.7	379.75	34.631 D	-0.007 E	27.838	1455.0
380.3	380.35	34.632 D	-0.007 E	27.838	1455.0
382.2	382.20	34.634 D	-0.008 E	27.840	1455.0
382.9	382.90	34.632 D	-0.007 E	27.838	1455.0
383.6	383.65	34.631 D	-0.006 E	27.838	1455.0
384.3	384.35	34.633 D	-0.007 E	27.839	1455.1
385.0	385.00	34.631 D	-0.006 E	27.837	1455.1
385.6	385.65	34.631 D	-0.006 E	27.837	1455.1
386.4	386.40	34.632 D	-0.006 E	27.838	1455.1
387.1	387.15	34.633 D	-0.007 E	27.839	1455.1

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
387.9	387.90	34.631 D	-0.006 E	27.838	1455.1
390.2	390.25	34.633 D	-0.006 E	27.839	1455.2
391.0	391.00	34.633 D	-0.006 E	27.839	1455.2
391.7	391.75	34.633 D	-0.006 E	27.839	1455.2
392.4	392.45	34.632 D	-0.005 E	27.838	1455.2
393.1	393.15	34.632 D	-0.005 E	27.838	1455.2
393.9	393.90	34.632 D	-0.004 E	27.838	1455.2
396.3	396.30	34.631 D	-0.004 E	27.838	1455.3
397.0	397.00	34.633 D	-0.005 E	27.839	1455.3
397.7	397.75	34.634 D	-0.005 E	27.839	1455.3
398.5	398.50	34.633 D	-0.005 E	27.839	1455.3
399.1	399.15	34.634 D	-0.004 E	27.839	1455.3
403.4	403.40	34.633 D	-0.003 E	27.839	1455.4
405.6	405.65	34.633 D	-0.003 E	27.839	1455.4
408.0	408.00	34.633 D	-0.002 E	27.839	1455.5
410.4	410.40	34.635 D	-0.003 E	27.840	1455.5
411.0	411.05	34.633 D	-0.002 E	27.839	1455.5
411.8	411.80	34.634 D	-0.002 E	27.839	1455.5
412.6	412.60	34.634 D	-0.002 E	27.839	1455.5
413.3	413.30	34.633 D	-0.001 E	27.839	1455.6
413.9	413.95	34.634 D	-0.002 E	27.839	1455.6
414.6	414.65	34.634 D	-0.002 E	27.840	1455.6
415.4	415.45	34.635 D	-0.002 E	27.840	1455.6
416.1	416.10	34.634 D	-0.002 E	27.840	1455.6
416.8	416.85	34.635 D	-0.002 E	27.841	1455.6
419.3	419.30	34.635 D	-0.001 E	27.840	1455.7
420.1	420.10	34.634 D	0.0 E	27.839	1455.7
420.7	420.75	34.633 D	0.0 E	27.839	1455.7
421.4	421.45	34.634 D	0.0 E	27.839	1455.7
422.2	422.25	34.636 D	-0.001 E	27.841	1455.7
422.9	422.95	34.634 D	0.0 E	27.839	1455.7
423.6	423.65	34.635 D	0.0 E	27.840	1455.7
424.4	424.45	34.635 D	0.0 E	27.840	1455.7
425.2	425.20	34.635 D	0.0 E	27.840	1455.8
425.8	425.85	34.634 D	0.001 E	27.839	1455.8
426.6	426.60	34.635 D	0.001 E	27.840	1455.8
427.3	427.35	34.635 D	0.001 E	27.840	1455.8
428.0	428.05	34.633 D	0.002 E	27.839	1455.8
428.7	428.70	34.635 D	0.001 E	27.840	1455.8
429.5	429.50	34.635 D	0.001 E	27.840	1455.8
430.2	430.25	34.634 D	0.001 E	27.840	1455.8
430.9	430.90	34.635 D	0.001 E	27.841	1455.9
431.6	431.65	34.635 D	0.002 E	27.840	1455.9
432.3	432.35	34.634 D	0.003 E	27.839	1455.9
433.0	433.05	34.635 D	0.003 E	27.840	1455.9
433.8	433.80	34.635 D	0.003 E	27.840	1455.9
434.5	434.50	34.636 D	0.003 E	27.841	1455.9
435.1	435.15	34.635 D	0.003 E	27.840	1455.9
435.8	435.85	34.636 D	0.002 E	27.841	1455.9
436.6	436.60	34.635 D	0.003 E	27.840	1456.0
437.2	437.25	34.635 D	0.003 E	27.840	1456.0
437.9	437.90	34.637 D	0.002 E	27.842	1456.0
438.7	438.70	34.635 D	0.003 E	27.840	1456.0
439.3	439.35	34.635 D	0.004 E	27.840	1456.0
440.0	440.00	34.635 D	0.003 E	27.840	1456.0
440.7	440.70	34.635 D	0.003 E	27.840	1456.0
441.4	441.45	34.635 D	0.003 E	27.840	1456.0
442.1	442.10	34.635 D	0.004 E	27.840	1456.1
442.8	442.80	34.636 D	0.003 E	27.841	1456.1
443.5	443.50	34.636 D	0.003 E	27.841	1456.1
444.2	444.20	34.636 D	0.003 E	27.841	1456.1
444.8	444.85	34.637 D	0.003 E	27.841	1456.1
445.6	445.60	34.636 D	0.003 E	27.841	1456.1
446.3	446.30	34.636 D	0.003 E	27.841	1456.1
446.9	446.95	34.635 D	0.004 E	27.840	1456.1
447.6	447.65	34.636 D	0.004 E	27.841	1456.1
448.4	448.40	34.635 D	0.004 E	27.840	1456.2
449.1	449.10	34.636 D	0.004 E	27.841	1456.2
449.7	449.75	34.636 D	0.004 E	27.841	1456.2

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
450.5	450.50	34.635 D	0.005 E	27.840	1456.2
451.2	451.20	34.636 D	0.004 E	27.841	1456.2
451.8	451.85	34.635 D	0.004 E	27.840	1456.2
452.6	452.60	34.635 D	0.005 E	27.840	1456.2
453.3	453.30	34.635 D	0.005 E	27.840	1456.2
453.9	453.95	34.636 D	0.005 E	27.841	1456.3
454.7	454.70	34.635 D	0.005 E	27.840	1456.3
455.4	455.40	34.635 D	0.005 E	27.840	1456.3
456.0	456.05	34.635 D	0.005 E	27.840	1456.3
456.7	456.75	34.635 D	0.005 E	27.840	1456.3
457.5	457.50	34.636 D	0.004 E	27.841	1456.3
458.2	458.20	34.637 D	0.004 E	27.842	1456.3
458.8	458.85	34.636 D	0.004 E	27.841	1456.3
459.6	459.65	34.637 D	0.004 E	27.842	1456.3
460.3	460.35	34.636 D	0.005 E	27.841	1456.4
460.9	460.95	34.637 D	0.005 E	27.841	1456.4
461.6	461.65	34.636 D	0.006 E	27.841	1456.4
462.4	462.40	34.636 D	0.006 E	27.841	1456.4
463.1	463.10	34.636 D	0.006 E	27.841	1456.4
463.7	463.75	34.638 D	0.005 E	27.842	1456.4
464.5	464.55	34.637 D	0.006 E	27.841	1456.4
465.1	465.15	34.637 D	0.005 E	27.842	1456.4
465.8	465.85	34.638 D	0.005 E	27.842	1456.5
466.6	466.60	34.637 D	0.006 E	27.841	1456.5
467.3	467.30	34.636 D	0.006 E	27.841	1456.5
467.9	467.95	34.637 D	0.006 E	27.842	1456.5
468.7	468.70	34.637 D	0.006 E	27.842	1456.5
469.4	469.40	34.636 D	0.007 E	27.841	1456.5
470.0	470.05	34.637 D	0.006 E	27.842	1456.5
470.7	470.75	34.639 D	0.005 E	27.843	1456.5
471.5	471.50	34.637 D	0.006 E	27.842	1456.5
472.1	472.15	34.636 D	0.007 E	27.841	1456.6
472.8	472.80	34.638 D	0.006 E	27.842	1456.6
473.6	473.60	34.638 D	0.006 E	27.842	1456.6
474.3	474.30	34.636 D	0.008 E	27.841	1456.6
474.9	474.95	34.636 D	0.007 E	27.841	1456.6

OCEANOGRAPHIC DATA

AUGUST 1974


EXPERIMENT 1050
TEMPERATURE, C
-2.00
-1.25
-0.50
0.25
1.00
1.75
2.50
SALINITY 0/00
12.00
16.00
20.00
24.00
28.00
32.00
36.00
SIGMAT
10.00
13.00
16.00
19.00
22.00
25.00
28.00
DEPTH M
1
10
100
1000

CRUISE 15-74-013 D'IBERVILLE FIORD-74 EXPER NO. 1050

LAT N.80-34-10 LONG W.80-16-10 WATER DEPTH 510

DEPTH INCR. DATE 230874 LOCAL TIME 1415

DEPTH	PRES	SAL	TEMP	SIGMAT	SOUND
3.2	3.25	17.044 C	1.336 D	13.695	1431.1
4.1	4.15	24.955 C	1.525 D	20.003	1442.5
5.0	5.05	28.720 C	1.131 D	23.033	1445.9
6.2	6.20	29.300 C	0.831 D	23.511	1445.3
7.2	7.20	29.556 C	0.545 D	23.729	1444.4
8.1	8.15	29.697 C	0.425 D	23.848	1444.0
9.0	9.05	29.874 C	0.206 D	23.999	1443.3
10.0	10.05	30.213 C	0.169 D	24.273	1443.6
11.1	11.15	30.759 C	0.118 D	24.714	1444.1
12.0	12.00	31.095 C	0.181 D	24.981	1444.9
13.2	13.20	31.289 C	0.153 D	25.139	1445.1
14.1	14.15	31.513 C	-0.048 D	25.327	1444.5
14.9	14.95	31.680 C	-0.160 D	25.467	1444.2
16.0	16.05	31.776 C	-0.298 D	25.549	1443.7
17.1	17.10	31.856 C	-0.451 D	25.619	1443.1
17.9	17.95	31.927 C	-0.630 D	25.683	1442.4
19.2	19.20	31.970 C	-0.727 D	25.720	1442.0
20.0	20.00	31.996 C	-0.813 D	25.745	1441.7
21.0	21.00	32.033 C	-0.910 D	25.777	1441.3
22.1	22.10	32.063 C	-0.981 D	25.803	1441.0
23.0	23.00	32.088 C	-1.058 D	25.826	1440.7
24.0	24.05	32.110 C	-1.107 D	25.845	1440.5
25.1	25.15	32.130 C	-1.159 D	25.862	1440.3
26.1	26.10	32.138 C	-1.185 D	25.870	1440.2
27.0	27.05	32.150 C	-1.216 D	25.880	1440.1
28.1	28.15	32.168 C	-1.269 D	25.896	1439.9
29.0	29.05	32.182 C	-1.299 D	25.908	1439.8
30.0	30.05	32.200 C	-1.337 D	25.924	1439.7
31.1	31.10	32.218 C	-1.366 D	25.939	1439.6
32.1	32.10	32.232 C	-1.405 D	25.952	1439.4
33.1	33.10	32.243 C	-1.426 D	25.960	1439.3
34.0	34.05	32.257 C	-1.447 D	25.973	1439.3
35.2	35.25	32.274 C	-1.463 D	25.986	1439.2
36.1	36.10	32.291 C	-1.471 D	26.000	1439.2
37.3	37.30	32.312 C	-1.467 D	26.018	1439.3
38.2	38.20	32.334 C	-1.468 D	26.035	1439.4
39.2	39.25	32.356 C	-1.461 D	26.053	1439.4
40.1	40.15	32.384 C	-1.449 D	26.075	1439.6
41.2	41.20	32.409 C	-1.444 D	26.095	1439.6
42.1	42.15	32.446 C	-1.432 D	26.125	1439.8
43.0	43.05	32.485 C	-1.424 D	26.157	1439.9
44.2	44.25	32.523 C	-1.423 D	26.187	1439.9
45.1	45.10	32.558 C	-1.408 D	26.215	1440.1
46.1	46.15	32.585 C	-1.416 D	26.237	1440.1
47.3	47.30	32.628 C	-1.407 D	26.272	1440.2
48.2	48.20	32.668 C	-1.397 D	26.304	1440.3
49.2	49.25	32.715 C	-1.407 D	26.342	1440.4
50.1	50.10	32.750 C	-1.410 D	26.371	1440.4
51.3	51.30	32.780 C	-1.408 D	26.395	1440.5
52.0	52.05	32.812 C	-1.404 D	26.421	1440.6
53.1	53.15	32.851 C	-1.405 D	26.452	1440.6
54.0	54.05	32.882 C	-1.403 D	26.477	1440.7
55.1	55.10	32.919 C	-1.409 D	26.507	1440.7
56.1	56.10	32.948 C	-1.407 D	26.531	1440.8
57.0	57.00	32.977 C	-1.399 D	26.555	1440.9
58.1	58.10	33.010 C	-1.384 D	26.581	1441.0
59.1	59.10	33.036 C	-1.374 D	26.601	1441.1
60.1	60.15	33.065 C	-1.368 D	26.625	1441.2
61.1	61.10	33.097 C	-1.357 D	26.650	1441.3
62.2	62.20	33.125 C	-1.351 D	26.673	1441.4
63.1	63.15	33.154 C	-1.340 D	26.696	1441.5
64.0	64.00	33.185 C	-1.329 D	26.721	1441.6

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
65.0	65.00	33.210	C	-1.321	D	26.741	1441.7
66.2	66.25	33.231	C	-1.304	D	26.758	1441.9
67.1	67.15	33.267	C	-1.286	D	26.786	1442.0
68.1	68.15	33.295	C	-1.272	D	26.808	1442.1
69.0	69.00	33.316	C	-1.264	D	26.825	1442.2
70.1	70.15	33.340	C	-1.249	D	26.844	1442.3
71.1	71.15	33.369	C	-1.236	D	26.867	1442.4
72.1	72.10	33.389	C	-1.241	D	26.884	1442.5
73.2	73.25	33.410	C	-1.231	D	26.900	1442.6
74.3	74.35	33.428	C	-1.211	D	26.914	1442.7
75.2	75.20	33.450	C	-1.182	D	26.931	1442.9
76.1	76.15	33.476	C	-1.152	D	26.951	1443.1
77.1	77.15	33.501	C	-1.141	D	26.971	1443.2
78.1	78.15	33.526	C	-1.115	D	26.990	1443.4
79.2	79.20	33.546	C	-1.089	D	27.006	1443.5
80.1	80.15	33.562	C	-1.072	D	27.018	1443.6
81.3	81.30	33.580	C	-1.047	D	27.032	1443.8
82.0	82.05	33.600	C	-1.031	D	27.048	1443.9
83.3	83.30	33.619	C	-1.007	D	27.062	1444.1
84.3	84.30	33.629	C	-0.993	D	27.070	1444.2
92.9	92.95	33.735	C	-0.897	D	27.152	1444.9
93.8	93.85	33.748	C	-0.885	D	27.163	1445.0
94.9	94.95	33.762	C	-0.872	D	27.174	1445.1
95.9	95.95	33.774	C	-0.863	D	27.182	1445.2
96.9	96.95	33.782	C	-0.854	D	27.189	1445.2
98.1	98.10	33.792	C	-0.844	D	27.196	1445.3
101.6	101.60	33.825	D	-0.816	E	27.222	1445.6
102.5	102.50	33.834	D	-0.811	E	27.229	1445.6
103.2	103.20	33.840	D	-0.805	E	27.234	1445.6
104.4	104.40	33.849	D	-0.801	E	27.241	1445.7
105.4	105.40	33.852	D	-0.796	E	27.243	1445.7
106.4	106.40	33.857	D	-0.793	E	27.247	1445.8
107.5	107.55	33.863	D	-0.786	E	27.251	1445.8
108.4	108.45	33.876	D	-0.778	E	27.262	1445.9
109.4	109.40	33.895	D	-0.772	E	27.269	1446.0
110.6	110.65	33.889	D	-0.767	E	27.272	1446.0
111.5	111.50	33.897	D	-0.763	E	27.278	1446.1
112.6	112.65	33.901	D	-0.757	E	27.282	1446.1
113.6	113.65	33.911	D	-0.751	E	27.289	1446.2
114.5	114.55	33.924	D	-0.738	E	27.299	1446.3
115.7	115.75	33.931	D	-0.731	E	27.305	1446.3
116.7	116.70	33.941	D	-0.723	E	27.312	1446.4
117.5	117.55	33.945	D	-0.720	E	27.316	1446.4
118.7	118.70	33.949	D	-0.719	E	27.319	1446.5
119.6	119.60	33.953	D	-0.716	E	27.322	1446.5
120.5	120.55	33.957	D	-0.714	E	27.325	1446.5
121.7	121.70	33.962	D	-0.711	E	27.329	1446.6
122.5	122.50	33.968	D	-0.706	E	27.333	1446.6
123.5	123.50	33.974	D	-0.698	E	27.338	1446.7
124.3	124.30	33.982	D	-0.691	E	27.344	1446.7
125.4	125.40	33.989	D	-0.685	E	27.349	1446.8
126.4	126.45	33.993	D	-0.682	E	27.353	1446.8
127.5	127.55	33.998	D	-0.679	E	27.357	1446.9
128.6	128.60	34.001	D	-0.676	E	27.359	1446.9
129.7	129.70	34.006	D	-0.672	E	27.363	1446.9
130.5	130.55	34.014	D	-0.666	E	27.369	1447.0
131.5	131.55	34.019	D	-0.661	E	27.373	1447.0
132.6	132.60	34.026	D	-0.651	E	27.378	1447.1
133.6	133.65	34.031	D	-0.646	E	27.382	1447.2
134.5	134.50	34.045	D	-0.639	E	27.393	1447.2
135.7	135.75	34.052	D	-0.628	E	27.398	1447.3
136.6	136.60	34.059	D	-0.624	E	27.403	1447.3
137.5	137.55	34.067	D	-0.615	E	27.410	1447.4
138.6	138.65	34.075	D	-0.609	E	27.416	1447.5
139.5	139.50	34.082	D	-0.603	E	27.422	1447.5
140.5	140.55	34.091	D	-0.597	E	27.429	1447.6
141.6	141.60	34.099	D	-0.593	E	27.435	1447.6
142.5	142.50	34.100	D	-0.588	E	27.435	1447.7
143.6	143.65	34.106	D	-0.584	E	27.441	1447.7

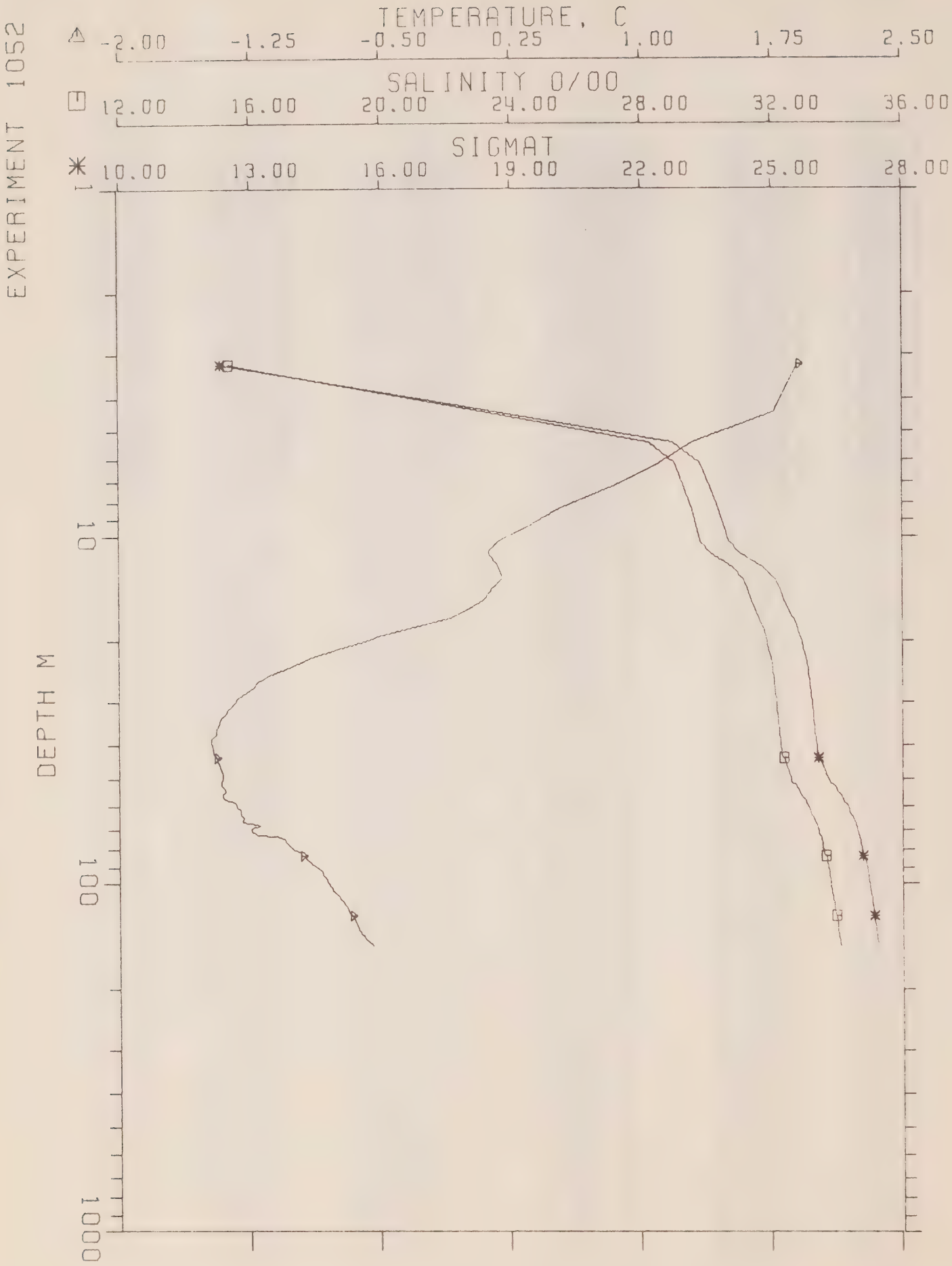
DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
144.5	144.55	34.112	D	-0.580	E	27.444	1447.8
145.6	145.65	34.119	D	-0.576	E	27.451	1447.8
146.7	146.70	34.123	D	-0.568	E	27.453	1447.9
147.7	147.75	34.136	D	-0.558	E	27.463	1447.9
148.7	148.70	34.145	D	-0.545	E	27.470	1448.0
149.7	149.75	34.158	D	-0.539	E	27.480	1448.1
150.8	150.85	34.168	D	-0.529	E	27.488	1448.2
151.8	151.80	34.173	D	-0.523	E	27.492	1448.2
152.8	152.80	34.177	D	-0.522	E	27.495	1448.2
153.9	153.90	34.183	D	-0.517	E	27.499	1448.3
154.8	154.85	34.187	D	-0.512	E	27.502	1448.3
155.8	155.85	34.197	D	-0.503	E	27.511	1448.4
156.7	156.70	34.207	D	-0.493	E	27.518	1448.5
157.7	157.75	34.218	D	-0.484	E	27.527	1448.6
159.1	159.15	34.228	D	-0.473	E	27.534	1448.7
159.8	159.85	34.242	D	-0.461	E	27.544	1448.7
161.0	161.05	34.253	D	-0.451	E	27.553	1448.8
162.0	162.00	34.262	D	-0.441	E	27.561	1448.9
162.9	162.95	34.273	D	-0.433	E	27.569	1449.0
163.9	163.95	34.288	D	-0.417	E	27.580	1449.1
164.9	164.90	34.296	D	-0.407	E	27.586	1449.1
166.0	166.00	34.307	D	-0.398	E	27.594	1449.2
166.7	166.70	34.319	D	-0.386	E	27.603	1449.3
167.6	167.65	34.327	D	-0.381	E	27.610	1449.4
169.0	169.00	34.332	D	-0.368	E	27.613	1449.4
170.1	170.15	34.343	D	-0.360	E	27.622	1449.5
171.1	171.10	34.350	D	-0.355	E	27.628	1449.6
172.0	172.05	34.355	D	-0.344	E	27.630	1449.6
173.0	173.00	34.365	D	-0.337	E	27.638	1449.7
173.9	173.95	34.372	D	-0.326	E	27.644	1449.8
174.9	174.95	34.379	D	-0.319	E	27.649	1449.8
175.9	175.90	34.387	D	-0.309	E	27.656	1449.9
176.8	176.80	34.396	D	-0.302	E	27.662	1450.0
177.9	177.90	34.399	D	-0.296	E	27.664	1450.0
178.7	178.75	34.407	D	-0.290	E	27.671	1450.1
179.9	179.90	34.411	D	-0.280	E	27.673	1450.1
180.9	180.90	34.419	D	-0.273	E	27.679	1450.2
182.0	182.00	34.428	D	-0.263	E	27.686	1450.3
183.0	183.05	34.438	D	-0.252	E	27.694	1450.4
183.8	183.80	34.442	D	-0.243	E	27.696	1450.4
185.0	185.00	34.453	D	-0.228	E	27.704	1450.5
186.0	186.00	34.463	D	-0.222	E	27.712	1450.6
187.0	187.00	34.467	D	-0.220	E	27.716	1450.6
187.8	187.85	34.468	D	-0.219	E	27.716	1450.6
188.9	188.90	34.473	D	-0.216	E	27.720	1450.7
190.0	190.05	34.478	D	-0.206	E	27.724	1450.7
191.0	191.00	34.486	D	-0.202	E	27.730	1450.8
191.9	191.95	34.486	D	-0.200	E	27.730	1450.8
193.0	193.05	34.492	D	-0.188	E	27.734	1450.9
194.1	194.15	34.501	D	-0.183	E	27.741	1450.9
195.1	195.15	34.500	D	-0.181	E	27.740	1451.0
195.9	195.90	34.507	D	-0.178	E	27.746	1451.0
197.1	197.15	34.512	D	-0.169	E	27.750	1451.1
198.1	198.10	34.518	D	-0.162	E	27.754	1451.1
199.2	199.20	34.522	D	-0.161	E	27.757	1451.2
200.3	200.30	34.525	D	-0.154	E	27.759	1451.2
205.8	205.85	34.546	D	-0.135	E	27.775	1451.4
206.7	206.75	34.546	D	-0.132	E	27.775	1451.4
207.7	207.70	34.550	D	-0.131	E	27.779	1451.5
208.8	208.80	34.550	D	-0.126	E	27.778	1451.5
209.7	209.75	34.553	D	-0.123	E	27.780	1451.5
210.7	210.70	34.556	D	-0.120	E	27.783	1451.6
211.7	211.75	34.562	D	-0.117	E	27.787	1451.6
212.8	212.80	34.561	D	-0.109	E	27.786	1451.7
219.2	219.20	34.588	D	-0.078	E	27.806	1452.0
225.2	225.25	34.604	D	-0.057	E	27.818	1452.2
226.3	226.30	34.608	D	-0.054	E	27.821	1452.2
227.3	227.30	34.610	D	-0.047	E	27.822	1452.3
228.2	228.25	34.615	D	-0.042	E	27.826	1452.3

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
229.3	229.35	34.619	D	-0.039	E	27.830	1452.3
230.3	230.30	34.622	D	-0.037	E	27.832	1452.4
231.3	231.35	34.625	D	-0.035	E	27.834	1452.4
232.3	232.30	34.628	D	-0.032	E	27.836	1452.4
233.1	233.15	34.629	D	-0.026	E	27.837	1452.5
234.1	234.15	34.634	D	-0.022	E	27.841	1452.5
235.2	235.20	34.635	D	-0.017	E	27.841	1452.6
236.3	236.30	34.637	D	-0.014	E	27.842	1452.6
237.4	237.45	34.639	D	-0.009	E	27.844	1452.6
238.3	238.30	34.641	D	-0.005	E	27.845	1452.7
239.2	239.25	34.643	D	0.0	E	27.847	1452.7
240.2	240.25	34.654	D	0.0	E	27.856	1452.7
241.2	241.25	34.661	D	0.0	E	27.861	1452.8
245.8	245.85	34.665	D	0.020	E	27.864	1452.9
246.9	246.95	34.669	D	0.024	E	27.866	1453.0
247.8	247.85	34.672	D	0.027	E	27.869	1453.0
248.9	248.90	34.674	D	0.031	E	27.870	1453.1
250.0	250.05	34.677	D	0.035	E	27.873	1453.1
251.2	251.25	34.679	D	0.040	E	27.874	1453.1
252.3	252.30	34.681	D	0.044	E	27.875	1453.2
253.1	253.15	34.688	D	0.044	E	27.881	1453.2
254.3	254.35	34.688	D	0.047	E	27.881	1453.2
255.4	255.40	34.689	D	0.051	E	27.881	1453.3
256.3	256.30	34.694	D	0.053	E	27.886	1453.3
257.2	257.20	34.696	D	0.055	E	27.887	1453.3
258.4	258.40	34.698	D	0.059	E	27.888	1453.4
259.3	259.35	34.702	D	0.061	E	27.891	1453.4
260.3	260.35	34.704	D	0.065	E	27.893	1453.4
261.4	261.45	34.707	D	0.071	E	27.894	1453.5
262.2	262.25	34.713	D	0.074	E	27.899	1453.5
263.4	263.40	34.715	D	0.078	E	27.900	1453.6
264.3	264.35	34.720	D	0.084	E	27.905	1453.6
265.4	265.40	34.723	D	0.087	E	27.907	1453.7
266.5	266.50	34.723	D	0.090	E	27.907	1453.7
267.5	267.50	34.724	D	0.093	E	27.907	1453.7
268.3	268.35	34.728	D	0.094	E	27.910	1453.7
269.3	269.30	34.731	D	0.097	E	27.913	1453.8
270.3	270.30	34.734	D	0.101	E	27.915	1453.8
271.4	271.40	34.737	D	0.104	E	27.917	1453.9
276.6	276.60	34.747	D	0.118	E	27.924	1454.0
277.6	277.65	34.748	D	0.120	E	27.925	1454.0
278.7	278.70	34.751	D	0.122	E	27.928	1454.1
279.7	279.70	34.752	D	0.123	E	27.928	1454.1
280.8	280.80	34.754	D	0.126	E	27.930	1454.1
281.8	281.80	34.755	D	0.128	E	27.931	1454.2
282.8	282.80	34.758	D	0.131	E	27.933	1454.2
283.8	283.85	34.759	D	0.135	E	27.933	1454.2
284.9	284.90	34.761	D	0.138	E	27.934	1454.3
285.9	285.90	34.762	D	0.140	E	27.935	1454.3
286.8	286.80	34.766	D	0.141	E	27.939	1454.3
287.7	287.75	34.766	D	0.143	E	27.938	1454.3
288.8	288.80	34.765	D	0.147	E	27.938	1454.4
289.9	289.95	34.768	D	0.148	E	27.939	1454.4
290.8	290.80	34.771	D	0.148	E	27.942	1454.4
291.7	291.75	34.773	D	0.150	E	27.944	1454.4
292.9	292.90	34.771	D	0.155	E	27.942	1454.5
293.9	293.90	34.775	D	0.154	E	27.946	1454.5
294.8	294.80	34.776	D	0.156	E	27.945	1454.5
296.0	296.00	34.777	D	0.158	E	27.946	1454.6
296.8	296.85	34.779	D	0.158	E	27.948	1454.6
298.0	298.00	34.778	D	0.161	E	27.947	1454.6
298.8	298.85	34.780	D	0.160	E	27.949	1454.6
299.8	299.85	34.781	D	0.162	E	27.950	1454.6
300.9	300.95	34.781	D	0.167	E	27.949	1454.7
306.5	306.55	34.791	D	0.176	E	27.957	1454.8
307.3	307.35	34.790	D	0.177	E	27.956	1454.8
313.6	313.65	34.798	D	0.183	E	27.962	1455.0
314.6	314.65	34.799	D	0.184	E	27.963	1455.0
315.7	315.75	34.800	D	0.186	E	27.964	1455.0

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
316.8	316.85	34.801	D	0.190	E	27.964	1455.1
317.8	317.85	34.804	D	0.190	E	27.967	1455.1
318.9	318.90	34.804	D	0.192	E	27.967	1455.1
319.9	319.95	34.805	D	0.193	E	27.968	1455.1
320.9	320.90	34.805	D	0.195	E	27.967	1455.2
321.9	321.95	34.808	D	0.195	E	27.969	1455.2
322.8	322.85	34.808	D	0.198	E	27.969	1455.2
323.9	323.90	34.810	D	0.198	E	27.971	1455.2
325.0	325.05	34.810	D	0.200	E	27.971	1455.3
326.0	326.00	34.812	D	0.200	E	27.973	1455.3
327.1	327.10	34.812	D	0.202	E	27.973	1455.3
328.0	328.05	34.812	D	0.204	E	27.973	1455.3
328.8	328.85	34.816	D	0.204	E	27.976	1455.4
329.9	329.90	34.817	D	0.204	E	27.976	1455.4
330.9	330.90	34.817	D	0.205	E	27.976	1455.4
332.0	332.00	34.819	D	0.205	E	27.978	1455.4
333.0	333.00	34.819	D	0.206	E	27.977	1455.4
334.0	334.00	34.820	D	0.207	E	27.978	1455.5
335.1	335.10	34.822	D	0.208	E	27.980	1455.5
336.0	336.05	34.822	D	0.210	E	27.980	1455.5
337.1	337.10	34.822	D	0.211	E	27.980	1455.5
338.1	338.10	34.821	D	0.212	E	27.979	1455.6
339.1	339.15	34.822	D	0.212	E	27.980	1455.6
340.1	340.15	34.825	D	0.212	E	27.982	1455.6
341.1	341.15	34.824	D	0.213	E	27.982	1455.6
342.0	342.00	34.825	D	0.214	E	27.983	1455.6
343.0	343.00	34.828	D	0.215	E	27.985	1455.7
344.0	344.00	34.829	D	0.216	E	27.985	1455.7
345.1	345.10	34.826	D	0.218	E	27.983	1455.7
346.1	346.15	34.829	D	0.220	E	27.985	1455.7
347.0	347.05	34.831	D	0.220	E	27.987	1455.8
347.9	347.95	34.832	D	0.220	E	27.988	1455.8
349.0	349.00	34.831	D	0.222	E	27.986	1455.8
349.8	349.85	34.832	D	0.222	E	27.987	1455.8
350.7	350.75	34.833	D	0.222	E	27.988	1455.8
351.5	351.50	34.832	D	0.223	E	27.988	1455.8
356.7	356.75	34.834	D	0.224	E	27.989	1455.9
357.6	357.60	34.833	D	0.224	E	27.988	1455.9
358.6	358.60	34.833	D	0.225	E	27.988	1456.0
359.5	359.50	34.835	D	0.224	E	27.990	1456.0
360.2	360.25	34.835	D	0.225	E	27.990	1456.0
361.3	361.30	34.836	D	0.225	E	27.990	1456.0
362.2	362.25	34.834	D	0.227	E	27.989	1456.0
363.3	363.30	34.834	D	0.228	E	27.989	1456.1
364.2	364.25	34.837	D	0.226	E	27.991	1456.1
365.2	365.25	34.838	D	0.226	E	27.992	1456.1
366.0	366.05	34.838	D	0.227	E	27.992	1456.1
367.1	367.15	34.835	D	0.229	E	27.989	1456.1
368.3	368.30	34.837	D	0.230	E	27.991	1456.2
369.3	369.30	34.838	D	0.230	E	27.992	1456.2
370.1	370.15	34.840	D	0.230	E	27.994	1456.2
371.4	371.45	34.840	D	0.231	E	27.993	1456.2
372.6	372.60	34.841	D	0.231	E	27.994	1456.2
373.6	373.60	34.840	D	0.232	E	27.994	1456.3
374.4	374.40	34.841	D	0.232	E	27.994	1456.3
375.4	375.40	34.842	D	0.232	E	27.995	1456.3
376.3	376.30	34.842	D	0.233	E	27.995	1456.3
377.1	377.15	34.842	D	0.233	E	27.994	1456.3
378.3	378.35	34.840	D	0.235	E	27.993	1456.3
379.3	379.35	34.844	D	0.233	E	27.997	1456.4
380.2	380.25	34.843	D	0.235	E	27.996	1456.4
381.2	381.25	34.843	D	0.236	E	27.995	1456.4
382.3	382.30	34.846	D	0.235	E	27.998	1456.4
383.4	383.45	34.843	D	0.237	E	27.996	1456.4
384.8	384.85	34.845	D	0.236	E	27.997	1456.5
386.0	386.00	34.845	D	0.237	E	27.997	1456.5
387.1	387.15	34.848	D	0.237	E	28.000	1456.5
388.2	388.20	34.848	D	0.237	E	27.999	1456.5
389.4	389.45	34.846	D	0.239	E	27.998	1456.6

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
390.4	390.45	34.848	D	0.238	E	27.999	1456.6
391.3	391.35	34.849	D	0.238	E	28.000	1456.6
392.2	392.20	34.849	D	0.239	E	28.000	1456.6
393.3	393.35	34.848	D	0.240	E	27.999	1456.6
394.0	394.05	34.850	D	0.239	E	28.001	1456.6
395.0	395.00	34.850	D	0.240	E	28.001	1456.7
396.1	396.10	34.850	D	0.241	E	28.001	1456.7
397.0	397.05	34.852	D	0.240	E	28.002	1456.7
398.2	398.25	34.851	D	0.241	E	28.002	1456.7
399.2	399.20	34.850	D	0.242	E	28.000	1456.7
400.2	400.20	34.850	D	0.242	E	28.001	1456.8
401.2	401.25	34.853	D	0.242	E	28.003	1456.8
402.1	402.15	34.851	D	0.243	E	28.002	1456.8
403.2	403.20	34.852	D	0.243	E	28.002	1456.8
404.1	404.15	34.853	D	0.243	E	28.003	1456.8
405.1	405.15	34.852	D	0.243	E	28.002	1456.8
406.1	406.15	34.854	D	0.243	E	28.004	1456.9
407.3	407.30	34.854	D	0.243	E	28.004	1456.9
408.4	408.45	34.854	D	0.243	E	28.004	1456.9
409.4	409.45	34.853	D	0.245	E	28.003	1456.9
410.4	410.40	34.854	D	0.244	E	28.004	1456.9
411.3	411.30	34.854	D	0.244	E	28.004	1456.9
412.1	412.10	34.857	D	0.243	E	28.006	1457.0
412.9	412.90	34.854	D	0.245	E	28.004	1457.0
413.8	413.80	34.854	D	0.244	E	28.004	1457.0
414.7	414.70	34.855	D	0.244	E	28.005	1457.0
415.8	415.80	34.855	D	0.244	E	28.004	1457.0
416.7	416.75	34.854	D	0.244	E	28.004	1457.0
417.8	417.85	34.854	D	0.245	E	28.004	1457.1
418.9	418.90	34.853	D	0.246	E	28.003	1457.1
419.8	419.85	34.855	D	0.245	E	28.005	1457.1
420.8	420.85	34.854	D	0.246	E	28.004	1457.1
421.7	421.75	34.855	D	0.246	E	28.004	1457.1
422.9	422.90	34.855	D	0.246	E	28.005	1457.1
423.9	423.90	34.854	D	0.248	E	28.004	1457.2
424.8	424.85	34.858	D	0.245	E	28.007	1457.2
425.8	425.85	34.858	D	0.246	E	28.007	1457.2
426.8	426.85	34.859	D	0.246	E	28.008	1457.2
427.9	427.95	34.858	D	0.247	E	28.007	1457.2
429.0	429.00	34.857	D	0.248	E	28.006	1457.3
430.0	430.05	34.857	D	0.248	E	28.006	1457.3
431.1	431.10	34.861	D	0.247	E	28.009	1457.3
432.1	432.10	34.860	D	0.248	E	28.009	1457.3
433.2	433.20	34.859	D	0.249	E	28.007	1457.3
434.2	434.20	34.861	D	0.248	E	28.009	1457.4
435.2	435.20	34.860	D	0.249	E	28.009	1457.4
436.3	436.35	34.861	D	0.249	E	28.009	1457.4
437.3	437.30	34.862	D	0.248	E	28.010	1457.4
438.3	438.30	34.862	D	0.248	E	28.011	1457.4
439.3	439.30	34.862	D	0.249	E	28.010	1457.4
440.4	440.40	34.860	D	0.250	E	28.009	1457.5
441.5	441.50	34.862	D	0.249	E	28.010	1457.5
442.3	442.35	34.861	D	0.251	E	28.009	1457.5
443.3	443.35	34.864	D	0.249	E	28.012	1457.5
444.5	444.50	34.864	D	0.250	E	28.011	1457.5
445.6	445.60	34.862	D	0.251	E	28.010	1457.6
446.5	446.55	34.863	D	0.251	E	28.011	1457.6
447.8	447.80	34.864	D	0.251	E	28.011	1457.6
448.6	448.60	34.863	D	0.251	E	28.011	1457.6
453.7	453.70	34.864	D	0.251	E	28.012	1457.7
454.6	454.60	34.865	D	0.251	E	28.013	1457.7
455.6	455.60	34.866	D	0.251	E	28.013	1457.7
456.6	456.65	34.866	D	0.252	E	28.013	1457.7
457.7	457.75	34.867	D	0.250	E	28.014	1457.8
458.6	458.60	34.867	D	0.251	E	28.014	1457.8
459.8	459.80	34.865	D	0.252	E	28.013	1457.8
460.6	460.65	34.866	D	0.251	E	28.013	1457.8
461.8	461.85	34.865	D	0.252	E	28.013	1457.8
462.8	462.80	34.866	D	0.252	E	28.013	1457.8

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
463.8	463.85	34.868	D	0.251	E	28.015	1457.9
464.7	464.75	34.867	D	0.252	E	28.014	1457.9
465.9	465.95	34.866	D	0.253	E	28.013	1457.9
466.8	466.80	34.868	D	0.251	E	28.015	1457.9
467.8	467.80	34.869	D	0.251	E	28.015	1457.9
468.9	468.95	34.867	D	0.253	E	28.014	1458.0
469.9	469.90	34.868	D	0.252	E	28.015	1458.0
470.9	470.95	34.868	D	0.251	E	28.015	1458.0
471.8	471.85	34.867	D	0.253	E	28.014	1458.0
473.1	473.10	34.869	D	0.252	E	28.015	1458.0
473.9	473.95	34.868	D	0.252	E	28.015	1458.0
475.0	475.05	34.868	D	0.253	E	28.015	1458.1
476.0	476.00	34.869	D	0.253	E	28.015	1458.1
476.9	476.95	34.869	D	0.252	E	28.016	1458.1
478.0	478.00	34.867	D	0.254	E	28.014	1458.1
479.0	479.05	34.868	D	0.253	E	28.015	1458.1
480.0	480.00	34.868	D	0.254	E	28.015	1458.1
481.1	481.10	34.868	D	0.254	E	28.014	1458.2
482.0	482.05	34.867	D	0.254	E	28.014	1458.2
482.9	482.95	34.869	D	0.253	E	28.016	1458.2
484.0	484.05	34.867	D	0.254	E	28.014	1458.2


EXPERIMENT 1052
TEMPERATURE, C
-2.00
-1.25
-0.50
0.25
1.00
1.75
2.50
SALINITY 0/00
12.00
16.00
20.00
24.00
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36.00
SIGMAT
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DEPTH M
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CRUISE 15-74-012 D'IBERVILLE FIORD-74 EXPER NO. 1052

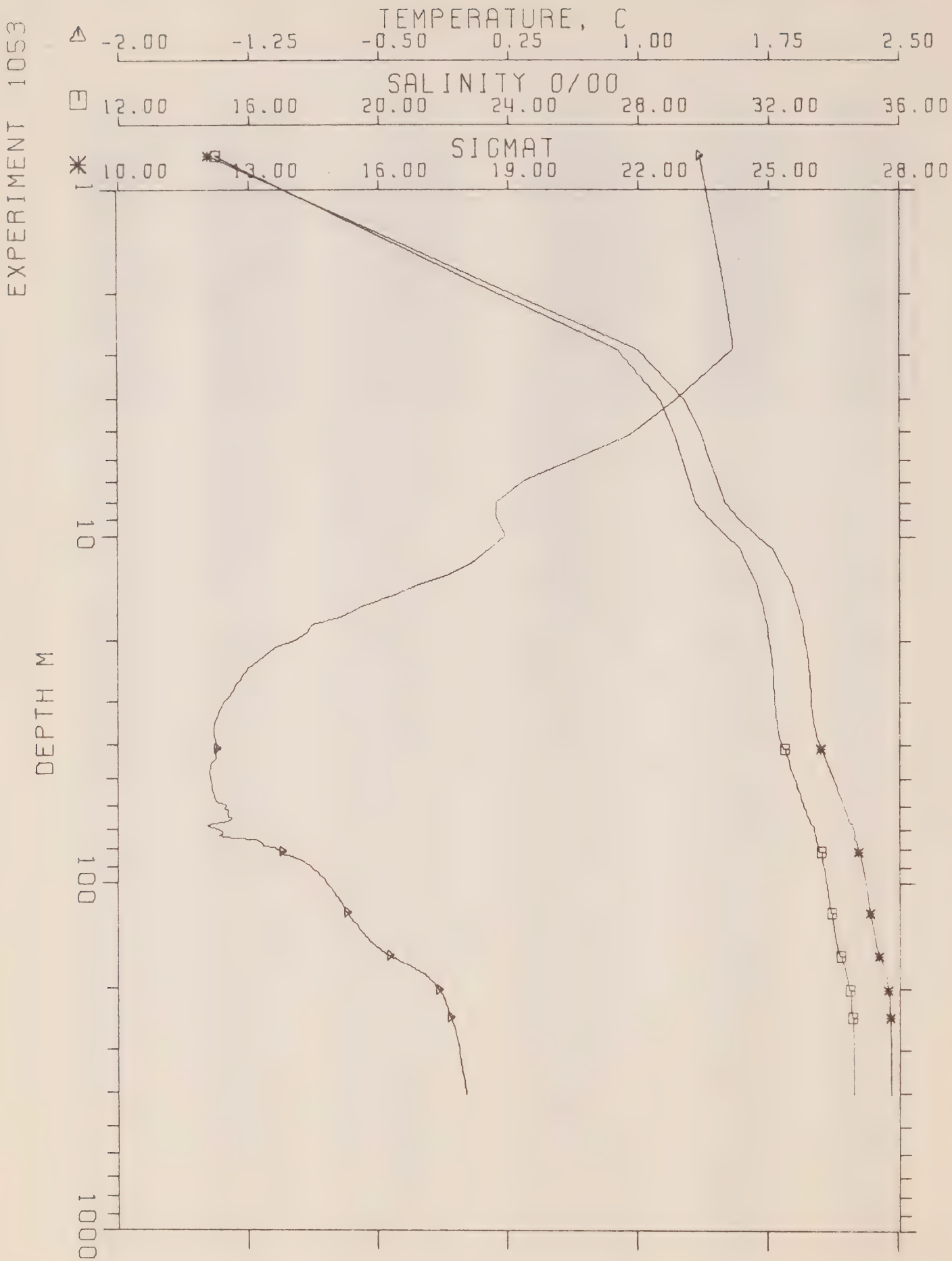
LAT N.80-34-45 LONG W.80-04-45 WATER DEPTH 250

DEPTH INCR. DATE 230874 LOCAL TIME 1652

DEPTH	PRES	SAL		TEMP		SIGMAT	SOUND
3.2	3.20	15.340	C	1.912	D	12.329	1431.5
4.4	4.40	23.411	C	1.770	D	18.760	1441.6
5.4	5.40	28.330	C	1.305	D	22.711	1446.1
6.2	6.20	29.101	C	1.123	D	23.338	1446.4
7.3	7.30	29.402	C	0.837	D	23.593	1445.5
8.3	8.35	29.621	C	0.541	D	23.782	1444.5
9.2	9.25	29.754	C	0.383	D	23.895	1443.9
10.3	10.35	29.888	C	0.192	D	24.011	1443.3
11.2	11.20	30.195	C	0.122	D	24.260	1443.4
12.3	12.30	30.863	C	0.185	D	24.795	1444.6
13.3	13.30	31.180	C	0.209	D	25.049	1445.2
14.2	14.20	31.340	C	0.158	D	25.179	1445.2
15.3	15.30	31.442	C	0.111	D	25.263	1445.1
16.2	16.20	31.543	C	0.028	D	25.349	1444.9
17.3	17.35	31.683	C	-0.089	D	25.466	1444.6
18.2	18.20	31.796	C	-0.263	D	25.563	1443.9
19.3	19.35	31.877	C	-0.474	D	25.637	1443.1
20.2	20.20	31.927	C	-0.583	D	25.681	1442.6
21.2	21.20	31.978	C	-0.739	D	25.728	1442.0
22.3	22.30	32.033	C	-0.883	D	25.776	1441.4
23.3	23.35	32.061	C	-0.965	D	25.802	1441.1
24.3	24.35	32.098	C	-1.056	D	25.834	1440.7
25.3	25.30	32.119	C	-1.139	D	25.853	1440.4
26.3	26.35	32.137	C	-1.194	D	25.869	1440.2
27.3	27.35	32.148	C	-1.217	D	25.879	1440.1
28.3	28.30	32.163	C	-1.266	D	25.892	1439.9
29.2	29.25	32.186	C	-1.312	D	25.912	1439.7
30.3	30.30	32.198	C	-1.334	D	25.922	1439.7
31.3	31.35	32.212	C	-1.362	D	25.934	1439.6
32.3	32.35	32.237	C	-1.386	D	25.955	1439.5
33.4	33.40	32.248	C	-1.404	D	25.964	1439.5
34.3	34.35	32.256	C	-1.420	D	25.971	1439.4
35.2	35.25	32.269	C	-1.428	D	25.981	1439.4
36.3	36.30	32.277	C	-1.443	D	25.988	1439.4
37.2	37.20	32.287	C	-1.443	D	25.996	1439.4
38.3	38.35	32.301	C	-1.464	D	26.009	1439.3
39.4	39.40	32.326	C	-1.481	D	26.029	1439.3
40.4	40.40	32.337	C	-1.474	D	26.038	1439.4
41.3	41.35	32.355	C	-1.468	D	26.052	1439.4
42.3	42.35	32.370	C	-1.466	D	26.065	1439.5
43.3	43.35	32.390	C	-1.444	D	26.080	1439.6
44.3	44.30	32.425	C	-1.444	D	26.108	1439.7
45.4	45.45	32.465	C	-1.434	D	26.141	1439.8
46.2	46.25	32.508	C	-1.428	D	26.175	1439.9
47.3	47.30	32.552	C	-1.424	D	26.211	1440.0
48.2	48.25	32.591	C	-1.409	D	26.242	1440.2
49.3	49.35	32.631	C	-1.406	D	26.275	1440.3
50.3	50.35	32.659	C	-1.410	D	26.297	1440.3
51.4	51.40	32.696	C	-1.414	D	26.327	1440.3
52.1	52.15	32.800	C	-1.420	D	26.411	1440.5
53.3	53.30	32.855	C	-1.409	D	26.456	1440.6
54.4	54.40	32.909	C	-1.393	D	26.499	1440.8
55.4	55.40	32.978	C	-1.413	D	26.555	1440.8
56.3	56.35	33.018	C	-1.413	D	26.588	1440.9
57.2	57.20	33.065	C	-1.401	D	26.626	1441.0
58.3	58.35	33.112	C	-1.344	D	26.662	1441.4
59.4	59.45	33.167	C	-1.334	D	26.706	1441.5
60.4	60.40	33.200	C	-1.329	D	26.733	1441.6
61.3	61.35	33.236	C	-1.312	D	26.761	1441.7
62.4	62.45	33.254	C	-1.307	D	26.777	1441.8
63.4	63.45	33.277	C	-1.309	D	26.795	1441.8
64.3	64.30	33.305	C	-1.295	D	26.817	1442.0

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
65.3	65.35	33.348 C	-1.289 D	26.851	1442.1
66.4	66.40	33.409 C	-1.306 D	26.901	1442.1
67.5	67.50	33.424 C	-1.221 D	26.911	1442.5
68.4	68.40	33.447 C	-1.193 D	26.929	1442.7
69.4	69.40	33.469 C	-1.247 D	26.949	1442.5
70.4	70.40	33.480 C	-1.252 D	26.958	1442.5
71.4	71.40	33.494 C	-1.236 D	26.969	1442.6
72.4	72.45	33.504 C	-1.220 D	26.976	1442.7
73.3	73.35	33.547 C	-1.108 D	27.008	1443.3
74.4	74.40	33.568 C	-1.063 D	27.023	1443.6
75.3	75.35	33.582 C	-1.052 D	27.034	1443.7
76.3	76.35	33.590 C	-1.044 D	27.040	1443.7
77.5	77.50	33.607 C	-1.032 D	27.053	1443.8
78.5	78.50	33.618 C	-1.026 D	27.062	1443.9
79.5	79.55	33.629 C	-1.010 D	27.071	1444.0
80.4	80.45	33.639 C	-0.992 D	27.078	1444.1
81.4	81.40	33.657 C	-0.972 D	27.092	1444.3
82.4	82.45	33.671 C	-0.963 D	27.103	1444.3
83.4	83.40	33.683 C	-0.950 D	27.112	1444.4
84.5	84.50	33.703 C	-0.937 D	27.127	1444.5
85.5	85.50	33.711 C	-0.929 D	27.134	1444.6
86.3	86.35	33.726 C	-0.918 D	27.145	1444.7
87.3	87.35	33.735 C	-0.905 D	27.153	1444.8
88.3	88.35	33.745 C	-0.893 D	27.160	1444.9
89.4	89.45	33.753 C	-0.880 D	27.166	1445.0
90.5	90.50	33.772 C	-0.860 D	27.181	1445.1
91.4	91.45	33.787 C	-0.852 D	27.193	1445.2
92.4	92.45	33.794 C	-0.844 D	27.198	1445.2
93.5	93.55	33.799 C	-0.838 D	27.202	1445.3
94.5	94.55	33.807 C	-0.835 D	27.208	1445.3
95.5	95.50	33.814 C	-0.829 D	27.214	1445.4
96.6	96.65	33.821 C	-0.825 D	27.219	1445.4
97.4	97.45	33.828 C	-0.815 D	27.225	1445.5
98.4	98.45	33.837 C	-0.813 D	27.232	1445.5
99.4	99.45	33.843 C	-0.808 D	27.236	1445.6
100.5	100.55	33.845 D	-0.802 E	27.238	1445.6
101.5	101.50	33.853 D	-0.800 E	27.244	1445.7
102.6	102.60	33.857 D	-0.794 E	27.247	1445.7
103.6	103.65	33.867 D	-0.788 E	27.255	1445.8
104.6	104.65	33.873 D	-0.785 E	27.260	1445.8
105.4	105.45	33.880 D	-0.781 E	27.265	1445.9
106.4	106.45	33.895 D	-0.765 E	27.277	1446.0
107.5	107.50	33.905 D	-0.754 E	27.285	1446.0
108.6	108.65	33.915 D	-0.746 E	27.292	1446.1
109.6	109.65	33.919 D	-0.739 E	27.295	1446.2
110.6	110.65	33.929 D	-0.739 E	27.303	1446.2
111.4	111.45	33.937 D	-0.731 E	27.309	1446.3
112.6	112.60	33.941 D	-0.726 E	27.312	1446.3
113.7	113.70	33.945 D	-0.720 E	27.315	1446.4
114.6	114.65	33.952 D	-0.719 E	27.321	1446.4
115.4	115.45	33.955 D	-0.713 E	27.323	1446.4
116.6	116.60	33.962 D	-0.706 E	27.329	1446.5
117.5	117.55	33.971 D	-0.703 E	27.336	1446.5
118.6	118.65	33.973 D	-0.697 E	27.337	1446.6
119.7	119.75	33.979 D	-0.695 E	27.342	1446.6
120.6	120.60	33.980 D	-0.689 E	27.343	1446.7
121.6	121.60	33.992 D	-0.686 E	27.352	1446.7
122.8	122.80	34.000 D	-0.677 E	27.358	1446.8
123.5	123.50	34.007 D	-0.668 E	27.364	1446.9
124.6	124.65	34.016 D	-0.666 E	27.370	1446.9
125.8	125.80	34.019 D	-0.663 E	27.373	1446.9
126.7	126.75	34.020 D	-0.661 E	27.374	1447.0
127.5	127.55	34.023 D	-0.659 E	27.377	1447.0
128.7	128.70	34.023 D	-0.653 E	27.376	1447.0
129.6	129.65	34.030 D	-0.650 E	27.381	1447.1
130.6	130.60	34.034 D	-0.647 E	27.385	1447.1
131.6	131.60	34.040 D	-0.642 E	27.389	1447.2
132.7	132.75	34.044 D	-0.639 E	27.393	1447.2
133.7	133.75	34.049 D	-0.637 E	27.396	1447.2

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
134.6	134.60	34.050 D	-0.636 E	27.397	1447.2
135.7	135.70	34.054 D	-0.634 E	27.400	1447.3
136.8	136.80	34.058 D	-0.631 E	27.403	1447.3
137.7	137.70	34.059 D	-0.625 E	27.404	1447.4
138.7	138.75	34.061 D	-0.621 E	27.405	1447.4
139.8	139.80	34.069 D	-0.618 E	27.411	1447.4
140.8	140.80	34.076 D	-0.608 E	27.417	1447.5
141.8	141.80	34.079 D	-0.605 E	27.419	1447.5
142.6	142.65	34.085 D	-0.602 E	27.424	1447.6
143.8	143.85	34.093 D	-0.594 E	27.430	1447.7
144.7	144.70	34.105 D	-0.587 E	27.439	1447.7
145.8	145.85	34.109 D	-0.580 E	27.443	1447.8
146.8	146.85	34.116 D	-0.575 E	27.448	1447.8
147.7	147.70	34.123 D	-0.570 E	27.453	1447.9
148.8	148.80	34.130 D	-0.561 E	27.458	1447.9
149.7	149.75	34.138 D	-0.557 E	27.465	1448.0
150.9	150.90	34.143 D	-0.552 E	27.469	1448.0


EXPERIMENT 1053
TEMPERATURE, C
-2.00
-1.25
-0.50
0.25
1.00
1.75
2.50
SALINITY 0/00
12.00
16.00
20.00
24.00
28.00
32.00
36.00
SIGMAT
10.00
13.00
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19.00
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DEPTH M
10
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CRUISE 15-74-013 D'IBERVILLE FIORD-74 EXPER NO. 1053

LAT N.80-36-00 LONG W.79-36-45 WATER DEPTH 435

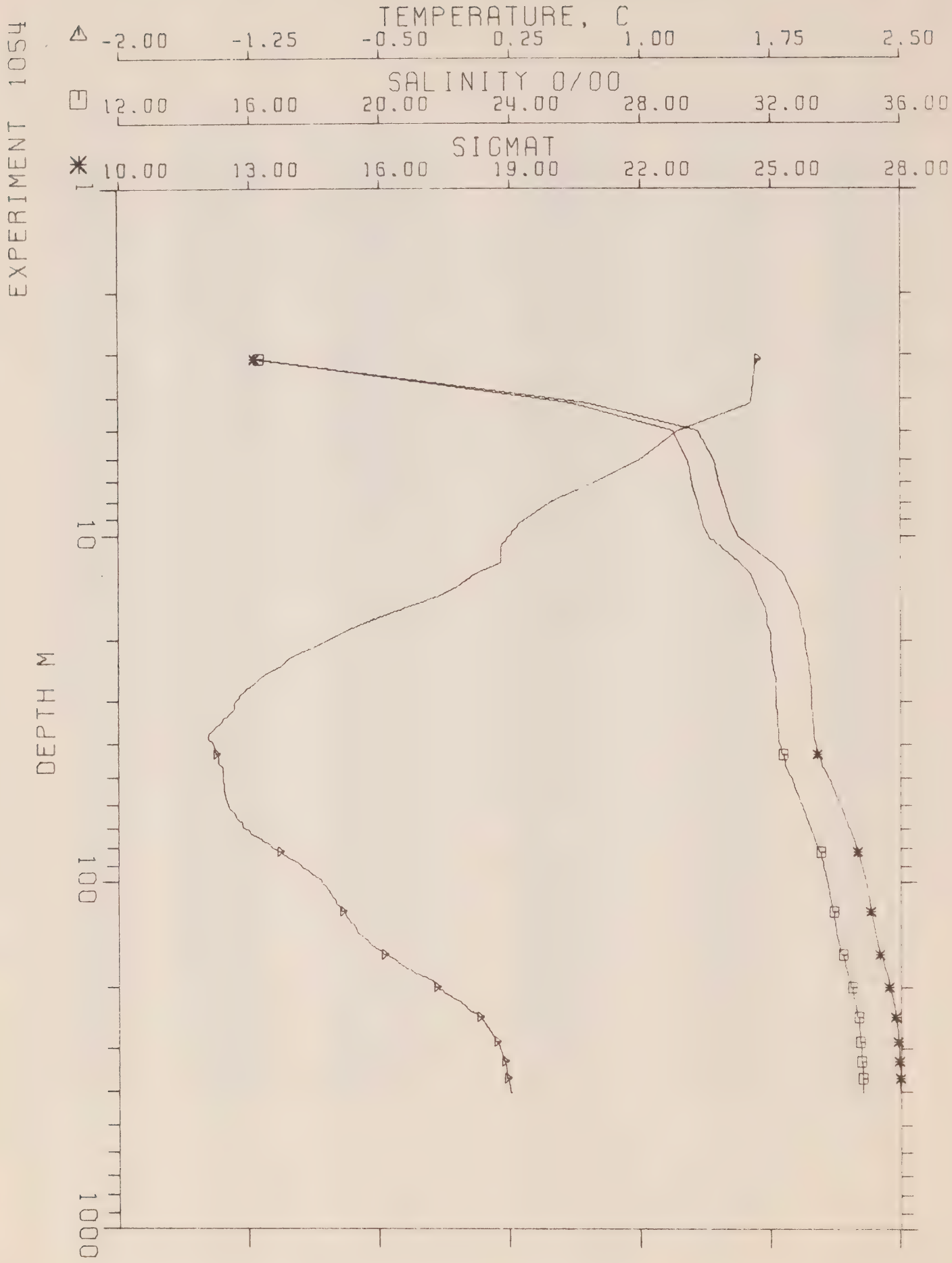
DEPTH INCR. DATE 230874 LOCAL TIME

DEPTH	PRES	SAL		TEMP		SIGMAT	SOUND
0.8	0.80	15.019	C	1.354	D	12.081	1428.5
1.9	1.90	23.241	C	1.496	D	18.635	1440.1
2.9	2.90	27.430	C	1.552	D	21.980	1446.0
4.0	4.05	28.750	C	1.226	D	23.052	1446.3
5.1	5.10	29.209	C	0.962	D	23.432	1445.8
6.0	6.00	29.434	C	0.641	D	23.627	1444.6
6.9	6.90	29.643	C	0.357	D	23.807	1443.6
8.0	8.00	29.842	C	0.191	D	23.973	1443.1
8.8	8.85	30.237	C	0.182	D	24.292	1443.7
10.0	10.05	30.797	C	0.239	D	24.740	1444.7
10.8	10.85	31.191	C	0.157	D	25.060	1444.9
12.0	12.00	31.401	C	0.048	D	25.234	1444.7
13.0	13.00	31.593	C	-0.096	D	25.393	1444.3
13.8	13.85	31.713	C	-0.254	D	25.497	1443.8
14.8	14.85	31.812	C	-0.396	D	25.582	1443.3
16.0	16.05	31.908	C	-0.592	D	25.666	1442.5
17.1	17.10	31.971	C	-0.712	D	25.721	1442.1
18.0	18.00	32.045	C	-0.876	D	25.786	1441.4
19.0	19.00	32.050	C	-0.905	D	25.790	1441.3
20.0	20.00	32.082	C	-0.973	D	25.818	1441.0
20.9	20.90	32.121	C	-1.084	D	25.853	1440.6
22.0	22.05	32.149	C	-1.145	D	25.877	1440.4
22.9	22.95	32.165	C	-1.191	D	25.892	1440.2
23.9	23.90	32.192	C	-1.241	D	25.915	1440.0
25.0	25.05	32.203	C	-1.271	D	25.924	1439.9
26.1	26.15	32.212	C	-1.294	D	25.932	1439.8
26.9	26.95	32.220	C	-1.319	D	25.939	1439.7
27.9	27.95	32.230	C	-1.333	D	25.947	1439.7
29.1	29.10	32.240	C	-1.353	D	25.957	1439.6
29.9	29.90	32.256	C	-1.382	D	25.970	1439.5
31.0	31.00	32.260	C	-1.400	D	25.974	1439.5
31.9	31.95	32.274	C	-1.415	D	25.986	1439.4
33.0	33.00	32.280	C	-1.424	D	25.991	1439.4
34.0	34.00	32.301	C	-1.436	D	26.008	1439.4
35.0	35.05	32.325	C	-1.447	D	26.027	1439.4
36.0	36.05	32.354	C	-1.454	D	26.051	1439.4
36.9	36.95	32.373	C	-1.456	D	26.066	1439.4
38.0	38.00	32.402	C	-1.451	D	26.090	1439.5
38.9	38.95	32.446	C	-1.444	D	26.125	1439.6
40.0	40.00	32.489	C	-1.434	D	26.160	1439.8
41.0	41.05	32.533	C	-1.441	D	26.196	1439.8
42.1	42.15	32.572	C	-1.441	D	26.227	1439.9
43.1	43.15	32.624	C	-1.442	D	26.269	1440.0
44.0	44.05	32.662	C	-1.441	D	26.300	1440.0
45.0	45.00	32.691	C	-1.461	D	26.324	1440.0
46.2	46.20	32.719	C	-1.473	D	26.348	1440.0
47.0	47.00	32.760	C	-1.469	D	26.381	1440.1
48.1	48.15	32.797	C	-1.484	D	26.410	1440.1
49.1	49.15	32.831	C	-1.482	D	26.438	1440.2
50.0	50.05	32.871	C	-1.472	D	26.470	1440.3
51.1	51.10	32.905	C	-1.474	D	26.498	1440.3
52.2	52.25	32.936	C	-1.470	D	26.523	1440.4
53.3	53.30	32.968	C	-1.465	D	26.549	1440.5
54.1	54.10	32.997	C	-1.468	D	26.573	1440.6
55.2	55.20	33.021	C	-1.458	D	26.592	1440.7
56.2	56.25	33.050	C	-1.455	D	26.615	1440.7
57.2	57.25	33.081	C	-1.452	D	26.640	1440.8
58.2	58.25	33.116	C	-1.442	D	26.668	1440.9
59.2	59.25	33.138	C	-1.392	D	26.685	1441.2
60.3	60.35	33.163	C	-1.379	D	26.704	1441.3
61.1	61.10	33.185	C	-1.391	D	26.722	1441.3
62.2	62.20	33.215	C	-1.364	D	26.746	1441.5

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
63.2	63.25	33.244	C	-1.370	D	26.770	1441.5
64.1	64.15	33.282	C	-1.369	D	26.801	1441.6
65.2	65.20	33.314	C	-1.340	D	26.826	1441.8
66.3	66.35	33.330	C	-1.359	D	26.840	1441.7
67.2	67.20	33.380	C	-1.397	D	26.880	1441.6
68.3	68.35	33.437	C	-1.496	D	26.930	1441.3
69.2	69.25	33.415	C	-1.470	D	26.911	1441.4
70.2	70.20	33.452	C	-1.432	D	26.940	1441.6
71.1	71.10	33.468	C	-1.411	D	26.952	1441.8
72.2	72.25	33.495	C	-1.401	D	26.974	1441.9
73.2	73.20	33.526	C	-1.427	D	27.000	1441.8
74.3	74.35	33.478	C	-1.341	D	26.959	1442.2
75.3	75.30	33.499	C	-1.209	D	26.971	1442.8
76.2	76.25	33.540	C	-1.189	D	27.004	1443.0
77.3	77.35	33.572	C	-1.168	D	27.030	1443.2
78.2	78.25	33.579	C	-1.176	D	27.035	1443.1
79.3	79.30	33.585	C	-1.111	D	27.038	1443.5
80.3	80.30	33.614	C	-1.093	D	27.061	1443.6
81.4	81.40	33.625	C	-1.062	D	27.069	1443.8
82.1	82.15	33.646	C	-1.067	D	27.086	1443.8
83.3	83.30	33.647	C	-1.037	D	27.086	1444.0
84.2	84.20	33.666	C	-1.000	D	27.100	1444.2
85.3	85.35	33.679	C	-0.975	D	27.110	1444.3
86.3	86.30	33.691	C	-0.951	D	27.118	1444.5
87.4	87.45	33.707	C	-0.931	D	27.131	1444.6
88.2	88.20	33.724	C	-0.915	D	27.144	1444.7
89.4	89.45	33.732	C	-0.907	D	27.150	1444.8
90.2	90.25	33.742	C	-0.894	D	27.158	1444.9
91.3	91.30	33.752	C	-0.883	D	27.166	1445.0
92.4	92.45	33.760	C	-0.870	D	27.172	1445.1
93.2	93.25	33.771	C	-0.862	D	27.180	1445.1
94.5	94.50	33.779	C	-0.850	D	27.186	1445.2
95.3	95.35	33.790	C	-0.841	D	27.195	1445.3
96.4	96.45	33.796	C	-0.830	D	27.199	1445.4
97.3	97.30	33.806	C	-0.824	D	27.207	1445.4
98.5	98.50	33.815	C	-0.817	D	27.214	1445.5
99.4	99.40	33.820	C	-0.809	D	27.218	1445.5
100.4	100.40	33.832	D	-0.804	E	27.227	1445.6
101.5	101.50	33.838	D	-0.795	E	27.232	1445.7
102.3	102.35	33.845	D	-0.790	E	27.238	1445.7
103.4	103.40	33.852	D	-0.785	E	27.243	1445.8
104.3	104.30	33.861	D	-0.779	E	27.250	1445.8
105.5	105.55	33.867	D	-0.773	E	27.254	1445.9
106.3	106.35	33.874	D	-0.767	E	27.260	1445.9
107.5	107.50	33.885	D	-0.758	E	27.268	1446.0
108.4	108.40	33.892	D	-0.752	E	27.274	1446.1
109.4	109.40	33.899	D	-0.748	E	27.279	1446.1
110.5	110.55	33.901	D	-0.741	E	27.280	1446.2
111.4	111.45	33.907	D	-0.736	E	27.286	1446.2
112.4	112.45	33.917	D	-0.733	E	27.293	1446.2
113.4	113.40	33.920	D	-0.724	E	27.296	1446.3
114.5	114.50	33.930	D	-0.721	E	27.303	1446.4
115.5	115.50	33.934	D	-0.716	E	27.306	1446.4
116.5	116.55	33.937	D	-0.711	E	27.309	1446.4
117.4	117.40	33.948	D	-0.708	E	27.318	1446.5
118.6	118.65	33.951	D	-0.702	E	27.319	1446.5
119.6	119.60	33.957	D	-0.699	E	27.324	1446.6
120.5	120.55	33.964	D	-0.695	E	27.330	1446.6
121.6	121.65	33.968	D	-0.689	E	27.333	1446.7
122.4	122.45	33.977	D	-0.683	E	27.340	1446.7
123.7	123.70	33.979	D	-0.679	E	27.341	1446.8
124.5	124.50	33.986	D	-0.674	E	27.346	1446.8
125.6	125.60	33.991	D	-0.670	E	27.350	1446.9
126.6	126.65	33.995	D	-0.665	E	27.353	1446.9
127.5	127.55	33.998	D	-0.657	E	27.356	1447.0
128.7	128.70	34.011	D	-0.656	E	27.366	1447.0
129.6	129.60	34.015	D	-0.651	E	27.369	1447.0
130.8	130.80	34.017	D	-0.643	E	27.370	1447.1
131.7	131.70	34.026	D	-0.638	E	27.378	1447.2

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
132.8	132.80	34.032 D	-0.631 E	27.383	1447.2
133.7	133.75	34.038 D	-0.625 E	27.387	1447.3
134.8	134.80	34.046 D	-0.622 E	27.393	1447.3
135.8	135.85	34.051 D	-0.617 E	27.397	1447.4
136.8	136.85	34.058 D	-0.612 E	27.402	1447.4
137.8	137.80	34.065 D	-0.607 E	27.408	1447.5
138.7	138.70	34.071 D	-0.603 E	27.413	1447.5
139.8	139.85	34.075 D	-0.598 E	27.416	1447.5
140.8	140.85	34.083 D	-0.590 E	27.422	1447.6
141.9	141.90	34.094 D	-0.586 E	27.430	1447.7
142.7	142.75	34.100 D	-0.580 E	27.435	1447.7
143.8	143.85	34.103 D	-0.575 E	27.438	1447.8
144.9	144.95	34.111 D	-0.568 E	27.443	1447.8
145.9	145.90	34.118 D	-0.563 E	27.449	1447.9
146.9	146.90	34.124 D	-0.560 E	27.454	1447.9
147.9	147.90	34.128 D	-0.554 E	27.457	1448.0
148.8	148.85	34.136 D	-0.546 E	27.463	1448.0
150.0	150.05	34.143 D	-0.538 E	27.469	1448.1
150.9	150.95	34.152 D	-0.528 E	27.475	1448.2
151.9	151.95	34.164 D	-0.520 E	27.484	1448.2
152.9	152.90	34.173 D	-0.513 E	27.491	1448.3
154.0	154.00	34.179 D	-0.504 E	27.496	1448.4
154.8	154.85	34.190 D	-0.500 E	27.505	1448.4
155.9	155.95	34.195 D	-0.492 E	27.508	1448.5
157.1	157.10	34.207 D	-0.485 E	27.517	1448.5
158.0	158.05	34.214 D	-0.480 E	27.523	1448.6
159.1	159.10	34.222 D	-0.470 E	27.529	1448.7
160.1	160.10	34.231 D	-0.458 E	27.536	1448.7
161.0	161.05	34.243 D	-0.453 E	27.546	1448.8
162.0	162.00	34.252 D	-0.443 E	27.552	1448.9
163.1	163.10	34.260 D	-0.433 E	27.558	1448.9
164.0	164.00	34.271 D	-0.425 E	27.566	1449.0
164.9	164.95	34.282 D	-0.411 E	27.575	1449.1
165.9	165.95	34.294 D	-0.398 E	27.584	1449.2
167.1	167.10	34.307 D	-0.386 E	27.594	1449.3
168.2	168.20	34.318 D	-0.373 E	27.602	1449.4
169.2	169.25	34.330 D	-0.362 E	27.612	1449.5
170.3	170.30	34.342 D	-0.352 E	27.620	1449.5
171.2	171.25	34.353 D	-0.341 E	27.629	1449.6
172.2	172.20	34.362 D	-0.330 E	27.636	1449.7
173.2	173.20	34.373 D	-0.319 E	27.644	1449.8
174.1	174.15	34.384 D	-0.310 E	27.653	1449.9
175.2	175.20	34.391 D	-0.299 E	27.658	1449.9
176.1	176.10	34.402 D	-0.294 E	27.667	1450.0
177.2	177.20	34.410 D	-0.283 E	27.673	1450.1
178.3	178.35	34.415 D	-0.275 E	27.676	1450.1
179.2	179.25	34.427 D	-0.267 E	27.686	1450.2
180.2	180.25	34.430 D	-0.259 E	27.688	1450.3
181.1	181.10	34.440 D	-0.255 E	27.695	1450.3
182.2	182.25	34.442 D	-0.246 E	27.696	1450.4
183.2	183.20	34.449 D	-0.240 E	27.702	1450.4
184.3	184.30	34.456 D	-0.233 E	27.707	1450.5
185.3	185.35	34.461 D	-0.228 E	27.711	1450.5
186.3	186.35	34.467 D	-0.222 E	27.715	1450.6
187.3	187.35	34.472 D	-0.217 E	27.719	1450.6
188.3	188.35	34.478 D	-0.213 E	27.724	1450.7
189.3	189.30	34.484 D	-0.208 E	27.728	1450.7
190.4	190.45	34.484 D	-0.203 E	27.729	1450.8
191.3	191.35	34.491 D	-0.197 E	27.734	1450.8
192.3	192.30	34.494 D	-0.191 E	27.736	1450.9
193.5	193.50	34.492 D	-0.187 E	27.734	1450.9
194.4	194.40	34.495 D	-0.185 E	27.736	1450.9
195.4	195.40	34.505 D	-0.181 E	27.745	1451.0
196.4	196.40	34.507 D	-0.177 E	27.746	1451.0
197.4	197.40	34.512 D	-0.174 E	27.750	1451.1
198.4	198.40	34.514 D	-0.170 E	27.751	1451.1
199.4	199.40	34.520 D	-0.166 E	27.756	1451.1
200.5	200.50	34.524 D	-0.163 E	27.758	1451.2
201.4	201.45	34.525 D	-0.158 E	27.759	1451.2

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
202.5	202.55	34.527	D	-0.156	E	27.761	1451.2
203.4	203.40	34.532	D	-0.154	E	27.765	1451.3
204.3	204.35	34.536	D	-0.149	E	27.767	1451.3
205.5	205.50	34.536	D	-0.145	E	27.768	1451.4
206.5	206.55	34.541	D	-0.145	E	27.772	1451.4
207.5	207.50	34.543	D	-0.142	E	27.773	1451.4
208.4	208.40	34.546	D	-0.139	E	27.775	1451.4
209.6	209.60	34.547	D	-0.135	E	27.776	1451.5
210.6	210.65	34.549	D	-0.133	E	27.778	1451.5
211.6	211.60	34.552	D	-0.131	E	27.780	1451.5
212.5	212.55	34.551	D	-0.129	E	27.779	1451.6
213.5	213.55	34.554	D	-0.128	E	27.781	1451.6
214.5	214.55	34.558	D	-0.127	E	27.784	1451.6
215.4	215.45	34.558	D	-0.125	E	27.784	1451.6
216.5	216.55	34.558	D	-0.122	E	27.784	1451.7
217.4	217.45	34.561	D	-0.121	E	27.786	1451.7
218.5	218.55	34.563	D	-0.120	E	27.788	1451.7
219.5	219.55	34.562	D	-0.116	E	27.787	1451.8
220.6	220.60	34.566	D	-0.117	E	27.790	1451.8
221.5	221.55	34.567	D	-0.116	E	27.791	1451.8
222.4	222.40	34.568	D	-0.115	E	27.792	1451.8
223.5	223.50	34.569	D	-0.114	E	27.793	1451.8
224.6	224.65	34.568	D	-0.110	E	27.792	1451.9
225.6	225.60	34.571	D	-0.109	E	27.794	1451.9
226.7	226.75	34.572	D	-0.108	E	27.795	1451.9
227.7	227.70	34.573	D	-0.106	E	27.796	1451.9
228.5	228.50	34.575	D	-0.103	E	27.797	1452.0
229.5	229.55	34.579	D	-0.103	E	27.800	1452.0
230.6	230.65	34.578	D	-0.102	E	27.800	1452.0
231.6	231.60	34.578	D	-0.101	E	27.800	1452.0
232.6	232.65	34.580	D	-0.099	E	27.801	1452.1
233.7	233.75	34.579	D	-0.098	E	27.800	1452.1
234.7	234.70	34.580	D	-0.097	E	27.801	1452.1
235.7	235.75	34.585	D	-0.099	E	27.805	1452.1
236.7	236.75	34.582	D	-0.096	E	27.803	1452.2
237.6	237.60	34.585	D	-0.095	E	27.805	1452.2
238.6	238.60	34.587	D	-0.095	E	27.807	1452.2
239.6	239.65	34.588	D	-0.091	E	27.807	1452.2
240.6	240.65	34.590	D	-0.090	E	27.809	1452.3
241.7	241.75	34.589	D	-0.087	E	27.808	1452.3
242.6	242.60	34.593	D	-0.088	E	27.811	1452.3
243.6	243.60	34.594	D	-0.086	E	27.812	1452.3
244.5	244.55	34.597	D	-0.085	E	27.814	1452.4
245.7	245.75	34.598	D	-0.084	E	27.814	1452.4
246.7	246.70	34.595	D	-0.081	E	27.812	1452.4
247.5	247.55	34.597	D	-0.082	E	27.814	1452.4
248.5	248.50	34.597	D	-0.080	E	27.814	1452.4
249.6	249.65	34.592	D	-0.077	E	27.809	1452.5
259.6	259.65	34.614	D	-0.065	E	27.826	1452.7
269.7	269.75	34.621	D	-0.054	E	27.832	1452.9
279.9	279.95	34.627	D	-0.047	E	27.836	1453.1
290.2	290.25	34.629	D	-0.039	E	27.838	1453.4
300.3	300.30	34.635	D	-0.037	E	27.842	1453.5
310.4	310.40	34.638	D	-0.032	E	27.844	1453.7
362.0	362.05	34.642	D	-0.010	E	27.846	1454.7
371.9	371.90	34.640	D	-0.006	E	27.844	1454.9
382.0	382.05	34.640	D	-0.002	E	27.844	1455.0
392.1	392.15	34.641	D	0.0	E	27.845	1455.2
402.2	402.25	34.645	D	0.0	E	27.849	1455.4


EXPERIMENT 1054
TEMPERATURE, C
-2.00
-1.25
-0.50
0.25
1.00
1.75
2.50
SALINITY 0/00
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16.00
20.00
24.00
28.00
32.00
36.00
SIGMAT
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DEPTH M
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CRUISE 15-74-013 D'IBERVILLE FIORD-74 EXPER NO. 1054

LAT N.80-33-30 LONG W.80-11-30 WATER DEPTH 399

DEPTH INCR. DATE 250874 LOCAL TIME

DEPTH	PRES	SAL		TEMP		SIGMAT	SOUND
3.1	3.10	16.327	C	1.675	D	13.118	1431.7
4.1	4.15	25.963	C	1.644	D	20.803	1444.4
5.0	5.00	29.034	C	1.227	D	23.279	1446.7
6.1	6.10	29.522	C	1.000	D	23.681	1446.4
7.1	7.15	29.651	C	0.704	D	23.799	1445.2
7.9	7.95	29.783	C	0.505	D	23.913	1444.5
9.2	9.20	29.965	C	0.315	D	24.068	1443.9
10.1	10.10	30.177	C	0.250	D	24.240	1443.9
10.8	10.85	30.574	C	0.206	D	24.561	1444.3
12.0	12.05	31.139	C	0.204	D	25.016	1445.1
12.9	12.90	31.454	C	0.062	D	25.276	1444.9
14.0	14.05	31.603	C	-0.043	D	25.399	1444.6
15.0	15.05	31.726	C	-0.166	D	25.504	1444.2
16.0	16.00	31.871	C	-0.315	D	25.626	1443.7
17.1	17.10	31.918	C	-0.475	D	25.670	1443.1
18.0	18.05	31.932	C	-0.591	D	25.686	1442.6
18.9	18.90	32.023	C	-0.683	D	25.762	1442.3
19.8	19.80	32.028	C	-0.770	D	25.769	1441.9
21.0	21.00	32.034	C	-0.869	D	25.776	1441.5
21.8	21.85	32.081	C	-0.951	D	25.817	1441.2
22.8	22.80	32.097	C	-1.014	D	25.832	1440.9
23.9	23.90	32.134	C	-1.066	D	25.863	1440.7
24.9	24.90	32.146	C	-1.128	D	25.874	1440.5
25.7	25.70	32.183	C	-1.172	D	25.906	1440.3
26.8	26.80	32.177	C	-1.216	D	25.902	1440.1
27.8	27.80	32.209	C	-1.260	D	25.929	1440.0
28.8	28.80	32.196	C	-1.287	D	25.919	1439.9
29.7	29.70	32.201	C	-1.311	D	25.924	1439.8
30.8	30.80	32.217	C	-1.331	D	25.938	1439.7
31.8	31.80	32.226	C	-1.334	D	25.945	1439.7
32.9	32.90	32.228	C	-1.363	D	25.947	1439.6
33.8	33.85	32.252	C	-1.392	D	25.967	1439.5
34.7	34.75	32.254	C	-1.410	D	25.969	1439.5
35.8	35.85	32.288	C	-1.445	D	25.998	1439.4
36.8	36.80	32.286	C	-1.467	D	25.997	1439.3
37.7	37.70	32.288	C	-1.483	D	25.999	1439.2
38.7	38.75	32.294	C	-1.487	D	26.003	1439.2
39.7	39.70	32.316	C	-1.470	D	26.021	1439.3
40.6	40.60	32.345	C	-1.462	D	26.044	1439.4
41.8	41.80	32.370	C	-1.454	D	26.064	1439.5
42.8	42.85	32.396	C	-1.445	D	26.085	1439.6
43.8	43.80	32.430	C	-1.433	D	26.112	1439.8
44.6	44.65	32.462	C	-1.429	D	26.138	1439.8
45.7	45.75	32.497	C	-1.429	D	26.166	1439.9
46.8	46.80	32.520	C	-1.416	D	26.185	1440.0
47.6	47.60	32.567	C	-1.411	D	26.223	1440.1
48.7	48.70	32.619	C	-1.406	D	26.264	1440.2
49.6	49.60	32.666	C	-1.400	D	26.303	1440.3
50.6	50.65	32.714	C	-1.402	D	26.341	1440.4
51.7	51.70	32.744	C	-1.410	D	26.366	1440.4
52.5	52.55	32.774	C	-1.403	D	26.390	1440.5
53.6	53.65	32.814	C	-1.398	D	26.422	1440.6
54.5	54.50	32.848	C	-1.402	D	26.450	1440.7
55.5	55.55	32.879	C	-1.397	D	26.475	1440.7
56.6	56.65	32.910	C	-1.393	D	26.500	1440.8
57.6	57.65	32.938	C	-1.389	D	26.523	1440.9
58.6	58.65	32.966	C	-1.388	D	26.545	1441.0
59.5	59.50	32.997	C	-1.386	D	26.571	1441.0
60.4	60.40	33.027	C	-1.381	D	26.594	1441.1
61.3	61.30	33.055	C	-1.370	D	26.617	1441.2
62.2	62.25	33.083	C	-1.361	D	26.639	1441.3
63.3	63.35	33.103	C	-1.350	D	26.655	1441.4

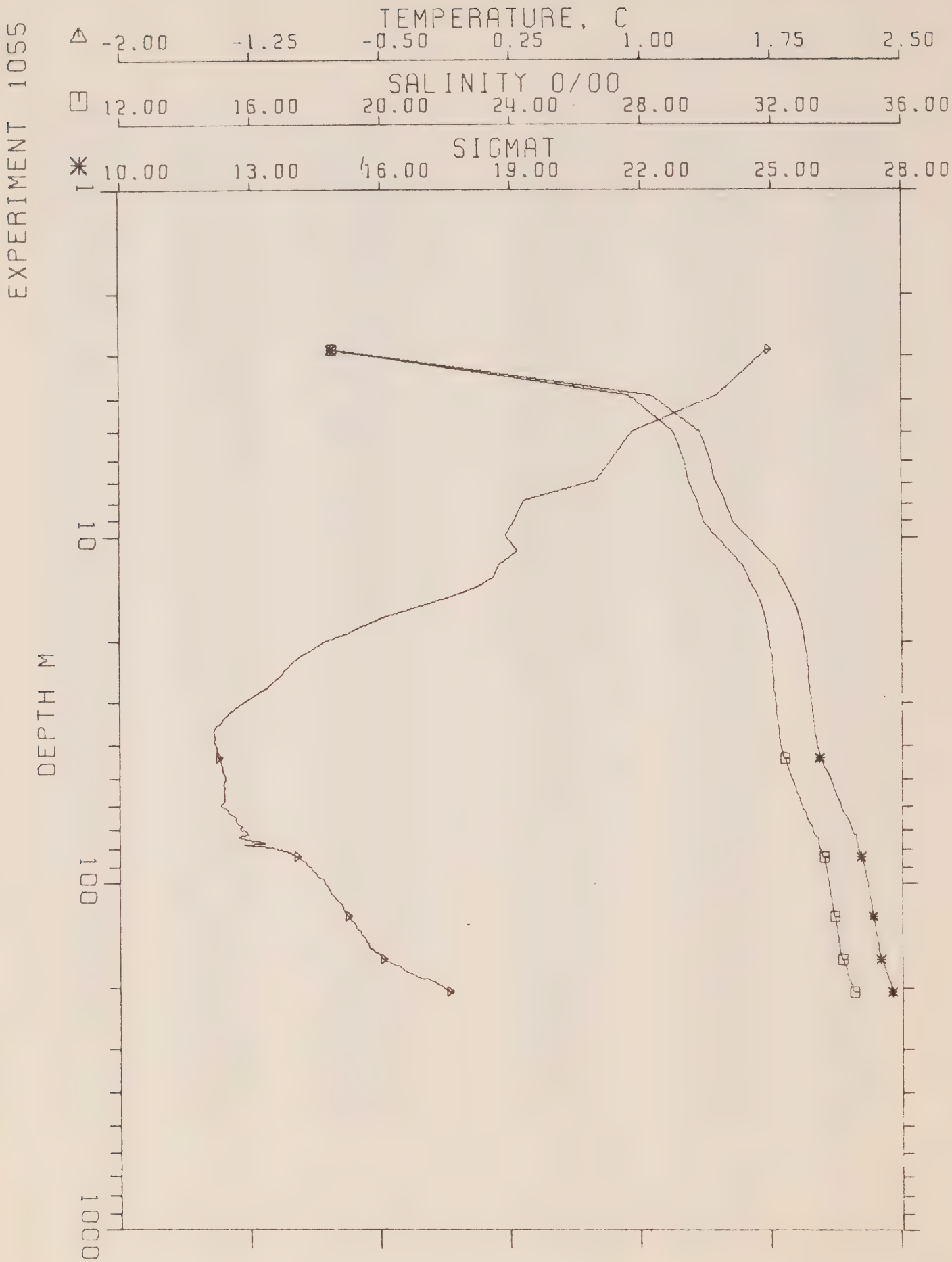
DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
64.4	64.40	33.126	C	-1.341	D	26.674	1441.5
65.3	65.30	33.154	C	-1.329	D	26.696	1441.6
66.4	66.40	33.187	C	-1.318	D	26.722	1441.7
67.2	67.25	33.217	C	-1.306	D	26.746	1441.8
68.3	68.30	33.236	C	-1.297	D	26.761	1441.9
69.1	69.15	33.265	C	-1.294	D	26.784	1442.0
70.2	70.25	33.287	C	-1.279	D	26.802	1442.1
71.3	71.35	33.313	C	-1.259	D	26.822	1442.3
72.3	72.35	33.345	C	-1.251	D	26.848	1442.4
73.1	73.10	33.365	C	-1.238	D	26.864	1442.5
74.1	74.15	33.391	C	-1.202	D	26.884	1442.7
75.2	75.25	33.419	C	-1.190	D	26.906	1442.8
76.2	76.20	33.436	C	-1.183	D	26.920	1442.9
77.1	77.10	33.457	C	-1.156	D	26.936	1443.0
78.2	78.20	33.477	C	-1.141	D	26.952	1443.2
79.3	79.35	33.500	C	-1.125	D	26.970	1443.3
80.2	80.25	33.515	C	-1.107	D	26.981	1443.4
81.1	81.10	33.532	C	-1.091	D	26.994	1443.5
82.1	82.10	33.548	C	-1.077	D	27.007	1443.6
83.2	83.20	33.561	C	-1.062	D	27.017	1443.7
84.3	84.30	33.576	C	-1.037	D	27.029	1443.9
85.2	85.20	33.591	C	-1.023	D	27.040	1444.0
86.1	86.15	33.605	C	-1.010	D	27.051	1444.1
87.2	87.20	33.621	C	-0.993	D	27.063	1444.2
88.3	88.35	33.637	C	-0.974	D	27.076	1444.3
89.2	89.20	33.644	C	-0.965	D	27.081	1444.4
90.2	90.25	33.658	C	-0.955	D	27.092	1444.5
91.3	91.30	33.678	C	-0.939	D	27.108	1444.6
92.3	92.30	33.689	C	-0.923	D	27.116	1444.7
93.2	93.20	33.709	C	-0.909	D	27.132	1444.8
94.3	94.30	33.720	C	-0.895	D	27.140	1444.9
95.2	95.20	33.733	C	-0.885	D	27.151	1445.0
96.2	96.25	33.747	C	-0.873	D	27.161	1445.1
97.2	97.25	33.761	C	-0.860	D	27.172	1445.2
98.3	98.30	33.773	C	-0.848	D	27.182	1445.3
99.3	99.35	33.782	C	-0.841	D	27.189	1445.3
100.2	100.25	33.794	D	-0.834	E	27.198	1445.4
101.1	101.15	33.802	D	-0.830	E	27.204	1445.4
102.2	102.25	33.807	D	-0.824	E	27.208	1445.5
103.3	103.30	33.815	D	-0.816	E	27.214	1445.6
104.2	104.20	33.826	D	-0.810	E	27.223	1445.6
105.1	105.15	33.833	D	-0.809	E	27.229	1445.7
106.0	106.00	33.838	D	-0.798	E	27.232	1445.7
107.2	107.20	33.844	D	-0.792	E	27.236	1445.8
108.2	108.20	33.850	D	-0.789	E	27.241	1445.8
109.1	109.15	33.858	D	-0.784	E	27.248	1445.9
110.1	110.15	33.863	D	-0.778	E	27.251	1445.9
111.0	111.05	33.872	D	-0.774	E	27.259	1446.0
112.0	112.00	33.880	D	-0.770	E	27.265	1446.0
113.0	113.00	33.885	D	-0.764	E	27.268	1446.1
114.0	114.00	33.892	D	-0.757	E	27.274	1446.1
115.0	115.05	33.900	D	-0.752	E	27.281	1446.2
116.0	116.05	33.903	D	-0.747	E	27.283	1446.2
116.9	116.90	33.911	D	-0.744	E	27.289	1446.3
117.8	117.85	33.916	D	-0.740	E	27.293	1446.3
118.8	118.80	33.924	D	-0.732	E	27.299	1446.4
119.9	119.90	33.931	D	-0.727	E	27.304	1446.4
120.9	120.95	33.937	D	-0.722	E	27.309	1446.5
121.9	121.95	33.944	D	-0.717	E	27.315	1446.5
123.0	123.00	33.950	D	-0.712	E	27.319	1446.6
124.0	124.05	33.956	D	-0.705	E	27.324	1446.6
124.9	124.95	33.964	D	-0.701	E	27.330	1446.7
125.9	125.95	33.967	D	-0.698	E	27.332	1446.7
127.0	127.00	33.972	D	-0.693	E	27.337	1446.7
128.0	128.00	33.977	D	-0.686	E	27.340	1446.8
128.8	128.85	33.984	D	-0.681	E	27.345	1446.8
129.9	129.90	33.993	D	-0.675	E	27.352	1446.9
130.9	130.90	34.001	D	-0.669	E	27.359	1447.0
131.9	131.90	34.008	D	-0.665	E	27.364	1447.0

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
132.8	132.80	34.014	D	-0.658	E	27.369	1447.1
133.7	133.75	34.020	D	-0.652	E	27.373	1447.1
134.7	134.70	34.021	D	-0.649	E	27.374	1447.1
135.7	135.75	34.030	D	-0.644	E	27.381	1447.2
136.7	136.70	34.036	D	-0.640	E	27.386	1447.2
137.7	137.70	34.038	D	-0.637	E	27.387	1447.3
138.5	138.55	34.043	D	-0.635	E	27.391	1447.3
139.5	139.50	34.046	D	-0.632	E	27.394	1447.3
140.5	140.55	34.050	D	-0.625	E	27.397	1447.4
141.5	141.50	34.060	D	-0.617	E	27.404	1447.5
142.5	142.55	34.070	D	-0.610	E	27.412	1447.5
143.3	143.35	34.075	D	-0.606	E	27.416	1447.6
144.4	144.45	34.087	D	-0.596	E	27.425	1447.6
145.5	145.50	34.096	D	-0.592	E	27.432	1447.7
146.5	146.50	34.101	D	-0.584	E	27.436	1447.8
147.4	147.45	34.104	D	-0.578	E	27.438	1447.8
148.1	148.15	34.116	D	-0.573	E	27.448	1447.9
149.3	149.30	34.121	D	-0.565	E	27.452	1447.9
150.2	150.25	34.126	D	-0.563	E	27.455	1447.9
150.9	150.95	34.131	D	-0.557	E	27.460	1448.0
152.1	152.10	34.140	D	-0.550	E	27.466	1448.1
153.1	153.10	34.151	D	-0.543	E	27.474	1448.1
154.2	154.20	34.155	D	-0.537	E	27.478	1448.2
154.9	154.95	34.158	D	-0.529	E	27.480	1448.2
155.9	155.95	34.169	D	-0.517	E	27.488	1448.3
157.3	157.35	34.177	D	-0.511	E	27.494	1448.4
158.2	158.25	34.183	D	-0.503	E	27.499	1448.4
159.2	159.20	34.198	D	-0.496	E	27.511	1448.5
160.0	160.05	34.210	D	-0.488	E	27.520	1448.6
161.0	161.05	34.224	D	-0.475	E	27.531	1448.7
162.0	162.00	34.234	D	-0.464	E	27.538	1448.7
163.1	163.10	34.239	D	-0.456	E	27.542	1448.8
164.0	164.00	34.246	D	-0.449	E	27.548	1448.9
164.9	164.95	34.256	D	-0.438	E	27.555	1448.9
165.7	165.75	34.263	D	-0.434	E	27.560	1449.0
166.6	166.65	34.270	D	-0.427	E	27.566	1449.0
167.5	167.55	34.285	D	-0.416	E	27.577	1449.1
168.5	168.55	34.292	D	-0.409	E	27.583	1449.2
169.5	169.50	34.300	D	-0.404	E	27.589	1449.2
170.5	170.55	34.303	D	-0.401	E	27.592	1449.3
171.5	171.50	34.309	D	-0.391	E	27.596	1449.3
172.5	172.50	34.314	D	-0.386	E	27.600	1449.4
173.4	173.45	34.318	D	-0.380	E	27.603	1449.4
174.5	174.50	34.327	D	-0.375	E	27.609	1449.5
175.5	175.50	34.332	D	-0.365	E	27.613	1449.6
176.4	176.40	34.342	D	-0.359	E	27.621	1449.6
177.4	177.40	34.347	D	-0.350	E	27.625	1449.7
178.5	178.55	34.356	D	-0.338	E	27.631	1449.8
179.3	179.30	34.366	D	-0.331	E	27.639	1449.8
180.4	180.40	34.378	D	-0.319	E	27.648	1449.9
181.5	181.50	34.382	D	-0.313	E	27.651	1450.0
182.5	182.55	34.390	D	-0.304	E	27.657	1450.0
183.7	183.75	34.403	D	-0.290	E	27.667	1450.1
184.8	184.80	34.407	D	-0.281	E	27.670	1450.2
185.8	185.85	34.420	D	-0.270	E	27.680	1450.3
186.8	186.80	34.433	D	-0.253	E	27.690	1450.4
187.9	187.90	34.444	D	-0.243	E	27.698	1450.5
188.9	188.95	34.452	D	-0.228	E	27.704	1450.6
189.9	189.95	34.463	D	-0.224	E	27.712	1450.6
190.9	190.90	34.467	D	-0.217	E	27.716	1450.7
191.8	191.80	34.480	D	-0.205	E	27.726	1450.8
192.9	192.90	34.483	D	-0.203	E	27.728	1450.8
194.0	194.00	34.485	D	-0.199	E	27.729	1450.8
194.9	194.95	34.490	D	-0.196	E	27.733	1450.9
195.8	195.80	34.490	D	-0.195	E	27.733	1450.9
197.0	197.05	34.488	D	-0.189	E	27.731	1450.9
197.8	197.85	34.486	D	-0.188	E	27.730	1451.0
198.8	198.85	34.488	D	-0.186	E	27.731	1451.0
199.9	199.95	34.491	D	-0.186	E	27.734	1451.0

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
200.8	200.85	34.501	D	-0.181	E	27.741	1451.1
201.9	201.95	34.508	D	-0.171	E	27.746	1451.1
202.7	202.75	34.515	D	-0.169	E	27.752	1451.2
204.0	204.00	34.515	D	-0.162	E	27.751	1451.2
204.7	204.75	34.525	D	-0.151	E	27.759	1451.3
205.7	205.70	34.531	D	-0.143	E	27.764	1451.4
206.8	206.85	34.538	D	-0.141	E	27.769	1451.4
207.7	207.75	34.539	D	-0.138	E	27.769	1451.4
208.6	208.65	34.544	D	-0.132	E	27.774	1451.5
209.8	209.80	34.548	D	-0.121	E	27.776	1451.5
210.7	210.70	34.556	D	-0.116	E	27.783	1451.6
211.5	211.50	34.562	D	-0.110	E	27.787	1451.6
212.7	212.70	34.565	D	-0.106	E	27.789	1451.7
213.6	213.65	34.572	D	-0.097	E	27.794	1451.8
214.4	214.45	34.575	D	-0.093	E	27.797	1451.8
215.6	215.60	34.580	D	-0.085	E	27.800	1451.9
216.5	216.50	34.591	D	-0.075	E	27.808	1451.9
217.6	217.60	34.592	D	-0.070	E	27.809	1452.0
218.6	218.60	34.596	D	-0.066	E	27.813	1452.0
219.4	219.45	34.604	D	-0.058	E	27.818	1452.1
220.6	220.60	34.612	D	-0.049	E	27.824	1452.1
221.5	221.55	34.615	D	-0.044	E	27.827	1452.2
222.7	222.75	34.622	D	-0.035	E	27.831	1452.3
223.9	223.95	34.624	D	-0.033	E	27.833	1452.3
225.1	225.15	34.628	D	-0.028	E	27.836	1452.3
226.5	226.50	34.632	D	-0.018	E	27.838	1452.4
227.7	227.70	34.642	D	-0.010	E	27.846	1452.5
229.0	229.05	34.643	D	-0.004	E	27.847	1452.5
230.2	230.20	34.647	D	-0.002	E	27.850	1452.6
231.7	231.70	34.658	D	0.0	E	27.859	1452.6
232.9	232.95	34.665	D	0.005	E	27.864	1452.7
234.2	234.20	34.669	D	0.012	E	27.867	1452.7
235.7	235.70	34.665	D	0.022	E	27.863	1452.8
236.8	236.80	34.672	D	0.030	E	27.869	1452.9
238.1	238.15	34.675	D	0.036	E	27.871	1452.9
239.4	239.45	34.685	D	0.045	E	27.878	1453.0
240.5	240.55	34.692	D	0.056	E	27.883	1453.1
241.9	241.90	34.694	D	0.060	E	27.885	1453.1
243.2	243.25	34.699	D	0.065	E	27.888	1453.2
244.4	244.40	34.702	D	0.070	E	27.891	1453.2
245.4	245.45	34.706	D	0.071	E	27.894	1453.2
246.8	246.80	34.708	D	0.074	E	27.895	1453.3
248.1	248.15	34.709	D	0.077	E	27.896	1453.3
249.3	249.35	34.710	D	0.082	E	27.897	1453.4
250.3	250.35	34.716	D	0.085	E	27.901	1453.4
251.6	251.60	34.720	D	0.090	E	27.904	1453.4
252.5	252.55	34.721	D	0.093	E	27.905	1453.5
253.6	253.65	34.724	D	0.093	E	27.907	1453.5
254.8	254.80	34.723	D	0.098	E	27.906	1453.5
255.8	255.85	34.727	D	0.099	E	27.909	1453.6
257.1	257.10	34.726	D	0.102	E	27.908	1453.6
258.0	258.05	34.733	D	0.104	E	27.914	1453.6
259.1	259.10	34.735	D	0.108	E	27.915	1453.7
260.3	260.35	34.736	D	0.110	E	27.916	1453.7
261.3	261.30	34.740	D	0.111	E	27.919	1453.7
262.7	262.75	34.737	D	0.114	E	27.917	1453.8
263.6	263.65	34.740	D	0.116	E	27.919	1453.8
264.8	264.85	34.746	D	0.119	E	27.923	1453.8
265.8	265.85	34.747	D	0.122	E	27.925	1453.9
267.1	267.10	34.748	D	0.122	E	27.925	1453.9
268.2	268.20	34.749	D	0.126	E	27.925	1453.9
269.0	269.05	34.750	D	0.127	E	27.926	1453.9
270.2	270.25	34.750	D	0.129	E	27.926	1454.0
271.2	271.25	34.753	D	0.131	E	27.928	1454.0
272.2	272.25	34.751	D	0.134	E	27.927	1454.0
273.4	273.40	34.755	D	0.135	E	27.930	1454.1
274.1	274.15	34.759	D	0.138	E	27.933	1454.1
275.4	275.40	34.759	D	0.141	E	27.933	1454.1
276.2	276.25	34.762	D	0.143	E	27.935	1454.1

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
277.3	277.35	34.762	D	0.147	E	27.935	1454.2
278.4	278.40	34.766	D	0.147	E	27.938	1454.2
279.2	279.20	34.767	D	0.148	E	27.939	1454.2
280.1	280.15	34.767	D	0.150	E	27.939	1454.2
281.3	281.30	34.767	D	0.153	E	27.939	1454.3
282.1	282.10	34.772	D	0.155	E	27.942	1454.3
282.9	282.90	34.774	D	0.155	E	27.944	1454.3
284.0	284.00	34.772	D	0.157	E	27.943	1454.3
285.2	285.20	34.772	D	0.159	E	27.943	1454.4
286.1	286.10	34.774	D	0.161	E	27.944	1454.4
287.0	287.05	34.777	D	0.163	E	27.946	1454.4
288.0	288.00	34.778	D	0.164	E	27.947	1454.5
288.8	288.80	34.779	D	0.164	E	27.948	1454.5
289.8	289.85	34.779	D	0.166	E	27.947	1454.5
290.8	290.85	34.781	D	0.166	E	27.949	1454.5
291.7	291.70	34.782	D	0.168	E	27.950	1454.5
292.7	292.70	34.783	D	0.171	E	27.950	1454.6
293.8	293.80	34.787	D	0.172	E	27.954	1454.6
294.6	294.65	34.787	D	0.175	E	27.954	1454.6
295.8	295.85	34.788	D	0.177	E	27.955	1454.7
297.0	297.05	34.790	D	0.180	E	27.956	1454.7
298.0	298.05	34.792	D	0.181	E	27.958	1454.7
299.3	299.30	34.795	D	0.183	E	27.960	1454.7
300.2	300.20	34.795	D	0.184	E	27.959	1454.8
301.4	301.40	34.796	D	0.185	E	27.960	1454.8
302.4	302.45	34.797	D	0.186	E	27.961	1454.8
303.5	303.55	34.798	D	0.188	E	27.962	1454.8
304.7	304.70	34.798	D	0.190	E	27.962	1454.9
305.7	305.75	34.800	D	0.190	E	27.964	1454.9
306.8	306.80	34.799	D	0.192	E	27.962	1454.9
307.8	307.80	34.803	D	0.192	E	27.965	1454.9
308.8	308.85	34.802	D	0.192	E	27.965	1455.0
309.7	309.70	34.803	D	0.193	E	27.966	1455.0
310.8	310.85	34.807	D	0.194	E	27.969	1455.0
311.9	311.90	34.804	D	0.196	E	27.966	1455.0
313.0	313.00	34.807	D	0.195	E	27.969	1455.0
313.9	313.95	34.806	D	0.198	E	27.968	1455.1
315.1	315.10	34.807	D	0.199	E	27.969	1455.1
316.2	316.20	34.807	D	0.200	E	27.968	1455.1
317.2	317.20	34.809	D	0.200	E	27.970	1455.1
318.4	318.40	34.810	D	0.201	E	27.971	1455.2
319.3	319.35	34.811	D	0.202	E	27.972	1455.2
320.3	320.30	34.814	D	0.202	E	27.974	1455.2
321.2	321.20	34.812	D	0.204	E	27.973	1455.2
322.1	322.15	34.812	D	0.206	E	27.972	1455.3
323.1	323.10	34.816	D	0.206	E	27.975	1455.3
324.2	324.20	34.817	D	0.208	E	27.976	1455.3
325.3	325.30	34.817	D	0.209	E	27.976	1455.3
326.1	326.10	34.818	D	0.210	E	27.977	1455.3
327.0	327.05	34.819	D	0.210	E	27.978	1455.4
328.0	328.05	34.819	D	0.211	E	27.977	1455.4
329.1	329.15	34.819	D	0.213	E	27.977	1455.4
330.2	330.20	34.820	D	0.213	E	27.978	1455.4
331.1	331.10	34.822	D	0.213	E	27.980	1455.4
332.2	332.20	34.822	D	0.214	E	27.979	1455.5
333.0	333.00	34.823	D	0.215	E	27.980	1455.5
334.1	334.15	34.822	D	0.216	E	27.980	1455.5
335.1	335.10	34.826	D	0.216	E	27.983	1455.5
336.1	336.10	34.823	D	0.218	E	27.980	1455.6
337.0	337.05	34.827	D	0.218	E	27.983	1455.6
338.1	338.10	34.827	D	0.219	E	27.983	1455.6
338.9	338.90	34.827	D	0.219	E	27.984	1455.6
340.1	340.15	34.825	D	0.221	E	27.981	1455.6
341.0	341.05	34.829	D	0.219	E	27.985	1455.6
342.0	342.05	34.828	D	0.221	E	27.984	1455.7
343.2	343.20	34.830	D	0.221	E	27.986	1455.7
344.2	344.20	34.828	D	0.222	E	27.984	1455.7
345.0	345.05	34.830	D	0.222	E	27.986	1455.7
346.2	346.25	34.829	D	0.224	E	27.985	1455.8

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
347.0	347.05	34.832	D	0.222	E	27.987	1455.8
348.1	348.15	34.832	D	0.224	E	27.987	1455.8
349.2	349.25	34.830	D	0.225	E	27.986	1455.8
350.1	350.10	34.831	D	0.225	E	27.987	1455.8
351.0	351.05	34.833	D	0.225	E	27.988	1455.8
352.3	352.30	34.832	D	0.226	E	27.987	1455.9
353.2	353.20	34.834	D	0.225	E	27.989	1455.9
354.1	354.15	34.831	D	0.227	E	27.986	1455.9
355.2	355.20	34.833	D	0.226	E	27.988	1455.9
355.5	355.50	34.835	D	0.225	E	27.990	1455.9
356.6	356.65	34.832	D	0.227	E	27.987	1455.9
357.4	357.45	34.833	D	0.226	E	27.988	1456.0
358.4	358.40	34.835	D	0.226	E	27.990	1456.0
359.5	359.55	34.835	D	0.227	E	27.989	1456.0
360.3	360.30	34.834	D	0.227	E	27.989	1456.0
361.1	361.10	34.832	D	0.230	E	27.987	1456.0
361.8	361.85	34.835	D	0.228	E	27.990	1456.0
362.8	362.80	34.837	D	0.228	E	27.991	1456.1
363.6	363.60	34.837	D	0.229	E	27.991	1456.1
364.5	364.55	34.834	D	0.231	E	27.989	1456.1
365.3	365.35	34.834	D	0.231	E	27.988	1456.1
366.1	366.15	34.839	D	0.229	E	27.992	1456.1
367.1	367.10	34.838	D	0.229	E	27.992	1456.1
368.0	368.00	34.837	D	0.231	E	27.991	1456.2
368.8	368.85	34.839	D	0.230	E	27.992	1456.2
369.7	369.75	34.839	D	0.232	E	27.992	1456.2
370.8	370.80	34.840	D	0.233	E	27.993	1456.2
371.8	371.80	34.841	D	0.233	E	27.994	1456.2
372.8	372.80	34.840	D	0.234	E	27.993	1456.3
373.8	373.85	34.840	D	0.235	E	27.993	1456.3
374.7	374.75	34.841	D	0.235	E	27.994	1456.3
375.7	375.75	34.841	D	0.236	E	27.994	1456.3
376.7	376.70	34.844	D	0.235	E	27.996	1456.3
377.8	377.85	34.841	D	0.237	E	27.994	1456.3
378.6	378.65	34.843	D	0.237	E	27.996	1456.4
379.7	379.75	34.843	D	0.238	E	27.995	1456.4
380.8	380.80	34.845	D	0.238	E	27.997	1456.4
381.9	381.90	34.845	D	0.238	E	27.997	1456.4
382.9	382.95	34.847	D	0.238	E	27.998	1456.4
384.1	384.15	34.846	D	0.238	E	27.998	1456.5
385.1	385.10	34.847	D	0.239	E	27.999	1456.5
386.1	386.10	34.847	D	0.239	E	27.998	1456.5
387.2	387.20	34.845	D	0.241	E	27.997	1456.5
388.0	388.00	34.847	D	0.240	E	27.999	1456.5
389.2	389.20	34.844	D	0.242	E	27.996	1456.6
390.2	390.25	34.846	D	0.241	E	27.998	1456.6
391.2	391.20	34.849	D	0.241	E	28.000	1456.6
392.2	392.20	34.847	D	0.242	E	27.998	1456.6
393.1	393.15	34.848	D	0.242	E	27.999	1456.6
394.0	394.00	34.850	D	0.242	E	28.001	1456.6
395.1	395.10	34.849	D	0.244	E	28.000	1456.7
396.1	396.10	34.848	D	0.244	E	27.999	1456.7
397.1	397.15	34.849	D	0.244	E	28.000	1456.7
398.0	398.00	34.851	D	0.244	E	28.002	1456.7
398.9	398.90	34.851	D	0.245	E	28.001	1456.7
400.1	400.10	34.852	D	0.245	E	28.002	1456.8
401.0	401.05	34.853	D	0.246	E	28.003	1456.8
402.0	402.00	34.854	D	0.246	E	28.003	1456.8
402.8	402.85	34.855	D	0.246	E	28.004	1456.8
403.9	403.95	34.855	D	0.246	E	28.005	1456.8
405.0	405.00	34.852	D	0.248	E	28.002	1456.9


EXPERIMENT 1055
TEMPERATURE, C
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-1.25
-0.50
0.25
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2.50
SALINITY O/OO
12.00
16.00
20.00
24.00
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32.00
36.00
SIGMAT
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13.00
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DEPTH M
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CRUISE 15-74-013 D'IBERVILLE FICRD-74 EXPER NO. 1055

LAT N.80-33-12 LONG W.80-05-35 WATER DEPTH 220

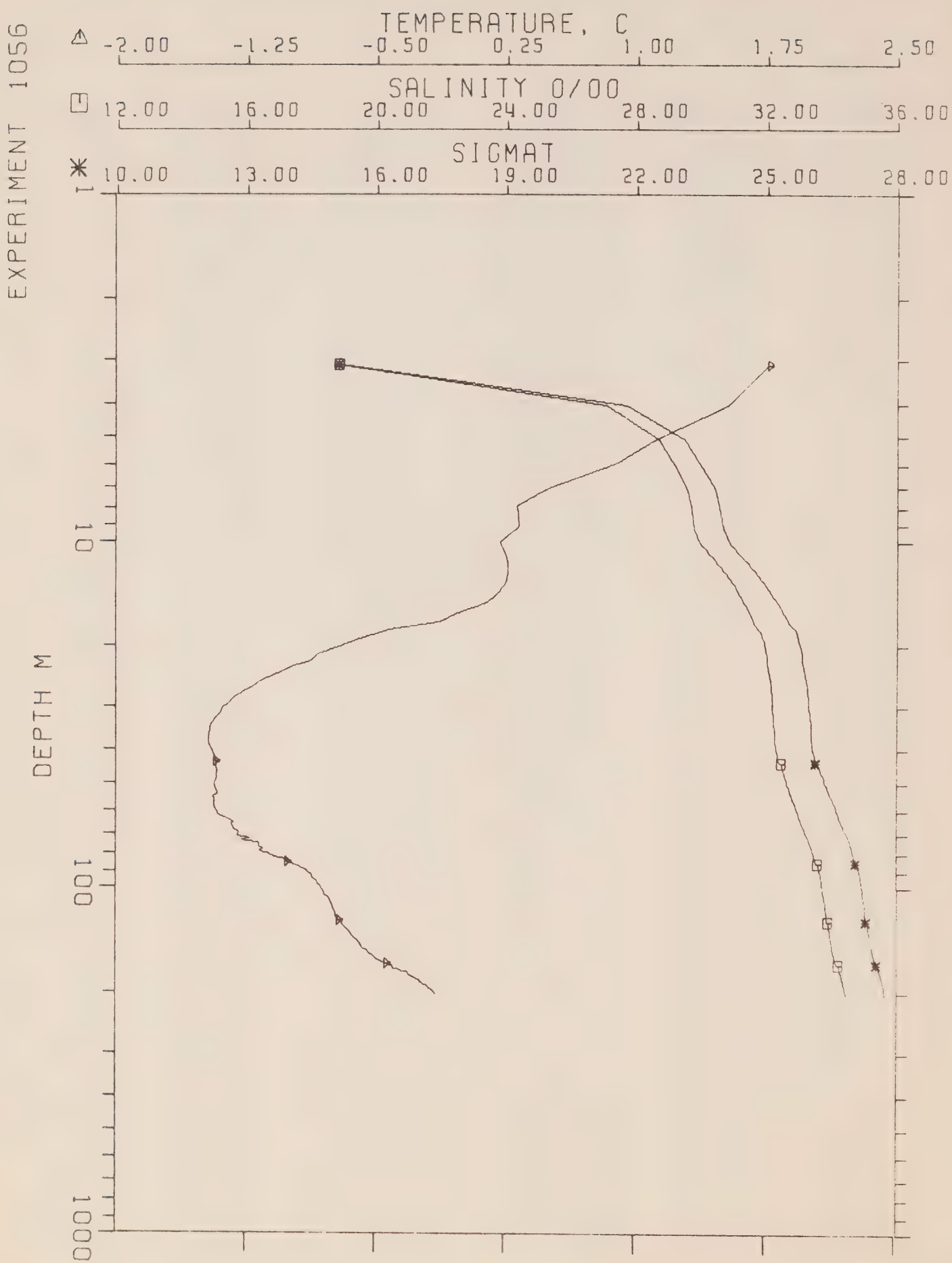
DEPTH INCR. DATE 250874 LOCAL TIME

DEPTH	PRES	SAL		TEMP		SIGMAT	SOUND
2.9	2.90	18.526	C	1.736	D	14.868	1434.9
3.9	3.90	27.719	C	1.450	D	22.216	1445.9
5.0	5.00	29.090	C	0.962	D	23.337	1445.6
6.0	6.00	29.397	C	0.845	D	23.588	1445.5
6.8	6.85	29.501	C	0.758	D	23.676	1445.3
7.9	7.90	29.786	C	0.339	D	23.923	1443.8
9.1	9.10	29.989	C	0.274	D	24.088	1443.7
10.0	10.05	30.407	C	0.217	D	24.427	1444.1
11.0	11.05	30.799	C	0.293	D	24.738	1445.0
12.1	12.10	31.209	C	0.190	D	25.073	1445.1
13.1	13.15	31.371	C	0.161	D	25.204	1445.2
14.1	14.10	31.531	C	0.063	D	25.338	1445.0
14.9	14.95	31.666	C	-0.084	D	25.452	1444.5
16.1	16.10	31.785	C	-0.307	D	25.556	1443.7
17.1	17.10	31.877	C	-0.475	D	25.637	1443.0
18.1	18.10	31.923	C	-0.586	D	25.678	1442.6
19.1	19.10	31.971	C	-0.697	D	25.721	1442.2
20.2	20.25	32.010	C	-0.819	D	25.756	1441.7
21.2	21.20	32.037	C	-0.887	D	25.779	1441.4
22.2	22.20	32.062	C	-0.959	D	25.802	1441.1
23.2	23.25	32.075	C	-1.001	D	25.814	1441.0
24.1	24.15	32.092	C	-1.039	D	25.828	1440.8
25.2	25.25	32.102	C	-1.071	D	25.838	1440.7
26.2	26.20	32.114	C	-1.107	D	25.848	1440.6
27.3	27.30	32.122	C	-1.145	D	25.855	1440.4
28.3	28.30	32.145	C	-1.195	D	25.876	1440.2
29.2	29.25	32.164	C	-1.242	D	25.892	1440.0
30.2	30.20	32.190	C	-1.291	D	25.914	1439.9
31.3	31.35	32.204	C	-1.330	D	25.927	1439.7
32.2	32.20	32.219	C	-1.362	D	25.940	1439.6
33.4	33.40	32.236	C	-1.391	D	25.954	1439.5
34.3	34.35	32.250	C	-1.417	D	25.966	1439.4
35.3	35.35	32.264	C	-1.443	D	25.978	1439.3
36.4	36.40	32.281	C	-1.460	D	25.992	1439.3
37.4	37.40	32.288	C	-1.465	D	25.998	1439.3
38.5	38.50	32.313	C	-1.451	D	26.017	1439.4
39.3	39.35	32.337	C	-1.469	D	26.038	1439.4
40.4	40.45	32.355	C	-1.456	D	26.052	1439.5
41.5	41.50	32.381	C	-1.446	D	26.072	1439.6
42.4	42.45	32.412	C	-1.446	D	26.098	1439.6
43.5	43.55	32.436	C	-1.438	D	26.117	1439.7
44.4	44.45	32.468	C	-1.430	D	26.143	1439.8
45.4	45.40	32.502	C	-1.424	D	26.170	1439.9
46.6	46.60	32.550	C	-1.416	D	26.209	1440.0
47.6	47.60	32.605	C	-1.413	D	26.253	1440.2
48.5	48.50	32.636	C	-1.407	D	26.279	1440.2
49.5	49.55	32.674	C	-1.396	D	26.309	1440.4
50.6	50.60	32.710	C	-1.396	D	26.338	1440.4
51.5	51.55	32.749	C	-1.400	D	26.370	1440.5
52.5	52.55	32.789	C	-1.410	D	26.402	1440.5
53.6	53.60	32.815	C	-1.395	D	26.423	1440.6
54.5	54.55	32.847	C	-1.406	D	26.449	1440.6
55.6	55.60	32.877	C	-1.402	D	26.474	1440.7
56.8	56.80	32.904	C	-1.397	D	26.495	1440.8
57.6	57.65	32.937	C	-1.398	D	26.522	1440.9
58.6	58.60	32.978	C	-1.403	D	26.556	1440.9
59.7	59.70	33.012	C	-1.433	D	26.584	1440.8
60.7	60.70	33.035	C	-1.405	D	26.602	1441.0
61.6	61.60	33.070	C	-1.377	D	26.629	1441.2
62.8	62.85	33.100	C	-1.382	D	26.654	1441.2
63.6	63.60	33.129	C	-1.366	D	26.677	1441.4
64.9	64.90	33.171	C	-1.335	D	26.710	1441.6

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
65.7	65.75	33.211 C	-1.342 D	26.742	1441.6
66.8	66.80	33.252 C	-1.343 D	26.776	1441.7
67.7	67.75	33.271 C	-1.332 D	26.790	1441.8
68.8	68.80	33.302 C	-1.297 D	26.815	1442.0
69.8	69.85	33.328 C	-1.314 D	26.836	1442.0
70.9	70.90	33.354 C	-1.276 D	26.856	1442.2
71.8	71.80	33.373 C	-1.274 D	26.872	1442.3
72.7	72.75	33.418 C	-1.255 D	26.907	1442.5
74.0	74.00	33.462 C	-1.323 D	26.945	1442.2
74.9	74.95	33.470 C	-1.282 D	26.950	1442.4
76.0	76.00	33.469 C	-1.173 D	26.946	1443.0
77.0	77.00	33.494 C	-1.163 D	26.966	1443.1
77.9	77.95	33.531 C	-1.297 D	27.000	1442.5
79.1	79.10	33.496 C	-1.128 D	26.967	1443.3
79.9	79.90	33.551 C	-1.116 D	27.011	1443.4
80.9	80.95	33.566 C	-1.060 D	27.021	1443.7
82.0	82.00	33.592 C	-1.026 D	27.041	1443.9
82.9	82.90	33.611 C	-1.007 D	27.056	1444.1
84.1	84.10	33.626 C	-0.990 D	27.068	1444.2
85.1	85.15	33.642 C	-0.974 D	27.079	1444.3
85.9	85.95	33.659 C	-0.960 D	27.093	1444.4
87.1	87.15	33.673 C	-0.944 D	27.104	1444.5
88.2	88.20	33.687 C	-0.935 D	27.115	1444.6
89.0	89.00	33.695 C	-0.926 D	27.121	1444.6
90.2	90.20	33.708 C	-0.916 D	27.131	1444.7
91.2	91.20	33.718 C	-0.904 D	27.138	1444.8
92.1	92.10	33.728 C	-0.899 D	27.146	1444.9
93.2	93.20	33.733 C	-0.891 D	27.150	1444.9
94.2	94.20	33.746 C	-0.883 D	27.161	1445.0
95.3	95.30	33.755 C	-0.873 D	27.168	1445.1
96.2	96.25	33.763 C	-0.859 D	27.174	1445.2
97.2	97.25	33.779 C	-0.847 D	27.186	1445.3
98.3	98.30	33.789 C	-0.840 D	27.194	1445.3
99.2	99.25	33.795 C	-0.831 D	27.198	1445.4
100.1	100.15	33.803 D	-0.829 E	27.205	1445.4
101.2	101.25	33.808 D	-0.822 E	27.209	1445.5
102.3	102.35	33.818 D	-0.817 E	27.216	1445.5
103.4	103.40	33.825 D	-0.811 E	27.222	1445.6
104.5	104.50	33.829 D	-0.806 E	27.225	1445.7
105.4	105.40	33.837 D	-0.801 E	27.232	1445.7
106.3	106.30	33.845 D	-0.798 E	27.238	1445.7
107.5	107.50	33.850 D	-0.790 E	27.241	1445.8
108.5	108.50	33.858 D	-0.787 E	27.247	1445.8
109.4	109.40	33.867 D	-0.778 E	27.255	1445.9
110.4	110.40	33.873 D	-0.769 E	27.259	1446.0
111.4	111.45	33.883 D	-0.763 E	27.267	1446.0
112.5	112.50	33.894 D	-0.755 E	27.275	1446.1
113.5	113.55	33.900 D	-0.748 E	27.280	1446.2
114.5	114.50	33.908 D	-0.736 E	27.286	1446.3
115.5	115.50	33.921 D	-0.732 E	27.297	1446.3
116.5	116.50	33.923 D	-0.729 E	27.298	1446.3
117.5	117.50	33.928 D	-0.725 E	27.302	1446.4
118.6	118.65	33.932 D	-0.725 E	27.305	1446.4
119.6	119.65	33.933 D	-0.724 E	27.306	1446.4
120.5	120.50	33.938 D	-0.720 E	27.310	1446.5
121.6	121.65	33.943 D	-0.717 E	27.314	1446.5
122.8	122.80	33.953 D	-0.708 E	27.321	1446.6
123.6	123.60	33.959 D	-0.700 E	27.326	1446.6
124.7	124.70	33.968 D	-0.693 E	27.333	1446.7
125.7	125.75	33.976 D	-0.690 E	27.339	1446.7
126.7	126.70	33.975 D	-0.685 E	27.339	1446.8
127.8	127.85	33.982 D	-0.681 E	27.344	1446.8
128.7	128.75	33.991 D	-0.677 E	27.351	1446.9
129.7	129.75	33.995 D	-0.672 E	27.354	1446.9
130.7	130.75	34.002 D	-0.668 E	27.359	1447.0
131.9	131.95	34.009 D	-0.658 E	27.364	1447.0
132.7	132.75	34.018 D	-0.650 E	27.372	1447.1
133.8	133.80	34.026 D	-0.649 E	27.378	1447.1
134.9	134.95	34.028 D	-0.647 E	27.379	1447.2

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
135.9	135.95	34.033 D	-0.642 E	27.384	1447.2
137.0	137.00	34.035 D	-0.638 E	27.385	1447.3
137.8	137.80	34.044 D	-0.627 E	27.392	1447.3
138.9	138.90	34.056 D	-0.623 E	27.402	1447.4
140.0	140.00	34.056 D	-0.621 E	27.402	1447.4
141.0	141.05	34.060 D	-0.620 E	27.405	1447.4
142.0	142.05	34.066 D	-0.613 E	27.409	1447.5
143.0	143.00	34.076 D	-0.605 E	27.417	1447.6
144.0	144.00	34.083 D	-0.599 E	27.422	1447.6
144.9	144.95	34.088 D	-0.598 E	27.427	1447.6
146.1	146.15	34.090 D	-0.596 E	27.428	1447.7
147.1	147.10	34.089 D	-0.593 E	27.427	1447.7
148.0	148.05	34.099 D	-0.588 E	27.434	1447.8
149.1	149.10	34.109 D	-0.582 E	27.442	1447.8
150.1	150.15	34.113 D	-0.576 E	27.445	1447.9
151.1	151.15	34.116 D	-0.573 E	27.448	1447.9
152.2	152.25	34.119 D	-0.572 E	27.450	1447.9
153.2	153.20	34.119 D	-0.572 E	27.451	1447.9
154.2	154.25	34.119 D	-0.568 E	27.450	1448.0
155.3	155.30	34.124 D	-0.559 E	27.454	1448.0
156.3	156.35	34.132 D	-0.553 E	27.460	1448.1
157.3	157.30	34.140 D	-0.542 E	27.466	1448.2
158.3	158.35	34.147 D	-0.535 E	27.471	1448.2
159.3	159.35	34.159 D	-0.529 E	27.480	1448.3
160.3	160.35	34.166 D	-0.518 E	27.486	1448.4
161.3	161.35	34.174 D	-0.514 E	27.492	1448.4
162.4	162.40	34.182 D	-0.505 E	27.498	1448.5
163.3	163.35	34.187 D	-0.505 E	27.502	1448.5
164.4	164.40	34.191 D	-0.498 E	27.506	1448.6
165.4	165.45	34.198 D	-0.489 E	27.511	1448.6
166.3	166.30	34.206 D	-0.484 E	27.517	1448.7
167.3	167.30	34.212 D	-0.483 E	27.521	1448.7
168.4	168.40	34.222 D	-0.473 E	27.529	1448.8
169.4	169.45	34.235 D	-0.459 E	27.539	1448.9
170.5	170.50	34.246 D	-0.450 E	27.548	1449.0
171.5	171.50	34.257 D	-0.436 E	27.556	1449.1
172.5	172.55	34.269 D	-0.424 E	27.565	1449.2
173.5	173.50	34.289 D	-0.404 E	27.581	1449.3
174.5	174.50	34.304 D	-0.393 E	27.592	1449.4
175.6	175.65	34.308 D	-0.387 E	27.595	1449.4
176.6	176.60	34.315 D	-0.386 E	27.600	1449.5
177.6	177.60	34.319 D	-0.381 E	27.603	1449.5
178.5	178.50	34.322 D	-0.377 E	27.606	1449.5
179.7	179.75	34.329 D	-0.365 E	27.611	1449.6
180.7	180.75	34.341 D	-0.359 E	27.620	1449.7
181.8	181.80	34.356 D	-0.337 E	27.631	1449.8
182.6	182.65	34.368 D	-0.327 E	27.641	1449.9
183.5	183.55	34.377 D	-0.320 E	27.648	1450.0
184.6	184.65	34.381 D	-0.311 E	27.650	1450.0
185.8	185.80	34.391 D	-0.303 E	27.658	1450.1
186.8	186.80	34.402 D	-0.292 E	27.667	1450.2
187.9	187.90	34.412 D	-0.281 E	27.674	1450.3
188.8	188.80	34.415 D	-0.272 E	27.676	1450.3
189.7	189.70	34.417 D	-0.239 E	27.676	1450.5
190.7	190.75	34.436 D	-0.221 E	27.691	1450.6
191.7	191.70	34.459 D	-0.206 E	27.708	1450.7
192.8	192.85	34.474 D	-0.202 E	27.720	1450.8
193.9	193.95	34.477 D	-0.195 E	27.722	1450.8
194.9	194.90	34.486 D	-0.187 E	27.729	1450.9
195.8	195.80	34.500 D	-0.174 E	27.740	1451.0
196.9	196.90	34.512 D	-0.167 E	27.749	1451.1
198.0	198.05	34.514 D	-0.159 E	27.750	1451.1
198.9	198.90	34.520 D	-0.154 E	27.755	1451.2
200.0	200.00	34.523 D	-0.151 E	27.758	1451.2
201.0	201.00	34.529 D	-0.146 E	27.762	1451.3
202.1	202.10	34.531 D	-0.135 E	27.763	1451.3
202.9	202.95	34.539 D	-0.127 E	27.769	1451.4
204.0	204.00	34.530 D	-0.121 E	27.762	1451.4
204.9	204.90	34.546 D	-0.120 E	27.774	1451.5

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
206.0	206.00	34.551 D	-0.113 E	27.778	1451.5


EXPERIMENT 1056
TEMPERATURE, C
-2.00
-1.25
-0.50
0.25
1.00
1.75
2.50
SALINITY 0/00
12.00
16.00
20.00
24.00
28.00
32.00
36.00
SIGMAT
10.00
13.00
16.00
19.00
22.00
25.00
28.00
DEPTH M
10
100
1000

CRUISE 15-74-013 D'IBERVILLE FIORD-74 EXPER NO. 1056

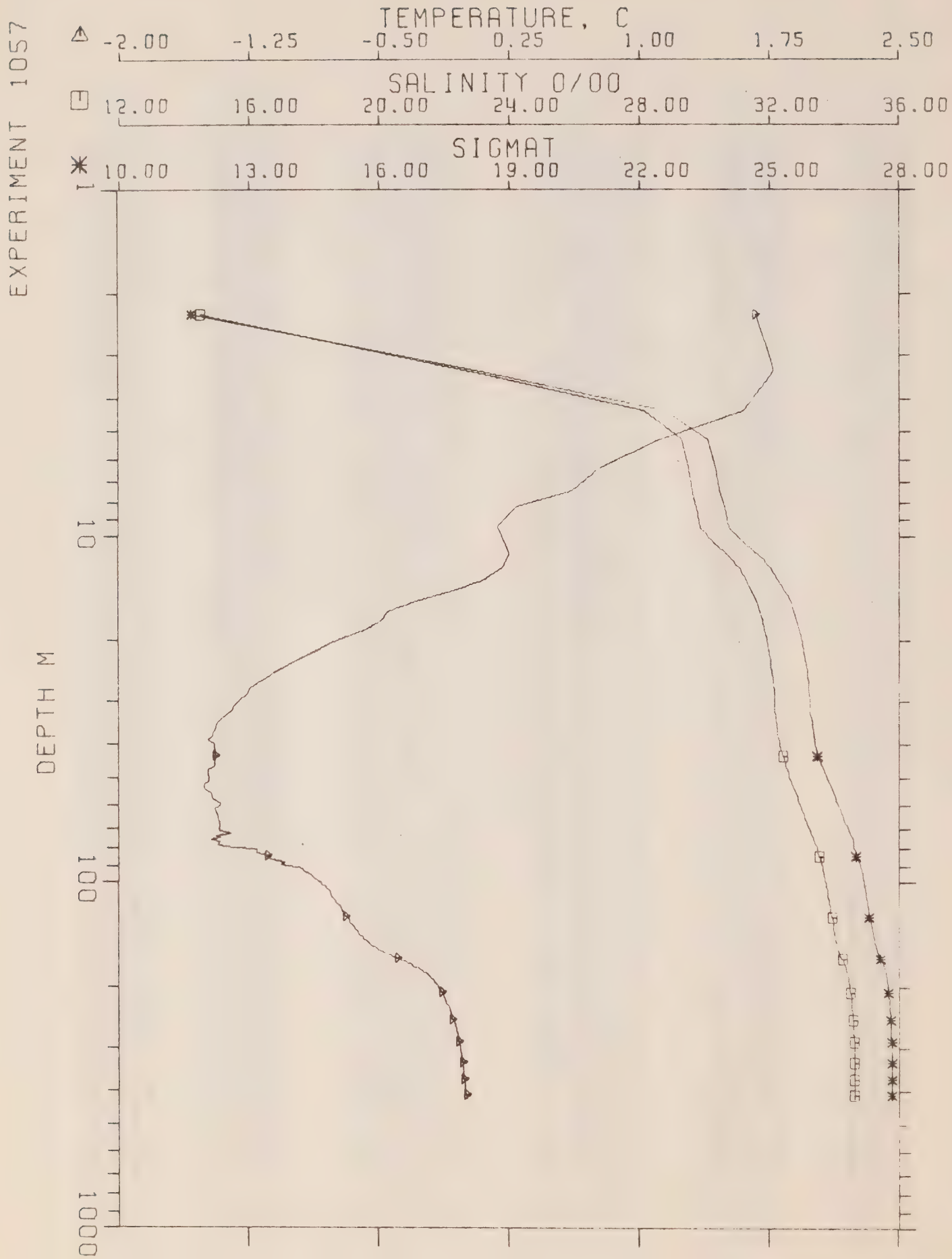
LAT N.80-33-07 LONG W.79-52-30 WATER DEPTH 222

DEPTH INCR. DATE 250874 LOCAL TIME

DEPTH	PRES	SAL		TEMP		SIGMAT	SOUND
3.1	3.10	18.840	C	1.770	D	15.117	1435.5
4.0	4.05	27.154	C	1.543	D	21.760	1445.6
5.0	5.05	28.770	C	1.125	D	23.073	1445.9
5.9	5.95	29.232	C	0.897	D	23.454	1445.5
7.0	7.05	29.645	C	0.504	D	23.803	1444.3
7.9	7.95	29.751	C	0.318	D	23.895	1443.6
9.1	9.15	29.839	C	0.330	D	23.965	1443.8
10.1	10.10	30.055	C	0.213	D	24.143	1443.6
11.1	11.10	30.422	C	0.260	D	24.437	1444.3
12.1	12.10	30.752	C	0.271	D	24.702	1444.8
13.1	13.10	31.026	C	0.268	D	24.922	1445.2
14.1	14.15	31.240	C	0.209	D	25.097	1445.3
15.0	15.05	31.417	C	0.149	D	25.242	1445.2
16.2	16.25	31.606	C	-0.033	D	25.402	1444.7
17.1	17.10	31.696	C	-0.125	D	25.477	1444.4
18.1	18.10	31.894	C	-0.414	D	25.648	1443.4
19.2	19.25	31.981	C	-0.602	D	25.725	1442.6
20.3	20.30	32.030	C	-0.722	D	25.769	1442.1
21.3	21.30	32.064	C	-0.832	D	25.800	1441.7
22.2	22.20	32.069	C	-0.870	D	25.805	1441.5
23.2	23.20	32.112	C	-0.986	D	25.843	1441.1
24.3	24.30	32.152	C	-1.063	D	25.878	1440.8
25.3	25.35	32.189	C	-1.155	D	25.910	1440.4
26.4	26.40	32.195	C	-1.204	D	25.916	1440.2
27.4	27.45	32.221	C	-1.271	D	25.939	1440.0
28.3	28.35	32.240	C	-1.312	D	25.955	1439.8
29.4	29.45	32.241	C	-1.350	D	25.958	1439.6
30.4	30.45	32.257	C	-1.383	D	25.971	1439.5
31.4	31.40	32.264	C	-1.395	D	25.977	1439.5
32.4	32.45	32.281	C	-1.425	D	25.991	1439.4
33.4	33.45	32.297	C	-1.448	D	26.005	1439.3
34.5	34.50	32.304	C	-1.457	D	26.010	1439.3
35.4	35.45	32.314	C	-1.462	D	26.019	1439.3
36.5	36.50	32.318	C	-1.465	D	26.023	1439.3
37.4	37.40	32.323	C	-1.471	D	26.026	1439.3
38.6	38.60	32.341	C	-1.473	D	26.041	1439.4
39.5	39.55	32.350	C	-1.471	D	26.048	1439.4
40.6	40.60	32.386	C	-1.455	D	26.077	1439.5
41.6	41.60	32.410	C	-1.447	D	26.096	1439.6
42.5	42.50	32.435	C	-1.441	D	26.116	1439.7
43.7	43.70	32.461	C	-1.433	D	26.137	1439.8
44.6	44.65	32.513	C	-1.423	D	26.179	1439.9
45.6	45.60	32.558	C	-1.427	D	26.216	1440.0
46.6	46.65	32.589	C	-1.417	D	26.241	1440.1
47.5	47.55	32.639	C	-1.421	D	26.281	1440.2
48.7	48.70	32.675	C	-1.422	D	26.310	1440.2
49.8	49.80	32.700	C	-1.431	D	26.331	1440.2
50.7	50.75	32.745	C	-1.436	D	26.367	1440.3
51.6	51.65	32.769	C	-1.437	D	26.387	1440.3
52.8	52.80	32.794	C	-1.431	D	26.407	1440.4
53.8	53.85	32.840	C	-1.417	D	26.444	1440.6
54.9	54.90	32.875	C	-1.449	D	26.473	1440.5
55.9	55.95	32.909	C	-1.435	D	26.500	1440.6
56.9	56.90	32.941	C	-1.435	D	26.526	1440.7
57.9	57.90	32.976	C	-1.441	D	26.555	1440.7
58.7	58.75	33.005	C	-1.442	D	26.578	1440.8
59.9	59.95	33.023	C	-1.438	D	26.593	1440.8
60.9	60.90	33.058	C	-1.424	D	26.620	1441.0
61.8	61.85	33.089	C	-1.422	D	26.646	1441.0
63.0	63.05	33.110	C	-1.387	D	26.662	1441.2
63.9	63.90	33.138	C	-1.363	D	26.683	1441.4
65.0	65.05	33.177	C	-1.323	D	26.714	1441.7

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
66.0	66.00	33.209 C	-1.346 D	26.741	1441.6
67.0	67.00	33.232 C	-1.338 D	26.759	1441.7
68.1	68.15	33.243 C	-1.333 D	26.768	1441.8
69.0	69.00	33.293 C	-1.310 D	26.808	1442.0
70.1	70.10	33.331 C	-1.296 D	26.838	1442.1
71.2	71.20	33.367 C	-1.312 D	26.868	1442.1
72.1	72.15	33.379 C	-1.224 D	26.875	1442.5
73.2	73.20	33.414 C	-1.284 D	26.905	1442.3
74.1	74.10	33.429 C	-1.198 D	26.914	1442.8
75.2	75.25	33.453 C	-1.176 D	26.934	1442.9
76.2	76.25	33.466 C	-1.185 D	26.944	1442.9
77.3	77.30	33.495 C	-1.152 D	26.966	1443.1
78.2	78.25	33.515 C	-1.181 D	26.983	1443.0
79.2	79.20	33.527 C	-1.174 D	26.993	1443.1
80.3	80.35	33.539 C	-1.126 D	27.001	1443.4
81.3	81.30	33.569 C	-1.117 D	27.026	1443.5
82.3	82.30	33.563 C	-1.067 D	27.019	1443.7
83.3	83.30	33.593 C	-1.011 D	27.042	1444.0
84.5	84.55	33.617 C	-1.017 D	27.061	1444.0
85.5	85.50	33.637 C	-1.003 D	27.077	1444.2
86.5	86.50	33.648 C	-0.957 D	27.084	1444.4
87.5	87.50	33.665 C	-0.939 D	27.098	1444.5
88.5	88.55	33.683 C	-0.924 D	27.111	1444.6
89.7	89.70	33.701 C	-0.908 D	27.125	1444.8
90.5	90.55	33.717 C	-0.895 D	27.137	1444.8
91.5	91.55	33.729 C	-0.886 D	27.147	1444.9
92.5	92.55	33.738 C	-0.876 D	27.154	1445.0
93.8	93.75	33.741 C	-0.873 D	27.157	1445.0
94.6	94.65	33.757 C	-0.865 D	27.169	1445.1
95.6	95.65	33.760 C	-0.856 D	27.171	1445.2
96.6	96.60	33.770 C	-0.853 D	27.179	1445.2
97.8	97.80	33.778 C	-0.844 D	27.185	1445.3
98.7	98.70	33.790 C	-0.833 D	27.194	1445.4
99.6	99.65	33.800 C	-0.827 D	27.202	1445.4
100.8	100.80	33.806 D	-0.824 E	27.207	1445.5
101.7	101.70	33.809 D	-0.819 E	27.209	1445.5
102.8	102.85	33.818 D	-0.810 E	27.217	1445.6
103.8	103.85	33.826 D	-0.807 E	27.223	1445.6
104.8	104.85	33.828 D	-0.804 E	27.224	1445.7
105.9	105.90	33.838 D	-0.793 E	27.232	1445.7
106.9	106.90	33.850 D	-0.783 E	27.241	1445.8
107.9	107.90	33.857 D	-0.781 E	27.247	1445.9
108.8	108.85	33.864 D	-0.775 E	27.252	1445.9
109.9	109.95	33.868 D	-0.771 E	27.255	1446.0
110.9	110.90	33.874 D	-0.769 E	27.260	1446.0
112.1	112.10	33.881 D	-0.763 E	27.265	1446.0
112.9	112.95	33.886 D	-0.760 E	27.269	1446.1
114.1	114.15	33.889 D	-0.758 E	27.271	1446.1
115.0	115.05	33.897 D	-0.753 E	27.278	1446.2
116.0	116.05	33.901 D	-0.748 E	27.281	1446.2
117.1	117.10	33.906 D	-0.745 E	27.285	1446.2
118.1	118.15	33.911 D	-0.742 E	27.289	1446.3
119.2	119.20	33.911 D	-0.739 E	27.289	1446.3
120.3	120.30	33.915 D	-0.739 E	27.292	1446.3
121.3	121.30	33.915 D	-0.737 E	27.292	1446.4
122.2	122.25	33.917 D	-0.732 E	27.294	1446.4
123.1	123.15	33.927 D	-0.727 E	27.301	1446.5
124.2	124.25	33.931 D	-0.722 E	27.304	1446.5
125.2	125.25	33.938 D	-0.718 E	27.309	1446.6
126.2	126.25	33.948 D	-0.708 E	27.317	1446.6
127.2	127.25	33.955 D	-0.702 E	27.323	1446.7
128.2	128.25	33.961 D	-0.700 E	27.327	1446.7
129.3	129.30	33.966 D	-0.696 E	27.331	1446.8
130.4	130.40	33.974 D	-0.690 E	27.338	1446.8
131.4	131.40	33.984 D	-0.677 E	27.345	1446.9
132.3	132.30	33.991 D	-0.672 E	27.351	1447.0
133.3	133.35	33.996 D	-0.667 E	27.355	1447.0
134.5	134.50	34.000 D	-0.661 E	27.358	1447.1
135.6	135.60	34.007 D	-0.656 E	27.363	1447.1

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
136.6	136.60	34.014	D	-0.651	E	27.368	1447.2
137.5	137.50	34.020	D	-0.649	E	27.373	1447.2
138.4	138.45	34.025	D	-0.644	E	27.377	1447.2
139.7	139.70	34.030	D	-0.635	E	27.381	1447.3
140.6	140.65	34.040	D	-0.626	E	27.389	1447.4
141.6	141.60	34.049	D	-0.622	E	27.396	1447.4
142.5	142.55	34.058	D	-0.616	E	27.403	1447.5
143.7	143.75	34.062	D	-0.611	E	27.406	1447.5
144.7	144.70	34.069	D	-0.606	E	27.411	1447.6
145.7	145.75	34.078	D	-0.599	E	27.418	1447.6
146.7	146.75	34.082	D	-0.596	E	27.421	1447.7
147.6	147.65	34.086	D	-0.593	E	27.424	1447.7
148.9	148.90	34.091	D	-0.587	E	27.428	1447.8
149.8	149.85	34.096	D	-0.580	E	27.432	1447.8
150.9	150.90	34.107	D	-0.570	E	27.440	1447.9
151.9	151.95	34.114	D	-0.561	E	27.445	1448.0
152.8	152.80	34.129	D	-0.553	E	27.457	1448.0
153.8	153.80	34.138	D	-0.550	E	27.464	1448.1
155.0	155.00	34.142	D	-0.543	E	27.468	1448.1
156.0	156.05	34.149	D	-0.533	E	27.473	1448.2
156.9	156.95	34.157	D	-0.525	E	27.479	1448.3
158.0	158.05	34.163	D	-0.521	E	27.484	1448.3
159.0	159.00	34.170	D	-0.515	E	27.489	1448.4
159.9	159.95	34.183	D	-0.506	E	27.499	1448.4
161.0	161.05	34.188	D	-0.500	E	27.503	1448.5
162.0	162.05	34.194	D	-0.491	E	27.507	1448.6
163.1	163.15	34.215	D	-0.476	E	27.524	1448.7
164.0	164.00	34.223	D	-0.468	E	27.530	1448.7
165.0	165.05	34.232	D	-0.461	E	27.536	1448.8
166.1	166.15	34.243	D	-0.440	E	27.545	1448.9
167.2	167.25	34.262	D	-0.425	E	27.559	1449.1
168.1	168.10	34.273	D	-0.420	E	27.568	1449.1
169.1	169.10	34.279	D	-0.412	E	27.573	1449.2
170.3	170.35	34.285	D	-0.409	E	27.577	1449.2
171.2	171.20	34.293	D	-0.405	E	27.584	1449.3
172.2	172.25	34.302	D	-0.383	E	27.590	1449.4
173.3	173.35	34.317	D	-0.374	E	27.602	1449.5
174.3	174.30	34.333	D	-0.350	E	27.613	1449.6
175.5	175.50	34.342	D	-0.331	E	27.620	1449.7
176.4	176.45	34.363	D	-0.322	E	27.637	1449.8
177.4	177.40	34.370	D	-0.322	E	27.642	1449.8
178.6	178.60	34.375	D	-0.313	E	27.646	1449.9
179.4	179.45	34.385	D	-0.305	E	27.654	1450.0
180.5	180.55	34.392	D	-0.295	E	27.659	1450.1
181.5	181.55	34.399	D	-0.289	E	27.664	1450.1
182.5	182.55	34.408	D	-0.278	E	27.670	1450.2
183.4	183.45	34.414	D	-0.270	E	27.675	1450.2
184.6	184.60	34.425	D	-0.260	E	27.684	1450.3
185.6	185.60	34.431	D	-0.256	E	27.688	1450.4
186.6	186.65	34.433	D	-0.249	E	27.689	1450.4
187.6	187.60	34.442	D	-0.244	E	27.697	1450.5
188.6	188.65	34.444	D	-0.238	E	27.698	1450.5
189.7	189.75	34.453	D	-0.225	E	27.704	1450.6
190.9	190.90	34.463	D	-0.217	E	27.712	1450.7
191.8	191.85	34.467	D	-0.212	E	27.715	1450.7
192.8	192.85	34.472	D	-0.208	E	27.719	1450.8
193.9	193.95	34.477	D	-0.203	E	27.723	1450.8
194.9	194.95	34.483	D	-0.200	E	27.728	1450.9
195.9	195.90	34.485	D	-0.195	E	27.729	1450.9
196.8	196.85	34.487	D	-0.188	E	27.730	1450.9
197.9	197.95	34.498	D	-0.177	E	27.739	1451.0
198.9	198.95	34.504	D	-0.174	E	27.743	1451.1
200.0	200.00	34.508	D	-0.170	E	27.746	1451.1
200.9	200.95	34.510	D	-0.167	E	27.747	1451.1
201.9	201.95	34.511	D	-0.166	E	27.748	1451.2


EXPERIMENT 1057
TEMPERATURE, C
-2.00
-1.25
-0.50
0.25
1.00
1.75
2.50
SALINITY 0/00
12.00
16.00
20.00
24.00
28.00
32.00
36.00
SIGMAT
10.00
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16.00
19.00
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DEPTH M
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1000

CRUISE 15-74-013 D'IBERVILLE FIORD-74 EXPER NO. 1057

LAT N.80-35-55 LONG W.79-31-00 WATER DEPTH 501

DEPTH INCR. DATE 250874 LOCAL TIME

DEPTH	PRES	SAL		TEMP		SIGMAT	SOUND
2.3	2.30	14.513	C	1.665	D	11.674	1429.3
3.3	3.35	22.891	C	1.782	D	18.345	1440.9
4.3	4.35	28.181	C	1.611	D	22.577	1447.3
5.2	5.25	29.375	C	1.131	D	23.557	1446.8
6.3	6.35	29.573	C	0.780	D	23.733	1445.5
7.4	7.40	29.667	C	0.616	D	23.815	1444.8
8.2	8.20	29.817	C	0.306	D	23.948	1443.6
9.4	9.40	29.915	C	0.183	D	24.032	1443.2
10.4	10.45	30.359	C	0.219	D	24.388	1444.0
11.4	11.45	30.811	C	0.261	D	24.750	1444.9
12.3	12.35	31.129	C	0.223	D	25.007	1445.1
13.5	13.50	31.352	C	0.111	D	25.191	1445.0
14.4	14.40	31.532	C	-0.066	D	25.343	1444.4
15.5	15.50	31.675	C	-0.275	D	25.467	1443.7
16.6	16.60	31.769	C	-0.443	D	25.549	1443.0
17.4	17.45	31.831	C	-0.467	D	25.600	1443.0
18.5	18.55	31.894	C	-0.549	D	25.653	1442.7
19.5	19.50	31.961	C	-0.676	D	25.711	1442.3
20.5	20.55	32.011	C	-0.784	D	25.755	1441.8
21.5	21.55	32.034	C	-0.860	D	25.776	1441.5
22.5	22.55	32.071	C	-0.940	D	25.808	1441.2
23.6	23.65	32.097	C	-1.013	D	25.831	1440.9
24.6	24.65	32.134	C	-1.088	D	25.864	1440.6
25.6	25.65	32.149	C	-1.137	D	25.877	1440.5
26.6	26.65	32.172	C	-1.191	D	25.898	1440.3
27.5	27.55	32.192	C	-1.232	D	25.915	1440.1
28.7	28.70	32.188	C	-1.256	D	25.912	1440.0
29.7	29.75	32.207	C	-1.293	D	25.928	1439.9
30.7	30.70	32.208	C	-1.326	D	25.930	1439.7
31.8	31.80	32.210	C	-1.341	D	25.932	1439.7
32.7	32.70	32.224	C	-1.372	D	25.944	1439.6
33.6	33.65	32.249	C	-1.399	D	25.965	1439.5
34.6	34.65	32.263	C	-1.429	D	25.977	1439.4
35.7	35.70	32.286	C	-1.437	D	25.995	1439.4
36.7	36.75	32.300	C	-1.445	D	26.007	1439.4
37.8	37.85	32.321	C	-1.460	D	26.025	1439.4
38.8	38.85	32.344	C	-1.487	D	26.044	1439.3
39.8	39.85	32.363	C	-1.455	D	26.059	1439.5
40.9	40.90	32.393	C	-1.453	D	26.083	1439.6
41.9	41.95	32.420	C	-1.446	D	26.104	1439.6
43.0	43.00	32.439	C	-1.444	D	26.120	1439.7
43.9	43.95	32.466	C	-1.442	D	26.142	1439.8
45.0	45.00	32.507	C	-1.445	D	26.175	1439.8
46.0	46.05	32.534	C	-1.442	D	26.197	1439.9
47.0	47.00	32.587	C	-1.472	D	26.240	1439.8
48.0	48.00	32.628	C	-1.486	D	26.274	1439.8
49.0	49.05	32.658	C	-1.491	D	26.298	1439.9
50.1	50.10	32.691	C	-1.485	D	26.325	1440.0
51.2	51.20	32.733	C	-1.484	D	26.359	1440.1
52.1	52.15	32.776	C	-1.505	D	26.395	1440.0
53.0	53.05	32.813	C	-1.513	D	26.424	1440.1
54.0	54.05	32.848	C	-1.516	D	26.453	1440.1
55.1	55.15	32.866	C	-1.479	D	26.466	1440.3
56.2	56.25	32.902	C	-1.467	D	26.496	1440.5
57.2	57.25	32.940	C	-1.468	D	26.526	1440.5
58.2	58.20	32.952	C	-1.437	D	26.535	1440.7
59.1	59.15	32.991	C	-1.407	D	26.566	1440.9
60.3	60.30	33.024	C	-1.412	D	26.593	1441.0
61.2	61.25	33.050	C	-1.455	D	26.615	1440.8
62.2	62.20	33.076	C	-1.449	D	26.635	1440.9
63.3	63.35	33.102	C	-1.444	D	26.657	1441.0
64.4	64.40	33.127	C	-1.439	D	26.677	1441.0

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
65.3	65.30	33.153 C	-1.428 D	26.697	1441.1
66.4	66.40	33.180 C	-1.427 D	26.720	1441.2
67.4	67.45	33.211 C	-1.422 D	26.745	1441.3
68.4	68.40	33.241 C	-1.416 D	26.768	1441.4
69.4	69.40	33.270 C	-1.415 D	26.792	1441.4
70.5	70.55	33.303 C	-1.421 D	26.819	1441.5
71.4	71.40	33.328 C	-1.419 D	26.839	1441.5
72.3	72.35	33.354 C	-1.346 D	26.858	1441.9
73.4	73.40	33.391 C	-1.443 D	26.890	1441.5
74.4	74.40	33.419 C	-1.407 D	26.913	1441.8
75.5	75.55	33.446 C	-1.475 D	26.936	1441.5
76.5	76.55	33.453 C	-1.418 D	26.940	1441.8
77.6	77.60	33.479 C	-1.422 D	26.961	1441.8
78.6	78.60	33.501 C	-1.437 D	26.979	1441.8
79.7	79.70	33.484 C	-1.338 D	26.963	1442.3
80.6	80.65	33.512 C	-1.216 D	26.983	1442.9
81.7	81.70	33.538 C	-1.205 D	27.003	1443.0
82.7	82.70	33.554 C	-1.211 D	27.016	1443.0
83.7	83.75	33.567 C	-1.144 D	27.025	1443.4
84.8	84.80	33.591 C	-1.149 D	27.044	1443.4
85.7	85.75	33.603 C	-1.126 D	27.053	1443.5
86.7	86.75	33.627 C	-1.085 D	27.071	1443.8
87.8	87.85	33.638 C	-1.040 D	27.078	1444.0
88.8	88.80	33.661 C	-1.067 D	27.098	1443.9
89.8	89.80	33.662 C	-1.029 D	27.098	1444.1
90.9	90.90	33.676 C	-0.974 D	27.107	1444.4
91.8	91.85	33.693 C	-0.948 D	27.120	1444.6
92.9	92.95	33.709 C	-0.942 D	27.133	1444.7
94.9	94.90	33.733 C	-0.903 D	27.151	1444.9
95.9	95.95	33.742 C	-0.893 D	27.158	1445.0
96.8	96.85	33.752 C	-0.879 D	27.165	1445.1
98.0	98.00	33.762 C	-0.864 D	27.173	1445.2
98.9	98.90	33.771 C	-0.857 D	27.180	1445.2
100.0	100.00	33.781 C	-0.845 D	27.187	1445.3
101.1	101.10	33.788 D	-0.834 E	27.193	1445.4
102.0	102.00	33.801 D	-0.823 E	27.203	1445.5
103.2	103.20	33.813 D	-0.811 E	27.213	1445.6
104.1	104.10	33.823 D	-0.806 E	27.220	1445.6
105.3	105.30	33.828 D	-0.798 E	27.224	1445.7
106.1	106.15	33.839 D	-0.792 E	27.232	1445.8
107.2	107.20	33.847 D	-0.786 E	27.239	1445.8
108.2	108.25	33.852 D	-0.783 E	27.243	1445.9
109.3	109.30	33.859 D	-0.781 E	27.248	1445.9
110.3	110.35	33.861 D	-0.777 E	27.250	1445.9
111.2	111.25	33.870 D	-0.773 E	27.257	1446.0
112.3	112.30	33.877 D	-0.763 E	27.262	1446.0
113.4	113.45	33.885 D	-0.757 E	27.269	1446.1
114.4	114.40	33.895 D	-0.753 E	27.276	1446.2
115.3	115.35	33.902 D	-0.747 E	27.282	1446.2
116.4	116.45	33.910 D	-0.734 E	27.288	1446.3
117.4	117.45	33.917 D	-0.729 E	27.293	1446.3
118.4	118.40	33.924 D	-0.724 E	27.298	1446.4
119.3	119.30	33.928 D	-0.724 E	27.302	1446.4
120.3	120.35	33.933 D	-0.719 E	27.306	1446.5
121.4	121.45	33.937 D	-0.714 E	27.309	1446.5
122.5	122.50	33.942 D	-0.710 E	27.313	1446.6
123.5	123.55	33.948 D	-0.706 E	27.318	1446.6
124.6	124.65	33.953 D	-0.699 E	27.321	1446.7
125.6	125.65	33.957 D	-0.698 E	27.324	1446.7
126.7	126.75	33.962 D	-0.689 E	27.328	1446.7
127.6	127.65	33.970 D	-0.683 E	27.334	1446.8
128.5	128.55	33.976 D	-0.679 E	27.339	1446.8
129.5	129.55	33.983 D	-0.673 E	27.345	1446.9
130.6	130.65	33.987 D	-0.670 E	27.347	1446.9
131.7	131.75	33.989 D	-0.670 E	27.349	1447.0
132.7	132.75	33.991 D	-0.667 E	27.350	1447.0
133.8	133.80	33.997 D	-0.659 E	27.355	1447.0
134.8	134.80	34.005 D	-0.651 E	27.361	1447.1
135.8	135.85	34.011 D	-0.645 F	27.365	1447.2

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
136.9	136.90	34.017	D	-0.640	E	27.371	1447.2
137.8	137.85	34.030	D	-0.635	E	27.381	1447.3
138.9	138.90	34.032	D	-0.632	E	27.382	1447.3
139.8	139.85	34.037	D	-0.629	E	27.386	1447.3
140.9	140.95	34.042	D	-0.623	E	27.390	1447.4
141.9	141.95	34.048	D	-0.618	E	27.394	1447.4
142.9	142.95	34.054	D	-0.609	E	27.399	1447.5
143.8	143.85	34.064	D	-0.604	E	27.407	1447.6
144.9	144.95	34.069	D	-0.599	E	27.411	1447.6
145.8	145.85	34.076	D	-0.594	E	27.416	1447.7
146.9	146.90	34.084	D	-0.585	E	27.423	1447.7
148.0	148.00	34.093	D	-0.577	E	27.430	1447.8
148.9	148.95	34.100	D	-0.572	E	27.435	1447.8
150.0	150.00	34.108	D	-0.565	E	27.441	1447.9
151.1	151.15	34.113	D	-0.561	E	27.445	1448.0
152.2	152.25	34.119	D	-0.552	E	27.450	1448.0
153.2	153.20	34.129	D	-0.541	E	27.457	1448.1
154.2	154.20	34.139	D	-0.532	E	27.465	1448.2
155.2	155.25	34.148	D	-0.524	E	27.472	1448.2
156.2	156.20	34.159	D	-0.515	E	27.480	1448.3
157.1	157.15	34.169	D	-0.508	E	27.488	1448.4
158.2	158.25	34.181	D	-0.497	E	27.497	1448.5
159.3	159.30	34.190	D	-0.486	E	27.504	1448.5
160.3	160.35	34.202	D	-0.473	E	27.513	1448.6
161.2	161.20	34.218	D	-0.460	E	27.526	1448.7
162.2	162.25	34.237	D	-0.441	E	27.540	1448.9
163.3	163.35	34.248	D	-0.434	E	27.549	1448.9
164.5	164.50	34.263	D	-0.417	E	27.560	1449.0
165.4	165.40	34.280	D	-0.404	E	27.573	1449.1
166.4	166.40	34.294	D	-0.393	E	27.584	1449.2
167.3	167.35	34.307	D	-0.378	E	27.593	1449.3
168.5	168.55	34.321	D	-0.367	E	27.604	1449.4
169.5	169.55	34.326	D	-0.357	E	27.608	1449.5
170.5	170.55	34.338	D	-0.344	E	27.618	1449.6
171.4	171.45	34.353	D	-0.331	E	27.629	1449.7
172.6	172.60	34.367	D	-0.319	E	27.639	1449.8
173.5	173.50	34.375	D	-0.312	E	27.646	1449.8
174.5	174.50	34.380	D	-0.309	E	27.649	1449.9
175.6	175.65	34.390	D	-0.297	E	27.657	1450.0
176.6	176.65	34.397	D	-0.286	E	27.662	1450.0
177.7	177.70	34.406	D	-0.276	E	27.669	1450.1
178.7	178.70	34.417	D	-0.269	E	27.678	1450.2
179.7	179.75	34.421	D	-0.260	E	27.680	1450.2
180.6	180.60	34.433	D	-0.251	E	27.690	1450.3
181.8	181.80	34.438	D	-0.247	E	27.693	1450.4
182.9	182.90	34.444	D	-0.240	E	27.698	1450.4
183.7	183.75	34.451	D	-0.232	E	27.703	1450.5
184.7	184.75	34.457	D	-0.224	E	27.708	1450.5
185.7	185.70	34.464	D	-0.219	E	27.713	1450.6
186.8	186.85	34.469	D	-0.215	E	27.717	1450.6
188.0	188.00	34.470	D	-0.210	E	27.717	1450.7
188.9	188.95	34.476	D	-0.205	E	27.722	1450.7
190.0	190.00	34.480	D	-0.199	E	27.725	1450.8
191.0	191.05	34.490	D	-0.194	E	27.733	1450.8
192.1	192.10	34.495	D	-0.191	E	27.736	1450.9
193.0	193.05	34.493	D	-0.188	E	27.735	1450.9
194.0	194.00	34.498	D	-0.185	E	27.739	1450.9
195.0	195.00	34.501	D	-0.182	E	27.741	1451.0
195.9	195.95	34.505	D	-0.177	E	27.744	1451.0
197.0	197.05	34.508	D	-0.174	E	27.747	1451.0
198.0	198.00	34.512	D	-0.170	E	27.749	1451.1
199.1	199.10	34.512	D	-0.168	E	27.749	1451.1
200.1	200.15	34.515	D	-0.164	E	27.752	1451.1
201.3	201.30	34.518	D	-0.161	E	27.754	1451.2
202.1	202.10	34.521	D	-0.159	E	27.756	1451.2
203.2	203.20	34.521	D	-0.156	E	27.756	1451.2
204.2	204.25	34.526	D	-0.154	E	27.760	1451.3
205.3	205.30	34.527	D	-0.149	E	27.760	1451.3
206.2	206.25	34.533	D	-0.146	E	27.765	1451.4

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
207.4	207.40	34.533	D	-0.142	E	27.765	1451.4
208.2	208.25	34.538	D	-0.140	E	27.769	1451.4
209.4	209.45	34.539	D	-0.138	E	27.770	1451.5
210.3	210.35	34.543	D	-0.137	E	27.773	1451.5
211.3	211.30	34.543	D	-0.135	E	27.773	1451.5
212.5	212.55	34.543	D	-0.133	E	27.773	1451.5
213.5	213.50	34.544	D	-0.132	E	27.774	1451.6
214.5	214.50	34.546	D	-0.129	E	27.775	1451.6
215.4	215.45	34.548	D	-0.129	E	27.777	1451.6
216.5	216.55	34.550	D	-0.126	E	27.778	1451.6
217.6	217.60	34.550	D	-0.123	E	27.778	1451.7
218.7	218.70	34.554	D	-0.122	E	27.781	1451.7
219.5	219.55	34.558	D	-0.122	E	27.784	1451.7
220.6	220.65	34.554	D	-0.119	E	27.781	1451.7
221.7	221.75	34.557	D	-0.119	E	27.784	1451.8
222.6	222.65	34.558	D	-0.116	E	27.784	1451.8
223.6	223.65	34.560	D	-0.116	E	27.786	1451.8
224.6	224.65	34.562	D	-0.114	E	27.787	1451.8
225.6	225.65	34.564	D	-0.112	E	27.789	1451.9
226.7	226.70	34.566	D	-0.109	E	27.790	1451.9
227.7	227.70	34.569	D	-0.106	E	27.793	1451.9
228.8	228.85	34.571	D	-0.103	E	27.794	1452.0
229.8	229.80	34.572	D	-0.099	E	27.794	1452.0
230.9	230.90	34.577	D	-0.098	E	27.798	1452.0
231.7	231.75	34.579	D	-0.095	E	27.800	1452.1
232.9	232.95	34.581	D	-0.093	E	27.802	1452.1
233.8	233.80	34.581	D	-0.092	E	27.802	1452.1
234.9	234.95	34.585	D	-0.092	E	27.804	1452.1
235.8	235.80	34.586	D	-0.092	E	27.805	1452.2
237.1	237.10	34.585	D	-0.087	E	27.804	1452.2
238.1	238.10	34.586	D	-0.086	E	27.805	1452.2
239.0	239.05	34.590	D	-0.087	E	27.808	1452.2
240.1	240.10	34.589	D	-0.084	E	27.807	1452.3
241.1	241.15	34.590	D	-0.085	E	27.809	1452.3
242.0	242.05	34.592	D	-0.084	E	27.810	1452.3
243.1	243.10	34.593	D	-0.083	E	27.810	1452.3
244.1	244.10	34.593	D	-0.081	E	27.810	1452.4
245.2	245.25	34.593	D	-0.079	E	27.810	1452.4
246.3	246.30	34.596	D	-0.079	E	27.813	1452.4
247.1	247.15	34.599	D	-0.079	E	27.815	1452.4
248.2	248.25	34.599	D	-0.077	E	27.815	1452.5
249.2	249.25	34.600	D	-0.076	E	27.816	1452.5
250.2	250.25	34.601	D	-0.074	E	27.817	1452.5
251.3	251.35	34.601	D	-0.073	E	27.816	1452.5
252.3	252.35	34.602	D	-0.072	E	27.817	1452.5
253.3	253.35	34.603	D	-0.072	E	27.818	1452.6
254.4	254.40	34.603	D	-0.069	E	27.818	1452.6
255.4	255.40	34.605	D	-0.069	E	27.820	1452.6
256.3	256.35	34.608	D	-0.068	E	27.822	1452.6
257.3	257.35	34.609	D	-0.066	E	27.823	1452.7
258.6	258.60	34.609	D	-0.065	E	27.823	1452.7
259.4	259.45	34.611	D	-0.065	E	27.824	1452.7
260.5	260.50	34.610	D	-0.063	E	27.823	1452.7
261.5	261.55	34.614	D	-0.063	E	27.826	1452.8
262.5	262.55	34.613	D	-0.062	E	27.826	1452.8
263.5	263.50	34.612	D	-0.060	E	27.825	1452.8
264.7	264.70	34.614	D	-0.060	E	27.826	1452.8
265.5	265.55	34.614	D	-0.059	E	27.826	1452.8
266.7	266.75	34.615	D	-0.058	E	27.827	1452.9
267.7	267.75	34.614	D	-0.055	E	27.826	1452.9
268.7	268.70	34.615	D	-0.055	E	27.827	1452.9
269.7	269.75	34.617	D	-0.055	E	27.828	1452.9
270.6	270.60	34.618	D	-0.054	E	27.829	1452.9
271.8	271.80	34.617	D	-0.051	E	27.828	1453.0
272.7	272.70	34.617	D	-0.049	E	27.828	1453.0
273.9	273.90	34.620	D	-0.049	E	27.831	1453.0
274.8	274.80	34.620	D	-0.049	E	27.831	1453.0
275.9	275.90	34.622	D	-0.049	E	27.832	1453.1
276.9	276.95	34.621	D	-0.047	E	27.831	1453.1

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
277.9	277.90	34.622	D	-0.047	E	27.832	1453.1
279.0	279.00	34.620	D	-0.044	E	27.831	1453.1
279.9	279.95	34.622	D	-0.045	E	27.832	1453.1
281.0	281.00	34.624	D	-0.044	E	27.833	1453.2
281.9	281.90	34.624	D	-0.044	E	27.834	1453.2
283.1	283.10	34.623	D	-0.043	E	27.832	1453.2
284.1	284.10	34.621	D	-0.041	E	27.831	1453.2
285.0	285.00	34.627	D	-0.043	E	27.836	1453.2
286.1	286.15	34.627	D	-0.042	E	27.836	1453.3
287.0	287.05	34.625	D	-0.041	E	27.834	1453.3
288.1	288.10	34.626	D	-0.041	E	27.835	1453.3
289.2	289.20	34.627	D	-0.041	E	27.836	1453.3
290.0	290.05	34.627	D	-0.040	E	27.835	1453.3
291.2	291.20	34.628	D	-0.041	E	27.837	1453.4
292.2	292.25	34.627	D	-0.040	E	27.836	1453.4
293.3	293.30	34.625	D	-0.038	E	27.834	1453.4
294.2	294.25	34.627	D	-0.039	E	27.836	1453.4
295.3	295.35	34.629	D	-0.039	E	27.838	1453.4
296.3	296.30	34.626	D	-0.038	E	27.835	1453.5
297.3	297.35	34.627	D	-0.038	E	27.836	1453.5
298.4	298.40	34.628	D	-0.037	E	27.837	1453.5
299.5	299.55	34.628	D	-0.036	E	27.836	1453.5
300.3	300.30	34.629	D	-0.036	E	27.837	1453.5
301.5	301.50	34.629	D	-0.035	E	27.837	1453.6
302.5	302.55	34.629	D	-0.035	E	27.837	1453.6
303.6	303.65	34.629	D	-0.034	E	27.837	1453.6
304.4	304.40	34.630	D	-0.033	E	27.838	1453.6
305.5	305.50	34.630	D	-0.033	E	27.838	1453.6
306.7	306.70	34.629	D	-0.032	E	27.837	1453.7
307.6	307.60	34.631	D	-0.033	E	27.839	1453.7
308.5	308.55	34.631	D	-0.031	E	27.839	1453.7
309.5	309.55	34.632	D	-0.032	E	27.839	1453.7
310.7	310.70	34.633	D	-0.032	E	27.840	1453.7
311.6	311.65	34.631	D	-0.030	E	27.839	1453.8
312.7	312.70	34.631	D	-0.029	E	27.838	1453.8
313.7	313.70	34.633	D	-0.030	E	27.840	1453.8
314.8	314.80	34.632	D	-0.029	E	27.840	1453.8
315.7	315.75	34.634	D	-0.028	E	27.841	1453.8
316.8	316.85	34.632	D	-0.027	E	27.839	1453.9
317.9	317.90	34.633	D	-0.027	E	27.840	1453.9
318.7	318.70	34.635	D	-0.027	E	27.842	1453.9
319.8	319.85	34.632	D	-0.025	E	27.839	1453.9
320.9	320.95	34.633	D	-0.024	E	27.840	1453.9
322.0	322.00	34.633	D	-0.022	E	27.840	1454.0
323.0	323.05	34.634	D	-0.023	E	27.840	1454.0
323.9	323.90	34.635	D	-0.025	E	27.842	1454.0
324.9	324.95	34.637	D	-0.024	E	27.843	1454.0
325.9	325.95	34.637	D	-0.022	E	27.843	1454.0
327.1	327.10	34.633	D	-0.021	E	27.840	1454.0
328.0	328.05	34.634	D	-0.021	E	27.841	1454.1
329.0	329.00	34.635	D	-0.021	E	27.841	1454.1
330.1	330.10	34.636	D	-0.022	E	27.842	1454.1
331.1	331.10	34.638	D	-0.023	E	27.843	1454.1
332.0	332.05	34.637	D	-0.022	E	27.843	1454.1
333.2	333.20	34.634	D	-0.020	E	27.841	1454.2
334.3	334.30	34.637	D	-0.020	E	27.843	1454.2
335.1	335.15	34.636	D	-0.020	E	27.842	1454.2
336.3	336.30	34.636	D	-0.019	E	27.842	1454.2
337.3	337.35	34.635	D	-0.019	E	27.841	1454.2
338.4	338.40	34.636	D	-0.018	E	27.842	1454.3
339.2	339.25	34.637	D	-0.019	E	27.843	1454.3
340.3	340.30	34.638	D	-0.019	E	27.843	1454.3
341.4	341.40	34.636	D	-0.018	E	27.842	1454.3
342.3	342.35	34.638	D	-0.018	E	27.844	1454.3
343.3	343.30	34.638	D	-0.018	E	27.843	1454.3
344.3	344.35	34.638	D	-0.018	E	27.844	1454.4
345.4	345.45	34.636	D	-0.016	E	27.842	1454.4
346.4	346.40	34.638	D	-0.016	E	27.843	1454.4
347.3	347.35	34.638	D	-0.017	E	27.844	1454.4

DEPTH	PRESS	SAL		TEMP		SIGMAT	SOUND
348.4	348.40	34.638	D	-0.016	E	27.844	1454.4
349.4	349.40	34.639	D	-0.016	E	27.844	1454.4
350.4	350.45	34.638	D	-0.016	E	27.844	1454.5
351.5	351.50	34.639	D	-0.016	E	27.844	1454.5
352.5	352.50	34.640	D	-0.016	E	27.845	1454.5
353.5	353.50	34.638	D	-0.015	E	27.844	1454.5
354.6	354.65	34.638	D	-0.014	E	27.843	1454.5
355.7	355.70	34.637	D	-0.014	E	27.843	1454.6
356.7	356.75	34.637	D	-0.013	E	27.842	1454.6
357.6	357.65	34.640	D	-0.014	E	27.845	1454.6
358.6	358.65	34.639	D	-0.013	E	27.844	1454.6
359.9	359.90	34.637	D	-0.012	E	27.842	1454.6
360.8	360.80	34.639	D	-0.012	E	27.844	1454.7
361.8	361.85	34.640	D	-0.012	E	27.845	1454.7
362.9	362.95	34.640	D	-0.013	E	27.845	1454.7
363.9	363.95	34.640	D	-0.012	E	27.845	1454.7
364.9	364.90	34.641	D	-0.012	E	27.846	1454.7
365.9	365.95	34.638	D	-0.010	E	27.843	1454.7
366.8	366.80	34.640	D	-0.012	E	27.845	1454.8
367.8	367.85	34.638	D	-0.010	E	27.844	1454.8
369.0	369.05	34.638	D	-0.010	E	27.843	1454.8
370.1	370.15	34.639	D	-0.010	E	27.844	1454.8
371.1	371.10	34.639	D	-0.010	E	27.844	1454.8
372.1	372.10	34.640	D	-0.010	E	27.845	1454.8
373.0	373.05	34.641	D	-0.010	E	27.846	1454.9
374.1	374.15	34.639	D	-0.009	E	27.844	1454.9
375.2	375.20	34.638	D	-0.008	E	27.843	1454.9
376.0	376.05	34.640	D	-0.009	E	27.844	1454.9
377.2	377.25	34.642	D	-0.009	E	27.846	1454.9
378.3	378.30	34.640	D	-0.008	E	27.845	1455.0
379.2	379.25	34.641	D	-0.008	E	27.845	1455.0
380.2	380.25	34.642	D	-0.008	E	27.846	1455.0
381.3	381.30	34.641	D	-0.008	E	27.846	1455.0
382.3	382.30	34.639	D	-0.007	E	27.844	1455.0
383.2	383.20	34.640	D	-0.007	E	27.845	1455.0
384.3	384.35	34.640	D	-0.007	E	27.844	1455.1
385.3	385.30	34.639	D	-0.004	E	27.843	1455.1
386.3	386.35	34.642	D	-0.006	E	27.846	1455.1
387.4	387.40	34.641	D	-0.006	E	27.845	1455.1
388.5	388.55	34.640	D	-0.006	E	27.845	1455.1
389.4	389.45	34.642	D	-0.005	E	27.846	1455.2
390.5	390.55	34.639	D	-0.005	E	27.844	1455.2
391.4	391.45	34.639	D	-0.004	E	27.844	1455.2
392.4	392.45	34.640	D	-0.005	E	27.844	1455.2
393.4	393.45	34.642	D	-0.005	E	27.846	1455.2
394.4	394.45	34.642	D	-0.004	E	27.846	1455.2
395.5	395.50	34.640	D	-0.003	E	27.844	1455.3
396.7	396.70	34.639	D	-0.003	E	27.844	1455.3
397.7	397.75	34.640	D	-0.003	E	27.845	1455.3
398.6	398.60	34.641	D	-0.003	E	27.845	1455.3
399.6	399.65	34.639	D	-0.002	E	27.844	1455.3
400.8	400.80	34.640	D	-0.002	E	27.844	1455.4
401.9	401.90	34.642	D	-0.003	E	27.846	1455.4
402.9	402.90	34.640	D	-0.002	E	27.845	1455.4
403.9	403.90	34.642	D	-0.003	E	27.846	1455.4
404.9	404.95	34.642	D	-0.003	E	27.846	1455.4
405.9	405.95	34.641	D	-0.002	E	27.846	1455.4
406.9	406.90	34.643	D	-0.003	E	27.847	1455.5
407.9	407.90	34.643	D	-0.002	E	27.847	1455.5
409.0	409.00	34.644	D	-0.002	E	27.848	1455.5
410.0	410.05	34.642	D	-0.001	E	27.846	1455.5
411.0	411.00	34.643	D	-0.001	E	27.847	1455.5
412.1	412.10	34.641	D	0.0	E	27.845	1455.6
413.0	413.05	34.643	D	-0.001	E	27.847	1455.6
413.9	413.95	34.644	D	-0.001	E	27.848	1455.6
414.9	414.95	34.645	D	-0.002	E	27.848	1455.6
416.1	416.15	34.642	D	0.0	E	27.846	1455.6
417.0	417.05	34.642	D	-0.001	E	27.846	1455.6
418.1	418.10	34.642	D	0.0	E	27.846	1455.7

DEPTH	PRESS	SAL	TEMP	SIGMAT	SOUND
419.3	419.30	34.644 D	-0.001 E	27.847	1455.7
420.1	420.15	34.644 D	0.0 E	27.847	1455.7
421.2	421.25	34.644 D	-0.001 E	27.848	1455.7

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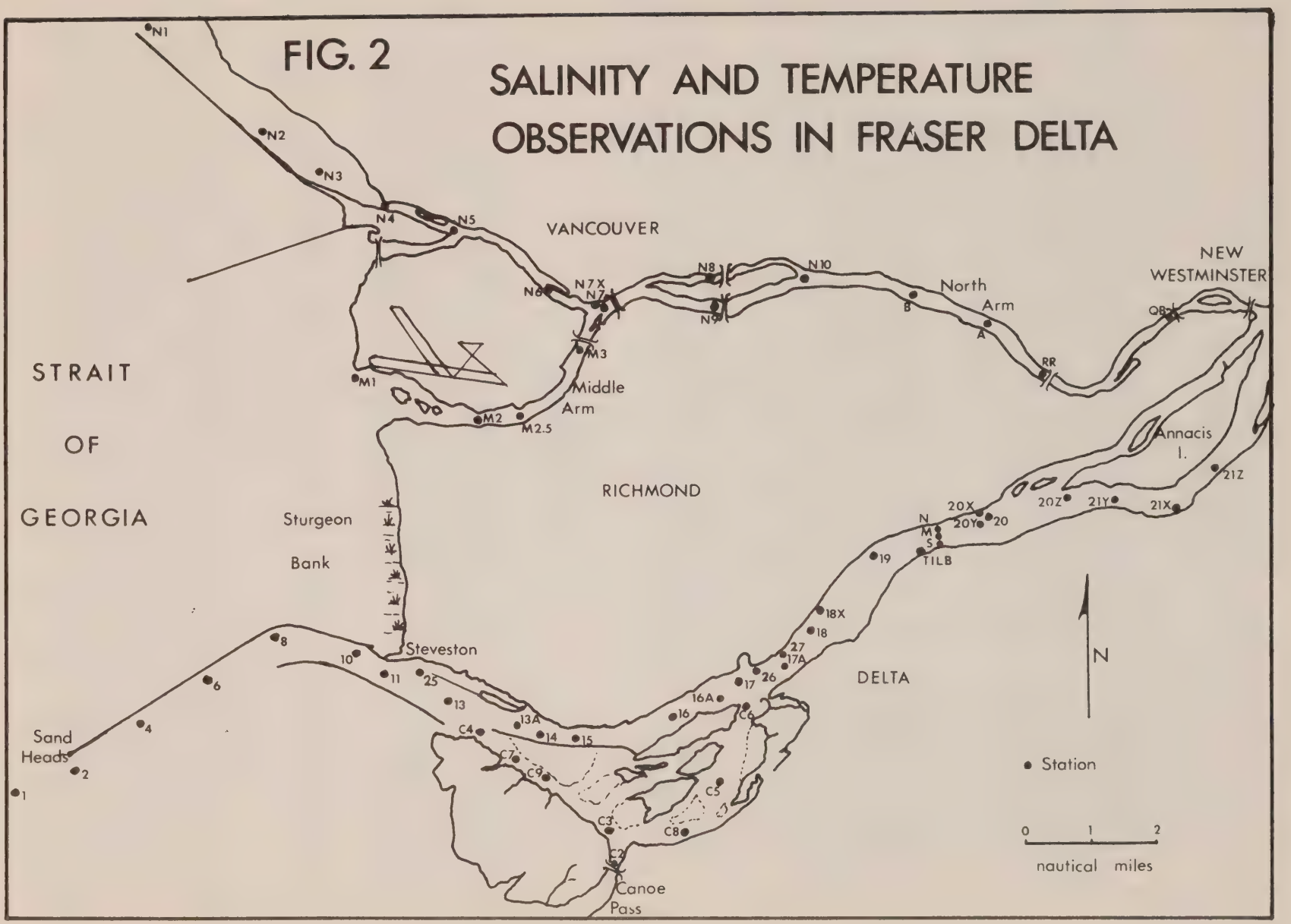
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Victoria, B.C.

April, 1975

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FIG. 1
THE FRASER RIVER BASIN
N
ALBERTA
Prince George
Fraser River
Jasper
FRASER RIVER
Scale in Miles
0 40 80
Thompson River
VANCOUVER ISLAND
STRAIT OF GEORGIA
Vancouver
Hope
Chilliwack
PACIFIC OCEAN


FIG. 2
SALINITY AND TEMPERATURE OBSERVATIONS IN FRASER DELTA
VANCOUVER
NEW WESTMINSTER
North Arm
Middle Arm
STRAIT OF GEORGIA
Sturgeon Bank
RICHMOND
Annacis I.
Steveston
DELTA
Sand Heads
Canoe Pass
TILB
N1
N2
N3
N4
N5
N7X
N7
N8
N9
N10
M1
M2
M2.5
M3
RR
A
B
QB
20X
20Y
20
20Z
21Y
21X
21Z
N
M
S
18X
18
17A
27
26
17
16A
16
C6
C4
C7
C9
C5
C3
C8
C2
13A
14
15
13
25
11
10
8
6
4
2
1
N
Station
0
1
2
nautical miles

INTRODUCTION

The Fraser River and its tributaries drain about 90,000 square miles of British Columbia into the Strait of Georgia. After descending swiftly from an elevation of more than 3,000 feet, the Fraser matures into a 60 mile long, gently sloping channel in a flood plain. The river finally divides into four arms, North Arm, Middle Arm, Main Arm and Canoe Pass. These four distributaries form the Fraser Delta, a fan-shaped region extending westward from New Westminster into the Strait of Georgia, with a radius of approximately 20 miles.

The interaction between the river outflow and the tides in the Strait of Georgia creates a complex flow regime in the estuarine system of the delta, which has been the object of a variety of studies pertinent to navigation, pollution and fisheries. As in any tidal estuary, the behaviour of the salinity wedge forms an integral part of this flow regime and a knowledge of its movement and boundaries is essential to studies of marine organisms, of waste disposal, of the availability of fresh water for industrial plants, and of salt intrusion into agricultural land.

It is hoped that the following data records will be useful to these studies, particularly since the need for salinity and temperature observations has been emphasized by the rapid development of the Fraser delta in recent years.

OBSERVATIONS

From August 1966 to March 1968, monthly salinity and temperature observations were taken by G.C. Hughes in the Main Arm, between Sandheads and New Westminster. In August 1971, the program was continued by A. Ages at a much lower frequency but including the other arms of the delta. The last series of measurements covered in this report was taken in March 1973. The dates of observations are listed on page 3.

Figure 2 shows the positions of the stations occupied. They were estimated by eye, using charts 3488 and 3489 of the Canadian Hydrographic Service.

The 1966-1972 observations were made with a Beckman RS5-3 portable salinometer, which measures electrical conductivity and temperature, and computes the salinity from the two measurements by a self-contained circuit. The manufacturer lists its accuracy at $\pm 0.3\,^{0}/_{00}$ for salinity and 0.5°C for temperature. During the 1966-68 cruises, the meter was weighted with 50-100 lbs., depending on the current velocity, and suspended from an auxiliary line operated from a hydrographic winch. In 1971 and 1972, weights between 20 and 50 lbs were used, since the launches were not equipped

with winches. In the winter of 1973, salinity and temperature measurements were carried out with an Interocean CSTD, which operates on the same principles as the Beckman meter, but which also measures the depth with a pressure transducer. Its listed accuracy is $\pm 0.05^{0}/_{00}$ and $0.05^{\circ}C$ for salinity and temperature respectively.

The Beckman salinometers were calibrated before each cruise in containers with water of known salinity and temperature. The Interocean instrument was calibrated at sea by collecting seawater samples (to be analyzed ashore) for salinity comparison, taking thermometer readings for temperature comparison and by comparing the depth readings with marks on the cable in still water.

Both types of salinometers appeared to be reasonably stable; the Beckman showed errors not exceeding a few percent of the measured values and the Interocean was found to have discrepancies in salinity readings not exceeding $0.1^{0}/_{00}$ and $0.2^{\circ}C$ for temperature. The depth reading of the Interocean instrument was unreliable near the surface where the depth could be obtained with good accuracy from marks on the cable.

The 1966 cruises were made by CGS EHKOLI, the 1967 and 1968 cruises by CGS VECTOR, both vessels being operated by the Department of Energy, Mines and Resources. The 1971-73 cruises were carried out by the launches CRANE and REVISOR of the Department of the Environment.

DATA RECORDS

The data are presented in tabular form as well as in profile sketches. They are tabulated chronologically, except for time series and some stations which had to be listed separately because they did not conform to the standard format. For the same reason, a few point measurements are not tabulated although they are shown on the profiles.

The records could not be arranged uniformly since the methods used to collect data differed, depending on the types of vessel and instrument.

The profile sketches show the corrected salinities and temperatures in $^{0}/_{00}$ and $^{\circ}C$ on the same horizontal scale, and the depth in metres on the vertical scale. Station numbers (e.g. STN 11, 20.08.66) refer to the chart of the delta, Fig. 2; the times of observations (e.g. 12.02 for STN 11) are Pacific Standard Times. Discharges (e.g. Q = 146,000 cfs, 20.08.66) were measured at Hope, well outside the tidal influence. The small sketches indicating the stage of the tide at the time of observation have a vertical scale from 0 to 15 feet above Sandheads datum and a horizontal scale from 0 to 24 hours PST of that day. The tide sketches are very approximate and should only be considered as an indication of the stage of the tide during the observation.

SCHEDULE OF OBSERVATIONS

PERIOD	AREA	INSTRUMENT
20-21 August 1966	Main Arm	Beckman
17-18 September 1966	Main Arm	Beckman
22-23 October 1966	Main Arm	Beckman
12-13 November 1966	Main Arm	Beckman
7-11 December 1966	Main Arm	Beckman
20-22 January 1967	Main Arm	Beckman
15-17 February 1967	Main Arm	Beckman
10-12 March 1967	Main Arm	Beckman
21-23 April 1967	Main Arm	Beckman
19-20 May 1967	Main Arm	Beckman
5 June 1967	Main Arm	Beckman
30 July 1967	Main Arm	Beckman
25-28 August 1967	Main Arm	Beckman
23 September 1967	Main Arm	Beckman
20 November 1967	Main Arm	Beckman
13-14 January 1968	Main Arm	Beckman
17 February 1968	Main Arm	Beckman
15-17 March 1968	Main Arm	Beckman
23-27 August 1971	Main/North/Middle Arm & Canoe Pass	Beckman
1- 6 November 1971	Main Arm/Canoe Pass	Beckman
10-13 January 1972	Main Arm/Canoe Pass	Beckman
15-16 January 1972	Canoe Pass/North Arm	Beckman
7-10 March 1972	Main/North/Middle Arm & Canoe Pass	Beckman
29 March 1972	Main Arm	Beckman
22-24 August 1972	Main/North/Middle Arm & Canoe Pass	Beckman
26 February - 2 March 1973	Main Arm	Interocean
26 March - 28 March 1973	Main/North/Middle Arm	Interocean

ACKNOWLEDGEMENTS

The collection and processing of the data presented in this report were made possible by the participation of many individuals at sea and ashore. We would like to thank Captain Victor Dale-Johnson, Captain Charles Macaulay, and the officers and men of the EHKOLI and VECTOR for their cooperation during the 1966-68 cruises. The program during these three years was supported financially by the National Research Council in Ottawa (Grant A 2561).

The field work between 1971 and 1973 was carried out by hydrographic launches and we commend, among others, coxswains Mike Craton and Ray Paulsen for their good work in rough weather, and we thank our assistant Rainier Schoenrank for his part in the observations, in particular the time series.

Finally, we appreciate the assistance of Bruce Cox, Nancy Bertoia, Anne Harrison and Dave Lock, who plotted the data, and of Anne Reay and Anne Nichol who did most of the typing.

DATA RECORD

1966 - 1968

MAIN ARM

STA	DATE	TIME (PST)	DEPTH TO BOT IN M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
2	20/08/66	1020	09.1	26.6	13.1	26.6	13.1	25.5	13.5	23.1	15.1	08.1	16.8
4	20/08/66	1050	09.1	25.9	14.4	25.9	14.4	25.1	14.5	18.4	16.4	11.8	16.4
6	20/08/66	1112	10.7	24.7	14.9	25.0	14.6	24.8	14.7	21.1	14.9	00.4	16.9
8	20/08/66	1134	07.0	07.0	16.6	-	-	04.8	16.7	00.5	17.1	00.1	17.1
11	20/08/66	1202	08.2	02.2	17.0	-	-	00.2	17.1	00.0	17.3	00.0	17.1
14	20/08/66	1230	09.1	00.0	17.5	00.0	17.5	00.0	17.3	-	-	00.0	17.3
17	20/08/66	1310	09.7	00.0	18.2	00.0	18.2	00.0	18.1	00.0	18.0	00.0	17.9
19	20/08/66	1335	07.3	00.0	18.2	-	-	00.0	18.1	00.0	18.0	00.0	17.9
21	20/08/66	1415	08.5	00.0	18.7	-	-	00.0	18.6	00.0	18.4	00.0	18.4
23	20/08/66	1500	12.2	00.0	17.8	00.0	17.6	00.0	17.6	00.0	17.5	00.0	17.5
24	20/08/66	1545	13.1	00.0	17.6	00.0	17.2	00.0	17.2	00.0	17.2	00.0	17.2
23	21/08/66	0655	09.1	00.1	15.9	00.0	16.0	00.0	16.0	00.0	16.0	00.0	16.0
21	21/08/66	0712	12.2	00.0	15.9	00.0	15.9	00.0	15.9	00.0	15.9	00.0	15.9
19	21/08/66	1742	09.1	00.0	16.0	00.0	16.0	00.0	15.9	00.0	16.0	00.0	16.0
16	21/08/66	0804	09.1	00.0	16.1	00.0	16.1	00.0	16.1	00.0	16.1	00.0	16.1
15	21/08/66	0815	10.7	00.0	16.1	00.0	16.1	00.0	16.2	00.0	16.3	00.0	16.4
14	21/08/66	0823	09.7	00.0	16.2	-	-	00.0	16.2	00.0	16.2	00.0	16.4
13	21/08/66	0835	08.5	00.0	16.5	-	-	00.0	16.5	00.0	16.5	00.0	16.6
11	21/08/66	0845	08.5	00.0	16.5	-	-	00.0	16.5	00.0	16.6	00.0	16.6
10	21/08/66	0925	09.7	19.7	15.1	18.7	15.5	02.0	16.5	00.1	16.5	00.0	16.7
9	21/08/66	0945	12.8	23.6	14.6	18.5	15.6	10.0	16.5	00.5	16.5	00.0	16.6
8	21/08/66	0950	10.9	24.3	14.7	24.1	15.1	18.5	16.2	01.1	16.4	00.0	16.4
7	21/08/66	0955	15.2	25.2	15.0	23.6	16.0	18.4	16.2	15.4	16.5	00.2	16.5
6	21/08/66	1005	15.2	25.4	14.4	23.1	16.3	18.3	16.5	10.5	16.5	00.6	16.5
5	21/08/66	1015	10.9	25.9	14.2	24.9	15.8	19.8	16.1	11.2	16.4	00.5	16.4
4	21/08/66	1025	10.9	25.5	14.3	25.1	14.8	22.7	15.5	14.5	16.4	00.3	16.3
3	21/08/66	1035	09.1	25.9	13.9	25.9	13.9	25.1	14.7	13.4	16.4	03.3	16.4
2	21/08/66	1042	09.1	26.2	13.6	26.2	13.6	25.2	15.3	17.8	16.7	01.8	16.7
11	21/08/66	1130	09.1	21.2	15.7	21.2	15.7	00.8	17.1	00.0	17.3	00.0	17.6
13	21/08/66	1140	08.5	03.8	16.4	-	-	00.1	16.7	00.0	16.8	00.0	17.3
12	21/08/66	1147	08.5	19.4	15.4	-	-	00.1	16.5	00.0	16.5	00.0	16.8
11	21/08/66	1152	09.1	21.4	15.4	21.4	15.4	01.3	16.4	00.0	16.4	00.0	16.6
10	21/08/66	1200	09.1	23.5	15.3	23.5	15.3	08.9	16.2	00.0	16.4	00.0	16.4
6	21/08/66	1215	15.2	25.6	14.4	24.3	15.6	20.6	15.9	03.9	16.7	00.0	16.5
4	21/08/66	1226	11.6	25.6	14.3	25.5	14.3	25.1	14.8	15.1	16.4	03.6	16.4

STA	DATE	TIME (PST)	DEPTH TO BOT IN M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
2	21/08/66	1235	08.5	26.5	13.6	-	-	25.7	14.8	16.6	16.1	04.5	16.5
2	17/09/66	1135	08.5	28.5	11.2	-	-	27.5	12.1	21.0	12.6	04.4	14.3
3	17/09/66	1147	09.1	29.0	10.8	29.0	10.8	28.7	11.1	27.3	12.9	03.2	14.5
4	17/09/66	1203	10.6	28.0	11.2	-	-	25.5	11.8	15.4	13.4	02.0	14.5
5	17/09/66	1217	10.9	27.7	11.4	-	-	25.0	13.0	07.3	14.2	02.2	14.5
7	17/09/66	1235	15.8	26.0	12.1	10.7	13.9	06.8	14.3	02.2	14.5	02.0	14.6
8	17/09/66	1250	11.6	24.3	12.1	10.8	13.8	03.2	14.5	02.2	14.6	01.2	14.6
9	17/09/66	1305	08.5	19.6	12.6	-	-	17.6	14.5	03.8	14.6	01.4	14.6
10	17/09/66	1314	09.1	19.6	13.1	19.6	13.1	10.8	13.9	05.3	14.4	01.8	14.6
11	17/09/66	1322	08.2	16.6	13.2	-	-	10.9	13.9	01.5	14.6	01.5	14.6
12	17/09/66	1330	07.9	16.3	13.4	-	-	05.0	14.3	00.5	14.7	00.0	14.7
14	17/09/66	1348	07.9	01.1	14.7	-	-	00.0	14.7	00.0	14.7	00.0	14.7
15	17/09/66	1358	09.7	00.0	14.7	-	-	00.0	14.7	00.0	14.7	00.0	14.7
18	17/09/66	1428	13.7	00.0	14.6	-	-	00.0	14.7	00.0	14.7	00.0	14.8
20	17/09/66	1500	13.1	00.0	14.7	00.0	14.7	00.0	14.7	00.0	14.7	00.0	14.7
22	17/09/66	1540	09.1	00.0	14.6	-	-	00.0	14.6	00.0	14.6	00.0	14.6
24	18/09/66	0735	13.1	00.0	14.6	00.0	14.6	00.0	14.6	00.0	14.7	00.0	14.7
23	18/09/66	0811	12.2	00.0	14.6	00.0	14.6	00.0	14.6	00.0	14.7	00.0	14.8
22	18/09/66	0828	10.7	00.0	14.6	00.0	14.6	00.0	14.6	00.0	14.6	00.0	14.6
20	18/09/66	0902	12.8	00.0	14.7	00.0	14.7	00.0	14.8	00.0	14.8	00.0	14.8
17	18/09/66	0937	06.7	00.0	14.6	-	-	00.0	14.6	00.0	14.7	00.0	14.7
15	18/09/66	0955	11.6	11.9	13.3	-	-	00.0	14.6	00.0	14.7	00.0	14.8
14	18/09/66	1005	09.7	18.5	13.0	17.6	13.2	02.3	14.5	00.0	14.6	00.0	14.6
12	18/09/66	1017	09.7	25.5	12.1	25.5	12.3	14.6	13.7	03.1	14.4	01.6	14.4
11	18/09/66	1025	09.5	26.1	12.0	-	-	19.4	13.0	02.1	14.3	00.0	14.7
10	18/09/66	1033	10.4	27.2	11.6	-	-	25.3	12.3	05.4	14.2	02.5	14.4
9	18/09/66	1040	08.8	27.5	11.5	-	-	24.5	12.4	09.9	13.8	00.4	14.5
8	18/09/66	1045	14.3	27.7	11.4	-	-	25.8	12.0	02.7	14.4	00.2	14.6
7	18/09/66	1052	13.4	27.7	11.1	27.7	11.4	26.5	12.0	06.7	13.8	05.2	14.3
6	18/09/66	1100	15.2	28.5	11.0	28.3	11.3	27.6	11.8	19.3	13.5	00.8	14.6
5	18/09/66	1108	12.2	28.6	10.9	28.6	11.2	27.7	11.8	20.0	13.4	02.2	14.4
4	18/09/66	1114	10.7	28.9	10.6	-	-	28.2	11.2	23.3	12.8	15.5	13.5
3	18/09/66	1121	10.1	29.0	10.6	-	-	28.3	11.5	22.3	13.1	12.0	13.9
2	18/09/66	1130	09.1	29.0	10.6	29.0	10.6	28.5	11.3	21.8	13.7	06.7	14.3

STA	DATE	TIME (PST)	DEPTH TO BOT IN M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
12	18/09/66	1227	08.5	20.1	13.4	-	-	17.6	14.4	10.9	15.0	00.0	15.4
11	18/09/66	1232	08.8	25.9	12.6	-	-	11.1	14.3	02.0	15.4	00.3	15.7
10	18/09/66	1238	09.6	26.4	12.3	26.4	12.3	10.3	14.3	01.2	15.1	00.7	15.3
9	18/09/66	1243	08.5	26.5	12.0	-	-	19.2	13.6	02.2	14.7	00.9	15.0
8	18/09/66	1249	10.1	14.6	13.4	14.2	13.7	04.1	14.6	01.3	14.7	00.7	14.8
7	18/09/66	1255	16.8	27.8	11.2	27.3	12.4	14.8	13.6	01.5	14.7	00.9	14.8
6	18/09/66	1300	15.6	27.4	11.4	-	-	06.5	14.2	01.5	14.7	00.9	14.5
5	18/09/66	1305	12.2	27.3	11.3	-	-	21.9	12.2	03.0	14.5	01.0	14.7
4	18/09/66	1311	11.6	28.7	10.8	28.7	10.8	28.3	11.2	20.5	12.9	01.6	14.6
3	18/09/66	1315	10.1	28.7	11.0	-	-	28.6	11.3	23.5	12.1	04.1	13.6
2	18/09/66	1320	09.1	28.4	11.3	28.4	11.3	24.2	11.8	22.2	12.3	08.3	14.0
2	22/10/66	1030	09.1	30.4	09.3	30.4	09.3	29.6	09.2	25.7	08.7	04.9	08.3
3	22/10/66	1040	10.7	30.1	09.3	30.1	09.3	29.9	09.3	22.7	08.8	06.0	08.3
4	22/10/66	1104	12.2	29.9	09.3	29.9	09.3	29.6	09.2	21.3	08.8	04.6	08.3
5	22/10/66	1113	12.2	29.6	09.4	29.2	09.3	24.4	09.1	20.2	08.7	01.9	08.3
6	22/10/66	1119	13.7	29.0	09.4	28.6	09.3	24.5	09.2	19.2	08.7	06.2	08.4
7	22/10/66	1126	16.8	28.9	09.4	28.8	09.4	26.6	09.3	20.6	08.8	01.5	08.5
8	22/10/66	1135	09.1	28.6	09.4	28.6	09.4	27.8	09.2	15.8	08.4	03.4	08.4
9	22/10/66	1144	09.1	28.2	09.3	28.2	09.3	20.3	08.8	06.7	08.4	01.2	08.3
10	22/10/66	1147	09.8	27.8	09.3	27.8	09.3	24.0	09.1	06.5	08.3	01.7	08.4
11	22/10/66	1154	10.4	26.9	09.3	26.9	09.3	23.3	09.0	10.5	08.5	01.6	08.3
12	22/10/66	1203	10.7	26.5	09.3	26.5	09.3	20.5	08.9	02.6	08.3	00.6	08.2
13	22/10/66	1208	10.4	25.5	09.2	25.2	09.1	17.1	08.5	00.8	08.2	00.4	08.2
14	22/10/66	1217	11.6	26.5	09.1	26.5	09.0	07.3	08.4	01.4	08.2	00.5	08.2
15	22/10/66	1228	12.8	18.1	08.9	17.6	08.7	01.6	08.2	00.0	08.2	00.0	08.2
16	22/10/66	1240	09.8	00.0	08.0	00.0	08.0	00.0	08.1	00.0	08.1	00.0	08.1
17	22/10/66	1249	07.6	00.0	08.1	-	-	00.0	08.1	00.0	08.1	00.0	08.1
18	22/10/66	1255	17.7	00.0	08.1	00.0	08.1	00.0	08.1	00.0	08.1	00.0	08.1
20	22/10/66	1319	15.2	00.0	08.1	00.0	08.1	00.0	08.1	00.0	08.1	00.0	08.2
22	22/10/66	1346	10.7	00.0	08.2	00.0	08.2	00.0	08.2	00.0	08.2	00.0	08.2
23	22/10/66	1355	13.7	00.0	08.2	00.0	08.2	00.0	08.2	00.0	08.2	00.0	08.1
24	22/10/66	1425	12.2	00.0	08.4	00.0	08.4	00.0	08.4	00.0	08.4	00.0	08.4

STA	DATE	TIME (PST)	DEPTH TO BOT IN M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
23	23/10/66	0715	11.9	00.0	08.4	00.0	08.4	00.0	08.4	00.0	08.5	00.0	08.6
22	23/10/66	0730	09.1	00.0	08.4	00.0	08.4	00.0	08.4	00.0	08.4	00.0	08.4
20	23/10/66	0755	09.6	00.0	08.7	00.0	08.7	00.0	08.7	00.0	08.7	00.0	08.8
18	23/10/66	0817	13.7	00.0	08.6	00.0	08.7	00.0	08.7	00.0	08.7	00.0	08.9
16	23/10/66	0835	06.7	00.0	08.7	-	-	00.0	08.7	00.0	08.7	00.0	08.9
15	23/10/66	0843	10.4	00.0	08.6	00.0	08.6	00.0	08.7	00.0	08.7	00.0	08.9
14	23/10/66	0852	08.5	00.0	08.6	-	-	00.0	08.6	00.0	08.7	00.0	08.8
13	23/10/66	0900	08.5	04.7	08.7	-	-	00.0	08.7	00.0	08.8	00.0	08.8
12	23/10/66	0904	08.5	05.2	08.6	-	-	01.1	08.6	00.0	08.6	00.0	08.8
11	23/10/66	0908	08.5	07.8	08.7	-	-	01.9	08.6	00.0	08.7	00.0	08.9
10	23/10/66	0914	09.5	07.3	08.6	06.9	08.7	01.4	08.5	00.5	08.6	00.0	08.9
9	23/10/66	0920	09.1	07.2	08.6	05.2	08.6	01.3	08.5	00.8	08.6	00.5	08.7
8	23/10/66	0927	10.7	20.1	09.2	14.2	08.9	01.3	08.7	00.7	08.7	00.6	08.8
7	23/10/66	0935	11.6	18.9	09.2	14.8	09.0	02.2	08.6	01.0	08.7	01.0	08.7
6	23/10/66	0940	13.7	24.8	09.3	13.5	08.9	07.7	08.6	01.8	08.7	01.0	08.8
5	23/10/66	0947	12.2	27.8	09.3	18.5	09.0	09.0	08.7	01.5	08.6	00.9	08.9
4	23/10/66	0953	11.3	29.0	09.5	21.0	09.3	15.5	09.0	03.8	08.7	01.1	08.8
3	23/10/66	0958	10.9	29.3	09.5	29.2	09.3	18.2	09.0	04.4	08.7	01.2	08.9
2	23/10/66	1005	10.4	30.4	09.6	29.6	09.7	27.7	09.5	02.8	09.1	02.5	09.0
2	23/10/66	1103	09.8	29.9	09.9	29.7	09.9	28.0	09.9	20.0	09.6	02.6	09.6
3	23/10/66	1111	10.9	29.6	09.8	29.5	09.7	29.3	09.7	12.5	09.4	02.8	09.4
4	23/10/66	1117	11.6	29.4	09.7	29.3	09.8	29.3	09.6	12.8	09.1	01.7	09.1
5	23/10/66	1125	11.9	29.1	09.7	28.9	09.6	20.4	09.3	11.3	09.0	04.6	09.2
6	23/10/66	1132	14.6	28.6	09.7	27.6	09.6	18.7	09.3	12.1	09.1	01.1	09.0
7	23/10/66	1139	14.9	28.4	09.6	27.5	09.5	19.0	09.3	12.2	09.1	00.9	08.9
8	23/10/66	1148	09.1	27.9	09.5	27.9	09.5	18.4	09.2	01.7	09.1	01.0	09.0
9	23/10/66	1155	09.6	26.9	09.5	26.9	09.5	16.2	09.3	05.6	08.8	01.4	08.9
11	23/10/66	1207	09.6	23.3	09.4	23.3	09.4	14.8	09.1	00.5	08.8	00.5	08.9
12	23/10/66	1214	09.1	19.6	09.2	19.6	09.2	04.7	08.8	00.4	08.8	00.4	08.9
14	23/10/66	1221	10.1	16.6	09.2	09.9	08.8	01.0	08.7	00.3	08.9	00.3	08.9
2	12/11/66	1031	09.8	26.5	08.0	26.5	08.0	26.0	07.8	24.5	07.8	20.4	07.2
3	12/11/66	1040	10.4	26.5	08.2	26.5	08.2	25.3	07.8	19.3	07.4	15.7	07.2
4	12/11/66	1050	10.9	26.2	08.3	26.2	08.2	25.8	08.1	22.5	07.4	05.5	06.4
5	12/11/66	1058	11.6	26.8	08.4	26.5	08.3	25.2	08.0	13.0	06.8	03.6	06.4
6	12/11/66	1107	13.4	26.6	08.5	26.1	08.4	25.0	08.1	08.4	06.6	03.6	06.4
7	12/11/66	1117	15.5	26.0	08.3	22.8	07.9	12.9	07.1	03.6	06.2	02.2	06.4

STA	DATE	TIME (PST)	DEPTH TO BOT IN M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
8	12/11/66	1127	12.2	25.7	08.2	16.6	07.3	04.0	06.2	02.8	06.2	02.3	06.2
9	12/11/66	1136	09.1	25.7	08.3	25.7	08.3	24.5	08.0	03.3	06.2	01.3	06.2
10	12/11/66	1146	09.8	23.6	08.1	23.6	08.1	12.2	07.2	03.5	06.3	01.7	06.3
11	12/11/66	1154	09.1	23.6	08.2	23.6	08.2	15.7	07.5	03.2	06.3	01.0	06.2
12	12/11/66	1201	08.5	23.5	08.2	-	-	10.2	06.8	02.6	06.2	01.0	06.3
14	12/11/66	1225	09.1	17.8	08.2	17.8	08.2	05.6	07.2	01.4	06.9	00.6	07.3
15	12/11/66	1234	10.4	16.7	07.3	05.1	06.4	01.4	06.2	00.9	06.2	00.0	06.6
16	12/11/66	1247	10.9	04.3	06.3	02.4	06.1	00.0	06.2	00.0	06.2	00.0	06.4
17	12/11/66	1258	06.1	00.0	06.0	-	-	00.0	06.0	00.0	06.0	00.0	06.2
18	12/11/66	1307	16.2	00.0	05.7	00.0	05.8	00.0	05.8	00.0	05.9	00.0	06.0
20	12/11/66	1335	13.1	00.0	06.0	00.0	06.1	00.0	06.2	00.0	06.3	00.0	06.5
22	12/11/66	1410	10.1	00.0	05.7	00.0	05.7	00.0	05.8	00.0	05.8	00.0	06.0
23	12/11/66	1424	15.2	00.0	05.4	00.0	05.4	00.0	05.5	00.0	05.5	00.0	05.7
24	12/11/66	1504	15.2	00.0	05.6	00.0	05.7	00.0	05.8	00.0	05.9	00.0	06.0
23	13/11/66	0802	12.2	00.0	04.7	00.0	04.7	00.0	04.8	00.0	04.8	00.0	04.9
22	13/11/66	0819	11.6	00.0	04.4	00.0	04.4	00.0	04.3	00.0	04.4	00.0	04.5
20	13/11/66	0913	14.6	00.0	04.7	00.0	04.8	00.0	04.8	00.0	04.8	00.0	05.0
18	13/11/66	0954	15.2	09.8	05.9	01.2	05.1	00.0	05.1	00.0	05.1	00.0	05.2
17	13/11/66	1017	08.5	09.3	05.9	-	-	02.2	05.2	00.0	05.0	00.0	05.1
16	13/11/66	1025	10.9	20.8	07.1	20.1	06.9	14.1	06.2	01.2	05.1	00.3	05.1
15	13/11/66	1038	13.4	22.6	07.4	22.3	07.3	20.7	06.5	03.6	05.5	02.0	05.3
14	13/11/66	1047	11.6	23.1	07.5	23.1	07.4	22.6	07.2	08.7	06.2	03.4	06.0
12	13/11/66	1056	09.1	24.5	07.6	24.4	07.6	23.3	07.3	21.4	06.9	03.1	05.5
11	13/11/66	1103	07.9	24.3	07.5	-	-	23.9	07.3	12.9	06.2	07.3	05.7
10	13/11/66	1107	09.7	26.0	07.8	25.1	07.6	24.0	07.4	17.8	06.5	11.3	06.1
9	13/11/66	1112	10.7	27.2	08.0	24.5	07.8	23.3	07.3	12.7	06.0	03.6	05.4
8	13/11/66	1116	14.0	-	-	24.2	07.6	22.7	07.2	06.6	05.8	03.4	05.6
7	13/11/66	1123	16.8	27.0	08.0	24.7	07.7	23.8	07.3	05.2	06.3	03.4	05.7
6	13/11/66	1130	14.0	27.4	08.1	27.2	08.1	26.0	07.8	24.2	07.3	05.6	06.2
5	13/11/66	1134	12.8	28.0	08.1	27.3	08.1	26.9	07.9	24.6	07.6	09.5	06.7
4	13/11/66	1140	12.2	28.2	08.2	27.8	08.1	26.6	07.9	21.6	07.3	17.4	06.8
3	13/11/66	1146	10.7	28.9	08.3	28.2	08.3	27.4	07.9	25.4	08.1	25.3	07.5
2	13/11/66	1152	09.1	30.0	08.4	29.3	08.3	27.6	07.9	25.6	07.9	25.5	07.7
12	13/11/66	1244	09.7	24.2	07.6	24.2	07.5	23.3	07.1	07.9	05.6	01.6	05.5
11	13/11/66	1250	09.1	24.0	07.6	24.5	07.4	18.6	07.1	09.8	06.1	02.0	05.7
10	13/11/66	1318	09.7	25.9	07.9	24.4	07.5	15.7	06.7	07.7	05.8	02.8	05.7
9	13/11/66	1324	09.1	24.7	07.8	24.7	07.6	21.3	07.1	07.1	05.9	02.8	05.6

STA	DATE	TIME (PST)	DEPTH TO BOT IN M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
8	13/11/66	1330	10.7	27.3	08.0	27.1	07.9	23.8	07.3	06.4	05.6	03.2	05.5
7	13/11/66	1335	13.7	27.8	08.1	26.3	08.0	25.8	07.7	15.9	15.8	03.4	05.5
6	13/11/66	1340	14.6	28.4	08.2	27.5	08.0	26.6	07.9	21.7	06.7	09.9	05.8
5	13/11/66	1346	12.8	28.5	08.1	27.4	08.0	25.5	07.7	17.3	06.7	09.2	06.2
4	13/11/66	1352	12.2	29.5	08.4	27.3	08.2	26.5	08.0	23.4	07.4	04.9	06.2
3	13/11/66	1358	10.7	30.0	08.5	27.8	08.3	26.8	08.0	20.9	07.2	06.4	06.2
2	13/11/66	1404	10.1	30.0	08.5	29.6	08.4	29.4	08.1	22.6	07.3	10.7	06.2
2	07/12/66	1555	12.2	31.4	07.8	31.4	07.7	29.5	07.3	23.0	06.4	18.0	05.8
4	07/12/66	1607	12.2	31.2	07.7	31.2	07.6	28.6	07.2	22.0	06.2	19.8	05.8
6	07/12/66	1617	15.9	31.3	07.7	31.1	07.6	29.4	07.0	16.6	05.6	12.5	05.3
8	07/12/66	1630	13.7	31.2	07.5	31.1	07.4	30.3	06.7	12.3	05.1	03.6	04.6
11	07/12/66	1700	10.7	30.3	07.4	30.3	07.2	26.7	06.3	10.3	04.4	03.2	04.2
2	08/12/66	0943	11.3	31.9	07.6	31.9	07.5	31.8	07.3	22.5	06.2	09.5	04.7
3	08/12/66	0953	11.3	31.5	07.8	31.5	07.8	31.5	07.6	26.5	06.9	04.8	04.8
5	08/12/66	1005	13.4	30.7	07.8	30.7	07.7	30.7	07.5	22.2	06.5	02.8	05.0
6	08/12/66	1016	14.6	30.4	07.9	30.3	07.8	30.1	07.6	19.9	06.4	00.8	05.2
7	08/12/66	1025	14.0	30.3	07.9	30.3	07.9	30.0	07.8	23.2	07.1	00.0	05.1
8	08/12/66	1032	10.9	30.2	07.8	30.2	07.8	30.2	07.4	07.4	06.2	00.6	05.0
9	08/12/66	1040	10.4	30.1	07.8	30.1	07.8	30.1	07.6	06.3	05.4	00.5	05.1
10	08/12/66	1047	10.7	29.9	07.7	29.9	07.6	29.9	07.3	01.5	04.8	00.0	04.7
11	08/12/66	1054	10.7	29.7	07.7	29.7	07.7	29.7	07.3	01.3	04.8	00.0	04.8
12	08/12/66	1059	10.7	29.4	07.6	29.4	07.6	29.5	07.5	01.4	04.9	00.0	04.9
13	08/12/66	1104	11.3	29.0	07.5	29.0	07.3	11.1	05.7	00.9	04.8	00.0	04.8
14	08/12/66	1115	13.7	28.0	07.5	27.3	07.1	09.3	05.5	00.5	04.8	00.0	04.9
15	08/12/66	1127	13.4	27.0	07.2	21.3	06.4	06.1	05.1	00.0	04.8	00.0	04.8
16	08/12/66	1141	11.9	16.9	06.3	16.7	06.2	01.9	04.8	00.0	04.8	00.0	04.9
17	08/12/66	1358	09.7	10.6	04.9	10.6	04.9	03.2	04.2	00.0	03.9	00.0	03.9
18	08/12/66	1409	17.7	16.4	05.5	05.3	04.5	00.3	03.9	00.0	03.9	00.0	03.9
19	08/12/66	1425	17.4	00.0	03.8	00.0	03.8	00.0	03.8	00.0	03.8	00.0	03.7
20	08/12/66	1437	14.3	00.0	03.7	00.0	03.7	00.0	03.7	00.0	03.7	00.0	03.7
22	08/12/66	1505	12.5	00.0	03.8	00.0	03.8	00.0	03.8	00.0	03.7	00.0	03.7
24	09/12/66	0825	16.5	00.0	03.3	00.0	03.3	00.0	03.3	00.0	03.3	00.0	03.2
23	09/12/66	0857	14.9	00.0	03.3	00.0	03.3	00.0	03.3	00.0	03.3	00.0	03.2
22	09/12/66	0910	11.9	00.0	03.4	00.0	03.4	00.0	03.4	00.0	03.4	00.0	03.2

STA	DATE	TIME (PST)	DEPTH TO BOT IN M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
20	09/12/66	0936	15.8	00.0	03.3	00.0	03.3	00.0	03.3	00.0	03.3	00.0	03.2
19	09/12/66	0953	12.5	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.3
18	09/12/66	1001	14.3	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.4
17	09/12/66	1011	10.1	01.9	04.1	01.9	04.1	00.0	03.7	00.0	03.7	00.0	03.6
16	09/12/66	1019	12.5	23.5	06.1	16.6	05.4	00.0	03.8	00.0	03.8	00.0	03.7
15	09/12/66	1028	12.2	26.6	06.8	25.2	06.4	20.2	05.0	00.5	03.9	00.0	03.8
14	09/12/66	1038	12.2	28.3	07.0	28.2	06.8	14.6	05.2	01.2	04.0	00.0	03.8
13	09/12/66	1049	12.8	29.3	07.2	29.3	07.0	20.0	06.1	10.5	04.8	02.9	04.0
12	09/12/66	1056	10.7	29.5	07.4	29.5	07.3	28.9	06.8	06.4	04.3	00.9	04.0
11	09/12/66	1103	11.3	29.6	07.5	29.6	07.4	29.4	07.0	04.4	04.3	01.5	04.2
8	09/12/66	1114	11.6	30.7	07.7	30.7	07.5	30.6	07.1	06.1	05.0	01.7	04.2
11	09/12/66	1130	11.3	29.9	07.3	29.9	07.3	29.8	06.9	07.3	04.4	00.8	04.0
14	09/12/66	1153	14.0	29.0	07.2	28.6	07.0	23.4	06.2	08.6	04.3	00.4	04.1
16	09/12/66	1217	12.8	26.7	06.7	26.6	06.6	22.5	05.8	00.8	03.8	00.3	03.6
17	09/12/66	1227	11.3	04.7	04.2	04.7	04.2	02.9	03.9	00.6	03.7	00.3	03.5
18	09/12/66	1238	13.7	17.5	04.9	03.4	03.8	00.0	03.5	00.0	03.3	00.0	03.2
171	09/12/66	1253	09.7	01.4	03.9	01.4	03.9	00.3	03.8	00.3	03.7	00.3	03.6
172	09/12/66	1300	13.7	25.5	06.3	09.2	04.6	00.7	04.2	00.7	03.7	00.0	03.6
19	11/12/66	0748	11.3	00.0	04.2	00.0	04.2	00.0	04.3	00.0	04.3	00.0	04.5
18	11/12/66	0800	17.7	00.8	04.1	00.8	04.2	00.8	04.2	00.4	04.3	00.4	04.5
171	11/12/66	0812	09.1	01.9	04.1	01.9	04.1	01.4	04.1	01.0	04.1	00.7	04.1
17	11/12/66	0817	10.1	10.4	05.0	10.4	05.0	04.4	04.4	01.4	04.2	01.1	04.3
16	11/12/66	0831	11.9	21.2	06.4	21.2	06.4	20.4	06.1	04.4	04.7	02.4	04.8
15	11/12/66	0853	12.8	23.9	06.7	23.8	06.7	23.6	06.3	11.5	05.7	04.6	04.8
14	11/12/66	0901	14.3	24.8	06.9	24.4	06.8	24.4	06.6	15.0	05.5	04.5	05.1
13	11/12/66	0909	11.6	25.7	07.0	25.5	06.9	25.4	06.8	24.3	06.4	03.5	04.7
12	11/12/66	0914	11.6	26.5	07.0	25.7	07.0	25.2	06.8	22.3	06.4	05.0	04.8
11	11/12/66	0916	11.6	26.6	07.1	26.6	07.0	25.4	06.9	24.9	06.6	09.5	05.3
10	11/12/66	0927	10.9	27.5	07.0	26.7	06.9	25.4	06.9	24.9	06.6	14.8	05.8
9	11/12/66	0933	09.1	26.7	07.1	26.7	07.1	26.0	06.9	25.0	06.3	07.1	05.1
8	11/12/66	0939	13.1	28.0	07.3	26.8	07.0	25.8	06.7	20.0	06.5	20.5	05.9
7	11/12/66	0944	14.9	28.2	07.2	26.4	07.0	26.1	06.8	19.7	06.3	15.0	06.1
6	11/12/66	0950	17.9	28.0	07.1	26.6	07.0	26.2	06.8	23.0	06.5	14.7	06.0
5	11/12/66	0957	14.6	28.3	07.2	27.5	07.1	26.5	06.7	19.8	06.4	18.0	06.4
4	11/12/66	1004	14.0	28.3	07.2	27.3	07.0	25.3	06.9	23.1	06.6	20.3	06.6
3	11/12/66	1009	11.9	29.0	07.3	28.3	07.2	27.2	07.1	25.5	07.0	25.1	06.9

STA	DATE	TIME (PST)	DEPTH .TO BOT IN M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
2	11/12/66	1016	10.9	30.3	07.8	29.7	07.4	27.9	07.3	27.5	07.2	27.5	07.2
11	11/12/66	1230	09.1	26.8	07.2	26.8	07.2	25.8	06.7	13.9	05.3	02.5	05.0
8	11/12/66	1236	10.9	27.9	07.2	27.3	07.1	24.7	06.7	09.0	05.4	07.5	05.4
6	11/12/66	1256	17.1	27.6	07.2	21.2	06.9	25.4	06.6	14.1	05.7	09.1	05.4
4	11/12/66	1303	13.1	29.2	07.5	26.9	06.9	25.8	06.8	21.1	06.2	12.6	06.0
2	11/12/66	1314	12.8	30.1	07.8	29.7	07.4	26.8	07.0	20.8	06.6	20.8	06.6
15	21/01/67	1325	10.1	27.5	06.2	27.4	05.9	15.3	05.2	09.1	03.5	00.0	03.6
16	21/01/67	1342	10.4	27.3	06.2	27.3	06.0	10.6	05.2	09.5	03.5	00.0	03.6
171	21/01/67	1351	07.6	24.6	05.8	-	-	08.2	03.8	00.0	03.5	00.0	03.7
18	21/01/67	1400	15.2	25.4	06.1	19.9	05.1	03.4	03.8	00.0	03.6	00.0	03.7
19	21/01/67	1415	08.8	21.9	05.5	-	-	00.0	03.3	00.0	03.4	00.0	03.4
20	21/01/67	1434	12.2	00.0	03.3	00.0	03.4	00.0	03.4	00.0	03.4	00.0	03.6
22	21/01/67	1505	09.1	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.6	00.0	03.8
23	21/01/67	1520	13.7	00.0	03.6	00.0	03.6	00.0	03.6	00.0	03.7	00.0	03.8
24	21/01/67	1555	16.7	00.0	03.4	00.0	03.4	00.0	03.4	00.0	03.5	00.0	03.7
23	22/01/67	0804	15.2	00.0	03.3	00.0	03.3	00.0	03.3	00.0	03.4	00.0	03.4
22	22/01/67	0819	09.1	00.0	03.0	00.0	03.0	00.0	03.1	00.0	03.0	00.0	03.1
20	22/01/67	0845	09.7	00.0	03.1	00.0	03.1	00.0	03.1	00.0	03.1	00.0	03.1
19	22/01/67	0905	06.2	00.0	03.2	-	-	00.0	03.2	00.0	03.2	00.0	03.2
18	22/01/67	0915	09.7	12.3	04.3	01.4	03.3	00.0	03.1	00.0	03.1	00.0	03.1
171	22/01/67	0923	06.5	02.1	03.4	-	-	02.1	03.3	01.0	03.3	00.0	03.3
16	22/01/67	0930	08.5	25.2	05.7	-	-	10.3	03.9	00.0	03.1	00.0	03.1
15	22/01/67	0945	09.1	27.2	06.1	27.1	06.0	24.5	05.5	00.7	03.4	00.5	03.4
14	22/01/67	0950	07.6	27.7	06.3	-	-	27.2	05.8	08.2	03.7	02.6	03.5
13	22/01/67	0958	09.7	28.3	06.4	28.3	06.2	17.2	05.4	03.4	03.6	01.9	03.6
11	22/01/67	1005	07.6	29.2	06.5	-	-	21.7	05.7	03.3	03.6	02.1	03.6
10	22/01/67	1012	09.1	29.3	06.6	29.3	06.4	29.2	05.8	04.9	03.7	02.6	03.7
8	22/01/67	1020	09.1	29.3	06.5	29.1	06.2	23.7	05.2	04.3	03.8	04.0	03.9
7	22/01/67	1025	09.1	29.4	06.3	28.8	06.1	25.5	05.2	05.8	03.9	05.8	04.0
6	22/01/67	1029	09.7	29.3	06.3	28.7	06.0	27.1	05.2	07.1	04.0	07.0	04.0
5	22/01/67	1039	10.7	29.0	05.9	28.1	05.6	25.2	05.1	22.4	04.5	17.2	04.3
4	22/01/67	1045	09.1	28.9	06.1	28.6	05.9	28.4	05.7	23.8	05.1	23.5	05.1
3	22/01/67	1053	08.2	28.8	06.1	-	-	28.7	06.0	28.7	06.0	28.6	05.8
2	22/01/67	1100	08.5	28.9	06.3	-	-	28.9	06.3	28.9	06.3	28.9	06.1

STA	DATE	TIME (PST)	DEPTH TO BOT IN M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
2	16/02/67	0832	08.8	30.7	06.6	-	-	30.3	06.3	25.2	05.3	12.5	04.5
3	16/02/67	0846	09.1	30.6	06.7	30.6	06.7	30.6	06.5	27.6	06.1	08.9	04.6
4	16/02/67	0854	10.7	30.4	06.7	30.3	06.7	30.3	06.5	21.7	05.3	11.5	04.3
5	16/02/67	0903	10.7	30.3	06.7	30.3	06.7	28.4	06.2	24.4	05.3	03.7	04.0
6	16/02/67	0911	12.2	30.3	06.8	30.3	06.7	27.9	06.3	22.8	05.3	03.5	03.8
7	16/02/67	0919	11.3	30.0	06.8	30.0	06.7	28.6	06.5	20.7	05.2	08.2	04.6
8	16/02/67	0927	09.1	29.7	06.7	29.7	06.7	29.7	06.3	21.8	05.3	01.9	04.0
9	16/02/67	0933	07.9	29.4	06.7	-	-	29.0	06.4	18.8	05.4	04.4	04.3
10	16/02/67	0940	07.3	29.3	06.6	-	-	29.0	06.3	11.5	04.6	04.0	04.2
11	16/02/67	0948	07.6	29.1	06.6	-	-	28.5	06.3	12.6	04.5	07.6	04.2
13	16/02/67	0958	07.9	29.4	06.5	-	-	24.6	05.8	12.6	04.6	04.7	04.0
14	16/02/67	1009	09.7	28.0	06.5	28.1	06.3	23.9	05.7	06.3	04.1	04.7	04.0
15	16/02/67	1024	09.1	27.8	06.5	27.7	06.3	25.6	06.0	07.7	04.2	00.7	03.8
16	16/02/67	1032	09.1	28.0	06.6	28.1	06.4	24.1	05.7	04.3	03.8	00.7	03.7
172	16/02/67	1042	10.1	26.6	06.2	21.9	05.9	04.9	04.0	00.3	03.6	00.0	03.7
18	16/02/67	1053	06.1	10.6	04.4	-	-	10.6	04.4	00.8	03.7	00.0	03.7
19	16/02/67	1106	08.5	19.6	05.2	-	-	02.7	03.7	00.3	03.6	00.0	03.7
20	16/02/67	1123	07.9	00.4	03.7	00.3	03.7	00.0	03.7	00.0	03.7	00.0	03.7
22	16/02/67	1154	09.1	00.0	03.5	00.0	03.5	00.0	03.6	00.0	03.6	00.0	03.7
23	16/02/67	1209	13.4	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.7
24	16/02/67	1240	12.8	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.6	00.0	03.7
23	17/02/67	0812	13.1	00.0	03.3	00.0	03.3	00.0	03.3	00.0	03.3	00.0	03.3
22	17/02/67	0842	07.9	00.0	03.1	-	-	00.0	03.1	00.0	03.1	00.0	03.1
20	17/02/67	0920	12.5	00.0	03.2	00.0	03.2	00.0	03.2	00.0	03.2	00.0	03.1
19	17/02/67	0955	08.5	21.0	05.4	-	-	00.3	03.2	00.0	03.2	00.0	03.2
18	17/02/67	1010	12.2	26.6	06.1	26.1	05.9	12.2	04.6	00.7	03.4	00.3	03.4
172	17/02/67	1020	09.1	27.6	06.1	27.5	05.9	09.8	04.2	00.7	03.5	00.4	03.4
16	17/02/67	1030	08.2	29.0	06.6	-	-	24.3	05.8	03.7	03.7	00.4	03.5
15	17/02/67	1043	09.1	30.0	06.7	30.0	06.7	29.0	06.3	10.1	04.1	00.9	03.7
14	17/02/67	1055	08.8	29.9	06.8	-	-	29.9	06.4	14.4	04.8	01.2	03.7
13	17/02/67	1102	08.8	30.0	06.9	-	-	28.6	06.5	18.3	05.3	01.7	04.3
11	17/02/67	1109	07.3	30.0	06.8	-	-	29.9	06.4	17.2	05.2	01.6	04.3
8	17/02/67	1142	07.3	30.3	06.7	-	-	30.3	06.6	27.5	06.0	04.1	04.0
11	17/02/67	1217	06.4	30.0	06.7	-	-	30.0	06.5	24.7	06.0	04.5	03.9
13	17/02/67	1228	07.6	29.9	06.7	-	-	29.9	06.5	23.0	05.3	11.7	04.7
14	17/02/67	1243	09.1	29.8	06.8	29.8	06.7	29.8	06.4	06.7	04.5	01.2	03.9

STA	DATE	TIME (PST)	DEPTH TO BOT IN M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
15	17/02/67	1307	07.6	29.7	06.7			29.7	06.1	10.2	04.4	02.1	04.1
16	17/02/67	1327	07.9	28.9	06.6	-	-	24.1	05.7	00.9	03.8	00.8	04.0
171	17/02/67	1330	06.1	17.5	05.5	-	-	17.5	05.3	11.8	04.7	00.0	04.1
18	17/02/67	1353	12.8	26.8	06.5	23.0	05.9	00.9	03.8	00.0	03.7	00.0	03.9
183	17/02/67	1358	12.2	26.3	06.2	02.1	05.8	00.5	03.7	00.3	03.7	00.0	03.8
184	17/02/67	1407	09.1	10.9	04.2	04.4	04.1	01.3	03.8	00.5	03.8	00.0	03.9
19	17/02/67	1415	07.3	15.8	05.1	-	-	02.1	03.8	00.7	03.8	00.0	03.9
193	17/02/67	1424	07.9	19.2	05.3	-	-	09.6	04.4	01.3	03.8	00.0	03.9
194	17/02/67	1432	10.9	19.9	06.0	16.8	05.3	10.1	04.7	00.4	03.9	00.0	03.9
20	17/02/67	1452	12.2	01.3	03.6	00.0	03.6	00.0	03.7	00.0	03.7	00.0	03.9
2	10/03/67	1300	07.3	30.5	06.8	-	-	29.4	06.6	22.2	06.0	14.6	05.7
4	10/03/67	1317	08.5	29.5	06.6	-	-	27.3	06.0	20.9	05.3	08.7	04.3
6	10/03/67	1335	10.4	28.8	06.4	27.3	06.2	25.2	06.0	12.0	05.1	05.5	04.2
8	10/03/67	1350	06.7	27.6	06.2	-	-	23.9	05.6	06.3	04.4	05.1	04.3
10	10/03/67	1402	06.7	21.5	05.8	-	-	20.8	05.5	07.0	04.4	04.6	04.1
11	10/03/67	1408	07.0	26.4	05.9	-	-	19.6	05.3	04.6	04.2	03.4	04.0
13	10/03/67	1418	07.3	26.0	05.8	-	-	15.3	05.0	11.4	04.7	03.8	04.0
14	10/03/67	1432	09.1	24.7	06.0	23.2	05.7	15.3	04.9	05.5	04.2	02.5	03.8
15	10/03/67	1448	09.1	25.1	05.8	20.2	05.1	11.0	04.6	01.1	03.9	01.0	03.8
16	10/03/67	1500	09.1	17.0	05.2	07.4	04.3	02.2	04.0	01.5	03.8	00.4	03.7
172	10/03/67	1510	10.4	13.0	04.6	02.0	03.9	01.3	03.7	00.0	03.7	00.0	03.7
18	10/03/67	1520	14.6	06.8	04.2	02.2	03.7	00.0	03.6	00.0	03.6	00.0	03.4
183	10/03/67	1528	12.8	00.0	03.7	00.0	03.6	00.0	03.5	00.0	03.5	00.0	03.4
203	10/03/67	1600	09.1	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.4
195	10/03/67	1610	15.2	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.4
172	11/03/67	1212	09.1	10.3	05.2	09.9	05.1	05.4	04.7	00.0	04.5	00.0	04.9
18	11/03/67	1225	12.2	00.0	04.3	00.0	04.4	00.0	04.4	00.0	04.4	00.0	04.8
19	11/03/67	1242	06.7	00.0	04.3	-	-	00.0	04.3	00.0	04.3	00.0	04.8
194	11/03/67	1251	10.4	00.0	04.2	00.0	04.3	00.0	04.3	00.0	04.3	00.0	04.7
195	11/03/67	1301	13.7	00.0	04.1	00.0	04.2	00.0	04.2	00.0	04.2	00.0	04.2
20	11/03/67	1309	11.6	00.0	04.2	00.0	04.2	00.0	04.2	00.0	04.2	00.0	04.2
22	11/03/67	1348	08.5	00.0	04.2	-	-	00.0	04.2	00.0	04.3	00.0	04.4
23	11/03/67	1406	12.2	00.0	04.1	00.0	04.2	00.0	04.2	00.0	04.3	00.0	04.6
24	11/03/67	1444	11.9	00.0	04.2	00.0	04.2	00.0	04.2	00.0	04.2	00.0	04.4

STA	DATE	TIME (PST)	DEPTH TO BOT IN M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
23	12/03/67	0805	10.7	00.0	03.3	00.0	03.2	00.0	03.2	00.0	03.2	00.0	03.0
22	12/03/67	0822	08.8	00.0	03.6	-	-	00.0	03.5	00.0	03.5	00.0	03.5
203	12/03/67	0850	10.4	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.4
20	12/03/67	0859	11.9	00.0	03.6	00.0	03.6	00.0	03.6	00.0	03.6	00.0	03.4
193	12/03/67	0916	10.9	00.0	03.8	00.0	03.8	00.0	03.7	00.0	03.7	00.0	03.7
19	12/03/67	0923	07.9	00.4	04.0	-	-	00.3	03.9	00.0	03.9	00.0	03.9
184	12/03/67	0930	09.1	01.9	04.1	01.8	04.1	01.2	04.1	00.6	04.0	00.0	04.1
16	12/03/67	1003	09.1	22.1	05.7	21.1	05.3	12.1	04.5	02.9	04.2	01.5	04.0
184	12/03/67	1037	09.1	01.9	04.6	01.0	04.6	00.4	04.6	00.0	04.7	00.0	04.8
172	12/03/67	1104	10.9	14.0	05.1	09.6	04.7	07.0	04.4	00.4	04.1	00.4	04.1
16	12/03/67	1112	08.5	22.1	05.5	-	-	04.1	04.1	02.7	04.0	00.4	04.0
15	12/03/67	1122	09.1	22.4	05.5	20.1	05.2	12.3	04.3	03.6	04.1	01.0	04.0
14	12/03/67	1131	07.9	22.9	05.5	-	-	12.8	04.2	05.3	04.2	02.7	04.1
12	12/03/67	1303	06.1	23.4	06.2	-	-	19.9	05.8	06.8	05.1	02.6	05.3
10	12/03/67	1311	07.0	21.6	05.8	-	-	12.2	05.1	05.6	04.8	04.6	04.9
8	12/03/67	1319	06.1	22.3	05.4	-	-	13.3	05.0	05.4	04.7	05.1	04.6
7	12/03/67	1327	10.7	24.1	06.2	18.0	05.5	13.0	05.0	05.2	04.8	05.0	04.8
6	12/03/67	1332	09.7	23.7	05.9	21.1	05.6	12.8	05.0	09.5	04.7	04.9	04.6
5	12/03/67	1337	09.1	26.2	06.2	22.5	05.8	17.9	05.1	09.7	04.8	06.8	04.6
4	12/03/67	1343	07.9	26.4	06.2	-	-	23.1	05.7	10.8	04.6	07.6	04.6
3	12/03/67	1348	07.6	27.4	06.3	-	-	25.4	05.9	18.4	05.2	08.8	04.8
2	12/03/67	1355	06.7	30.1	06.8	-	-	29.3	06.2	20.9	05.4	08.5	04.9
2	21/04/67	1348	07.6	30.2	08.2	-	-	30.0	08.5	27.4	08.8	06.6	08.9
3	21/04/67	1356	08.5	30.1	08.1	-	-	30.1	08.3	21.7	08.6	13.3	08.7
4	21/04/67	1405	09.1	30.0	08.0	29.9	08.0	29.8	08.2	19.6	08.3	06.5	08.0
5	21/04/67	1412	10.4	29.9	08.0	29.9	08.2	22.5	08.4	15.7	08.1	11.2	08.2
6	21/04/67	1420	11.6	29.7	08.1	29.5	08.2	25.1	08.4	17.5	08.0	06.6	08.0
7	21/04/67	1432	10.7	29.0	08.1	26.2	08.3	22.2	08.4	19.4	08.1	04.6	07.9
8	21/04/67	1442	07.3	27.2	08.1	-	-	24.9	08.2	17.2	08.0	03.8	07.9
9	21/04/67	1447	08.8	27.2	08.3	-	-	25.8	08.2	14.8	07.9	03.5	07.9
10	21/04/67	1455	08.5	26.9	08.1	-	-	25.3	08.2	13.8	07.7	03.2	07.9
11	21/04/67	1517	06.1	25.2	08.3	-	-	24.5	08.3	03.9	07.8	02.9	07.9
13	21/04/67	1522	06.4	24.6	08.2	-	-	23.5	08.0	05.5	07.7	02.6	07.9
14	21/04/67	1532	09.1	23.3	08.1	23.0	08.0	14.5	07.8	05.9	07.5	01.5	07.6
15	21/04/67	1545	09.1	18.8	08.0	17.9	07.9	09.7	07.7	03.4	07.6	01.7	07.8
16	21/04/67	1557	09.1	15.3	07.9	14.9	07.6	05.6	07.5	01.4	07.4	00.3	07.7

STA	DATE	TIME (PST)	DEPTH TO BOT IN M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
17	21/04/67	1608	10.7	13.9	07.7	04.7	07.3	00.8	07.3	00.0	07.4	00.0	07.8
173	21/04/67	1614	11.6	07.8	07.3	03.2	07.2	00.4	07.1	00.0	07.1	00.0	07.3
18	21/04/67	1620	12.2	07.1	07.2	01.7	07.0	00.3	07.0	00.0	07.1	00.0	07.2
183	21/04/67	1625	11.6	02.6	07.0	00.4	07.0	00.0	07.0	00.0	07.1	00.0	07.1
184	21/04/67	1633	08.5	00.0	07.0	-	-	00.0	07.0	00.0	07.0	00.0	07.1
194	21/04/67	1645	12.8	00.0	07.0	00.0	07.1	00.0	07.1	00.0	07.1	00.0	07.4
204	23/04/67	0807	08.5	00.0	07.2	-	-	00.0	07.2	00.0	07.2	00.0	07.3
203	23/04/67	0812	09.7	00.0	07.1	00.0	07.1	00.0	07.1	00.0	07.2	00.0	07.3
20	23/04/67	0816	09.7	00.0	07.1	00.0	07.1	00.0	07.1	00.0	07.2	00.0	07.2
194	23/04/67	0826	14.3	00.0	07.1	00.0	07.1	00.0	07.1	00.0	07.1	00.0	07.1
193	23/04/67	0832	09.1	00.0	07.0	00.0	07.0	00.0	07.0	00.0	07.0	00.0	07.1
19	23/04/67	0836	07.6	00.0	07.0	-	-	00.0	07.0	00.0	07.1	00.0	07.1
184	23/04/67	0842	07.9	00.0	07.0	-	-	00.0	07.0	00.0	07.0	00.0	07.1
183	23/04/67	0846	11.6	00.0	07.1	00.0	07.0	00.0	07.0	00.0	07.1	00.0	07.0
18	23/04/67	0850	12.8	00.0	07.0	00.0	07.0	00.0	07.0	00.0	07.1	00.0	07.1
173	23/04/67	0900	13.1	05.8	07.5	00.0	07.2	00.0	07.2	00.0	07.2	00.0	07.1
172	23/04/67	0906	12.2	08.6	07.6	05.4	07.5	00.0	07.3	00.0	07.3	00.0	07.5
16	23/04/67	0914	08.5	04.2	07.4	-	-	03.2	07.3	02.4	07.3	00.8	07.3
15	23/04/67	0922	07.6	09.3	07.6	-	-	04.7	07.5	03.2	07.4	01.9	07.5
14	23/04/67	0931	09.1	12.6	07.9	11.9	07.8	05.9	07.5	05.0	07.5	03.8	07.5
18	23/04/67	1139	11.3	00.0	08.1	00.0	08.1	00.0	08.3	00.0	08.3	00.0	08.6
173	23/04/67	1148	12.8	00.0	07.7	00.0	07.7	00.0	07.9	00.0	08.0	00.0	08.6
17	23/04/67	1154	10.1	00.0	07.7	00.0	07.7	00.0	07.8	00.0	07.8	00.0	07.9
16	23/04/67	1200	06.7	00.0	07.7	-	-	00.0	07.7	00.0	07.8	00.0	08.0
15	23/04/67	1213	06.1	00.0	07.7	-	-	00.0	07.7	00.0	07.8	00.0	08.1
14	23/04/67	1220	07.6	00.0	07.8	-	-	00.0	07.9	00.0	07.9	00.0	08.1
13	23/04/67	1227	06.1	00.0	07.8	-	-	00.0	07.8	00.0	07.9	00.0	08.1
12	23/04/67	1231	06.1	00.0	07.7	-	-	00.0	07.7	00.0	07.8	00.0	08.0
11	23/04/67	1235	06.1	00.0	07.6	-	-	00.0	07.6	00.0	07.7	00.0	08.0
10	23/04/67	1242	06.7	01.4	07.6	-	-	01.0	07.5	00.5	07.6	00.0	07.8
8	23/04/67	1248	08.5	01.4	07.5	-	-	01.0	07.4	00.5	07.5	00.4	07.7
6	23/04/67	1254	09.1	02.9	07.4	01.8	07.4	01.5	07.5	01.2	07.4	01.0	07.5
4	23/04/67	1304	09.7	11.3	08.1	08.6	08.1	05.0	08.0	04.1	08.0	02.3	08.2
2	23/04/67	1316	06.7	29.2	08.7	-	-	26.5	08.7	13.3	08.8	06.8	08.5

STA	DATE	TIME (PST)	DEPTH TO BOT IN M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
2	19/05/67	1025	06.7	30.2	08.6	-	-	29.6	09.2	06.9	10.1	00.0	10.9
4	19/05/67	1052	09.1	29.5	08.8	25.3	09.0	15.3	09.6	00.0	10.4	00.0	10.9
5	19/05/67	1100	09.7	28.5	08.8	24.5	09.1	10.0	10.0	00.0	10.3	00.0	10.7
6	19/05/67	1107	10.7	22.6	09.2	11.2	09.8	00.0	10.3	00.0	10.3	00.0	10.5
7	19/05/67	1114	11.6	00.0	10.1	00.0	10.1	00.0	10.2	00.0	10.2	00.0	10.4
8	19/05/67	1123	09.7	00.0	10.2	00.0	10.2	00.0	10.3	00.0	10.3	00.0	10.4
9	19/05/67	1130	09.7	00.0	10.3	00.0	10.3	00.0	10.3	00.0	10.4	00.0	10.5
10	19/05/67	1135	08.2	00.0	10.2	-	-	00.0	10.2	00.0	10.3	00.0	10.3
2	19/05/67	1203	07.0	30.2	08.5	-	-	29.5	09.2	04.4	10.4	02.8	10.6
3	19/05/67	1213	07.6	30.0	08.7	-	-	29.0	09.2	00.6	10.4	00.0	10.7
4	19/05/67	1221	09.1	29.7	08.5	28.1	08.9	22.2	09.3	01.6	10.3	00.0	10.8
5	19/05/67	1229	10.7	29.4	08.7	26.3	09.2	08.0	10.1	00.3	10.4	00.0	10.6
6	19/05/67	1238	12.2	27.3	08.7	24.5	09.2	06.0	10.2	01.0	10.3	00.0	10.6
7	19/05/67	1247	11.3	27.5	09.0	15.0	09.6	00.7	10.3	00.0	10.4	00.0	10.5
8	19/05/67	1256	09.2	18.9	09.5	09.5	10.0	00.0	10.3	00.0	10.4	00.0	10.6
9	19/05/67	1305	09.7	08.4	09.9	04.7	10.1	00.0	10.4	00.0	10.4	00.0	10.5
10	19/05/67	1312	08.5	00.0	10.4	-	-	00.0	10.4	00.0	10.5	00.0	10.7
2	19/05/67	1339	06.7	30.4	08.6	-	-	28.7	09.6	08.2	11.0	03.4	11.0
3	19/05/67	1350	08.5	30.2	08.6	-	-	27.5	09.2	11.0	11.6	00.5	11.0
4	19/05/67	1358	09.4	30.2	08.5	30.2	08.7	23.1	09.6	03.2	10.7	00.0	10.9
5	19/05/67	1406	10.4	29.7	08.6	28.9	08.8	19.1	10.1	07.3	10.6	00.0	10.9
6	19/05/67	1415	13.1	29.2	08.7	26.6	08.9	16.6	09.7	07.6	10.6	00.0	10.8
7	19/05/67	1425	15.8	28.5	08.9	25.3	09.1	17.3	09.7	00.0	10.7	00.0	10.9
8	19/05/67	1434	14.9	27.5	08.9	24.5	09.4	00.2	10.6	00.0	10.6	00.0	10.8
9	19/05/67	1442	10.7	26.5	09.0	20.9	09.5	00.0	10.5	00.0	10.6	00.0	10.8
10	19/05/67	1450	07.0	08.4	10.3	-	-	00.0	10.5	00.0	10.6	00.0	10.7
11	19/05/67	1457	06.7	00.0	10.5	-	-	00.0	10.6	00.0	10.7	00.0	10.7
251	19/05/67	1705	07.0	00.0	11.4			00.0	11.4	00.0	11.1	00.0	11.1
2	20/05/67	0830	09.1	30.1	08.7	29.9	09.0	21.6	09.8	04.5	10.7	03.2	11.3
3	20/05/67	0842	06.7	00.8	10.2	-	-	00.7	10.2	00.7	10.3	00.5	10.6
4	20/05/67	0852	07.6	00.0	10.2	-	-	00.0	10.3	00.0	10.5	00.0	10.5
5	20/05/67	0900	08.2	00.0	10.3	-	-	00.0	10.4	00.0	10.6	00.0	10.6
6	20/05/67	0915	12.2	00.0	10.6	00.0	10.6	00.0	10.6	00.0	10.5	00.0	10.5
7	20/05/67	0926	13.7	00.0	10.4	00.0	10.4	00.0	10.5	00.0	10.5	00.0	10.7
8	20/05/67	0935	10.4	00.0	10.3	00.0	10.4	00.0	10.5	00.0	10.5	00.0	10.7
9	20/05/67	0943	06.1	00.0	10.3	-	-	00.0	10.4	00.0	10.5	00.0	10.7

STA	DATE	TIME (PST)	DEPTH TO BOT IN M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
10	20/05/67	0953	06.1	00.0	10.3	-	-	00.0	10.4	00.0	10.5	00.0	10.7
11	20/05/67	1000	06.4	00.0	10.2	-	-	00.0	10.3	00.0	10.4	00.0	10.6
2	20/05/67	1120	06.4	29.2	09.3	-	-	27.9	09.7	16.2	10.7	03.0	11.2
3	20/05/67	1129	07.6	29.1	09.2	-	-	26.5	09.6	03.7	10.7	00.0	11.0
4	20/05/67	1137	09.1	27.9	09.4	13.9	10.0	00.3	10.6	00.0	10.7	00.0	11.0
5	20/05/67	1144	09.1	00.0	10.5	00.0	10.5	00.0	10.5	00.0	10.6	00.0	10.8
6	20/05/67	1151	12.2	00.0	10.5	00.0	10.5	00.0	10.6	00.0	10.6	00.0	10.9
7	20/05/67	1158	13.7	00.0	10.5	00.0	10.6	00.0	10.6	00.0	10.7	00.0	10.9
8	20/05/67	1205	12.8	00.0	10.5	00.0	10.5	00.0	10.5	00.0	10.7	00.0	10.8
9	20/05/67	1211	09.7	00.0	10.5	00.0	10.5	00.0	10.5	00.0	10.6	00.0	10.8
10	20/05/67	1219	07.6	00.0	10.5	-	-	00.0	10.5	00.0	10.6	00.0	10.7
11	20/05/67	1225	07.0	00.0	10.5	-	-	00.0	10.6	00.0	10.6	00.0	10.7
14	20/05/67	1238	08.5	00.0	10.8	-	-	00.0	10.8	00.0	10.8	00.0	11.1
16	20/05/67	1303	08.5	00.0	11.2			00.0	11.3	00.0	11.3	00.0	11.6
18	20/05/67	1340	12.8	00.0	11.5	-	-	00.0	11.8	00.0	11.9	00.0	12.1
19	20/05/67	1400	07.6	00.0	11.6	-	-	00.0	11.7	00.0	11.7	00.0	12.2
20	20/05/67	1425	12.2	00.0	11.4	00.0	11.5	00.0	11.6	00.0	11.7	00.0	12.0
22	20/05/67	1500	09.1	00.0	11.9	00.0	12.1	00.0	12.2	00.0	12.4	00.0	12.6
23	20/05/67	1520	10.7	00.0	11.9	00.0	12.0	00.0	12.0	00.0	12.2	00.0	12.5
24	20/05/67	1600	12.8	00.0	11.6	00.0	11.7	00.0	11.9	00.0	12.0	00.0	12.4
23	05/06/67	1050	13.4	00.0	12.4	00.0	12.5	00.0	12.6	00.0	12.8	00.0	12.8
22	05/06/67	1100	10.7	00.0	12.3	00.0	12.3	00.0	12.4	00.0	12.6	00.0	12.9
20	05/06/67	1120	09.0	00.0	12.3	00.0	12.3	00.0	12.4	00.0	12.6	00.0	12.9
19	05/06/67	1132	09.4	00.0	12.3	-	-	00.0	12.4	00.0	12.6	00.0	13.0
18	05/06/67	1140	11.9	00.0	12.1	00.0	12.2	00.0	12.4	00.0	12.5	00.0	12.8
17	05/06/67	1145	11.5	00.0	11.9	00.0	11.9	00.0	11.9	00.0	12.1	00.0	12.3
16	05/06/67	1156	09.1	00.0	11.9	00.0	11.9	00.0	11.9	00.0	12.0	00.0	12.1
15	05/06/73	1200	09.1	00.0	11.9	00.0	11.9	00.0	11.9	00.0	12.0	00.0	12.2
14	05/06/67	1205	08.2	00.0	11.8	-	-	00.0	11.9	00.0	11.9	00.0	12.0
13	05/06/67	1210	06.7	00.0	11.8	-	-	00.0	11.8	00.0	11.9	00.0	11.8
12	05/06/67	1215	05.8	00.0	11.7	-	-	00.0	11.8	00.0	11.8	00.0	11.8
11	05/06/67	1217	05.8	00.0	11.8	-	-	00.0	11.8	00.0	11.8	00.0	11.9
10	05/06/67	1221	06.1	00.0	11.8	-	-	00.0	11.8	00.0	11.8	00.0	12.0
9	05/06/67	1224	07.6	00.0	11.8	-	-	00.0	11.8	00.0	11.9	00.0	12.0
8	05/06/67	1227	06.7	00.0	11.7	-	-	00.0	11.8	00.0	11.9	00.0	11.9
7	05/06/67	1231	10.1	00.0	11.8	00.0	11.8	00.0	11.8	00.0	11.8	00.0	11.9

STA	DATE	TIME (PST)	DEPTH TO BOT IN M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
6	05/06/67	1235	12.2	00.0	11.8	00.0	11.8	00.0	11.8	00.0	11.8	00.0	11.9
5	05/06/67	1240	10.1	00.0	11.8	00.0	11.8	00.0	11.9	00.0	11.8	00.0	11.9
4	05/06/67	1246	09.8	00.0	11.9	00.0	11.9	00.0	11.9	00.0	11.9	00.0	12.1
3	05/06/67	1250	07.6	00.0	11.9	-	-	00.0	11.9	00.0	11.9	00.0	11.9
2	05/06/67	1255	06.1	23.7	10.4	-	-	13.9	10.9	00.5	11.9	00.0	12.0
2	05/06/67	1325	06.1	29.5	09.4	-	-	19.3	11.6	05.3	12.0	01.5	12.0
4	05/06/67	1340	09.1	00.0	12.0	00.0	12.0	00.0	12.0	00.0	12.1	00.0	12.2
6	05/06/67	1352	10.7	00.0	11.9	00.0	12.0	00.0	12.1	00.0	12.2	00.0	12.4
8	05/06/67	1405	08.5	00.0	12.0	-	-	00.0	12.1	00.0	12.1	00.0	12.4
10	05/06/67	1416	06.7	00.0	12.0	-	-	00.0	12.0	00.0	12.1	00.0	12.4
11	05/06/67	1425	06.7	00.0	12.0	-	-	00.0	12.0	00.0	12.0	00.0	12.2
12	05/06/67	1428	06.1	00.0	11.9	-	-	00.0	11.9	00.0	12.0	00.0	12.1
2	05/06/67	1500	07.6	28.2	10.2	-	-	24.1	11.7	08.8	12.1	00.0	12.8
4	05/06/67	1512	11.3	27.1	10.6	17.2	11.5	10.7	12.6	00.0	12.7	00.0	13.2
6	05/06/67	1522	10.7	00.0	12.9	00.0	13.0	00.0	13.0	00.0	13.2	00.0	13.2
8	05/06/67	1532	07.1	00.0	12.5	-	-	00.0	12.5	00.0	12.7	00.0	13.1
10	05/06/67	1543	08.5	00.0	12.4	-	-	00.0	12.4	00.0	12.5	00.0	12.9
11	05/06/67	1551	08.2	00.0	12.3	-	-	00.0	12.4	00.0	12.5	00.0	12.9
12	05/06/67	1555	07.6	00.0	12.3	-	-	00.0	12.3	00.0	12.4	00.0	12.9
2	05/06/67	1647	07.6	30.1	09.3	-	-	25.2	11.3	07.8	13.8	04.3	13.5
22	30/07/67	1405	08.5	00.0	17.1	-	-	00.0	17.6	00.0	17.6	00.0	18.0
20	30/07/67	1430	09.7	00.0	17.1	00.0	17.6	00.0	17.6	00.0	17.6	00.0	17.8
194	30/07/67	1454	14.6	00.0	17.5	00.0	17.6	00.0	17.5	00.0	17.6	00.0	17.8
19	30/07/67	1504	07.1	00.0	17.4	-	-	00.0	17.6	00.0	17.6	00.0	17.9
18	30/07/67	1515	10.9	00.0	17.5	00.0	17.5	00.0	17.6	00.0	17.6	00.0	17.9
17	30/07/67	1525	15.2	00.0	17.6	00.0	17.6	00.0	17.7	00.0	17.8	00.0	18.0
16	30/07/67	1625	07.6	00.0	17.8	-	-	00.0	17.8	00.0	17.9	00.0	18.1
15	30/07/67	1635	09.4	00.0	17.9	00.0	17.7	00.0	17.7	00.0	17.7	00.0	18.0
14	30/07/67	1646	09.1	00.0	17.6	00.0	17.6	00.0	17.6	00.0	17.8	00.0	18.0
13	30/07/67	1652	07.3	03.7	17.2	-	-	00.0	17.5	00.0	17.6	00.0	17.8
12	30/07/67	1659	06.1	24.8	13.7	-	-	01.8	17.5	00.0	17.5	00.0	17.7
11	30/07/67	1704	06.1	25.5	13.3	-	-	04.6	16.5	00.0	17.4	00.0	17.5
10	30/07/67	1710	09.1	27.1	12.5	26.7	13.5	04.9	16.4	00.0	17.3	00.0	17.6
9	30/07/67	1716	09.1	27.5	12.3	26.8	13.7	13.6	16.0	00.0	17.5	00.0	17.4
8	30/07/67	1721	06.1	27.3	13.2	-	-	25.2	15.8	00.8	17.3	00.3	17.5
7	30/07/67	1726	05.5	27.5	12.9	-	-	25.6	14.6	01.9	17.3	00.3	17.5

STA	DATE	TIME (PST)	DEPTH TO BOT IN M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
6	30/07/67	1733	09.7	28.2	12.5	27.7	13.6	26.8	13.8	10.9	16.4	01.0	17.6
5	30/07/67	1734	09.7	29.1	11.8	28.3	12.3	25.8	13.7	17.2	15.7	02.7	17.6
4	30/07/67	1744	07.6	29.4	11.1	-	-	26.3	14.2	19.2	14.9	00.8	17.5
3	30/07/67	1749	09.1	29.4	11.1	29.0	11.7	27.5	13.5	17.9	15.2	10.1	16.3
2	30/07/67	1755	09.1	29.3	11.2	28.9	11.7	27.8	12.8	15.7	15.7	04.3	16.3
2	26/08/67	0828	08.0	30.2	10.5	-	-	29.6	11.9	18.6	17.7	09.0	18.0
3	26/08/67	0837	09.0	29.7	11.0	29.7	11.0	28.8	12.5	13.4	16.6	07.9	18.1
4	26/08/67	0845	10.0	29.7	10.9	29.5	11.2	29.1	12.2	19.2	15.6	05.0	18.3
5	26/08/67	$08^{5}2$	10.0	29.4	11.1	29.3	11.5	25.7	14.9	15.0	16.9	03.3	17.9
6	26/08/67	0900	11.0	29.1	11.5	29.1	11.9	23.3	13.5	16.4	16.1	01.7	18.7
7	26/08/67	0907	12.0	28.7	11.8	27.4	12.6	24.1	13.7	19.4	15.9	03.3	18.0
8	26/08/67	0918	07.0	27.6	12.6	-	-	26.5	13.8	01.0	16.4	00.0	18.7
9	26/08/67	0923	08.0	27.2	12.5	-	-	26.7	12.8	00.5	18.4	00.0	18.7
10	26/08/67	0930	08.3	26.1	12.8	-	-	21.7	14.9	00.3	18.6	00.0	18.7
11	26/08/67	0937	07.0	24.4	13.1	-	-	17.0	14.9	14.0	18.6	00.0	18.6
12	26/08/67	0942	07.3	23.1	13.4	-	-	10.1	16.6	00.0	18.5	00.0	18.5
13	26/08/67	0947	08.2	18.0	15.1	-	-	00.0	18.5	00.0	18.5	00.0	18.5
14	26/08/67	0954	11.0	00.0	18.6	00.0	18.6	00.0	18.6	00.0	18.6	00.0	18.6
15	26/08/67	1005	12.0	00.0	18.6	00.0	18.7	00.0	18.7	00.0	18.7	00.0	18.8
16	26/08/67	1018	10.0	00.0	18.6	00.0	18.6	00.0	18.6	00.0	18.6	00.0	18.8
17	26/08/67	1027	12.0	00.0	18.6	00.0	18.6	00.0	18.6	00.0	18.6	00.0	19.8
18	26/08/67	1140	12.3	00.0	18.8	00.0	18.8	00.0	18.9	00.0	18.9	00.0	19.3
19	26/08/67	1152	07.0	00.0	18.8	-	-	00.0	18.8	00.0	18.8	00.0	19.0
20	26/08/67	1209	10.0	00.0	18.6	00.0	18.7	00.0	18.7	00.0	18.7	00.0	19.1
22	26/08/67	1244	09.0	00.0	18.9	-	-	00.0	18.9	00.0	18.9	00.0	19.2
23	26/08/67	1259	15.0	00.0	18.9	00.0	18.9	00.0	18.9	00.0	18.9	00.0	19.2
24	26/08/67	1336	09.0	00.0	19.3	00.0	19.3	00.0	19.3	00.0	19.3	00.0	19.6
2	27/08/67	1159	09.0	29.3	11.9	29.3	11.9	28.5	13.0	23.4	17.4	02.5	19.2
3	27/08/67	1210	10.0	28.8	12.3	28.6	12.5	27.8	14.0	22.9	15.7	01.0	18.5
4	27/08/67	1218	10.0	29.1	11.9	29.0	12.1	27.5	14.4	21.8	17.8	00.7	19.2
5	27/08/67	1226	07.0	28.7	12.1	-	-	27.3	14.4	19.6	18.1	00.7	18.8
6	27/08/67	1235	13.5	28.3	12.8	28.0	13.2	26.0	15.2	20.6	17.5	00.4	19.2
7	27/08/67	1244	15.0	28.0	13.2	27.3	14.4	26.7	15.3	20.5	17.8	00.3	19.1
8	27/08/67	1253	08.0	27.1	14.4	-	-	26.5	15.5	13.7	18.6	00.0	19.1
9	27/08/67	1301	08.0	26.8	14.5	-	-	26.4	15.3	09.3	17.7	00.0	19.1

STA	DATE	TIME (PST)	DEPTH TO BOT IN M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
10	27/08/67	1310	09.3	26.7	14.3	26.5	14.7	25.6	16.3	06.8	18.4	00.0	19.2
11	27/08/67	1318	09.0	26.3	14.7	26.3	14.7	24.6	16.3	00.8	18.8	00.0	19.2
12	27/08/67	1324	08.0	26.1	14.8	-	-	22.0	16.5	01.0	18.5	00.0	19.1
2	28/08/67	1327	09.0	28.5	13.5	28.5	13.5	26.9	15.5	22.1	17.7	03.4	19.1
4	28/08/67	1338	10.0	27.6	14.5	27.3	15.1	23.4	17.9	22.8	18.0	05.2	19.5
6	28/08/67	1348	09.0	27.2	15.1	27.2	15.1	23.2	17.7	17.9	18.4	00.0	19.5
8	28/08/67	1358	07.5	26.6	16.2	-	-	26.2	16.7	15.4	18.7	00.0	19.8
10	28/08/67	1410	09.0	25.7	16.7	25.7	16.7	25.6	17.1	05.1	18.4	00.0	19.8
12	28/08/67	1418	08.5	25.2	16.9	-	-	13.1	18.3	00.5	19.2	00.0	19.7
2	23/09/67	1116	08.0	30.1	10.9	-	-	29.7	11.3	25.2	13.9	23.1	14.6
3	23/09/67	1127	09.0	29.8	11.3	29.8	11.3	29.4	11.5	24.0	13.9	18.2	14.6
4	23/09/67	1135	10.0	30.1	11.0	29.8	11.1	29.4	11.5	25.3	13.3	03.9	15.2
5	23/09/67	1145	09.0	29.8	11.0	29.8	11.0	29.4	11.5	24.4	13.7	03.4	16.0
6	23/09/67	1152	10.0	29.8	10.9	29.8	11.0	28.7	11.9	25.5	13.6	01.5	16.0
7	23/09/67	1200	07.0	28.3	12.1	-	-	28.2	12.1	27.0	12.8	07.3	16.4
8	23/09/67	1210	07.0	29.1	11.8	-	-	28.9	12.1	18.9	14.2	01.0	16.7
9	23/09/67	1217	08.0	28.4	12.0	-	-	27.3	12.9	20.6	14.3	00.7	16.9
10	23/09/67	1226	09.0	28.9	11.9	28.9	11.9	26.5	13.3	10.4	15.7	01.1	17.1
11	23/09/67	1234	09.0	28.7	12.1	28.7	12.1	27.6	12.9	07.0	16.1	00.3	17.2
12	23/09/67	1241	08.0	28.0	12.4	-	-	27.3	13.1	14.0	15.2	00.0	17.2
13	23/09/67	1248	09.0	27.8	12.5	27.8	12.5	26.3	13.4	15.5	15.0	00.0	17.3
14	23/09/67	1257	12.0	26.8	13.0	26.3	13.2	22.3	14.0	01.2	17.2	00.0	17.3
15	23/09/67	1305	10.5	25.8	13.4	25.5	13.8	12.6	15.8	00.7	17.2	00.0	17.4
16	23/09/67	1324	08.0	02.8	16.8	-	-	00.7	17.3	00.0	17.4	00.0	17.6
17	23/09/67	1339	12.0	02.8	17.0	01.1	17.3	00.0	17.4	00.0	17.5	00.0	17.6
18	23/09/67	1349	07.0	00.0	17.3	-	-	00.0	17.3	00.0	17.3	00.0	17.5
20	23/09/67	1416	09.0	00.0	17.4	00.0	17.4	00.0	17.4	00.0	17.5	00.0	17.5
22	23/09/67	1452	07.0	00.0	17.4	-	-	00.0	17.4	00.0	17.4	00.0	17.6
24	23/09/67	1549	08.5	00.0	17.1	-	-	00.0	17.1	00.0	17.2	00.0	17.4
2	20/11/67	1110	09.1	29.7	09.0	28.8	08.9	28.4	09.0	25.9	08.9	23.0	08.6
3	20/11/67	1118	10.5	29.7	09.1	29.4	09.1	28.3	09.1	25.9	08.8	22.6	08.6
4	20/11/67	1129	09.1	28.9	09.0	28.9	09.1	27.7	09.1	25.0	08.8	22.1	08.3
5	20/11/67	1141	09.1	28.9	09.0	28.8	09.0	27.7	09.0	24.7	08.6	21.2	08.1
6	20/11/67	1153	09.1	28.5	09.0	27.9	09.0	26.3	08.8	25.1	08.6	14.3	07.2

STA	DATE	TIME (PST)	DEPTH TO BOT IN M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
8	20/11/67	1226	12.8	28.6	08.9	27.9	09.0	26.8	08.8	25.0	08.6	04.1	06.8
9	20/11/67	1239	09.5	28.3	08.9	28.0	08.9	27.0	08.8	19.6	08.1	01.8	07.1
10	20/11/67	1251	09.0	28.6	08.9	28.6	08.9	27.2	08.8	21.6	07.9	01.6	06.7
11	20/11/67	1302	10.9	28.1	08.9	28.1	08.9	26.3	08.7	20.7	07.2	01.1	06.7
12	20/11/67	1310	08.0	26.8	08.9	-	-	23.7	08.2	06.4	06.9	02.7	06.7
13	20/11/67	1318	13.7	26.4	08.9	26.4	08.8	25.7	08.4	21.7	08.1	00.7	06.7
14	20/11/67	1330	10.3	25.5	08.6	24.8	08.6	23.5	08.2	21.7	06.7	00.4	06.5
15	20/11/67	1345	10.5	23.8	08.4	23.1	08.4	15.9	07.7	00.6	06.4	00.0	06.5
16	20/11/67	1400	09.7	21.0	08.1	15.9	07.7	00.9	06.5	00.5	06.5	00.0	06.5
17	20/11/67	1412	10.9	18.9	07.9	06.8	06.9	01.7	06.5	00.0	06.4	00.0	06.4
18	20/11/67	1427	10.9	00.0	06.4	00.0	06.3	00.0	06.3	00.0	06.3	00.0	06.4
19	20/11/67	1440	13.7	00.0	06.3	00.0	06.3	00.0	06.3	00.0	06.3	00.0	06.3
20	20/11/67	1455	11.5	00.0	06.3	00.0	06.3	00.0	06.3	00.0	06.3	00.0	06.3
2	13/01/68	1020	12.8	30.9	06.6	30.9	06.6	30.8	06.5	30.0	06.3	30.2	06.4
5	13/01/68	1043	09.7	29.9	06.4	29.7	06.4	29.4	06.4	27.6	06.1	20.5	05.8
8	13/01/68	1057	11.6	29.4	06.4	29.4	06.4	29.2	06.4	28.5	06.1	08.6	03.2
11	13/01/68	1113	07.5	28.7	06.2	-	-	28.5	06.2	27.3	04.8	07.5	03.1
14	13/01/68	1128	10.9	27.1	05.8	26.9	05.8	26.7	05.7	11.8	03.3	05.4	02.6
15	13/01/68	1205	11.6	26.2	05.6	26.2	05.5	25.7	05.5	05.0	02.3	02.8	02.1
16	13/01/68	1220	10.4	25.1	05.4	24.7	05.1	14.2	03.3	04.0	02.2	02.4	01.9
17	13/01/68	1230	11.6	24.6	05.3	21.8	04.8	17.1	03.9	01.9	02.0	00.8	01.7
18	13/01/68	1242	12.2	23.8	05.2	22.4	04.9	03.6	02.1	01.5	01.9	00.5	01.6
19	13/01/68	1252	09.0	19.8	04.6	19.8	04.6	01.7	01.7	00.7	01.6	00.3	01.5
20	13/01/68	1310	12.8	11.4	03.1	00.3	01.5	00.0	01.5	00.0	01.5	00.0	01.5
21	13/01/68	1334	09.1	00.0	01.6	00.0	01.6	00.0	01.6	00.0	01.6	00.0	01.5
204	13/01/68	1344	08.5	00.0	01.5	-	-	00.0	01.5	00.0	01.5	00.0	01.5
203	13/01/68	1352	10.9	00.0	01.5	00.0	01.5	00.0	01.5	00.0	01.5	00.0	01.5
20	13/01/68	1400	10.9	11.0	03.0	00.3	01.5	00.0	01.5	00.0	01.5	00.0	01.5
193	13/01/68	1426	10.4	22.1	04.7	17.2	04.2	02.4	01.8	01.8	01.7	00.2	01.6
19	13/01/68	1436	10.7	23.0	05.0	23.0	04.9	01.4	01.8	00.4	01.6	00.3	01.6
184	13/01/68	1445	12.2	23.5	05.0	22.5	04.8	02.8	01.9	00.4	01.5	00.4	01.5
183	13/01/68	1455	12.8	23.9	05.3	21.8	04.9	04.3	02.2	00.8	01.7	00.5	01.6
18	13/01/68	1503	12.2	24.4	05.1	22.9	04.8	03.0	02.0	01.4	01.8	01.4	01.7
173	13/01/68	1512	11.6	24.7	05.2	23.5	04.9	15.3	03.8	01.6	01.8	01.0	01.7
17	13/01/68	1523	11.6	25.4	05.5	24.1	05.0	12.5	03.3	03.3	02.0	00.8	01.7
18	13/01/68	1534	12.2	24.5	05.2	22.3	04.7	02.7	01.9	01.0	01.7	00.3	01.6

STA	DATE	TIME (PST)	DEPTH to Bot In M	12M or Bot		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
183	13/01/68	1545	12.8	24.2	05.0	23.6	05.0	04.0	02.1	00.6	01.7	00.3	01.6
184	13/01/68	1550	10.9	23.8	05.1	22.3	04.5	02.4	01.8	00.5	01.6	00.2	01.6
19	13/01/68	1600	09.1	21.8	04.7	21.8	04.7	01.3	01.7	00.6	01.6	00.0	01.6
193	13/01/68	1609	10.4	22.3	04.9	22.3	04.9	03.3	01.9	01.2	01.6	00.0	01.5
20	14/01/68	0843	12.8	00.0	02.0	00.0	02.0	00.0	02.0	00.0	02.0	00.0	02.0
19	14/01/68	0914	09.7	09.1	03.1	08.9	03.0	02.0	02.1	00.6	02.0	00.5	02.0
184	14/01/68	0922	09.7	12.7	03.6	12.2	03.6	09.5	03.2	01.6	02.1	00.9	02.3
18	14/01/68	0932	12.1	19.2	04.7	16.5	04.3	11.9	03.6	02.8	02.4	01.9	02.4
173	14/01/68	0941	15.2	21.1	05.0	19.5	04.8	15.3	04.1	06.2	02.5	02.9	02.4
17	14/01/68	0946	12.8	22.5	05.3	20.6	05.0	17.8	04.4	04.8	03.1	03.4	02.4
16	14/01/68	0958	09.7	23.6	05.5	23.5	05.5	22.9	05.3	13.1	04.0	03.6	02.7
15	14/01/68	1010	09.7	24.2	05.6	24.2	05.5	22.8	05.4	17.5	03.8	04.8	02.8
14	14/01/68	1022	09.7	24.8	05.7	24.8	05.6	24.6	05.6	20.3	04.6	08.8	03.4
12	14/01/68	1032	09.1	28.5	06.3	28.5	06.1	24.9	05.6	23.6	05.7	06.9	03.3
11	14/01/68	1045	08.2	28.5	06.2	-	-	26.0	05.9	21.0	05.2	05.9	03.1
9	14/01/68	1235	09.7	29.3	06.5	28.9	06.5	27.6	06.2	08.1	03.3	04.1	02.7
7	14/01/68	1248	12.2	29.5	06.5	29.3	06.4	27.3	06.0	08.2	03.4	05.1	02.8
5	14/01/68	1304	10.9	30.1	06.5	30.0	06.5	29.0	06.3	24.5	05.6	15.8	04.3
2	14/01/68	1320	09.1	30.8	06.7	30.4	06.7	29.7	06.6	27.8	06.2	18.3	05.1
24	17/02/68	0915	11.6	00.0	01.8	00.0	01.8	00.0	01.8	00.0	01.8	00.0	01.7
23	17/02/68	0954	14.0	00.0	01.7	00.0	01.7	00.0	01.7	00.0	01.6	00.0	01.6
21	17/02/68	1025	09.7	00.0	01.8	00.0	01.8	00.0	01.8	00.0	01.8	00.0	01.8
20	17/02/68	1045	11.9	00.0	01.8	00.0	01.8	00.0	01.8	00.0	01.8	00.0	01.8
19	17/02/68	1107	09.1	00.4	01.9	00.3	01.9	00.3	01.9	00.3	01.9	00.3	01.9
18	17/02/68	1119	12.8	10.7	03.1	04.3	02.3	01.2	02.0	00.7	01.9	00.4	02.0
17	17/02/68	1130	10.9	14.2	03.6	13.2	03.5	07.3	02.7	04.8	02.4	01.9	02.0
16	17/02/68	1141	08.5	22.3	04.8	-	-	16.0	04.2	05.0	02.2	01.2	02.0
2	17/02/68	1248	20.7	30.7	06.6	29.1	06.2	28.3	05.8	25.8	05.2	10.8	03.4
3	17/02/68	1301	07.3	28.3	06.0	-	-	28.3	05.8	22.5	04.4	05.1	02.0
4	17/02/68	1315	07.9	28.0	05.8	-	-	26.6	05.5	16.9	04.0	05.8	02.7
5	17/02/68	1325	09.7	27.3	05.7	27.3	05.7	22.8	04.6	11.2	03.3	05.6	02.6
6	17/02/68	1343	10.7	25.3	05.3	22.5	04.9	15.7	04.0	09.8	03.2	05.3	02.6
7	17/02/68	1350	08.5	24.3	03.7	-	-	08.5	02.9	07.6	02.9	06.8	02.7
8	17/02/68	1400	10.7	23.2	04.9	18.9	04.2	10.7	03.3	06.2	02.6	03.5	02.3
9	17/02/68	1410	09.1	20.8	04.5	20.7	04.5	16.0	03.9	06.4	02.7	04.2	02.3

STA	DATE	TIME (PST)	DEPTH to Bot In M	12M or Bot		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
10	17/02/68	1433	07.3	22.2	04.8	-	-	13.0	03.5	05.4	02.5	03.5	02.3
11	17/02/68	1442	06.7	20.4	04.3	-	-	13.5	03.6	04.0	02.3	02.8	02.1
13	17/02/68	1455	07.9	19.3	04.4	-	-	17.4	04.1	03.5	02.2	02.2	02.1
14	17/02/68	1505	09.7	15.4	03.4	15.4	03.4	03.1	02.6	02.3	02.3	01.4	02.2
15	17/02/68	1517	09.7	11.6	03.5	01.4	02.5	01.3	02.4	00.9	02.3	00.5	02.2
16	17/02/68	1530	07.3	00.4	02.1	-	-	00.3	02.1	00.3	02.2	00.0	02.1
17	17/02/68	1542	12.2	00.0	02.1	-	-	00.0	02.1	00.0	02.1	00.0	02.1
2	15/03/68	1030	08.5	29.0	07.9	-	-	28.4	07.1	10.6	05.4	03.8	04.6
4	15/03/68	1050	08.5	28.5	07.8	-	-	28.5	07.6	07.6	05.4	02.4	04.8
6	15/03/68	1104	11.6	27.4	08.2	26.9	07.8	16.4	06.4	05.6	05.4	02.7	05.2
8	15/03/68	1118	10.9	13.2	06.4	10.1	06.4	03.7	05.5	02.6	05.2	01.5	05.2
10	15/03/68	1138	07.9	12.1	06.8	-	-	11.8	06.4	02.7	05.4	01.2	05.5
11	15/03/68	1141	07.3	16.1	06.8	-	-	03.9	05.5	02.2	05.4	00.7	05.5
13	15/03/68	1152	07.3	16.9	06.9	-	-	16.9	06.9	03.6	05.6	00.6	05.5
2	15/03/68	1320	07.3	29.0	08.7	-	-	29.0	08.4	08.2	06.3	03.8	05.8
4	15/03/68	1333	08.5	23.1	08.0	-	-	17.4	07.0	05.9	06.1	04.4	05.8
6	15/03/68	1345	10.9	17.1	07.1	16.2	07.0	05.2	06.2	03.7	06.0	02.6	05.9
8	15/03/68	1400	10.4	05.8	05.8	05.1	05.7	02.1	05.5	01.8	05.4	01.3	05.3
10	15/03/68	1411	07.9	03.5	05.9	-	-	02.4	06.0	01.5	06.0	00.7	05.9
12	15/03/68	1422	07.3	05.8	06.2	-	-	04.9	06.3	01.2	05.9	00.4	05.9
14	15/03/68	1434	10.4	00.0	05.8	00.0	05.8	00.0	05.8	00.0	05.7	00.0	05.7
16	15/03/68	1455	06.7	00.0	05.9	-	-	00.0	05.8	00.0	05.8	00.0	05.8
18	15/03/68	1513	09.7	00.0	05.7	00.0	05.7	00.0	05.7	00.0	05.7	00.0	05.7
20	15/03/68	1557	11.6	00.0	05.7	00.0	05.5	00.0	05.5	00.0	05.5	00.0	05.5
22	15/03/68	1633	09.1	00.0	05.4	00.0	05.4	00.0	05.4	00.0	05.3	00.0	05.3
2	16/03/68	1427	08.5	28.7	09.0	-	-	28.2	08.9	06.2	06.8	04.8	06.8
4	16/03/68	1437	08.3	08.6	07.1	-	-	05.1	06.8	04.1	06.6	02.8	06.5
6	16/03/68	1449	11.6	04.9	06.8	03.2	06.8	02.4	06.6	01.7	06.5	00.8	06.5
8	16/03/68	1504	09.1	00.7	06.6	00.7	06.6	00.6	06.5	00.0	06.5	00.0	06.4
10	16/03/68	1515	07.3	00.3	06.7	-	-	00.0	06.6	00.0	06.4	00.0	06.4
12	16/03/68	1524	07.3	00.0	06.2	-	-	00.0	06.2	00.0	06.4	00.0	06.4
14	16/03/68	1535	09.1	00.0	06.3	00.0	06.3	00.0	06.3	00.0	06.3	00.0	06.3
16	16/03/68	1554	07.3	00.0	06.0	-	-	00.0	06.0	00.0	06.0	00.0	06.0
18	16/03/68	1610	07.5	00.0	06.2	-	-	00.0	06.1	00.0	06.1	00.0	06.1
20	16/03/68	1635	09.1	00.0	06.1	00.0	06.1	00.0	06.0	00.0	06.0	00.0	06.0

STA	DATE	TIME (PST)	DEPTH to Bot In M	12M or Bot		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
203	17/03/68	0834	10.1	00.0	05.7	00.0	05.7	00.0	05.6	00.0	05.6	00.0	05.6
20	17/03/68	0849	12.8	00.0	06.1	00.0	06.0	00.0	05.9	00.0	05.8	00.0	05.8
19	17/03/68	0923	10.4	00.0	05.6	00.0	05.6	00.0	05.6	00.0	05.6	00.0	05.7
184	17/03/68	0929	10.4	00.0	05.4	00.0	05.4	00.0	05.4	00.0	05.4	00.0	05.6
183	17/03/68	0936	12.2	00.0	05.2	00.0	05.2	00.0	05.2	00.0	05.4	00.0	05.4
18	17/03/68	0942	12.8	00.0	05.2	00.0	05.2	00.0	05.2	00.0	05.4	00.0	05.4
17	17/03/68	0950	13.4	05.2	05.7	01.7	05.3	00.0	05.3	00.0	05.3	00.0	05.3

STATION 1 AND

INTERMEDIATE STATIONS

STA	DATE	TIME PST	DEPTH M	12M 0/00	°C	9M 0/00	°C	6M 0/00	°C	3M 0/00	°C	SURF 0/00	°C
1	20/08/66	0950	54.8	30.3	12.2					07.1	17.5		
1	21/08/66	1250	54.9	28.1	11.9	27.8	12.2	25.9	13.9	11.4	16.8		
1	17/09/66	1115	50.2			29.1	10.7			17.2	14.5		
1	18/09/66	1330	38.1			28.8	11.0			12.7	14.1		
1	22/10/66	0943	36.6	30.6	09.3	30.5	09.3			21.0	08.8		
1	23/10/66	1012	36.6	30.4	09.7	30.3	09.7			03.0	09.0		
1	12/11/66	1020	54.8	29.9	08.7	29.9	08.7	26.3	07.9	24.9	07.9		
1	13/11/66	1410	54.8	30.3	08.7	30.2	08.6	29.0	08.6	12.0	06.7		
1	11/12/66	1320	25.0	31.2	08.0	31.2	08.0	29.2	07.3	22.8	06.8		
1	22/01/67	1104	51.8			29.5	06.9	29.0	06.5	29.0	06.3		
1	10/03/67	1248	51.8			30.3	07.2	30.2	07.1	29.6	06.9	27.2	06.6
1	12/03/67	1400	54.8			30.4	06.9	30.2	06.5	29.4	06.5	17.6	05.2
1	21/04/67	1245	45.7	30.0	08.3	29.9	08.4	29.7	08.7	16.7	09.3		
1	23/04/67	1324	36.6	30.7	07.8	30.4	08.0	29.5	08.3	24.4	08.8		
1	19/05/67	1010	33.6	30.3	08.5	30.3	08.7	29.1	09.6	14.9	10.9		
1	05/06/67	1258	24.4			30.2	08.9	30.1	08.9	29.0	09.8	06.1	12.0
1	30/07/67	1800	57.8					30.0	10.6	28.3	12.8	07.4	16.8
1	26/08/67	0816	16.5					30.4	10.0	29.2	11.8	19.1	18.0
1	23/09/67	1106	54.8					30.9	10.2	29.7	11.1	20.3	14.8
1	20/11/67	1105	43.9					31.0	09.0	30.5	09.1	25.0	08.5
1	13/01/68	1009	27.1					31.2	06.7	30.9	06.6	30.3	06.4
1	14/01/68	1332	64.0					31.3	06.9	30.6	06.7	21.4	05.6
1	17/02/68	1235	42.7					30.8	06.4	27.0	05.5	22.3	04.4
1	16/03/68	1401	76.8					29.1	09.5	29.0	08.7	16.5	07.4

STA	DATE	TIME (PST)	DEPTH To Bot In M	BOTTOM		12M		9M		6M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
195	17/02/67	1442	15.2	23.9	06.0	19.2	05.2	00.0	03.6	00.0	03.8	00.0	03.9
* 195	18/02/67	1001	15.2	00.0	03.2	00.0	03.2	00.0	03.2	00.0	03.1	00.0	03.2
194	18/02/67	1008	14.6	00.0	03.1	00.0	03.1	00.0	03.1	00.0	03.1	00.0	03.1
193	18/02/67	1015	09.1	11.4	04.5	-	-	11.3	04.3	00.0	03.2	00.0	03.2
184	18/02/67	1024	09.1	17.9	05.2	-	-	16.7	04.9	04.2	04.2	00.0	03.2
183	18/02/67	1031	12.5	21.1	05.6	21.0	05.5	19.2	05.2	09.7	04.6	00.0	03.3
18	18/02/67	1037	14.0	23.6	05.9	23.0	05.9	20.0	05.5	12.3	04.6	00.0	03.2
172	18/02/67	1046	12.8	26.8	06.3	26.4	06.0	20.0	05.2	10.1	04.3	00.0	03.5
17	18/02/67	1055	07.6	28.0	06.6	-	-	28.0	06.5	23.8	05.8	00.9	03.5
195	12/03/67	0904	15.2	00.0	03.8	00.0	03.8	00.0	03.8	00.0	03.7	00.0	03.7
194	12/03/67	0910	14.0	00.0	03.8	00.0	03.8	00.0	03.8	00.0	03.8	00.0	03.7
183	12/03/67	0937	12.2	06.1	04.4	05.3	04.2	03.8	04.1	02.1	04.0	00.7	03.9
18	12/03/67	0942	12.5	09.2	04.5	08.4	04.4	05.1	04.1	02.4	03.9	00.6	03.8
173	12/03/67	0949	12.2	14.3	04.9	13.0	04.6	08.6	04.3	02.0	03.9	01.3	03.8
172	12/03/67	0955	13.7	11.5	05.1	10.6	04.6	08.9	04.4	05.6	04.1	00.7	03.8
183	12/03/67	1044	11.6	06.8	04.6	-	-	02.4	04.4	00.4	04.2	00.0	04.5
18	12/03/67	1050	12.2	08.5	04.6	05.6	04.5	02.4	04.1	00.6	04.1	00.0	04.3
173	12/03/67	1058	12.8	15.8	05.1	14.3	04.9	06.3	04.3	00.9	04.0	00.0	04.1
195	21/04/67	1652	15.2	00.0	06.9	00.0	06.9	00.0	07.1	00.0	07.1	00.0	07.3
195	23/04/67	0820	14.3	00.0	07.1	00.0	07.1	00.0	07.1	00.0	07.1	00.0	07.1
195	13/01/68	1408	14.0	15.7	03.8	13.5	03.5	05.6	02.2	00.0	01.5	00.0	01.5
194	13/01/68	1416	13.4	20.3	04.5	19.9	04.2	05.1	02.2	03.8	02.0	00.7	01.8
194	13/01/68	1620	14.6	21.5	04.7	17.4	04.3	11.1	03.2	06.8	02.4	00.0	01.4
195	14/01/68	0850	16.5	00.4	01.9	-	-	00.4	02.0	00.4	02.0	00.0	02.0
194	14/01/68	0900	14.6	00.7	02.0	-	-	00.6	01.9	00.5	02.0	00.0	02.0
193	14/01/68	0905	10.9	02.4	02.0	-	-	01.9	02.0	01.2	02.0	00.6	02.0
194	17/02/68	1055	15.2	00.0	01.8	00.0	01.8	00.0	01.8	00.0	01.8	00.0	01.9
194	15/03/68	1533	14.6	00.0	05.9	00.0	05.8	00.0	05.6	00.0	05.6	00.0	05.6
195	17/03/68	0858	15.8	00.0	05.9	00.0	05.9	00.0	05.9	00.0	05.9	00.0	05.9
194	17/03/68	0906	14.0	00.0	05.8	00.0	05.7	00.0	05.7	00.0	05.6	00.0	05.9
193	17/03/68	0915	09.7	00.0	05.5	-	-	00.0	05.5	00.0	05.6	00.0	05.7
* 20	18/02/67	0955	07.9	00.0	03.1	-	-	00.0	03.1	00.0	03.1	00.0	03.?

TIME SERIES

STA	DATE	TIME (PST)	DEPTH To BOT In M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
25	07/12/66	1800	09.1	26.2	06.5	24.2	06.2	21.7	05.6	02.0	04.1	01.6	03.9
25	07/12/66	1900	08.5	14.5	05.4	-	-	13.4	05.3	04.9	04.4	02.7	04.0
25	07/12/66	2000	08.2	06.0	04.6	-	-	05.5	04.4	03.1	04.2	02.0	03.8
25	07/12/66	2100	07.9	01.3	04.1	-	-	01.3	04.0	01.1	04.0	01.0	03.9
25	07/12/66	2200	07.6	01.3	04.1	-	-	01.3	04.0	01.2	03.9	00.3	03.7
25	07/12/66	2300	07.9	01.0	03.8	-	-	00.8	03.9	00.8	03.8	00.1	03.7
25	07/12/66	2400	08.2	00.0	04.1	-	-	00.0	04.0	00.0	04.0	00.0	03.8
25	08/12/66	0100	09.5	00.6	04.1	00.6	04.1	00.5	04.0	00.0	03.9	00.0	03.8
25	08/12/66	0200	09.5	01.5	04.2	01.5	04.2	01.5	04.2	01.5	04.0	01.4	03.7
25	08/12/66	0300	09.5	21.3	06.1	16.1	05.5	06.6	04.6	02.3	04.0	00.0	03.6
25	08/12/66	0400	10.1	25.8	06.5	25.8	06.3	09.8	04.5	01.8	04.0	00.0	03.8
25	08/12/66	0500	09.8	27.5	06.8	27.4	06.4	09.3	04.7	01.8	04.2	00.0	03.8
25	08/12/66	0600	09.1	29.0	06.4	29.0	06.4	14.4	05.3	04.4	04.3	00.0	03.8
25	08/12/66	0700	08.8	28.2	06.3	-	-	17.2	05.4	02.1	04.0	00.4	03.8
25	08/12/66	0800	08.5	17.9	05.4	-	-	14.3	05.0	01.1	04.1	00.3	03.9
25	08/12/66	0900	09.1	17.6	05.5	17.6	05.5	12.0	04.9	00.7	03.8	00.0	03.7

STA	DATE	TIME (PST)	DEPTH To BOT In M	5M or BOT		4M		3M		2M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
26	08/12/66	1215	04.0	-	-	00.0	04.2	00.0	04.2	00.0	04.2	00.0	04.3
26	08/12/66	1230	04.0	-	-	00.0	04.0	00.0	04.0	00.0	04.0	00.0	04.0
26	08/12/66	1245	04.0	-	-	00.0	04.0	00.0	04.0	00.0	04.0	00.0	04.0
26	08/12/66	1300	04.0	-	-	00.0	04.0	00.0	04.0	00.0	04.0	00.0	04.0
26	08/12/66	1315	05.0	00.0	04.0	00.0	04.0	00.0	04.0	00.0	04.0	00.0	04.0
26	08/12/66	1330	05.0	00.0	04.0	00.0	03.9	00.0	03.9	00.0	03.9	00.0	03.8
26	08/12/66	1345	05.0	00.0	03.9	00.0	03.9	00.0	03.9	00.0	03.9	00.0	03.8

STA	DATE	TIME (PST)	DEPTH To Bot In M	BOTTOM		5M		4M		2M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
26	09/12/66	1330	06.0	00.0	03.7	00.0	03.7	00.0	03.6	00.0	03.6	00.0	03.4
26	09/12/66	1400	06.0	00.4	03.7	00.3	03.7	00.3	03.6	00.0	03.6	00.0	03.5
26	09/12/66	1430	06.0	02.7	03.5	00.0	03.5	00.0	03.4	00.0	03.4	00.0	03.3
26	09/12/66	1500	06.0	08.6	04.5	04.5	03.9	01.6	03.6	00.5	03.4	00.0	03.0
26	09/12/66	1515	06.0	13.0	04.6	04.2	03.9	01.0	03.7	00.9	03.6	00.6	03.4
26	09/12/66	1530	06.0	14.9	05.1	11.4	04.8	03.2	03.9	00.9	03.7	00.6	03.4
26	09/12/66	1545	05.5	15.2	05.0	13.7	04.7	02.0	03.8	00.9	03.7	00.8	03.5
26	09/12/66	1600	05.5	17.2	05.1	13.1	04.6	02.6	03.8	00.6	03.6	00.4	03.5
26	09/12/66	1615	05.3	17.6	05.3	15.5	05.0	03.0	04.1	00.6	03.7	00.5	03.4
26	09/12/66	1630	05.3	20.0	05.8	19.6	05.7	09.5	04.5	01.6	03.8	00.5	03.6
26	09/12/66	1700	05.2	16.9	05.5	15.1	05.2	07.5	04.3	01.9	03.8	01.7	03.6
26	09/12/66	1715	05.0	11.9	04.8	11.9	04.8	07.9	04.5	01.9	03.8	01.9	03.6
26	09/12/66	1730	04.6	14.6	05.4	-	-	13.4	05.1	01.9	03.8	01.4	03.6
26	09/12/66	1745	04.6	18.5	05.7	-	-	10.8	04.7	01.8	03.8	01.6	03.7
26	09/12/66	1800	04.5	14.4	04.5	-	-	05.7	04.1	02.5	03.8	02.1	03.7
26	09/12/66	1815	04.5	17.8	04.9	-	-	05.1	04.4	02.4	03.9	02.1	03.8
26	09/12/66	1830	04.3	03.8	04.0	-	-	03.7	04.1	02.1	03.8	02.0	03.6
26	09/12/66	1845	04.1	02.7	03.9	-	-	-	-	02.3	03.8	02.3	03.7

STA	DATE	TIME (PST)	DEPTH To Bot In M	BOTTOM		12M		9M		6M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
27	10/12/66	0430	16.0	00.0	03.8	00.0	03.8	00.0	03.8	00.0	03.8	00.0	03.8
27	10/12/66	0500	16.0	00.3	03.8	00.0	03.8	00.0	03.8	00.0	03.8	00.0	03.8
27	10/12/66	0530	16.0	01.0	03.9	01.0	03.8	01.0	03.8	00.8	03.8	00.6	03.8
27	10/12/66	0545	16.0	01.1	03.9	01.1	03.8	01.1	03.8	01.0	03.8	00.7	03.8
27	10/12/66	0600	16.0	01.2	03.9	00.8	03.8	00.6	03.8	00.6	03.8	00.6	03.7
27	10/12/66	0615	16.0	01.5	03.9	01.1	03.9	01.0	03.8	00.8	03.9	00.8	03.7
27	10/12/66	0630	15.7	02.0	04.0	02.0	04.0	01.8	04.0	01.7	03.9	00.8	03.8
27	10/12/66	0645	15.5	02.5	04.0	02.5	04.0	02.3	04.0	02.1	04.0	01.0	03.9
27	10/12/66	0700	15.5	04.4	04.1	04.0	04.1	02.8	04.0	02.6	04.0	01.0	03.9
27	10/12/66	0715	15.5	06.2	04.3	05.3	04.2	02.9	04.0	02.5	04.0	01.4	04.0
27	10/12/66	0730	15.2	07.2	04.4	06.3	04.2	04.4	04.1	03.7	04.0	00.8	04.0
27	10/12/66	0745	15.0	09.9	04.7	07.9	04.5	05.5	04.2	03.9	04.0	01.2	03.9
27	10/12/66	0800	15.0	11.0	04.8	10.0	04.7	07.6	04.4	04.3	04.1	01.1	04.0
27	10/12/66	0815	15.0	13.3	05.1	12.6	04.9	08.1	04.4	04.5	04.1	01.4	04.0
27	10/12/66	0830	15.0	14.6	05.2	13.2	05.0	09.7	04.6	04.5	04.1	01.3	04.0
27	10/12/66	0845	15.0	16.0	05.4	15.2	05.1	10.4	04.7	05.8	04.3	01.2	04.0
27	10/12/66	0900	15.0	16.8	05.5	16.0	05.2	10.8	04.7	05.9	04.3	00.7	03.9
27	10/12/66	0915	14.5	17.5	05.6	16.0	05.4	12.1	04.9	03.9	04.0	00.6	04.1
27	10/12/66	0930	14.5	17.7	05.8	17.4	05.5	14.3	05.1	02.8	04.0	00.4	04.1
27	10/12/66	0945	14.5	17.9	05.7	16.5	05.5	14.2	05.1	03.0	04.1	00.4	04.0
27	10/12/66	1000	14.5	18.5	05.8	18.2	05.7	14.7	05.1	02.8	04.2	00.4	04.1
27	10/12/66	1030	14.2	18.8	05.8	17.8	05.5	14.1	05.0	00.9	04.2	00.0	04.0
27	10/12/66	1100	14.5	19.3	05.8	17.2	05.5	14.0	05.1	00.6	04.1	00.4	04.1
27	10/12/66	1130	14.2	19.9	05.8	16.7	05.3	12.3	05.0	00.8	04.3	00.4	04.3
27	10/12/66	1200	14.0	20.1	05.9	15.1	05.3	10.4	04.8	03.9	04.4	00.3	04.3
27	10/12/66	1230	15.0	20.2	05.9	12.6	05.1	06.9	04.6	04.7	04.4	00.0	04.2
27	10/12/66	1300	15.5	20.2	06.0	15.9	05.5	07.7	04.8	04.0	04.4	00.0	04.3
27	10/12/66	1330	15.5	19.9	06.0	18.8	05.7	07.8	04.7	03.9	04.4	00.0	04.6
27	10/12/66	1400	15.5	20.3	06.1	20.0	05.9	12.3	04.7	04.4	04.4	00.0	04.3
27	10/12/66	1430	15.7	21.4	06.2	21.2	06.1	13.9	05.1	05.4	04.4	00.0	04.3
27	10/12/66	1500	16.0	22.0	06.2	21.8	06.2	19.9	05.9	06.9	04.7	00.0	04.3
27	10/12/66	1530	16.0	22.1	06.2	22.0	06.2	20.1	05.9	08.8	04.9	00.0	04.4
27	10/12/66	1600	15.5	22.4	06.3	22.3	06.2	20.5	05.9	12.7	05.0	00.0	04.3
27	10/12/66	1630	15.5	22.7	06.3	22.7	06.2	21.1	06.0	17.4	05.4	00.0	04.1
27	10/12/66	1700	14.3	22.7	06.3	22.7	06.2	22.0	06.1	19.9	05.6	00.0	04.2
27	10/12/66	1715	14.0	22.7	06.3	22.7	06.3	22.4	06.1	21.5	05.7	00.0	04.1
27	10/12/66	1730	14.0	22.7	06.3	22.7	06.2	22.1	06.2	21.4	05.9	00.3	04.2
27	10/12/66	1745	14.0	22.6	06.3	22.5	06.3	21.9	06.1	08.6	05.8	00.0	04.2
27	10/12/66	1800	14.5	22.4	06.2	22.1	06.2	21.7	05.9	01.5	04.1	00.0	04.1

STA	DATE	TIME (PST)	DEPTH To Bot In M	BOTTOM		12M		9M		6M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
27	10/12/66	1815	14.0	21.8	06.2	21.8	06.0	10.1	05.1	01.0	04.0	00.3	04.1
27	10/12/66	1830	14.0	21.5	06.0	-	-	01.1	04.1	01.4	04.0	00.8	04.1
27	10/12/66	1845	14.0	20.7	06.0	20.2	05.1	01.9	04.3	00.8	04.0	00.4	04.2
27	10/12/66	1900	14.0	19.3	05.7	14.4	05.0	03.5	04.1	01.4	04.1	00.9	04.1
27	10/12/66	1930	14.0	10.2	05.0	09.1	04.7	03.5	04.6	03.2	04.1	02.0	04.1
27	10/12/66	2000	13.7	05.4	04.3	04.9	04.3	04.4	04.3	04.1	04.4	03.6	04.3
27	10/12/66	2030	13.5	03.4	04.1	03.4	04.2	03.0	04.1	03.0	04.1	02.4	04.2
27	10/12/66	2100	13.2	00.9	03.9	00.9	03.9	00.8	03.9	00.8	04.0	00.7	04.0
27	10/12/66	2130	13.0	00.5	03.9	00.5	03.9	00.5	03.9	00.4	03.9	00.4	04.1

STA	DATE	TIME (PST)	DEPTH To Bot In M	BOTTOM		12M		9M		6M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
27	20/01/67	1730	13.3	01.2	03.8	01.2	03.9	01.2	03.9	01.2	04.0	01.2	04.3
27	20/01/67	1745	13.3	00.8	03.7	00.8	03.8	00.7	03.8	00.7	03.8	00.7	03.8
27	20/01/67	1800	13.3	00.4	03.6	00.4	03.6	00.4	03.7	00.4	03.7	00.4	03.7
27	20/01/67	1815	13.3	00.4	03.6	00.4	03.6	00.4	03.6	00.4	03.6	00.4	03.7
27	20/01/67	1830	13.3	00.0	03.6	00.0	03.6	00.0	03.6	00.0	03.6	00.0	03.7
27	20/01/67	1900	13.3	00.0	03.6	00.0	03.6	00.0	03.6	00.0	03.6	00.0	03.7
27	20/01/67	1930	12.7	00.0	03.6	00.0	03.6	00.0	03.6	00.0	03.6	00.0	03.8
27	20/01/67	2000	12.7	00.0	03.6	00.0	03.6	00.0	03.6	00.0	03.6	00.0	03.7
27	20/01/67	2030	12.7	00.0	03.6	00.0	03.6	00.0	03.6	00.0	03.6	00.0	03.7
27	20/01/67	2100	12.7	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.7
27	20/01/67	2130	12.7	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.7
27	20/01/67	2200	13.3	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.6
27	20/01/67	2230	13.3	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.5	00.0	03.6
27	20/01/67	2300	13.3	00.0	03.4	00.0	03.4	00.0	03.4	00.0	03.4	00.0	03.5
27	20/01/67	2330	13.7	00.0	03.3	00.0	03.3	00.0	03.3	00.0	03.3	00.0	03.4
27	20/01/67	2400	13.7	00.0	03.3	00.0	03.3	00.0	03.3	00.0	03.3	00.0	03.4
27	21/01/67	0030	14.1	00.0	03.3	00.0	03.3	00.0	03.3	00.0	03.3	00.0	03.5
27	21/01/67	0100	14.1	00.0	03.3	00.0	03.3	00.0	03.3	00.0	03.3	00.0	03.4
27	21/01/67	0130	14.6	00.0	03.2	00.0	03.2	00.0	03.3	00.0	03.3	00.0	03.4
27	21/01/67	0200	14.6	00.0	03.2	00.0	03.2	00.0	03.2	00.0	03.3	00.0	03.4
27	21/01/67	0230	14.7	00.0	03.1	00.0	03.2	00.0	03.2	00.0	03.3	00.0	03.2
27	21/01/67	0300	14.0	00.0	03.1	00.0	03.2	00.0	03.2	00.0	03.2	00.0	03.3
27	21/01/67	0330	14.9	00.0	03.2	00.0	03.2	00.0	03.3	00.0	03.3	00.0	03.4
27	21/01/67	0400	14.9	00.0	03.2	00.0	03.3	00.0	03.3	00.0	03.3	00.0	03.4
27	21/01/67	0430	14.9	00.0	03.2	00.0	03.2	00.0	03.2	00.0	03.2	00.0	03.4
27	21/01/67	0500	14.9	00.0	03.2	00.0	03.2	00.0	03.2	00.0	03.2	00.0	03.4
27	21/01/67	0530	14.9	00.0	03.2	00.0	03.2	00.0	03.2	00.0	03.3	00.0	03.4
27	21/01/67	0600	14.9	00.0	03.2	00.0	03.2	00.0	03.2	00.0	03.2	00.0	03.4
27	21/01/67	0630	14.7	00.0	03.2	00.0	03.2	00.0	03.2	00.0	03.2	00.0	03.4
27	21/01/67	0700	14.6	00.0	03.2	00.0	03.2	00.0	03.2	00.0	03.3	00.0	03.4
27	21/01/67	0730	14.6	00.0	03.2	00.0	03.2	00.0	03.2	00.0	03.2	00.0	03.4
27	21/01/67	0800	14.7	00.0	03.1	00.0	03.1	00.0	03.1	00.0	03.2	00.0	03.3
27	21/01/67	0830	14.7	00.0	03.1	00.0	03.1	00.0	03.1	00.0	03.1	00.0	03.3
27	21/01/67	0900	14.7	09.6	04.0	01.9	03.3	00.5	03.1	00.0	03.1	00.0	03.2
27	21/01/67	0915	14.7	12.1	04.2	04.4	03.6	01.2	03.2	00.0	03.2	00.0	03.2
27	21/01/67	0930	15.0	14.4	04.3	04.5	03.6	00.5	03.3	00.0	03.2	00.0	03.2
27	21/01/67	0945	15.0	16.6	04.7	08.0	04.0	02.4	03.4	00.0	03.2	00.0	03.3
27	21/01/67	1000	15.0	18.4	05.0	10.5	04.1	03.0	03.6	00.0	03.3	00.0	03.4
27	21/01/67	1015	15.0	19.4	05.2	17.2	04.7	03.7	03.7	00.4	03.4	00.0	03.4

STA	DATE	TIME (PST)	DEPTH To Bot In M	BOTTOM		12M		9M		6M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
27	21/01/67	1030	15.0	20.1	05.8	17.5	05.4	05.8	04.3	00.0	03.9	00.0	04.0
27	21/01/67	1045	15.0	21.0	05.7	19.2	05.4	07.2	04.2	00.7	03.7	00.0	04.0
27	21/01/67	1100	15.0	21.4	05.5	20.0	05.3	07.9	04.1	01.5	03.6	00.0	03.7
27	21/01/67	1115	15.0	21.9	05.5	21.0	05.3	09.1	04.1	01.8	03.6	00.0	03.7
27	21/01/67	1130	15.3	22.5	05.7	21.9	05.2	10.7	04.4	02.0	03.5	00.0	03.6
27	21/01/67	1145	15.3	22.8	05.7	22.3	05.4	11.8	04.4	01.9	03.5	00.0	03.7
27	21/01/67	1200	15.3	23.3	05.7	22.8	05.4	16.8	04.7	02.2	03.4	00.0	03.6
27	21/01/67	1215	15.3	23.8	05.7	23.4	05.6	17.8	04.6	02.0	03.4	00.0	03.5
27	21/01/67	1230	15.5	24.4	05.8	24.3	05.6	19.9	05.0	02.6	03.6	00.0	03.6
27	21/01/67	1245	15.5	24.7	05.8	24.5	05.7	20.8	05.3	03.5	03.8	00.0	03.6
27	21/01/67	1300	15.5	25.0	05.9	24.8	05.7	21.6	05.2	04.6	03.8	00.0	03.6

STA	DATE	TIME (PST)	Depth to Bot In M	12M or Bot		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
251	15/02/67	0030	07.7	29.3	06.4	-	-	11.9	04.5	04.9	03.9	00.0	03.4
251	15/02/67	0100	07.7	29.4	06.4	-	-	11.9	04.5	04.0	03.8	00.0	03.2
251	15/02/67	0130	07.2	29.5	06.3	-	-	14.1	04.6	02.9	03.6	00.0	03.1
251	15/02/67	0200	07.0	29.7	06.3	-	-	15.2	04.4	01.6	03.4	00.0	03.1
251	15/02/67	1900	06.9	04.5	04.2	-	-	03.0	04.1	02.3	04.0	01.6	03.9
251	15/02/67	1930	07.0	03.9	04.1	-	-	02.9	04.0	02.4	03.9	01.1	03.8
251	15/02/67	2000	07.2	05.1	04.2	-	-	02.6	03.9	02.0	03.8	00.9	03.8
251	15/02/67	2015	07.5	05.3	04.2	-	-	02.7	03.8	02.0	03.8	00.7	03.5
251	15/02/67	2030	07.5	06.0	04.2	-	-	02.7	03.9	02.2	03.8	00.6	03.5
251	15/02/67	2045	07.5	12.0	04.7	-	-	02.8	03.8	02.1	03.8	00.5	03.6
251	15/02/67	2100	07.5	14.3	04.9	-	-	03.2	03.9	02.1	03.7	00.5	03.5
251	15/02/67	2115	07.5	18.3	05.2	-	-	03.0	03.8	02.2	03.7	00.4	03.5
251	15/02/67	2130	07.7	20.3	05.5	-	-	03.5	03.9	02.1	03.7	00.6	03.5
251	15/02/67	2145	07.7	22.7	05.7	-	-	04.1	03.9	01.0	03.7	00.6	03.5
251	15/02/67	2200	07.7	24.2	05.9	-	-	04.8	03.9	01.0	03.6	00.5	03.5
251	15/02/67	2230	07.7	26.4	06.0	-	-	05.8	03.9	01.1	03.6	00.3	03.4
251	15/02/67	2300	07.7	27.4	06.2	-	-	08.0	03.9	01.2	03.5	00.3	03.4
251	15/02/67	2330	07.7	28.2	06.3	-	-	08.8	04.1	01.9	03.6	00.1	03.4
251	15/02/67	2400	07.7	29.0	06.3	-	-	09.6	04.3	03.4	03.7	00.1	03.4

STA	DATE	TIME (PST)	DEPTH To Bot In M	BOTTOM		12M		9M		6M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
27	17/02/67	1800	13.0	02.7	03.7	02.7	03.7	02.1	03.6	01.8	03.5	01.5	03.5
27	17/02/67	1830	13.0	01.8	03.6	01.8	03.6	01.7	03.5	01.4	03.5	01.4	03.5
27	17/02/67	1900	12.8	01.8	03.5	01.6	03.5	01.5	03.5	01.5	03.5	01.5	03.5
27	17/02/67	1930	12.8	01.1	03.4	01.1	03.4	00.9	03.5	00.9	03.4	00.6	03.4
27	17/02/67	2000	13.0	00.9	03.4	00.9	03.4	00.7	03.4	00.7	03.4	00.7	03.4
27	17/02/67	2030	13.0	00.8	03.4	00.8	03.4	00.8	03.4	00.8	03.3	00.5	03.4
27	17/02/67	2100	13.0	00.9	03.3	00.9	03.3	00.9	03.3	00.7	03.3	00.3	03.4
27	17/02/67	2130	13.3	00.6	03.3	00.6	03.3	00.4	03.3	00.3	03.3	00.0	03.3
27	17/02/67	2200	13.5	00.5	03.2	00.4	03.2	00.4	03.2	00.2	03.2	00.0	03.2
27	17/02/67	2230	13.7	00.4	03.2	00.4	03.2	00.3	03.3	00.3	03.3	00.0	03.2
27	17/02/67	2300	14.0	00.4	03.3	00.4	03.3	00.4	03.3	00.2	03.3	00.0	03.3
27	17/02/67	2330	14.0	00.3	03.1	00.3	03.1	00.3	03.2	00.3	03.2	00.0	03.2
27	17/02/67	2400	14.0	00.9	03.1	00.4	03.1	00.3	03.1	00.3	03.1	00.0	03.0
27	18/02/67	0030	14.0	01.0	03.3	00.9	03.2	00.4	03.1	00.2	03.1	00.0	03.0
27	18/02/67	0100	14.0	01.1	03.3	00.8	03.3	00.2	03.2	00.2	03.1	00.0	03.1
27	18/02/67	0130	14.0	01.2	03.3	01.0	03.2	00.6	03.2	00.3	03.2	00.0	03.0
27	18/02/67	0530	14.0	03.8	03.4	03.4	03.3	02.1	03.2	00.7	02.9	00.0	02.7
27	18/02/67	0600	14.0	05.0	03.6	04.6	03.5	02.5	03.3	01.2	03.1	00.0	02.9
27	18/02/67	0630	14.0	08.0	03.9	05.6	03.7	02.8	03.4	01.3	03.2	00.0	02.9
27	18/02/67	0700	14.0	10.6	04.2	08.2	03.9	03.9	03.5	02.1	03.2	00.2	02.9
27	18/02/67	0730	14.0	12.5	04.3	11.6	04.2	04.5	03.5	02.2	03.2	00.0	02.8
27	18/02/67	0800	15.0	15.0	04.6	13.6	04.4	07.1	03.7	02.8	03.3	00.0	02.9
27	18/02/67	0830	15.0	17.1	04.9	15.8	04.7	07.2	03.9	02.7	03.4	00.0	03.1
27	18/02/67	0900	15.0	18.3	05.2	17.4	05.0	14.3	04.6	02.9	03.6	00.0	03.3

STA	DATE	TIME (PST)	DEPTH To Bot In M	BOTTOM		12M		9M		6M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
27	10/03/67	1800	14.0	17.5	05.2	17.0	05.0	06.9	04.2	02.0	03.8	00.0	03.6
27	10/03/67	1900	14.0	18.5	05.2	18.3	04.9	13.3	04.4	08.8	04.1	00.0	03.2
27	10/03/67	2000	13.5	19.7	05.2	19.5	05.1	17.6	04.8	09.7	04.2	00.0	03.2
27	10/03/67	2100	13.0	19.3	05.2	18.3	05.0	06.3	04.2	00.5	03.6	00.5	03.2
27	10/03/67	2200	13.0	09.2	04.3	03.6	04.0	01.0	03.5	01.0	03.5	00.5	03.2
27	10/03/67	2300	13.0	00.0	03.4	00.0	03.4	00.0	03.4	00.0	03.4	00.0	03.0
27	10/03/67	2400	13.5	00.0	03.4	00.0	03.4	00.0	03.4	00.0	03.3	00.0	03.0
27	11/03/67	0600	15.0	00.0	03.2	00.0	03.2	00.0	03.2	00.0	03.2	00.0	03.0
27	11/03/67	0700	15.0	00.8	03.5	00.8	03.5	00.8	03.4	00.5	03.4	00.5	03.0
27	11/03/67	0800	14.0	07.0	04.0	06.1	03.9	04.3	03.7	02.6	03.6	01.2	03.1
27	11/03/67	0900	14.0	12.4	04.8	12.2	04.7	08.8	04.5	06.5	04.3	01.0	03.9
27	11/03/67	1000	13.5	16.4	05.6	15.8	05.5	13.2	05.2	07.2	04.8	00.5	04.6
27	11/03/67	1100	14.0	17.1	05.8	16.9	05.7	11.8	05.2	00.7	04.6	00.7	04.9
27	11/03/67	1200	14.0	11.5	05.6	04.7	05.1	01.3	04.8	01.3	04.7	00.5	05.0

STA	DATE	TIME (PST)	DEPTH To Bot In M	BOTTOM		12M		9M		6M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
27	21/04/67	1730	13.3	12.7	07.8	12.4	07.7	08.0	07.6	00.8	07.5	00.0	07.7
27	21/04/67	1800	13.3	13.1	07.7	12.2	07.6	05.5	07.5	00.5	07.2	00.0	07.6
27	21/04/67	1830	12.0	-	-	12.7	07.6	03.4	07.0	00.8	07.0	00.3	07.3
27	21/04/67	1900	10.0	10.6	07.3	10.2	07.2	00.8	07.0	00.4	06.9	00.4	07.0
27	21/04/67	1930	09.3	00.0	06.8	-	-	00.0	06.8	00.0	06.9	00.0	07.0
27	22/04/67	0500	14.3	08.7	07.2	08.0	07.0	06.7	07.0	04.7	06.9	02.1	06.9
27	22/04/67	0530	14.3	10.1	07.1	09.2	07.0	07.7	07.0	05.2	06.9	02.0	06.7
27	22/04/67	0600	14.0	11.5	07.2	11.0	07.2	09.8	07.1	08.5	07.0	03.7	06.7
27	22/04/67	0630	14.0	13.4	07.3	13.2	07.3	10.7	07.1	07.7	06.8	02.0	06.7
27	22/04/67	0700	13.6	14.0	07.3	14.0	07.3	12.8	07.2	07.9	06.9	01.0	06.6
27	22/04/67	0730	13.5	14.5	07.5	14.3	07.4	11.4	07.2	05.2	06.9	00.8	06.8
27	22/04/67	0800	13.9	12.2	07.4	11.0	07.3	09.1	07.1	02.4	06.9	00.8	06.8
27	22/04/67	0830	13.3	07.2	07.0	07.2	07.0	04.8	07.0	01.2	06.8	00.9	06.9
27	22/04/67	0900	13.3	00.6	06.9	00.6	06.9	00.6	06.9	00.6	06.9	00.6	07.0
27	22/04/67	0930	13.3	00.0	07.3	00.0	07.3	00.0	07.3	00.0	07.3	00.0	07.7
27	22/04/67	1000	13.0	00.0	07.6	00.0	07.6	00.0	07.8	00.0	07.9	00.0	07.8
27	22/04/67	1030	12.5	00.0	07.4	00.0	07.4	00.0	07.5	00.0	07.5	00.0	07.8
27	22/04/67	1100	13.0	00.0	07.4	00.0	07.4	00.0	07.4	00.0	07.5	00.0	07.9
27	22/04/67	1130	13.0	00.0	07.3	00.0	07.3	00.0	07.3	00.0	07.3	00.0	07.4

STA	DATE	TIME (PST)	DEPTH to Bot In M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
251	20/05/67	0700	06.8	00.0	10.0	-	-	00.0	10.2	00.0	10.2	00.0	10.3
251	20/05/67	0730	06.8	00.0	10.1	-	-	00.0	10.2	00.0	10.2	00.0	10.3
251	20/05/67	0800	06.0	00.0	10.0	-	-	00.0	10.1	00.0	10.1	00.0	10.3

STA	DATE	TIME (PST)	DEPTH to Bot In M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
251	25/08/67	1930	07.0	28.1	11.8	-	-	08.0	16.7	00.2	18.4	00.2	18.4
251	25/08/67	2000	07.0	28.1	11.9	-	-	08.5	16.7	00.8	18.3	00.2	18.4
251	25/08/67	2030	07.0	28.3	12.0	-	-	10.9	16.4	00.6	18.4	00.4	18.5
251	25/08/67	2100	07.0	28.3	12.1	-	-	11.4	16.2	00.7	18.4	00.0	18.4
251	25/08/67	2130	07.0	28.4	12.1	-	-	09.4	16.5	00.3	18.3	00.0	18.2
251	25/08/67	2200	07.0	28.4	12.2	-	-	08.6	17.4	01.0	18.3	00.0	18.3
251	25/08/67	2230	07.0	28.4	12.2	-	-	10.4	16.7	03.2	17.9	00.0	18.4
251	25/08/67	2300	07.0	28.4	12.2	-	-	16.9	15.2	01.2	18.2	00.0	18.3
251	25/08/67	2330	07.0	28.3	12.0	-	-	28.4	12.9	01.8	18.0	00.0	18.3
251	25/08/67	2400	07.0	28.2	12.2	-	-	27.5	13.6	01.2	18.0	00.0	18.2
251	26/08/67	0030	07.0	28.3	12.1	-	-	26.0	13.5	03.1	17.6	00.0	18.2
251	26/08/67	0100	06.5	27.9	12.2	-	-	23.8	13.3	03.0	17.8	00.8	18.2
251	26/08/67	0300	05.0	16.0	15.1	-	-	-	-	02.4	17.9	02.2	17.8
251	26/08/67	0330	05.0	11.4	16.7	-	-	-	-	01.4	18.1	01.1	17.9
251	26/08/67	0400	05.0	07.9	16.7	-	-	-	-	00.0	18.2	00.8	17.8
251	26/08/67	0430	05.0	00.5	18.2	-	-	-	-	00.0	18.2	00.0	17.6
251	26/08/67	0500	05.0	00.0	18.2	-	-	-	-	00.0	18.2	00.0	18.0
251	26/08/67	0530	05.3	00.0	18.2	-	-	-	-	00.0	18.1	00.0	18.0
251	26/08/67	0600	05.3	00.0	18.3	-	-	-	-	00.0	18.3	00.0	18.0
251	26/08/67	0630	06.0	00.0	18.3	-	-	00.0	18.3	00.0	18.3	00.0	18.2
251	26/08/67	0700	06.0	00.0	18.3	-	-	00.0	18.4	00.0	18.4	00.0	18.3
251	26/08/67	0730	06.0	00.0	18.8	-	-	00.0	18.8	00.0	18.9	00.0	19.0

STA	DATE	TIME (PST)	DEPTH to Bot In M	12M or BOT		9M		6M		3M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
28	28/08/67	1800	08.5	25.3	16.7	-	-	11.3	18.1	00.5	18.6	00.0	19.2
28	28/08/67	1900	09.0	25.6	16.5	-	-	13.3	18.0	00.9	18.9	00.0	19.8
28	28/08/67	2100	09.0	26.4	16.0	-	-	12.5	17.8	01.4	18.3	00.0	18.6
28	28/08/67	2200	09.0	26.8	15.3	-	-	13.1	17.7	09.6	18.1	00.0	18.5
28	28/08/67	2300	09.0	27.1	15.2	-	-	13.8	17.6	01.3	18.4	00.0	18.5
28	28/08/67	2400	09.0	27.1	15.0	-	-	18.3	17.2	02.7	18.3	00.0	18.5
28	29/08/67	0100	09.0	27.3	14.8	-	-	26.9	15.9	02.7	18.2	00.0	18.3
28	29/08/67	0200	09.0	27.1	15.3	-	-	04.7	17.7	03.1	18.3	00.4	18.3
28	29/08/67	0700	08.0	00.4	18.3	-	-	00.4	18.3	00.3	18.3	00.3	18.2
28	29/08/67	0800	07.5	00.0	18.5	-	-	00.0	18.5	00.0	18.4	00.0	18.4
28	29/08/67	0900	07.0	00.0	18.5	00.0	18.5	00.0	18.5	00.0	18.5	00.0	18.5

STA	DATE	TIME (PST)	DEPTH to Bot In M	BOTTOM		12M		9M		6M		SURF	
				0/00	°C	0/00	°C	0/00	°C	0/00	°C	0/00	°C
27	13/01/68	1730	18.0	24.8	05.3	24.1	05.1	03.1	02.4	01.8	01.8	00.4	01.6
27	13/01/68	1800	18.0	24.3	05.1	02.0	01.6	01.3	01.6	01.1	01.7	00.5	01.6
27	13/01/68	1830	18.0	23.3	04.9	02.1	01.8	02.1	01.7	01.7	01.7	01.0	01.7
27	13/01/68	1900	18.0	21.7	04.6	03.9	01.9	02.2	01.8	02.2	01.7	01.7	01.8
27	13/01/68	1930	17.0	06.5	02.4	05.1	02.1	04.2	02.1	03.7	02.0	02.3	01.8
27	13/01/68	2000	15.0	04.0	02.1	02.8	02.0	03.0	02.0	02.1	01.9	02.2	01.8
27	13/01/68	2030	15.0	02.8	01.8	02.8	01.8	02.6	01.9	01.9	01.8	01.5	01.9
27	13/01/68	2100	15.0	00.4	01.6	00.4	01.6	00.4	01.6	00.4	01.6	00.4	01.7
27	13/01/68	2130	15.0	00.0	01.8	00.0	01.8	00.0	01.8	00.0	01.8	00.0	01.8
27	14/01/68	0800	17.5	14.2	04.3	13.5	04.0	11.0	03.6	08.2	03.0	01.6	02.4

DATA RECORD

1971 - 1973

MAIN ARM

NORTH ARM

MIDDLE ARM

LADNER AND SEA REACHES

STA	DATE	TIME PST	12.2M 0/00	12.2M °C	9.1M 0/00	9.1M °C	6.1M 0/00	6.1M °C	4.6M 0/00	4.6M °C	3.0M 0/00	3.0M °C	SURF 0/00	SURF °C
01	23/08/71	1117					23.3	13.6			16.2	14.6	03.0	17.6
	23/08/71	1121			26.9	11.9								
02	23/08/71	1128			23.4	11.8	22.9	12.2			12.3	14.9	01.7	17.7
	23/08/71	1132	25.2	11.5										
04	23/08/71	1141					12.0	15.2			03.0	17.1	01.8	17.3
	23/08/71	1143			21.8	12.6								
06	23/08/71	1150			07.1	16.2	03.0	17.2			02.4	17.3	01.7	17.6
	23/08/71	1153	14.6	14.0										
08	23/08/71	1200					01.9	17.3			01.7	17.6	01.2	17.5
	23/08/71	1202			03.4	16.9								
10	23/08/71	1208									01.2	17.5	00.6	17.4
	23/08/71	1210							02.7	17.4				
02	23/08/71	1224									05.0	16.4	02.4	17.0
	23/08/71	1226					22.9	11.8						
04	23/08/71	1233					07.0	16.1			02.6	17.1	02.1	17.4
	23/08/71	1235			12.7	14.4								
06	23/08/71	1242			04.6	16.5	02.3	17.5			02.2	17.0	01.5	17.5
	23/08/71	1244	08.9	15.8										
08	23/08/71	1250			02.2	17.3	01.8	17.2			01.5	17.4	00.7	17.5
	23/08/71	1253	04.4	16.8										
10	23/08/71	1307					01.9	17.0			00.0	17.6	00.0	17.9
	23/08/71	1309			07.1	16.1								
11	23/08/71	1313					00.0	17.6			00.0	17.7	00.0	17.7
	23/08/71	1318			06.9	16.5								
13	23/08/71	1333					00.0	18.1			00.0	18.2	00.0	18.2
	23/08/71	1335			00.0	18.0								
02	23/08/71	1351					21.3	12.4			06.3	16.5	02.2	17.7
	23/08/71	1353			28.1	10.4								
04	23/08/71	1359					03.2	16.9			02.7	17.1	01.6	17.3
	23/08/71	1402			08.6	14.8								
06	23/08/71	1409					02.0	17.3			00.9	17.3	00.6	17.7
	23/08/71	1412	04.3	16.6	02.5	17.1								
08	23/08/71	1419			01.0	17.6	00.7	17.7			00.3	17.5	00.3	17.8
	23/08/71	1422	01.9	17.4										
10	23/08/71	1427			00.9	17.5	00.2	17.6			00.1	17.7	00.0	17.7
	23/08/71	1430	01.8	17.3										
11	23/08/71	1433			00.0	17.7	00.0	17.7			00.0	17.7	00.0	17.7
	23/08/71	1435	00.0	17.7										
8NOR	23/08/71	1443									00.2	17.6	00.2	17.6
	23/08/71	1444					00.2	17.6						

STA	DATE	TIME PST	12.2M 0/00	°C	9.1M 0/00	°C	6.1M 0/00	°C	4.6M 0/00	°C	3.0M 0/00	°C	SURF 0/00	°C
8Cen	23/08/71	1446									00.3	17.6	00.2	17.6
	23/08/71	1447					01.1	17.4						
8Sou.	23/08/71	1449											00.3	17.8
	23/08/71	1451									00.3	17.9		
6	23/08/71	1456			01.9	17.3	01.6	17.7			01.0	17.7	00.6	17.7
	23/08/71	1458	03.3	16.8										
8	23/08/71	1505					00.8	17.4			00.1	17.6	00.1	17.6
	23/08/71	1507			01.6	17.3								
2	23/08/71	1527									07.5	16.6	01.5	17.4
	23/08/71	1529					20.9	13.8						
4	23/08/71	1540									03.9	16.8	00.7	17.8
	23/08/71	1542					17.0	13.6						
6	23/08/71	1547					05.9	16.6			01.0	17.8	00.2	17.8
	23/08/71	1549	18.8	13.2	10.5	15.6								
8	23/08/71	1559					00.7	17.4			00.2	17.5	00.1	17.7
	23/08/71	1602			03.3	16.9								
10	23/08/71	1612			00.1	17.6	00.0	17.7			00.0	17.7	00.0	17.7
	23/08/71	1614	00.1	17.6										
2	23/08/71	1712			28.4	10.3	27.0	11.3			10.8	16.8	01.2	18.0
	23/08/71	1715	28.6	10.2										
4	23/08/71	1720			27.6	10.6	21.6	12.9			11.3	16.6	01.0	17.3
	23/08/71	1723	28.1	10.2										
6	23/08/71	1727			22.8	12.7	12.7	15.3			07.4	17.3	01.1	17.3
	23/08/71	1729	27.6	10.7										
8	23/08/71	1735			26.4	11.1	12.5	14.9			03.4	17.1	00.0	17.5
10	23/08/71	1742			24.5	11.8	09.6	15.2			00.0	17.6	00.0	17.6
	23/08/71	1745	24.5	11.4										
11	23/08/71	1747			23.2	11.9	09.7	15.6			00.4	17.2	00.0	17.5
	23/08/71	1749	23.3	11.7										
13	23/08/71	1754					00.0	17.5			00.0	17.5	00.0	17.5
	23/08/71	1756			00.8	17.3								
	23/08/71	1758			12.9	14.7								
	23/08/71	1800			13.8	14.1								
14	23/08/71	1807			00.0	17.5	00.0	17.5			00.0	17.5	00.0	17.5
	23/08/71	1808	00.0	17.5										
13A	23/08/71	1853			01.2	17.6								
14	23/08/71	1902			01.2	17.0	00.0	17.7			00.0	17.7	00.0	17.7
	23/08/71	1903	11.3	15.1										

STA	DATE	TIME PST	12.2M 0/00	°C	9.1M 0/00	°C	6.1M 0/00	°C	4.6M 0/00	°C	3.0M 0/00	°C	SURF 0/00	°C
15	23/08/71	1908			00.0	17.5	00.0	17.5			00.0	17.5	00.0	17.5
	23/08/71	1909	00.0	17.5										
15	23/08/71	1919	01.9	17.4										
15	23/08/71	1925	03.4	16.7										
14	23/08/71	1929			07.8	16.0	00.7	17.4			00.0	17.3	00.0	17.3
	23/08/71	1932	17.7	13.2										
13	23/08/71	1939			25.1	11.7	02.1	16.9			00.2	17.4	00.0	17.4
	23/08/71	1942	25.8	11.5										
11	23/08/71	1952			26.5	11.3	14.3	15.2			00.7	17.1	00.0	16.8
	23/08/71	1955	26.7	10.9										
C4	24/08/71	0527									00.0	16.8	00.0	16.8
	24/08/71	0528					00.0	16.8						
C2	24/08/71	0542			00.0	16.9	00.0	16.9			00.0	16.9	00.0	16.9
	24/08/71	0543	00.0	16.9										
C1	24/08/71	0552									00.0	16.9	00.0	16.9
C1	24/08/71	0750									00.0	17.5	00.0	17.5
C2	24/08/71	0756									00.0	17.2	00.0	17.2
C5	24/08/71	0807									00.0	17.2	00.0	17.2
	24/08/71	0808							00.0	17.2				
C6	24/08/71	0813			00.0	17.2	00.0	17.2			00.0	17.2	00.0	17.2
	24/08/71	0814	00.0	17.2										
17	24/08/71	0816			00.0	17.2	00.0	17.2			00.0	17.2	00.0	17.2
	24/08/71	0818	00.0	17.2										
16	24/08/71	0822			00.0	17.2	00.0	17.2			00.0	17.2	00.0	17.2
	24/08/71	0824	00.0	17.2										
15	24/08/71	0829			02.0	16.8	00.0	17.2			00.0	17.2	00.0	17.2
14	24/08/71	0833			12.8	14.3	00.0	17.2			00.0	17.2	00.0	17.2
	24/08/71	0835	22.2	12.0										
C4	24/08/71	0838									00.0	17.2	00.0	17.4
	24/08/71	0839					03.3	16.6						
C7	24/08/71	0843									00.0	17.5	00.0	17.5
	24/08/71	0844					00.0	17.5						
13	24/08/71	0847					06.7	15.7			01.0	17.0	00.0	17.5
	24/08/71	0850			26.4	10.7								
11	24/08/71	0853					16.6	12.8			00.7	17.2	00.0	17.2
	24/08/71	0856			27.3	10.6								
10	24/08/71	0858									00.8	17.1	00.0	17.5

STA	DATE	TIME PST	12.2M 0/00	°C	9.1M 0/00	°C	6.1M 0/00	°C	4.6M 0/00	°C	3.0M 0/00	°C	SURF 0/00	°C
10	24/08/71	0859					27.3	10.5						
8	24/08/71	0903									00.5	17.4	00.0	17.4
	24/08/71	0904					26.6	10.9						
8NOR	24/08/71	0905									00.3	17.4	00.1	17.5
	24/08/71	0906					26.9	10.7						
8CEN	24/08/71	0908									02.3	16.9	00.1	17.3
	24/08/71	0910					27.5	10.4						
8SOU	24/08/71	0912									17.6	12.6	00.0	17.4
6	24/08/71	0917					21.0	10.2			16.8	13.2	00.1	17.4
	24/08/71	0919			28.3	09.9								
8	24/08/71	0924					27.0	10.5			00.4	17.2	00.0	17.5
	24/08/71	0926			28.1	10.1								
10	24/08/71	0930					15.6	13.5			02.3	16.7	00.3	17.3
	24/08/71	0932			27.7	10.3								
11	24/08/71	0934					21.4	12.1			00.5	17.2	00.2	17.2
	24/08/71	0937			27.5	10.5								
13	24/08/71	0941					09.8	14.6			00.1	16.8	00.0	17.1
	24/08/71	0943			26.8	10.6								
14	24/08/71	0947			06.1	15.3	00.2	16.8			00.0	16.9	00.0	17.2
	24/08/71	0949	24.0	11.3										
15	24/08/71	0952			09.5	15.1	00.0	17.0			00.0	17.0	00.0	17.7
	24/08/71	0954	22.9	11.8										
16	24/08/71	1003					00.0	16.9			00.0	16.9	00.0	16.9
	24/08/71	1004			00.0	16.9								
C4	24/08/71	1012									00.0	17.4	00.0	17.4
	24/08/71	1013					04.4	16.6						
C7	24/08/71	1015									00.0	17.5	00.0	17.5
C1	24/08/71	1130									00.0	17.9	00.0	17.9
C4	24/08/71	1143									00.0	18.0	00.0	18.0
	24/08/71	1144					00.0	18.0						
13	24/08/71	1147			17.9	12.8	10.7	15.0			00.6	17.4	00.0	17.6
	24/08/71	1149	26.9	10.7										
11	24/08/71	1152					08.6	15.2			01.0	17.0	00.4	17.2
	24/08/71	1154			16.4	12.6								
10	24/08/71	1156			11.6	14.5	05.2	16.0			01.1	17.0	00.5	17.2
8	24/08/71	1202			04.2	16.2	02.4	16.9			01.3	17.1	00.9	17.2
	24/08/71	1204	10.5	14.8										
6	24/08/71	1207			18.7	11.6	05.1	16.1			01.6	17.0	01.1	17.1
	24/08/71	1210	27.0	10.5										

STA	DATE	TIME PST	12.2M 0/00	12.2M °C	9.1M 0/00	9.1M °C	6.1M 0/00	6.1M °C	4.6M 0/00	4.6M °C	3.0M 0/00	3.0M °C	SURF 0/00	SURF °C
4	24/08/71	1213			27.0	10.2	20.8	12.1			03.2	16.5	01.0	17.1
	24/08/71	1215	27.9	10.1										
6	24/08/71	1220			16.6	12.9	03.6	16.3			02.3	16.6	00.9	17.0
	24/08/71	1223	25.6	10.6										
8	24/08/71	1228			05.3	16.0	02.1	16.9			01.5	16.9	00.3	17.2
	24/08/71	1230	08.5	15.2										
10	24/08/71	1234			12.1	14.4	05.2	16.0			01.4	16.9	01.1	17.1
11	24/08/71	1239					08.9	15.1			01.4	17.0	01.1	16.9
	24/08/71	1241			17.8	13.0								
13	24/08/71	1244					02.5	16.6			00.6	17.0	00.3	17.1
	24/08/71	1246			17.6	13.2								
14	24/08/71	1252			02.3	16.9	00.2	17.2			00.0	17.1	00.0	17.1
	24/08/71	1254	09.3	15.2										
15	24/08/71	1256			01.7	16.8	00.5	17.0			00.0	17.1	00.0	17.1
	24/08/71	1258	05.1	15.9										
16	24/08/71	1304					00.0	17.2			00.0	17.2	00.0	17.2
	24/08/71	1305			00.0	17.2								
M1	26/08/71	0606									00.6	16.2	00.6	16.2
M1	26/08/71	0700									00.8	16.9	00.8	17.1
M1	26/08/71	0722									01.5	17.0		
	26/08/71	0724									02.3	16.9		
M1	26/08/71	0730									03.1	16.7	00.7	17.0
	26/08/71	0746									04.7	16.5		
M1	26/08/71	0800									05.2	16.4	01.0	17.1
	26/08/71	0816									06.5	16.1	00.8	17.0
M2	26/08/71	0830									00.1	16.9	00.0	17.0
M1	26/08/71	0839									06.8	16.4	01.0	17.2
	26/08/71	0900									07.6	15.9	01.0	16.9
M1	26/08/71	0930									09.5	15.9	00.8	17.1
	26/08/71	1000									10.6	15.8	00.8	17.1
M2	26/08/71	1010									00.0	17.2	00.0	17.2
M1	26/08/71	1011							00.0	17.2				
M2	26/08/71	1100									00.0	17.2	00.0	17.2
	26/08/71	1101							00.0	17.2				
M2	26/08/71	1150							00.0	17.2	00.0	17.2	00.0	17.2
M1	26/08/71	1312									06.3	17.0	00.0	18.5
M1½	26/08/71	1317									00.0	18.0	00.0	18.0

STA	DATE	TIME PST	12.2M 0/00	°C	9.1M 0/00	°C	6.1M 0/00	°C	4.6M 0/00	°C	3.0M 0/00	°C	SURF 0/00	°C
M2	26/08/71	1322									00.0	17.8	00.0	18.0
	26/08/71	1323							00.0	17.8				
N6	26/08/71	1346									00.0	18.4	00.0	18.4
	26/08/71	1347					00.5	18.0						
N5	26/08/71	1352					12.7	15.8			01.3	17.6	00.6	18.0
N7	27/08/71	0540			00.0	16.6	00.0	16.5			00.0	16.5	00.0	16.4
	27/08/71	0542	00.0	16.6										
N6	27/08/71	0548									00.0	16.4	00.0	16.3
	27/08/71	0549					00.0	16.4						
N5	27/08/71	0556					01.7	16.6			00.5	16.6	00.2	16.6
		0558			08.2 (8m)	15.8								
N4	27/08/71	0602									00.7	16.6	00.4	16.5
	27/08/71	0603					01.4	16.6						
N3	27/08/71	0608									02.7	16.3	01.6	16.4
	27/08/71	0609					08.4	15.5						
N2	27/08/71	0613									13.2	14.5	03.9	16.0
	27/08/71	0615					24.2	12.5						
N1	27/08/71	0622									26.8	11.8	09.0	15.1
	27/08/71	0624					26.9	11.5						
N2	27/08/71	0629									13.2	14.5	03.9	16.2
	27/08/71	0630					24.7	12.3						
N3	27/08/71	0634									04.5	16.1	01.4	16.3
	27/08/71	0635					09.1	15.3						
N4	27/08/71	0640									01.1	16.7	00.4	16.5
	27/08/71	0641					01.8	16.4						
N5	27/08/71	0645			11.7 (8m)	14.9	02.9	16.3			00.2	16.7	00.0	16.5
N6	27/08/71	0652					00.0	16.9			00.0	16.9	00.0	16.9
N6	27/08/71	0658					00.3	17.3			00.3	17.3	00.3	17.3
	27/08/71	0707			01.0 (7m)	17.3								
	27/08/71	0716			01.3 (7m)	17.3								
N5	27/08/71	0723					03.1	17.0			00.8	17.3	00.6	17.1
	27/08/71	0725			08.3 (7m)	16.0								
N4	27/08/71	0729					05.1	16.6			02.1	17.2	01.3	17.1

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N3	27/08/71	0736					19.4	13.8			10.4	15.7	02.4	17.0
	27/08/71	0738												
N2	27/08/71	0743					21.1	13.6			16.7	15.2	08.0	16.1
	27/08/71	0744												
N1	27/08/71	0752									23.8	12.1	12.0	15.6
	27/08/71	0753					24.0	11.9						
N2	27/08/71	0759									17.9	15.2	09.0	15.8
	27/08/71	0801					21.1	13.5						
N3	27/08/71	0804					19.6	13.5			11.7	15.3	02.9	16.8
	27/08/71	0806												
N4	27/08/71	0812					10.3	15.4			05.0	16.2	01.6	16.8
	27/08/71	0813												
N5	27/08/71	0817			09.0 (8m)	16.0	02.5	16.8			01.4	16.9	00.8	17.0
N6	27/08/71	0823					00.5	17.2			00.3	17.1	00.3	17.1
	27/08/71	0824												
N7	27/08/71	0840			00.3	17.2	00.3	17.2			00.3	17.2	00.3	17.2
	27/08/71	0842	00.3	17.2										
N6	27/08/71	0859									00.4	17.8	00.4	17.8
	27/08/71	0900					00.4	17.6						
N5	27/08/71	0907			08.5 (8m)	16.9	04.4	16.8			02.4	17.2	01.1	17.6
N4	27/08/71	0913					15.2	14.7			08.6	16.0	01.9	17.4
	27/08/71	0915			17.3 (8m)	14.4								
N3	27/08/71	0920					20.7	13.8			14.7	15.6	05.7	16.7
	27/08/71	0922												
N2	27/08/71	0927									19.6	14.7	10.4	16.4
	27/08/71	0928					22.9	13.0						
N1	27/08/71	0937									23.8	12.1	16.3	15.8
	27/08/71	0940					23.7	11.7						
N2	27/08/71	0946					23.1	12.7			20.8	14.3	09.4	16.4
	27/08/71	0947												
N3	27/08/71	0952					20.9	13.8			15.7	15.2	06.3	16.4
	27/08/71	0953												
N4	27/08/71	0956					18.2	14.1			12.3	15.2	02.1	17.2
N5	27/08/71	1001					11.2	15.3			03.3	16.3	01.5	17.0
	27/08/71	1003			12.3	14.9								
N6	27/08/71	1007									00.5	17.1	00.3	17.1
	27/08/71	1008					00.6	17.1						

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N2	27/08/71	1025									20.4	14.6	11.2	16.5
	27/08/71	1027					23.0	12.9						
N3	27/08/71	1031					21.2	13.8			14.9	15.4	05.1	17.1
N4	27/08/71	1036					19.6	14.0			12.2	15.4	00.7	17.2
N5	27/08/71	1042					13.0	14.8			02.3	17.0	01.7	17.2
		1044			16.4 (8 m)	14.4								
N6	27/08/71	1048					00.7	17.1			00.7	17.0	00.5	17.3
		1050			00.9 (7.5m)	17.1								
N6	27/08/71	1217									00.8	18.3	00.6	19.3
	27/08/71	1218					05.3	17.6						
N5	27/08/71	1223					17.3	14.8			01.8	17.9	01.1	18.2
		1225			18.4 (8 m)	14.6								
N4	27/08/71	1229					20.0	14.2			11.1	15.9	01.9	17.8
		1231			20.3 (7.5m)	14.1								
N3	27/08/71	1237					21.8	13.5			13.4	15.7	04.8	17.5
		1238			22.2 (7.5m)	13.3								
N2	27/08/71	1243									17.0	15.3	08.0	16.9
	27/08/71	1244					23.1	12.9						
N1	27/08/71	1252									21.0	14.0	14.4	16.6
	27/08/71	1253					23.8	12.1						
N2	27/08/71	1300					23.2	12.9			17.3	15.3	07.0	17.0
N3	27/08/71	1305					21.9	13.3			14.7	15.1	03.7	17.2
N4	27/08/71	1312					20.3	13.8			08.6	15.9	01.7	17.8
N5	27/08/71	1316					17.9	14.4			01.7	17.4	01.1	17.9
		1318			19.0 (8m)	14.2								
N6	27/08/71	1324									00.4	17.5	00.3	17.8
	27/08/71	1326					09.1	16.0						
N7	27/08/71	1345					00.2	18.6			00.2	18.6	00.2	18.6
N6	27/08/71	1356									00.5	18.0	00.3	18.2
	27/08/71	1358					08.0	16.0						
N2	27/08/71	1412					23.2	13.0			14.1	15.2	04.4	17.7
N3	27/08/71	1419					22.1	13.3			08.7	15.8	02.7	17.5

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N4	27/08/71	1426					20.4	13.9			04.8	16.8	01.6	17.7
N5	27/08/71	1432					18.3	14.6			01.2	17.5	00.6	17.8
		1434			19.1 (7.5m)	14.3								
N6	27/08/71	1439									00.4	17.9	00.2	18.1
	27/08/71	1441					07.9	16.2						
N3	27/08/71	1452					22.0	13.3			11.4	15.9	02.5	17.9
		1453			22.6 (7m)	13.1								
N4	27/08/71	1457					19.8	14.0			06.3	16.7	01.4	17.7
N5	27/08/71	1503					18.3	14.4			01.9	17.5	00.8	17.9
		1505			19.3 (8m)	14.2								
N6	27/08/71	1510									00.3	18.1	00.3	18.1
	27/08/71	1511					07.2	16.5						
N1	27/08/71	1531									19.5	15.6	08.6	17.3
	27/08/71	1532					24.2	10.6						
N2	27/08/71	1538									14.6	15.3	03.4	17.7
	27/08/71	1539					23.4	13.0						
N3	27/08/71	1543									08.5	16.3	02.0	17.8
	27/08/71	1545					22.5	13.2						
N4	27/08/71	1549					20.6	14.0			04.4	17.2	00.9	17.8
		1551			20.8 (7m)	13.8								
N5	27/08/71	1554					18.3	14.6			01.2	17.6	00.4	18.1
		1556			19.4 (7.5m)	14.2								
N6	27/08/71	1600									00.4	17.9	00.3	18.0
	27/08/71	1602					08.1	16.3						

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M1	01/11/71	0751											06.4	05.8
	01/11/71	0752									13.0	06.2		
M1½	01/11/71	0756											04.5	05.9
	01/11/71	0757									09.5	06.0		
	01/11/71	0758							10.8	06.1				
M2	01/11/71	0804									05.1	05.9	03.0	05.6
	01/11/71	0806							05.7	05.9				
M2½	01/11/71	0815									02.2	05.7	02.3	05.7
	01/11/71	0817					02.3	05.8						
M3	01/11/71	0829									01.2	05.8	01.0	05.6
	01/11/71	0831							01.2	05.8				
M1	01/11/71	0903											04.5	05.9
	01/11/71	0904									04.5	06.2		
M2	01/11/71	0911											02.1	05.8
	01/11/71	0912									03.4	05.8		
M3	01/11/71	0927											00.4	05.6
	01/11/71	0928									00.4	05.6		
M2	01/11/71	0944									02.7	05.8	02.0	05.9
	01/11/71	0946					02.9	06.0						
M1	01/11/71	0952											04.4	06.1
	01/11/71	0953									06.8	06.0		
M2	01/11/71	1000									02.1	05.7	01.9	05.8
	01/11/71	1002							02.5	05.7				
M3	01/11/71	1018											00.1	06.3
	01/11/71	1019									00.1	06.2		
M2	01/11/71	1035									02.1	06.0	01.7	06.0
	01/11/71	1036							02.5	05.9				
M1	01/11/71	1043											03.8	06.0
		1044									06.1	06.0		
M2	01/11/71	1050									02.1	05.8	01.7	05.9
	01/11/71	1052							02.9	05.9				
M3	01/11/71	1106											00.0	06.2
	01/11/71	1107									00.0	06.2		
M2½	01/11/71	1114									00.8	05.8	00.5	06.0
	01/11/71	1116					00.9	05.7						
M2	01/11/71	1126									02.3	05.9	01.8	05.9
	01/11/71	1127							03.3	05.9				
M1	01/11/71	1134											03.9	06.2
	01/11/71	1135									06.9	06.1		
M2	01/11/71	1141									02.3	05.9	01.8	05.9

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M2	01/11/71	1143							02.9	05.9				
M2½	01/11/71	1151									01.0	05.9	01.9	05.9
	01/11/71	1152					01.5	05.8						
M1	01/11/71	1217											05.3	06.5
	01/11/71	1218									10.3	06.4		
M2	01/11/71	1224									02.7	05.9	00.0	06.0
	01/11/71	1226							03.2	05.9				
M2½	01/11/71	1233									01.4	05.8	01.1	06.0
	01/11/71	1234					01.7	05.8						
M3	01/11/71	1241									00.5	05.8	00.2	06.1
	01/11/71	1243							00.5	05.8				
M3	01/11/71	1337									01.0	06.2	00.6	06.5
M2½	01/11/71	1347					02.9	06.0			02.5	06.1	01.9	06.3
M2	01/11/71	1357									05.5	06.5	03.7	06.6
	01/11/71	1358					06.7	06.4						
M1	01/11/71	1405									17.2	06.8	06.9	07.0
	01/11/71	1407							18.6	06.8				
M1½	01/11/71	1410									15.6	06.6	08.0	07.0
	01/11/71	1411							16.2	06.7				
M2	01/11/71	1417									06.4	06.7	04.2	07.0
	01/11/71	1418					08.9	06.5						
M2	01/11/71	1430									07.6	06.3	05.3	06.8
	01/11/71	1432					10.2	06.3						
M2	01/11/71	1448									08.7	06.6	05.3	06.6
	01/11/71	1450					11.1	06.4						
M1	01/11/71	1457											10.3	07.2
	01/11/71	1458									18.8	07.1		
M1½	01/11/71	1500									18.2	06.9	07.3	07.2
	01/11/71	1502							18.6	06.8				
M2	01/11/71	1505									08.9	06.8	04.9	06.7
	01/11/71	1507					12.7	06.5						
M2½	01/11/71	1513					05.2	06.3			04.6	06.4	02.7	06.5
		1515			05.2 (8 m)	06.3								
M3	01/11/71	1523									02.5	06.0	01.9	06.0
	01/11/71	1524							02.7	06.1				
M1	01/11/71	1542									19.8	07.0	11.0	07.5
	01/11/71	1544							20.1	07.0				
M1½	01/11/71	1546									19.1	06.9	06.7	07.0
	01/11/71	1547							19.1	06.9				

STA	DATE	TIME PST	12.2M 0/00	°C	9.1M 0/00	°C	6.1M 0/00	°C	4.6M 0/00	°C	3.0M 0/00	°C	SURF 0/00	°C
M2	01/11/71	1552									10.3	06.6	07.5	06.6
	01/11/71	1553					14.8	06.6						
M2½	01/11/71	1559					06.8	06.3			05.2	06.2	03.3	06.2
M3	01/11/71	1614									02.4	06.0	01.5	06.0
	01/11/71	1616					03.0	06.1						
M1	01/11/71	1633											07.2	06.1
	01/11/71	1634									20.3	07.0		
M1½	01/11/71	1636									18.4	06.8	06.7	06.9
	01/11/71	1637							19.5	06.9				
M2	01/11/71	1642									11.0	06.5	04.0	06.5
	01/11/71	1643					16.8	06.7						
M2	01/11/71	1651					07.1	06.2			03.8	06.1	02.6	06.0
M3	01/11/71	1700									02.9	05.9	01.6	05.9
	01/11/71	1702							07.5	06.2				
N7	02/11/71	0722					06.7	05.9			01.3	05.5	00.5	05.2
	02/11/71	0724			15.1	06.4								
N9	02/11/71	0737					00.2	05.2			00.1	05.2	00.0	05.2
		0738			00.2 (8m)	05.2								
N10	02/11/71	0743									00.0	05.2	00.0	05.2
	02/11/71	0744							00.0	05.2				
N8	02/11/71	0754									00.0	05.2	00.0	05.2
	02/11/71	0755					00.0	05.2						
N7	02/11/71	0816					08.5	06.2			01.6	05.6	00.7	05.6
	02/11/71	0818			15.6	06.7								
N6	02/11/71	0824									07.1	06.0	01.4	05.7
	02/11/71	0826					21.4	06.9						
N5	02/11/71	0831					22.5	07.1			07.7	06.1	02.9	05.7
	02/11/71	0834			22.6	07.1								
N4	02/11/71	0838									17.9	06.9	04.7	05.9
	02/11/71	0839					22.9	07.1						
N3	02/11/71	0843									21.8	06.9	06.9	06.0
	02/11/71	0844					23.1	07.1						
N2	02/11/71	0847									21.7	07.0	10.6	06.1
	02/11/71	0848					22.8	07.2						
N1	02/11/71	0853									24.0	07.2	19.9	06.7
	02/11/71	0855					24.3	07.4						

STA	DATE	TIME PST	12.2M 0/00	°C	9.1M 0/00	°C	6.1M 0/00	°C	4.6M 0/00	°C	3.0M 0/00	°C	SURF 0/00	°C
N2	02/11/71	0902									20.8	06.9	14.4	06.4
	02/11/71	0903					22.8	07.1						
N3	02/11/71	0907									19.0	06.8	07.9	06.1
	02/11/71	0909					23.0	07.2						
N4	02/11/71	0914									20.6	07.0	02.8	05.7
	02/11/71	0916					22.9	07.1						
N5	02/11/71	0921					21.2	07.0			08.4	06.0	01.9	05.7
	02/11/71	0923			22.4	07.1								
N6	02/11/71	0928									04.3	05.8	01.3	05.7
	02/11/71	0930					21.2	07.0						
N7	02/11/71	0937					04.8	05.8			00.0	05.4	00.0	05.4
	02/11/71	0939			14.5	06.5								
N9	02/11/71	0945									00.0	05.3	00.0	05.3
	02/11/71	0946					00.0	05.3						
N7	02/11/71	0952					04.7	05.5			00.1	05.3	00.0	05.3
	02/11/71	0954			10.4	06.2								
N6	02/11/71	0959									03.2	05.7	00.9	05.5
	02/11/71	1001					20.9	07.1						
N5	02/11/71	1006					19.2	07.1			05.4	05.9	02.4	05.8
	02/11/71	1008			22.0	07.1								
N4	02/11/71	1012									09.7	06.1	03.2	06.0
	02/11/71	1014					22.3	07.1						
N3	02/11/71	1017									15.1	06.6	04.1	05.9
	02/11/71	1018					22.5	07.3						
N2	02/11/71	1022									19.8	07.0	08.2	06.2
	02/11/71	1024					22.4	07.3						
N1	02/11/71	1029									22.6	07.2	19.2	06.9
	02/11/71	1031					25.5	07.9						
N9	02/11/71	1100									00.0	05.6	00.0	05.6
	02/11/71	1101					00.0	05.6						
N7	02/11/71	1106					01.8	05.6			00.1	05.6	00.0	05.6
	02/11/71	1108			04.6	05.9								
N6	02/11/71	1112									02.0	05.6	00.4	05.5
	02/11/71	1114					19.7	06.8						
N5	02/11/71	1118					21.3	07.1			06.4	06.0	02.4	05.8
N4	02/11/71	1123									07.3	06.1	02.8	05.6
	02/11/71	1125					22.5	07.0						
N3	02/11/71	1128									13.0	06.4	03.9	05.9
	02/11/71	1130					22.3	07.1						

STA	DATE	TIME PST	12.2M 0/00	°C	9.1M 0/00	°C	6.1M 0/00	°C	4.6M 0/00	°C	3.0M 0/00	°C	SURF 0/00	°C
N2	02/11/71	1134									17.9	06.8	06.7	06.1
	02/11/71	1135					22.3	07.1						
N1	02/11/71	1140									22.8	07.3	19.2	06.9
	02/11/71	1142					27.8	08.3						
N9	02/11/71	1331					00.0	05.5			00.0	05.5	00.0	05.5
	02/11/71	1332			00.0	05.5								
N7	02/11/71	1337					01.8	05.6			00.6	05.5	00.1	05.5
	02/11/71	1339			12.5	06.3								
N6	02/11/71	1344									03.0	05.8	00.3	05.4
	02/11/71	1346					17.6	07.0						
N5	02/11/71	1351					17.2	06.8			04.3	05.8	01.7	05.6
	02/11/71	1353			22.3	07.1								
N4	02/11/71	1357									11.4	06.3	03.2	05.8
	02/11/71	1358					20.5	07.1						
N3	02/11/71	1402					20.9	07.0			16.6	06.6	07.0	06.1
	02/11/71	1404			20.9	07.0								
N2	02/11/71	1407					24.1	07.5			22.4	07.3	15.2	06.7
		1409			24.3 (8 m)	07.5								
N1	02/11/71	1415									22.7	07.4	21.5	07.2
	02/11/71	1417					25.0	07.8						
N7	02/11/71	1441					04.6	05.9			01.2	05.6	00.9	05.7
	02/11/71	1443			16.0	06.6								
N6	02/11/71	1447					16.5	06.7			03.5	05.8	00.7	05.5
					20.7 (8m)	07.0								
N5	02/11/71	1455					17.1	06.8			07.8	06.1	02.9	05.8
	02/11/71	1457			21.0	07.1								
N4	02/11/71	1500					20.7	06.9			15.3	06.7	04.6	06.0
	02/11/71	1503			20.7	06.9								
N3	02/11/71	1506					23.0	07.5			21.9	07.1	11.0	06.5
	02/11/71	1508			23.1	07.3								
N2	02/11/71	1512					23.7	07.4			23.1	07.3	20.3	07.0
	02/11/71	1514			24.3	07.4								
N1	02/11/71	1518					25.9	07.7			24.3	07.6	21.9	07.4
		1520			26.4 (8 m)	08.0								
N9	02/11/71	1552					02.0	05.8			01.0	05.6	00.7	05.8
	02/11/71	1554			03.1	05.9								
N7	02/11/71	1558					06.0	06.0			03.7	05.9	02.2	05.8
	02/11/71	1600			17.2	06.8								
N6	02/11/71	1604					19.5	07.1			07.9	06.2	02.0	06.0
	02/11/71	1606			20.3	07.2								

STA	DATE	TIME PST	12.2M 0/00	°C	9.1M 0/00	°C	6.1M 0/00	°C	4.6M 0/00	°C	3.0M 0/00	°C	SURF 0/00	°C
N5	02/11/71	1611					20.5	07.1			10.8	06.5	03.2	05.9
	02/11/71	1613			20.4	07.1								
N4	02/11/71	1617					21.9	07.2			20.6	06.8	06.6	06.2
	02/11/71	1619			22.2	07.2								
N3	02/11/71	1623					24.0	07.4			21.7	07.3	11.1	06.5
	02/11/71	1626			23.9	07.6								
N2	02/11/71	1628					23.6	07.5			22.9	07.2	16.8	06.9
	02/11/71	1630			23.8	07.6								
N1	02/11/71	1634					26.7	08.1			25.7	07.7	22.7	07.2
	02/11/71	1636			27.1 (8m)	08.0								
2	05/11/71	0746			28.7	07.8	27.1	07.3			24.2	06.8	17.5	05.6
		0749	29.0 (11m)	07.8										
4	05/11/71	0754					24.2	07.2			23.5	07.0	22.9	06.7
	05/11/71	0757			28.4	07.8								
6	05/11/71	0802					23.2	06.9			22.2	06.6	18.0	06.0
	05/11/71	0804			25.0	07.3								
8	05/11/71	0808					23.8	07.2			20.6	06.4	03.4	05.1
	05/11/71	0811			25.6	07.5								
10	05/11/71	0816			26.9	07.5	22.3	06.9			11.3	05.4	00.8	04.9
		0819	26.6 (11 m)	07.6										
11	05/11/71	0822			26.2	07.5	22.6	06.9			10.1	05.4	00.2	04.9
		0825	26.0 (11 m)	07.5										
13	05/11/71	0828			24.1	07.1	16.3	06.1			03.7	05.0	01.1	04.7
		0831	24.7 (11 m)	07.2										
14	05/11/71	0835			22.7	06.9	22.1	06.7			00.8	04.6	00.0	04.6
		0838	22.8 (11 m)	07.0										
16	05/11/71	0845			12.4	06.0	04.0	05.1			00.3	04.8	00.0	04.6
	05/11/71	0847	12.8	06.0										
17	05/11/71	0852			00.0	04.7	00.0	04.7			00.0	04.7	00.0	04.7
	05/11/71	0854	00.0	04.7										
16A	05/11/71	0857					00.9	05.7			00.0	04.7	00.0	04.7
	05/11/71	0858			04.3	05.3								
17	05/11/71	0903	00.6	05.0										
17	05/11/71	0920	00.9	05.1										
17	05/11/71	0930	02.4	05.3										
16A	05/11/71	0934					02.9	05.3			00.4	05.0	00.0	05.1
	05/11/71	0936			11.3	06.1								
16	05/11/71	0940			17.0	06.5	07.2	05.6			01.3	05.0	00.0	04.9

STA	DATE	TIME PST	12.2M 0/00	12.2M °C	9.1M 0/00	9.1M °C	6.1M 0/00	6.1M °C	4.6M 0/00	4.6M °C	3.0M 0/00	3.0M °C	SURF 0/00	SURF °C
16	05/11/71	0942	17.1	06.5										
14	05/11/71	0947			23.3	06.8	20.8	06.4			02.3	04.9	00.9	04.8
	05/11/71	0950	23.6	06.8										
13	05/11/71	0954			25.5	07.3	21.5	06.6			15.7	06.2	01.6	04.8
		0957	25.6 (11m)	07.3										
11	05/11/71	1000			26.6	07.5	24.7	07.2			20.7	06.4	00.9	05.0
		1003	26.6 (11m)	07.7										
17	05/11/71	1017			03.4	05.3	00.0	04.8			00.0	04.8	00.0	04.8
	05/11/71	1019	09.8	05.9										
17A	05/11/71	1023			00.1	04.9	00.0	04.9			00.0	04.9	00.0	04.9
	05/11/71	1025	09.5	05.8										
18	05/11/71	1028			00.0	04.9	00.0	04.9			00.0	04.9	00.0	04.9
	05/11/71	1030	00.0	04.9										
18	05/11/71	1036	02.3	05.2										
18	05/11/71	1045			00.7	05.2	00.0	05.2			00.0	05.2	00.0	05.2
	05/11/71	1047	03.0	05.3										
11	05/11/71	1105			27.5	07.6	24.8	07.1			17.0	06.2	00.6	05.2
		1108	27.2 (11m)	07.7										
13	05/11/71	1112			25.9	07.5	24.4	07.2			18.0	06.5	01.3	05.1
		1114	26.0 (11m)	07.5										
14	05/11/71	1118			23.4	07.1	22.9	06.9			06.8	05.3	00.2	05.2
	05/11/71	1121	23.5	07.2										
16	05/11/71	1128			20.8	06.8	11.3	05.8			00.4	05.0	00.0	05.2
		1130	21.2 (11m)	06.9										
17	05/11/71	1134			12.3	06.1	02.4	05.2			00.0	05.0	00.0	05.2
	05/11/71	1136	15.6	06.2										
18	05/11/71	1140			00.5	05.2	00.0	05.2			00.0	05.2	00.0	05.2
	05/11/71	1142	10.7	06.0										
19	05/11/71	1150			00.0	05.3	00.0	05.3			00.0	05.3	00.0	05.3
		1152	00.0	05.3										
19	05/11/71	1210	00.0	05.3										
18	05/11/71	1214			00.0	05.3	00.0	05.3			00.0	05.3	00.0	05.3
	05/11/71	1216	08.0	05.6										
17	05/11/71	1220			09.2	05.6	05.0	05.3			00.0	05.4	00.0	05.4
	05/11/71	1223	15.5	06.3										
16	05/11/71	1226					01.4	05.1			00.8	05.0	00.0	04.9
	05/11/71	1227			20.5	06.7								
14	05/11/71	1233			23.0	06.9	17.7	06.3			10.0	05.7	00.1	04.9
13	05/11/71	1239			24.6	07.2	23.8	07.0			07.6	05.4	00.3	05.2

STA	DATE	TIME PST	12.2M 0/00	°C	9.1M 0/00	°C	6.1M 0/00	°C	4.6M 0/00	°C	3.0M 0/00	°C	SURF 0/00	°C
11	05/11/71	1245					22.3	06.6			09.0	05.5	00.6	05.4
	05/11/71	1247			26.9	07.4								
2	05/11/71	1400			26.9	07.8	27.0	07.6			23.6	07.0	07.9	05.5
	05/11/71	1403	26.1	07.6										
4	05/11/71	1408			28.8	08.0	28.5	08.0			23.7	06.9	02.2	05.5
5	05/11/71	1411	28.8	08.2										
6	05/11/71	1416			28.5	08.2	27.7	07.8			17.5	06.6	01.6	05.4
	05/11/71	1419	28.5	07.8										
8	05/11/71	1423					23.8	07.1			02.6	05.4	01.0	05.2
	05/11/71	1425			26.8	07.6								
10	05/11/71	1429					18.8	06.4			03.5	05.3	00.8	05.2
	05/11/71	1432			27.6	07.7								
11	05/11/71	1434			26.5	07.5	18.4	06.5			03.0	05.5	00.5	05.4
		1437	27.0 (11m)	07.7										
13	05/11/71	1441			24.8	07.2	18.0	06.4			02.5	05.4	00.5	05.4
		1443	25.3 (11m)	07.3										
14	05/11/71	1447			23.5	07.0	09.4	05.8			01.0	05.2	00.2	05.1
	05/11/71	1450	23.7	07.2										
16	05/11/71	1458			04.5	05.4	01.1	05.2			00.3	05.2	00.0	05.1
		1500	09.0 (11m)	05.9										
17	05/11/71	1504			03.1	05.3	00.0	05.1			00.0	05.1	00.0	05.1
	05/11/71	1507	06.6	05.7										
18	05/11/71	1510			00.0	05.0	00.0	05.0			00.0	05.0	00.0	05.0
2	05/11/71	1540					27.2	07.5			24.4	07.1	05.1	05.4
	05/11/71	1543			27.9	07.6								
4	05/11/71	1547			26.8	07.6	25.5	07.3			21.4	06.7	02.3	05.3
	05/11/71	1549	29.0	07.8										
6	05/11/71	1553			27.9	07.8	27.0	07.5			23.5	07.0	01.7	05.3
	05/11/71	1556	28.6	07.8										
8	05/11/71	1600			28.5	07.8	27.8	07.7			04.9	05.6	01.5	05.3
		1603	28.4 (11 m)	07.8										
10	05/11/71	1607			28.0	07.7	26.8	07.5			06.5	05.5	00.9	05.1
		1608	28.0 (11m)	07.7										
11	05/11/71	1610			27.5	07.7	25.4	07.3			04.8	05.5	00.6	05.1
13	05/11/71	1615			26.2	07.3	15.4	06.3			03.5	05.3	00.4	05.0
14	05/11/71	1622			21.0	06.8	08.7	05.6			02.2	05.2	00.0	04.7

STA	DATE	TIME PST	12.2M 0/00	12.2M °C	9.1M 0/00	9.1M °C	6.1M 0/00	6.1M °C	4.6M 0/00	4.6M °C	3.0M 0/00	3.0M °C	SURF 0/00	SURF °C
14	05/11/71	1624	25.0 (11m)	07.3										
16	05/11/71	1631			10.8	05.8	01.3	05.0			00.1	05.0	00.0	04.9
		1633	20.8 (11m)	06.8										
17	05/11/71	1636			02.9	05.2	00.4	05.0			00.0	04.9	00.0	04.9
17A	05/11/71	1640			01.8	05.0	00.0	04.9			00.0	04.9	00.0	04.9
	05/11/71	1642	07.6	05.6										
18	05/11/71	1644			00.0	04.9	00.0	04.9			00.0	04.9	00.0	04.9
		1645	07.0 (11m)	05.5										
C1	06/11/71	0749									11.8	04.4	03.2	04.0
	06/11/71	0751							14.9	05.0				
C2	06/11/71	0756			02.1	04.8	01.5	04.7			01.0	04.6	00.7	04.4
	06/11/71	0759	02.0	04.8										
C3	06/11/71	0803									00.0	04.4	00.0	04.4
	06/11/71	0804					00.0	04.4						
C8	06/11/71	0807											00.3	04.5
	06/11/71	0808									00.3	04.6		
C5	06/11/71	0816									00.0	04.6	00.0	04.6
	06/11/71	0817					00.0	04.6						
C1	06/11/71	0834									19.0	05.5	05.6	04.1
	06/11/71	0836							19.4	05.5				
C2	06/11/71	0841					05.7	04.7			05.3	04.8	02.2	04.7
	06/11/71	0843			06.7	04.9								
C3	06/11/71	0849					00.0	04.5			00.0	04.5	00.0	04.5
		0850			00.0 (8 m)	04.5								
C8	06/11/71	0853											00.3	04.6
	06/11/71	0854									01.1	04.8		
C5	06/11/71	0901									00.0	04.4	00.0	04.4
	06/11/71	0902					00.0	04.4						
C1	06/11/71	0920									19.0	05.3	09.6	04.3
	06/11/71	0922							20.6	05.7				
C2	06/11/71	0927									08.5	04.7	04.5	04.5
	06/11/71	0929					09.6	04.7						
C3	06/11/71	0932					01.9	04.9			01.8	04.9	00.6	04.6
		0934			02.5 (8m)	04.9								
	06/11/71	0936											00.4	04.6
	06/11/71	0937									01.7	04.6		
	06/11/71	0946									00.2	04.4	00.2	04.4

STA	DATE	TIME PST	12.2M 0/00	°C	9.1M 0/00	°C	6.1M 0/00	°C	4.6M 0/00	°C	3.0M 0/00	°C	SURF 0/00	°C
C5	06/11/71	0947					00.2	04.4						
C1	06/11/71	1046									15.1	05.2	03.6	04.9
	06/11/71	1047							21.2	05.9				
C2	06/11/71	1054			12.9	04.9	11.0	04.9			07.0	04.9	02.4	04.8
	06/11/71	1056	13.2	05.0										
C3	06/11/71	1059			10.7 (8 m)	05.8	10.1	05.7			03.5	04.9	00.7	04.8
C9	06/11/71	1106					14.2	05.9			08.9	05.4	00.3	04.8
C4	06/11/71	1111									15.5	06.1	01.1	04.9
	06/11/71	1112					22.0	06.8						
C6	06/11/71	1123	16.9 (11 m)	06.4	16.5	06.3	05.9	05.3			01.5	04.9	00.0	04.6
C5	06/11/71	1129									00.4	04.5	00.2	04.5
	06/11/71	1131					00.6	04.5						
C8	06/11/71	1138											00.3	04.5
	06/11/71	1139									01.3	04.7		
C1	06/11/71	1147									14.5	05.1	01.9	04.9
	06/11/71	1149							21.4	05.8				
C2	06/11/71	1157			08.3	05.1	05.7	04.9			03.8	05.0	02.6	04.9
	06/11/71	1159	14.1	05.0										
C3	06/11/71	1201									02.0	04.8	00.0	03.9
	06/11/71	1202					12.3	05.8						
C9	06/11/71	1208			21.0 (8 m)	06.8	19.5	06.7			06.7	05.2	00.9	04.8
C4	06/11/71	1214									16.3	06.3	00.9	04.9
	06/11/71	1215					21.9	06.7						
C6	06/11/71	1227					09.4	05.5			02.5	04.9	00.7	04.8
	06/11/71	1228			18.4	06.5								
C5	06/11/71	1232									00.4	04.7	00.0	03.6
	06/11/71	1233					00.4	04.7						
C8	06/11/71	1242											00.1	04.7
	06/11/71	1243									00.7	04.8		
C1	06/11/71	1402									05.1	05.1	00.0	04.8
	06/11/71	1404							09.1 (4 m)	05.2				
C2	06/11/71	1410			02.9 (8 m)	05.1	02.7	05.1			02.2	05.1	01.2	05.0
C3	06/11/71	1415									01.4	05.0	00.6	04.9
	06/11/71	1416					14.0	06.0						
C9	06/11/71	1421			21.7 (8 m)	06.7	21.6	06.7			07.7	05.4	00.0	04.0
C4	06/11/71	1425									02.0	05.1	00.2	04.8
	06/11/71	1427					22.0	06.7						
C6	06/11/71	1438					08.5	05.5			03.3	05.2	00.0	04.5
	06/11/71	1440			19.2	06.6								
C5	06/11/71	1443									04.8	05.2	01.3	04.8

STA	DATE	TIME PST	12.2M 0/00	°C	9.1M 0/00	°C	6.1M 0/00	°C	4.6M 0/00	°C	3.0M 0/00	°C	SURF 0/00	°C
C5	06/11/71	1444							08.5	05.5				
C8	06/11/71	1454											00.2	04.8
	06/11/71	1455									00.2	04.8		
C1	06/11/71	1502									06.3	05.0	02.3	04.8
C2	06/11/71	1508					01.9	04.9			01.4	04.9	00.0	03.9
	06/11/71	1510			02.0	05.0								
C3	06/11/71	1512									00.9	05.0	00.4	05.0
	06/11/71	1513					15.1	06.1						
C9	06/11/71	1516			21.6 (8m)	06.8	21.1	06.6			07.0	05.2	00.1	04.8
C4	06/11/71	1521									02.4	05.0	00.4	04.9
	06/11/71	1523					23.0	06.9						

STA	DATE	TIME PST	12.2M 0/00	°C	9.1M 0/00	°C	6.1M 0/00	°C	3.0M 0/00	°C	SURF 0/00	°C
C2	10/01/72	1328							00.4	02.2	00.4	02.2
		1330					00.4	02.2				
C2		1345					00.5	01.3				
C2		1358							00.6	01.2	00.6	01.2
		1400					00.6	01.2				
C2	11/01/72	1015					00.7	01.3				
C2		1044							00.8	00.9	00.8	00.9
		1046					00.8	00.9				
C2		1114							00.8	00.9	00.8	00.9
		1116					00.8	00.9				
C2		1144							00.8	00.9	00.8	00.9
		1146					00.8	00.9				
C2		1214							00.8	00.8	00.8	00.8
		1216					00.8	00.8				
C2		1245					00.8	00.8				
N7	12/01/72	1142					11.0	02.0	05.9	01.3	05.2	01.3
		1147			17.8 (7.6m)	02.5						
		1212					12.5	01.8	05.2	01.2	04.9	01.2
		1216			19.5 (7.6m)	02.8						
N7		1242					10.9	01.7	05.9	01.2	05.0	01.2
		1246			21.0 (7.6m)	02.7						
N7		1313					10.6	01.5	05.4	01.1	04.4	01.1
		1316			15.7 (7.6m)	02.2						
N7		1342					11.0	01.5	05.3	01.1	04.1	01.1
		1345			18.7 (7.6m)	02.2						
		1412			15.7	02.2	13.0	01.7	04.7	01.0	04.1	01.0
		1442					06.0	01.3	04.2	01.0	04.1	01.0
		1446			09.5 (7.6m)	01.6						

STA	DATE	TIME PST	12.2M 0/00	°C	9.1M 0/00	°C	6.1M 0/00	°C	4.6M 0/00	°C	3.0M 0/00	°C	SURF 0/00	°C
M1	7/3/72	0943											01.0	03.2
M1	7/3/72	0944									17.5	04.2		
M1.5	7/3/72	0948									17.2	04.3	00.5	03.2
	7/3/72	0949							17.3	04.3				
M2	7/3/72	0953									07.7	03.6	00.1	02.9
	7/3/72	0954							14.8	04.3				
M2.5	7/3/72	0958									00.3	02.8	00.0	02.7
	7/3/72	0959					06.6	03.6						
M3	7/3/72	1007											00.0	02.9
	7/3/72	1008									01.3	03.1		
M1	7/3/72	1020											02.0	03.0
	7/3/72	1021									17.3	04.3		
M2	7/3/72	1027									06.7	03.3	00.2	02.9
	7/3/72	1028					15.0	04.3						
M3	7/3/72	1040											00.7	02.9
	7/3/72	1041									02.5	02.9		
M1	7/3/72	1053											01.1	03.1
	7/3/72	1054									17.7	04.2		
M2	7/3/72	1100									08.1	03.5	00.4	02.9
	7/3/72	1101							15.2	04.2				
M3	7/3/72	1113											00.3	02.9
	7/3/72	1114									02.6	03.1		
M1	7/3/72	1128											01.2	03.3
	7/3/72	1129									17.5	04.2		
M2	7/3/72	1133									03.7	03.1	00.9	02.9
	7/3/72	1135							13.6	04.1				
M3	7/3/72	1146											00.6	03.0
	7/3/72	1147									02.8	03.1		
M1	7/3/72	1200											01.1	03.2
	7/3/72	1201									14.9	04.0		
M2	7/3/72	1206									04.1	03.2	01.2	03.0
	7/3/72	1208							11.3	03.9				
M3	7/3/72	1220											01.1	03.0
	7/3/72	1221									04.3	03.2		
M1	7/3/72	1345									07.6 (1.5m)	03.9	04.5	03.8
M1.5	7/3/72	1349											04.1	03.4
	7/3/72	1350									04.8	03.5		
M2	7/3/72	1353											02.9	03.3
	7/3/72	1354									04.2	03.2		

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M2.5	7/3/72	1357									03.5	03.1	02.3	03.1
	7/3/72	1358							04.0	03.1				
M3	7/3/72	1406											01.2	03.1
	7/3/72	1407									03.7	03.1		
N7	7/3/72	1415					01.6	03.1			00.1	03.0	00.0	03.0
		1417			02.1	03.3								
M1	7/3/72	1448			(7.6m)								04.0	03.4
		1449									04.0 (1.5m)	03.4		
M1.5	7/3/72	1453											04.0	03.4
		1454									04.0 (1.5m)	03.4		
M2	7/3/72	1500											02.8	03.6
	7/3/72	1501									04.0	03.4		
M2.5	7/3/72	1504											01.9	03.3
	7/3/72	1505									03.0	03.2		
M3	7/3/72	1514											00.5	03.2
	7/3/72	1515									01.9	03.2		
M1	7/3/72	1553											03.9	03.5
		1554									03.9 (1.5m)	03.5		
M1.5	7/3/72	1558											03.7	03.4
		1559									03.7 (1.5m)	03.5		
M2	7/3/72	1605											02.5	03.5
	7/3/72	1606									03.6	03.4		
M2.5	7/3/72	1613											01.4	03.1
	7/3/72	1614									02.1	03.1		
M3	7/3/72	1624											00.3	03.2
	7/3/72	1625									00.7	03.1		
M1	7/3/72	1653											03.5	03.3
		1654									03.5 (1.5m)	03.3		
M1.5	7/3/72	1700											03.3	03.3
		1701									03.3 (1.5m)	03.3		
M2	7/3/72	1708											02.0	03.1
	7/3/72	1709									03.1	03.1		
M2.5	7/3/72	1712											00.9	03.0
	7/3/72	1713									01.3	02.9		
	7/3/72	1714							01.5	02.9				
M3	7/3/72	1721											00.1	03.0
		1722									00.2 (2.1m)	02.9		
M1	7/3/72	1754											03.3	02.9
		1755									03.4 (1.5m)	03.0		
M1.5	7/3/72	1759											03.0	03.0
		1800									03.0 (2.4m)	03.0		

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M2	7/3/72	1805											01.5	02.9
	7/3/72	1806									02.4	02.9		
M2.5	7/3/72	1810									00.7	02.9	00.5	02.9
	7/3/72	1811							00.8	02.9				
M3	7/3/72	1819											00.0	02.9
	7/3/72	1820									00.2	02.9		
N1	8/3/72	0756											18.2	04.5
	8/3/72	0758									20.3	04.5		
N2	8/3/72	0803					25.4	05.0			21.7	04.6	12.8	03.9
		0805			25.9 (7.6m)	05.0								
N3	8/3/72	0808									18.0	04.4	07.5	03.6
	8/3/72	0810					24.4	04.9						
N4	8/3/72	0813					22.6	05.0			15.3	04.2	04.5	03.3
		0815			24.5 (7.6m)	05.0								
N5	8/3/72	0818					22.9	04.7			12.4	04.0	02.9	03.2
		0820			23.9 (7.6m)	04.9								
N6	8/3/72	0825									04.2	03.8	01.8	03.4
	8/3/72	0827					21.9	04.7						
N7	8/3/72	0830					09.7	03.7			00.9	03.1	00.1	03.0
	8/3/72	0832			17.7	04.3								
N9	8/3/72	0837			02.5	03.2	00.0	02.9			00.0	02.9	00.0	02.9
	8/3/72	0839	05.3	03.3										
N10	8/3/72	0843									00.0	02.8	00.0	02.8
	8/3/72	0844					00.0	02.8						
N8	8/3/72	0852									00.0	02.9	00.0	02.9
	8/3/72	0853					00.0	02.9						
N7	8/3/72	0858			17.6	04.6	11.9	03.9			00.8	03.2	00.2	03.0
		0900	18.2 (10.7m)	04.6										
N6	8/3/72	0903									10.7	03.9	00.9	03.4
	8/3/72	0905					21.4	04.6						
N5	8/3/72	0909					22.8	04.8			11.8	03.9	02.9	03.3
	8/3/72	0911			24.0	05.0								
N4	8/3/72	0915					23.6	04.7			13.1	04.1	04.0	03.3
		0916			24.7 (7.6m)	04.9								
N3	8/3/72	0920					24.9	05.0			17.7	04.3	08.9	03.8
		0922			25.3 (7.6m)	05.0								
N2	8/3/72	0925					26.2	05.1			20.4	04.8	13.6	04.3
		0927			26.3 (7.6m)	05.2								

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N1	8/3/72	0934					28.2	05.5			25.3	05.1	17.4	04.5
		0936			29.4 (7.6m)	05.5								
N2	8/3/72	0942					25.8	05.0			19.6	04.6	14.2	04.2
		0944			26.0 (7.6m)	05.1								
N3	8/3/72	0947					23.3	04.9			16.1	04.3	09.7	04.0
		0949			25.4 (7.6m)	05.0								
N4	8/3/72	0952					24.4	04.9			15.0	04.3	04.8	03.5
		0954			24.5 (7.6m)	05.0								
N5	8/3/72	0958			23.5 (7.6m)	04.7	19.0	04.6			08.8	03.8	02.1	03.4
N6	8/3/72	1004			22.7 (7.6m)	04.8	20.3	04.8			06.0	03.6	00.6	03.5
N7	8/3/72	1010	19.4 (10.7m)	04.6	18.9	04.6	12.6	04.1			00.8	03.2	00.1	03.1
N9	8/3/72	1016			09.9	03.6	00.6	03.2			00.0	03.0	00.0	03.0
	8/3/72	1018	10.6	03.9										
N10	8/3/72	1023									00.0	02.9	00.0	02.9
	8/3/72	1024					00.0	02.9						
N8	8/3/72	1036									00.0	03.2	00.0	03.2
	8/3/72	1037					00.0	03.2						
N7	8/3/72	1045			19.6	04.6	12.8	04.2			00.3	03.2	00.0	03.2
	8/3/72	1047	19.8	04.6										
N6	8/3/72	1050									07.7	03.6	01.3	03.3
	8/3/72	1052					21.8	04.7						
N5	8/3/72	1056					21.5	04.8			11.4	04.0	02.8	03.7
	8/3/72	1058			23.9	05.0								
N4	8/3/72	1101			24.4 (7.6m)	05.0	23.4	04.9			16.5	04.3	04.8	03.7
N3	8/3/72	1106			25.6 (7.6m)	05.0	25.1	04.9			17.1	04.3	09.5	04.0
N2	8/3/72	1112			26.2 (7.6m)	05.1	25.6	05.1			18.2	04.5	11.0	04.1
N1	8/3/72	1122					27.7	05.3			24.9	05.0	17.7	05.0
N2	8/3/72	1132									16.4	04.6	14.7	04.4
	8/3/72	1134					26.1	05.1						
N3	8/3/72	1138			25.7 (7.6m)	05.0	24.8	05.0			13.8	04.2	07.8	03.9
N4	8/3/72	1144			24.5 (7.6m)	05.0	23.0	04.8			14.7	04.3	04.0	03.8
N5	8/3/72	1149			24.0 (7.6m)	04.9	22.5	04.9			07.0	03.6	02.5	03.6
N6	8/3/72	1157									07.8	03.8	00.6	03.3
	8/3/72	1159					21.0	04.8						
N7	8/3/72	1201			20.1	04.5	16.8	04.2			01.1	03.3	00.0	03.1
	8/3/72	1203	20.4	04.8										
N9	8/3/72	1208	11.7 (10.7m)	04.0	11.3	04.0	00.4	03.1			00.1	03.1	00.0	03.1
N10	8/3/72	1213									00.0	03.1	00.0	03.1
	8/3/72	1215					00.0	03.1						
N1	8/3/72	1402									24.0	05.5	14.2	05.3

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N1	8/3/72	1405					26.8	05.8						
N2	8/3/72	1412									10.6	04.7	05.2	04.1
	8/3/72	1414					22.2	05.1						
N3	8/3/72	1417									07.1	04.0	03.6	03.9
	8/3/72	1419					22.0	04.9						
N4	8/3/72	1422									10.4	04.1	02.6	03.7
	8/3/72	1424					22.9	04.9						
N5	8/3/72	1428			20.6 (7.6m)	04.6	14.7	04.4			08.6	04.0	02.7	03.7
N6	8/3/72	1437									04.0	03.6	01.1	03.5
	8/3/72	1438					14.0	04.2						
N7	8/3/72	1442					02.8	03.3			00.6	03.1	00.4	03.1
	8/3/72	1444			16.4	04.2								
N9	8/3/72	1449			00.0	02.9	00.0	02.9			00.0	02.9	00.0	02.9
N1	8/3/72	1513											10.0	04.3
	8/3/72	1515									22.6	04.9		
N2	8/3/72	1522									15.0	04.2	05.4	03.7
	8/3/72	1524					19.0	04.6						
N3	8/3/72	1528									07.4	03.8	04.1	03.6
	8/3/72	1530					18.1	04.4						
N4	8/3/72	1532									08.9	04.0	03.4	03.4
	8/3/72	1534					17.3	04.5						
N5	8/3/72	1538			11.9 (7.9m)	04.0	10.9	03.9			03.8	03.4	02.6	03.4
N6	8/3/74	1547									02.1	03.3	01.5	03.2
	8/3/72	1548					02.2	03.3						
N7	8/3/72	1552					00.8	03.1			00.0	02.9	00.0	02.9
	8/3/72	1553			00.6	03.1								
N1	8/3/72	1612									19.9	04.5	07.3	03.9
	8/3/72	1614					25.9	05.2						
N2	8/3/72	1621									10.7	04.1	05.2	03.7
	8/3/72	1622					14.5	04.4						
N3	8/3/72	1627									09.5	03.9	05.1	03.7
	8/3/72	1628					13.4	04.2						
N4	8/3/72	1636									07.0	03.8	06.8	03.7
	8/3/72	1638					07.5	03.7						
N5	8/3/72	1642									04.4	03.5	02.2	03.5
	8/3/72	1643					08.1	03.9						
N6	8/3/72	1647									00.3	03.1	00.3	03.1
	8/3/72	1648					00.3	03.1						
N7	8/3/72	1652					00.2	03.1			00.0	03.1	00.0	03.1
	8/3/72	1653			00.2	03.1								

STA	DATE	TIME PST	12.2M 0/00	°C	9.1M 0/00	°C	6.1M 0/00	°C	4.6M 0/00	°C	3.0M 0/00	°C	SURF 0/00	°C
N1	8/3/72	1732									23.6	05.1	07.8	04.2
	8/3/72	1734							25.6	05.3				
N2	8/3/72	1741									10.1	03.9	06.9	03.8
	8/3/72	1742					11.3	04.0						
N3	8/3/72	1747									06.8	03.8	05.3	03.6
	8/3/72	1748					08.2	03.9						
N4	8/3/72	1752									03.8	03.4	02.9	03.3
	8/3/72	1753					04.2	03.3						
N5	8/3/72	1757									02.0	03.3	00.3	03.2
	8/3/72	1759					02.7	03.3						
N6	8/3/72	1804									00.0	03.1	00.0	03.1
	8/3/72	1805							00.0	03.1				
C4	9/3/72	0917									11.6	04.2	02.9	03.7
	9/3/72	0919							26.8	05.4				
C9	9/3/72	0923											02.6	03.5
	9/3/72	0924									12.0	04.2		
C3	9/3/72	0929									04.4	03.5	03.6	03.5
	9/3/72	0930					20.7	04.9						
C2	9/3/72	0933			05.1	03.5	05.0	03.5			04.7	03.5	03.8	03.4
C1	9/3/72	0940											03.9	03.4
	9/3/72	0941									13.3	04.8		
C8	9/3/72	0951											02.1	03.5
	9/3/72	0952									03.2	03.5		
C5	9/3/72	1000									04.4	03.4	01.0	03.2
	9/3/72	1001							07.6	03.6				
C6	9/3/72	1006					**11.4**	04.0			02.7	03.2	00.3	03.0
	9/3/72	1008			24.4	05.1								
11	10/3/72	0745									18.7	05.1	02.8	03.7
	10/3/72	0747					27.9	05.5						
13	10/3/72	0759									15.7	04.7	03.2	03.5
	10/3/72	0801					26.8	05.4						
14	10/3/72	0814					17.0	04.8			10.3	04.1	03.2	03.5
	10/3/72	0816			27.0	05.4								
16	10/3/72	0843			15.3 (7.6m)	04.4	03.8	03.4			02.6	03.4	00.3	03.3
17	10/3/72	0857					10.4	04.0			01.1	03.1	00.2	03.1
	10/3/72	0859			16.9	04.5								
18	10/3/72	0912					01.7	03.3			00.3	03.3	00.1	03.3
	10/3/72	0914			14.8	04.5								

STA	DATE	TIME PST	12.2M 0/00	°C	9.1M 0/00	°C	6.1M 0/00	°C	4.6M 0/00	°C	3.0M 0/00	°C	SURF 0/00	°C
19	10/3/72	0925			06.9	03.5	00.2	03.2			00.1	03.2	00.0	03.2
	10/3/72	0927	16.7	04.5										
20	10/3/72	0940									00.0	03.2	00.0	03.2
	10/3/72	0942					00.0	03.2						
11	10/3/72	1125									10.6	04.3	02.0	03.9
	10/3/72	1127					27.8	05.6						
13	10/3/72	1130									12.1	04.2	00.9	03.5
	10/3/72	1132					25.1	05.4						
14	10/3/72	1135			27.5 (7.6m)	05.6	13.2	04.4			06.8	03.8	00.8	03.2
16	10/3/72	1144	25.7 (10.7m)	05.4	24.9	05.3	02.4	03.5			00.9	03.5	00.2	03.6
17	10/3/72	1150			10.8 (7.6m)	03.9	05.1	03.6			00.7	03.5	00.0	03.5
18	10/3/72	1155			17.8	04.6	01.1	03.4			00.1	03.4	00.0	03.4
	10/3/72	1158	21.2	04.9										
19	10/3/72	1201			16.7	04.5	00.2	03.3			00.1	03.3	00.0	03.3
	10/3/72	1203	19.9	04.9										
20	10/3/72	1210			00.0	03.4	00.0	03.4			00.0	03.4	00.0	03.4
	10/3/72	1211	00.0	03.4										
11	10/3/72	1249					27.1	05.7			05.5	03.7	02.8	03.8
	10/3/72	1251			27.9	05.9								
13	10/3/72	1258					24.7	05.2			12.7	04.6	00.9	03.7
	10/3/72	1300			28.1	05.7								
14	10/3/72	1304			27.5	05.6	13.6	04.2			02.7	03.7	00.5	03.6
	10/3/72	1306	27.8	05.7										
16	10/3/72	1312					02.5	03.6			00.9	03.6	00.2	03.6
	10/3/72	1314			20.6	04.9								
17	10/3/72	1317			12.4 (7.6m)	04.2	04.1	03.6			00.8	03.5	00.0	03.5
18	10/3/72	1322			09.2	03.8	00.8	03.5			00.1	03.5	00.0	03.5
	10/3/72	1324	21.5	05.0										
19	10/3/72	1328			01.2	03.4	00.3	03.4			00.1	03.4	00.0	03.4
	10/3/72	1330	20.1	04.8										
20	10/3/72	1340			00.0	03.4	00.0	03.4			00.0	03.4	00.0	03.4
	10/3/72	1342	00.0	03.4										
11	10/3/72	1417	27.8 (10.7m)	05.7	27.9	05.7	21.5	05.2			06.7	04.1	00.7	04.2
13	10/3/72	1425					26.8	05.5			06.5	04.0	02.0	03.6
	10/3/72	1427			27.8	05.7								
14	10/3/72	1432	27.2 (10.7m)	05.5	25.6	05.4	11.9	04.2			03.6	03.8	00.6	03.5
16	10/3/72	1442					03.1	03.5			01.5	03.5	00.3	03.5
17	10/3/72	1448									01.3	03.5	00.1	03.5
	10/3/72	1450					06.2	03.9						
18	10/3/72	1453			00.9	03.4	00.3	03.4			00.1	03.4	00.0	03.4

STA	DATE	TIME PST	12.2M 0/00	12.2M °C	9.1M 0/00	9.1M °C	6.1M 0/00	6.1M °C	4.6M 0/00	4.6M °C	3.0M 0/00	3.0M °C	SURF 0/00	SURF °C
18	10/3/72	1455	17.1	04.5										
19	10/3/72	1459	13.8 (10.7m)	04.2	00.8	03.4	00.4	03.4			00.2	03.4	00.0	03.4
C6	10/3/72	1507					12.7	04.2			02.8	03.5	00.8	03.4
	10/3/72	1509			20.7	04.8								
C5	10/3/72	1513											02.8	04.0
	10/3/72	1514									06.2	04.0		
C8	10/3/72	1519											02.9	04.0
	10/3/72	1520									04.3	04.0		
C2	10/3/72	1523			05.3	04.0	04.8	04.0			04.3	04.0	04.4	04.0
C1	10/3/72	1529											05.4	04.0
	10/3/72	1530									05.4	04.0		
C3	10/3/72	1537			21.3	05.3	05.6	04.0			04.2	04.0	04.1	04.0
	10/3/72	1539	22.3	05.3										
C9	10/3/72	1543									04.8	04.3	03.3	04.3
	10/3/72	1544							20.7	05.0				
C4	10/3/72	1548									04.5	04.2	03.6	04.2
	10/3/72	1550							14.8	04.6				

STA	DATE	TIME PST	12.0M 0/00	12.0M °C	9.0M 0/00	9.0M °C	6.0M 0/00	6.0M °C	3.0M 0/00	3.0M °C	SURF 0/00	SURF °C
1.5	22/08/72	0830	21.6	15.6	19.1	16.0	15.3	15.5	09.9	16.4	07.0	17.3
4		0850	05.3	17.6	05.3	17.8	05.3	17.7	05.4	17.8	04.0	18.0
6		0940	02.5	18.5	02.5	18.5	02.0	18.7	01.9	18.7	01.8	18.6
8		1010	00.5	18.9	00.5	18.9	00.4	18.9	00.4	18.9	00.4	18.9
10		1015	00.4	18.9	00.3	18.9	00.2	18.9	00.1	19.0	00.2	18.1
11		1025	00.1	18.9	00.1	18.9	00.1	18.8	00.1	18.9	00.2	19.0
13		1035	00.1	19.0	00.1	19.1	00.1	19.1	00.1	19.1	00.2	19.2
C4		1050	01.1	18.9	01.1	19.0	00.7	19.1	01.1	19.0	01.1	19.1
C7		1130			00.6	19.1	00.6	19.2	00.6	19.3	00.5	19.6
C9		1145							00.3	19.2	00.4	19.3
C3		1155			00.1	19.1	00.1	19.1	00.1	19.1	00.1	19.1
C2		1205									00.2	19.5
C1		1230							00.5	19.3	00.5	19.5
C8		1300							00.1	20.1	00.1	20.5
C5		1415							00.1	20.3	00.1	21.0
C6		1430					00.2	18.9	00.2	19.7	00.1	20.1
13A		1450	00.2	19.2	00.2	18.3	00.2	19.3	00.2	19.5	00.2	19.8
14		1455	00.2	19.2	00.2	19.2	00.2	19.2	00.2	19.3	00.2	19.7
15		1505	00.2	19.1	00.1	19.1	00.1	19.1	00.2	19.2	00.2	19.5

STA	DATE	TIME PST	12.0M 0/00	12.0M °C	9.0M 0/00	9.0M °C	6.0M 0/00	6.0M °C	3.0M 0/00	3.0M °C	SURF 0/00	SURF °C
16	22/08/72	1515	00.2	19.3	00.2	19.3	00.1	19.3	00.2	19.3	00.2	19.9
17		1525					00.2	19.4	00.2	19.4	00.2	19.9
18		1530	00.1	19.4	00.1	19.1	00.2	19.1	00.1	19.3	00.2	19.6
M3	23/08/72	0735			00.0	18.8	00.0	18.8	00.0	18.8	00.0	18.8
M2		0810							00.8	19.1	00.8	19.2
M1.5		0830							01.3	19.1	01.3	19.3
M2		0900							00.5	19.3	00.4	19.3
M3		0920							00.0	19.5	00.0	19.5
N6		0940					00.0	19.2	00.0	19.3	00.0	19.3
N5		1035			01.9	19.3	01.6	19.4	00.2	19.8	00.0	20.0
N4		1045					00.6	19.3	00.6	19.3	00.3	19.4
N3		1050					00.5	19.1	00.5	19.2	00.6	19.3
N2		1055							00.8	19.2	00.7	19.3
N1		1105							07.1	19.3	06.4	19.2
N7		1140			00.0	19.0	00.0	19.0	00.0	19.1	00.0	19.0
N7	24/08/72	0740			01.2	18.8	00.2	19.0	00.1	19.0	00.1	19.1
N10		0830					00.0	18.9	00.0	18.9	00.0	18.8
N8.5		0845							00.1	19.0	00.1	19.0
N8		0855					00.0	19.1	00.0	19.1	00.0	19.1

STA	DATE	TIME PST	12.0M 0/00	12.0M °C	9.0M 0/00	9.0M °C	6.0M 0/00	6.0M °C	3.0M 0/00	3.0M °C	SURF 0/00	SURF °C
N6	24/08/72	0910					00.1	19.2	00.1	19.2	00.1	19.2
N5		0920					04.4	18.4	02.7	18.8	01.5	19.0
N4		0925					06.0	18.2	04.7	18.5	04.0	18.8
N3		0930					07.5	18.0	07.3	18.1	06.3	18.3
N2		0935					08.8	17.9	08.8	17.8	07.6	18.2
N1		0945							09.0	17.7	08.2	18.3
N5		1015			02.4	18.9	01.7	19.0	00.1	19.1	00.1	19.2
N6		1025							00.0	19.1	00.0	19.1

STA	DATE	TIME (PST)	DEPTH To Bottom In M	DEPTH In M	0/00	°C
1	26/02/73	1450	11.1	00.0	16.9	06.3
				02.2	21.7	06.8
				03.5	23.8	07.0
				05.5	25.1	06.7
				11.1	27.9	06.6
2	26/02/73	1515	11.5	01.0	22.9	05.9
				05.2	27.0	06.9
				08.3	27.0	06.9
				11.5	28.0	06.9
4	26/02/73	1530	09.8	01.3	05.8	04.9
				03.7	20.1	06.3
				07.3	28.9	06.9
				09.8	28.9	07.0
8	26/02/73	1550	10.1	01.5	04.9	04.7
				03.6	06.3	04.7
				06.1	07.4	04.8
				10.1	24.4	06.3
13	26/02/73	1605	09.8	01.2	04.7	04.7
				05.4	21.7	06.1
				09.6	27.9	06.8
				09.8	27.9	06.9
				02.8	08.7	04.9
15	26/02/73	1620	12.2	01.3	03.0	04.4
				03.9	06.0	04.5
				06.6	15.9	05.4
				12.2	26.4	06.6
16	26/02/73	1635	10.7	01.6	03.1	04.5
				03.4	05.3	04.4
				05.9	08.3	04.7
				10.7	24.7	06.3
17	26/02/73	1645	10.4	01.4	02.5	04.3
				04.8	10.0	04.9
				10.4	20.4	06.0
18	26/02/73	1650	14.4	01.4	01.2	04.3
				04.1	02.6	04.2
				11.2	09.7	04.8
				14.4	14.8	05.3

STA	DATE	TIME (PST)	DEPTH To Bottom In M	DEPTH in M	0/00	°C
19	26/02/73	1705	09.7	01.6	00.6	04.3
				03.8	01.9	04.0
				04.5	02.2	04.0
				09.7	05.1	04.3
20	26/02/73	1720	12.1	01.5	00.2	04.2
				05.5	00.3	03.4
				12.1	00.5	03.9
QB	27/02/73	1220	04.0	00.0	00.0	04.2
				02.0	00.0	04.2
				04.0	00.0	04.1
RR	27/02/73	1338	06.0	00.0	00.0	04.0
				02.0	00.0	04.0
				04.0	00.0	04.0
				06.0	00.0	04.0
A	27/02/73	1350	06.0	00.0	00.0	03.9
				02.0	00.0	03.9
				04.0	00.0	04.0
				06.0	00.0	04.0
N10	27/02/73	1500	07.0	00.0	00.2	-
				02.0	00.2	04.0
				04.0	00.2	04.0
				07.0	01.2	04.1
N9	27/02/73	1510	08.0	00.0	00.0	04.0
				02.0	00.0	04.0
				04.0	00.6	03.8
				06.0	02.3	04.6
				08.0	17.0	05.2
N8	27/02/73	1530	07.0	00.0	00.6	04.0
				02.0	00.9	04.0
				04.0	01.4	04.1
				07.0	07.6	04.6
N7	27/02/73	1555	10.0	00.0	01.6	04.1
				02.0	01.6	04.1
				04.0	01.9	04.1
				06.0	12.0	04.8
				08.0	22.3	05.9
				10.0	22.6	05.8

STA	DATE	TIME (PST)	DEPTH To Bottom In M	DEPTH In M	0/00	°C
M3	27/02/73	1600	08.0	00.0	02.0	04.3
				02.0	03.0	04.3
				04.0	10.4	04.8
				06.0	22.3	06.0
				08.0	22.5	05.8
20	28/02/73	0955	12.9	01.2	00.2	04.2
				04.9	00.2	04.1
				11.3	01.7	04.1
				12.9	04.5	04.4
20X	28/02/73	1005	23.7	01.2	00.1	04.3
				05.7	00.1	04.1
				11.5	00.4	03.9
				18.4	09.4	04.8
				23.2	10.1	04.9
				23.7	10.1	04.9
				13.1	06.2	04.5
19	28/02/73	1020	09.8	01.3	00.2	04.3
				05.7	00.9	04.2
				07.9	03.5	04.2
				08.7	08.8	04.7
				09.8	16.8	05.5
18	28/02/73	1035	14.1	01.9	00.5	04.2
				05.1	02.8	04.4
				08.3	13.4	05.2
				10.6	21.8	06.2
				14.1	23.0	06.4
17	28/02/73	1042	09.3	01.1	00.7	04.4
				06.4	13.2	05.3
				07.9	14.0	05.4
				09.3	18.2	05.9
16	28/02/73	1055	10.2	01.8	01.3	04.4
				04.2	06.1	04.7
				07.9	14.1	05.4
				08.4	17.1	05.6
				10.2	24.9	06.5

STA	DATE	TIME (PST)	DEPTH To Bottom In M	DEPTH In M	0/00	°C
15	28/02/73	1110	13.0	01.6	02.4	04.4
				05.2	13.8	05.4
				06.5	21.5	06.3
				08.3	24.9	06.6
				10.2	26.7	06.8
				13.0	26.7	06.8
13	28/02/73	1125	10.6	01.8	03.8	04.6
				03.8	20.4	06.0
				05.1	21.7	06.4
				06.8	27.3	06.9
				09.8	28.3	07.0
				10.6	28.3	07.0
10	28/02/73	1135	11.5	02.1	05.6	04.9
				04.8	17.9	06.0
				05.2	26.4	06.7
				08.9	28.6	07.0
				11.5	28.2	07.1
				05.5	26.0	06.7
				03.9	13.0	05.7
6	28/02/73	1150	12.1	01.8	08.6	05.2
				01.9	17.4	06.1
				05.6	27.3	06.9
				09.3	29.4	07.2
				12.1	29.2	07.2
16	28/02/73	1345	10.9	00.8	01.1	04.5
				05.8	06.8	04.7
				06.8	14.7	05.2
				07.4	21.1	05.9
				08.6	26.7	06.8
				10.9	26.5	06.8
18	28/02/73	1410	13.3	03.1	00.9	04.3
				08.0	14.1	05.0
				10.6	23.6	06.3
				13.3	24.0	06.5
				08.2	15.9	05.6

STA	DATE	TIME (PST)	DEPTH To Bottom In M	DEPTH In M	0/00	°C
19	28/02/73	1425	11.8	01.6	00.2	04.3
				06.8	01.3	04.2
				09.0	13.7	05.0
				09.3	20.3	06.0
				11.8	22.4	06.3
20X	28/02/73	1445	16.6	01.5	00.0	04.4
				06.3	00.0	04.3
				10.7	11.5	05.0
				16.6	14.1	05.4
21X	28/02/73	1520	14.5	01.8	00.1	04.4
				06.2	00.2	04.2
				14.5	00.2	04.1
RR	28/02/73	1610	10.3	01.6	00.0	04.6
				05.8	00.0	04.6
				10.3	00.1	04.5
N10	28/02/73	1640	07.9	01.9	00.0	05.4
				07.9	00.0	04.7
N9	28/02/73	1650	11.2	02.4	00.1	04.7
				06.3	02.5	04.8
				09.8	15.5	05.9
				11.2	17.2	06.1
N7	28/02/73	1705	08.5	02.5	00.7	04.8
				02.7	02.5	05.1
				06.5	16.8	06.0
				08.5	20.0	06.4
M3	28/02/73	1720	05.9	02.7	01.8	04.9
				02.5	07.6	05.4
				05.9	13.1	05.8
				05.9	12.7	05.8
N1	01/03/73	0945	08.8	01.8	22.9	06.9
				05.7	26.3	07.1
				08.8	27.3	07.1
N2	01/03/73	1050	08.3	01.5	22.4	06.8
				03.9	24.4	07.0
				08.3	27.3	07.1
N3	01/03/73	1110	07.9	02.5	19.9	05.7
				05.5	23.8	07.1
				07.9	25.2	07.1

STA	DATE	TIME (PST)	DEPTH To Bottom In M	DEPTH In M	0/00	^{o}C
N4	01/03/73	1115	05.8	01.9	11.3	06.0
				03.4	18.9	06.6
				05.8	25.6	07.0
N5	01/03/73	1125	08.9	02.4	08.7	05.6
				04.2	18.8	06.5
				07.1	25.5	07.0
				08.9	25.4	07.0
N6	01/03/73	1140	07.8	02.4	04.8	05.3
				04.7	14.1	06.1
				05.7	18.6	06.4
				07.8	23.2	06.9
N7	01/03/73	1150	10.4	02.5	03.0	05.1
				05.8	09.6	05.6
				07.9	17.1	06.2
				10.4	22.1	06.7
N9	01/03/73	1205	09.5	02.4	01.0	05.0
				05.8	02.4	05.1
				08.2	12.1	05.7
				09.5	13.4	05.9
N10	01/03/73	1220	08.8	02.7	00.3	05.0
				05.8	00.3	04.9
				08.8	03.0	04.9
RR	01/03/73	1245	09.6	02.4	00.0	04.7
				04.9	00.0	04.7
				09.6	00.1	04.6
20X	01/03/73	1450	22.8	02.1	00.1	04.6
				06.2	00.1	05.0
				10.9	09.3	05.1
				17.2	13.3	05.4
				22.8	13.5	05.5
20X	01/03/73	1520	22.8	02.2	00.1	04.7
				05.8	00.1	04.5
				10.4	08.3	04.9
				13.7	13.0	05.4
				17.2	13.5	05.5
				22.8	13.6	05.6

STA	DATE	TIME (PST)	DEPTH To Bottom In M	DEPTH In M	0/00	°C
20X	02/03/73	1045	21.8	01.5	00.1	04.6
				07.4	00.1	04.4
				13.1	00.1	04.3
				18.1	00.1	04.3
				21.8	00.1	04.3
18	02/03/73	1105	11.9	02.1	00.6	04.5
				06.5	01.2	04.6
				10.6	10.3	05.0
				11.9	18.4	06.0
16	02/03/73	1117	08.0	02.2	01.5	04.6
				06.1	04.1	04.8
				07.4	09.9	05.2
				08.0	12.1	05.4
13	02/03/73	1135	07.2	02.2	03.4	04.8
				03.2	12.4	05.6
				05.1	20.0	06.2
				07.2	20.0	06.3
6	02/03/73	1255	11.2	01.6	05.3	05.1
				02.9	18.7	06.2
				05.2	25.4	06.8
				08.0	28.2	07.1
				11.2	28.3	07.1
2	02/03/73	1305	07.5	02.1	08.9	05.5
				03.3	21.8	06.5
				06.3	27.2	07.0
				07.5	27.7	07.0
8	26/03/73	1410	05.4	00.0	03.4	06.7
				02.7	03.8	06.8
				05.4	08.4	06.6
15	26/03/73	1435	09.3	01.3	01.9	06.6
				03.6	02.6	06.6
				03.2	03.0	06.6
				06.8	15.0	07.0
				09.3	24.3	07.4
				09.2	25.2	07.4

STA	DATE	TIME (PST)	DEPTH To Bottom In M	DEPTH In M	0/00	°C
16	26/03/73	1450	09.8	01.6	00.6	06.4
				06.6	05.0	06.5
				08.2	14.4	06.9
				09.2	22.1	07.5
				09.8	25.1	07.5
18X	26/03/73	1515	11.3	01.4	00.9	06.5
				02.8	01.1	06.5
				06.7	01.4	06.4
				11.3	05.7	06.5
				11.3	06.0	06.5
RR	26/03/73	1638	08.2	08.2	00.0	06.3
N10	26/03/73	1705	06.9	01.3	00.0	06.6
				06.9	00.0	06.5
N9	26/03/73	1715	06.7	01.4	00.0	06.5
				06.7	00.0	05.5
				06.5	00.1	05.1
N7	26/03/73	1732	09.9	02.1	00.2	06.6
				09.8	04.1	06.8
				09.9	02.2	06.7
N1	27/03/73	0805	08.5	01.5	27.1	08.1
				06.4	29.7	07.6
				08.5	29.8	07.4
N2	27/03/73	0823	08.2	02.1	19.1	07.9
				05.4	26.0	08.5
				08.2	27.2	08.3
N3	27/03/73	0832	07.9	02.1	17.3	07.8
				05.5	26.1	08.4
				07.9	27.1	08.3
N4	27/03/73	0840	07.4	03.1	10.5	07.3
				05.6	24.2	08.2
				07.4	27.2	08.3
N5	27/03/73	0850	08.5	02.1	08.7	07.2
				05.4	24.6	08.3
				08.5	27.0	08.3
N6	27/03/73	0903	08.2	02.2	05.3	07.0
				03.8	17.9	08.0
				08.2	26.3	07.9

STA	DATE	TIME (PST)	DEPTH To Bottom In M	DEPTH In M	0/00	°C
N7	27/03/73	0915	11.6	02.3	03.0	06.8
				05.5	17.2	07.5
				10.4	23.9	08.0
				11.6	24.0	08.1
N9	27/03/73	0930	08.3	02.2	00.9	06.9
				06.3	12.2	07.2
				08.3	16.0	07.5
N10	27/03/73	0942	08.0	02.1	00.0	06.8
				07.6	04.0	06.9
				08.0	04.6	06.9
B	27/03/73	1000	06.8	01.9	00.0	06.5
				06.8	00.0	06.5
20X	27/03/73	1125	18.6	01.7	00.1	06.2
				04.7	00.1	06.3
				08.9	02.1	06.3
				10.4	14.6	07.0
				18.6	18.6	07.3
20Y	27/03/73	1127	09.5	02.2	00.1	06.1
				04.8	00.1	06.2
				09.3	08.8	06.8
				09.5	12.3	06.8
20Z	27/03/73	1140	12.5	02.3	00.1	06.1
				03.6	00.1	06.2
				10.2	11.2	06.5
				12.5	13.0	06.9
21X	27/03/73	1153	13.5	02.2	00.0	06.2
				04.9	00.0	06.2
				13.5	00.1	06.0
21Y	27/03/73	1200	12.9	02.3	00.1	06.1
				05.1	00.1	06.2
				12.8	01.7	06.1
				12.9	01.1	06.1
21Z	27/03/73	1217	13.1	02.1	00.1	06.5
				04.8	00.1	06.2
				13.1	00.1	06.0

STA	DATE	TIME (PST)	DEPTH To Bottom In M	DEPTH In M	0/00	°C
B	27/03/73	1408	05.5	01.6	00.0	06.6
				05.5	00.0	06.6
N10	27/03/73	1420	07.9	01.9	00.0	06.6
				04.4	00.0	06.8
				07.9	00.0	06.6
N9	27/03/73	1433	13.1	02.3	00.1	06.8
				04.6	01.2	06.9
				06.7	16.4	-
				07.9	07.0	07.0
				13.1	12.6	07.7
				11.9	19.9	07.7
N7	27/03/73	1452	09.6	02.1	01.6	07.1
				03.7	13.1	07.4
				09.6	24.0	08.0
N6	27/03/73	1502	05.8	02.1	02.7	07.0
				04.1	18.6	08.0
				05.8	19.1	08.0
N5	27/03/73	1515	07.5	02.2	03.3	07.7
				02.7	10.1	07.6
				07.5	25.9	08.2
N4	27/03/73	1535	06.2	02.3	05.9	07.5
				03.9	19.1	08.0
				06.2	22.5	08.1
N1	28/03/73	0810	08.8	02.5	23.6	08.4
				05.1	28.2	08.1
				08.8	29.2	07.6
N2	28/03/73	0827	07.6	02.4	22.0	07.8
				03.5	25.2	08.3
				07.6	27.2	08.2
N3	28/03/73	0837	07.7	02.4	22.1	07.9
				04.2	22.6	08.3
				07.7	26.0	08.2
				00.1	14.1	07.8

STA	DATE	TIME (PST)	DEPTH To Bottom In M	DEPTH In M	0/00	°C
N4	28/03/73	0852	07.9	00.1	10.6	07.5
				02.6	17.8	08.0
				07.9	26.6	08.3
N5	28/03/73	0900	08.4	00.1	09.3	07.3
				04.5	21.8	08.1
				08.2	26.2	08.4
N6	28/03/73	0913	06.8	00.1	05.5	07.2
				01.9	10.4	07.5
				05.2	17.8	08.0
				06.8	24.6	08.3
M3	28/03/73	0930	04.7	01.9	05.0	07.1
				03.7	11.3	07.6
				04.7	13.4	07.7
M2.5	28/03/73	0941	07.3	00.1	05.9	07.2
				03.7	12.1	07.6
				07.3	14.1	07.7
N7	28/03/73	1000	10.7	00.1	02.9	07.1
				05.8	11.9	07.6
				10.7	22.4	08.0
N9	28/03/73	1022	06.6	00.1	00.7	06.9
				06.6	04.3	07.0
N9(b)	28/03/73	1027	09.8	00.1	00.9	06.9
				08.3	05.5	07.1
				09.8	05.8	07.1
N10	28/03/73	1040	08.4	00.1	00.1	06.8
				08.2	02.7	06.9
21Z	28/03/73	1152	11.3	00.1	00.0	06.5
				11.3	00.0	06.2
21X	28/03/73	1200	11.4	00.1	00.0	06.2
				11.4	00.1	06.1
21Y	28/03/73	1208	15.6	00.1	00.0	06.2
				15.6	00.1	06.1
20Z	28/03/73	1216	12.5	00.1	00.0	06.3
				12.5	00.1	06.2
20X	28/03/73	1225	19.9	00.1	00.1	06.6
				12.4	11.8	06.9
				19.9	12.9	07.0

STA	DATE	TIME (PST)	DEPTH To Bottom In M	DEPTH In M	0/00	°C
S	28/03/73	1235	10.4	00.1	00.3	06.5
				05.1	03.1	06.6
				06.9	04.4	06.5
				10.4	05.6	06.6
M	28/03/73	1242	13.8	00.1	00.1	06.2
				05.5	01.2	06.4
				07.6	03.0	06.4
				10.1	06.1	06.5
				13.1	13.2	07.2
				13.8	19.0	07.3
N	28/03/73	1250	14.3	00.1	00.1	06.4
				06.4	01.7	06.5
				09.3	05.3	06.5
				14.3	17.6	07.2
M	28/03/73	1300	12.6	00.1	00.1	06.4
				05.4	00.9	06.5
				10.5	06.7	06.6
				11.7	10.2	06.7
				12.6	14.9	07.0
N7X	28/03/73	1545	04.5	00.1	01.4	07.4
				03.6	09.1	07.6
				04.3	11.0	07.6
				04.5	03.7	07.5
N7	28/03/73	1645	07.8	00.1	00.8	07.0
				03.1	02.7	07.2
				06.2	10.3	07.5
				07.8	13.4	07.5
M3	28/03/73	1650	03.4	00.1	02.6	07.1
				02.2	04.4	07.3
				03.4	05.1	07.3

STA	DATE	TIME (PST)	DEPTH To Bottom In M	DEPTH In M	0/00	°C
N7X	29/03/73	0820	04.9	00.1	04.7	07.1
				01.6	07.9	07.4
				04.7	13.7	07.7
				04.9	15.8	07.9
N7X	29/03/73	0850	05.6	00.1	04.5	07.0
				02.7	06.9	07.2
				05.6	12.8	07.6
N7X	29/03/73	0920	05.7	00.1	03.8	07.0
				03.5	07.0	07.3
				05.6	08.7	07.3
				05.7	14.1	07.6
N7X	29/03/73	0950	05.7	00.1	03.6	07.0
				02.8	05.1	07.2
				05.3	08.5	07.3
				05.7	10.7	07.5
N7X	29/03/73	1020	03.7	00.1	03.3	07.0
				02.9	04.5	07.2
				03.7	07.0	07.3
N7X	29/03/73	1023	05.8	05.8	07.7	07.3
N7X	29/03/73	1025	05.8	05.8	16.1	07.6
N7X	29/03/73	1027	05.7	05.7	08.5	07.4
N7X	29/03/73	1050	05.8	00.1	03.0	07.0
				03.7	05.9	07.2
				05.7	11.8	07.4
				05.8	11.8	07.4
N7X	29/03/73	1120	05.7	00.1	02.4	06.9
				03.3	04.9	07.2
				05.6	10.0	07.3
				05.7	11.5	07.4
N7X	29/03/73	1150	05.7	00.1	02.3	06.9
				03.4	04.8	07.1
				05.3	12.4	07.4
				05.7	12.2	07.5
N7X	29/03/73	1220	06.1	00.1	02.1	07.0
				03.2	05.0	07.1
				04.7	09.3	07.3
				06.1	14.1	07.6

STA	DATE	TIME (PST)	DEPTH To Bottom In M	DEPTH In M	0/00	°C
N7X	29/03/73	1250	00.1	00.1	01.8	07.0
N7X	29/03/73	1052	03.7	03.7	04.3	07.1
N7X	29/03/73	1053	04.1	04.1	10.3	07.3
N7X	29/03/73	1054	03.7	03.7	07.8	07.2
N7X	29/03/73	1055	05.7	05.7	14.2	07.6
N7X	29/03/73	1056	05.8	05.8	13.8	07.6
N7X	29/03/73	1320	05.8	00.1	01.8	07.0
				03.4	04.6	07.1
				04.6	11.5	07.4
				05.8	15.7	07.7
N7X	29/03/73	1350	06.0	00.1	01.5	07.1
				02.4	02.9	07.1
				05.1	11.8	07.6
				06.0	17.1	07.8
N7X	29/03/73	1420	06.0	00.1	01.4	07.0
				03.1	05.8	07.2
				05.7	15.9	07.6
				06.0	18.5	07.8
N7X	29/03/73	1450	06.0	00.1	01.6	07.0
				02.2	04.5	07.2
				05.9	19.8	07.8
				05.8	18.0	07.8
				06.0	17.5	07.8
N7X	29/03/73	1520	05.9	00.1	01.5	07.0
				02.7	05.1	07.3
				05.5	20.3	07.8
				05.9	20.9	07.9
N7X	29/03/73	1550	05.7	00.1	01.8	07.0
				03.3	06.8	07.3
				05.3	18.5	07.8
				05.7	20.7	07.9
N7X	29/03/73	1620	05.4	00.1	01.7	06.9
				02.7	05.5	07.3
				05.4	20.6	07.8

TIME SERIES

STA	DATE	TIME PST	12.2M 0/00	°C	9.1M 0/00	°C	6.1M 0/00	°C	3.0M 0/00	°C	SURF 0/00	°C
N7	12/01/72	1530							03.0	01.0	02.6	01.0
		1532					11.2	01.8				
N7	12/01/72	1600							02.6	00.9	02.3	00.9
		1602					10.9	01.5				
N7	12/01/72	1630							01.9	00.7	01.9	00.7
		1632					12.4	01.2				
N7	12/01/72	1701							01.9	00.8	01.7	00.8
		1703					02.6	00.8				
N7	12/01/72	1730							02.4	00.9	01.9	00.9
		1732					03.1	00.9				
N7	12/01/72	1802							01.6	00.9	01.6	00.9
		1804					02.6 (4.6m)	00.9				
N7	12/01/72	1840							01.3	00.8	01.3	00.8
		1842					01.7	00.8				
N7	12/01/72	1945							01.1	00.8	00.5	00.8
		1947					01.3	00.8				
N7	12/01/72	2030							00.8	00.8	00.7	00.8
		2032					01.1	00.8				
N7	12/01/72	2130							00.5	00.6	00.5	00.6
		2132					00.7	00.6				
N7	12/01/72	2230							00.5	00.6	00.2	00.6
		2232					00.6	00.6				
N7	12/01/72	2330							01.0	00.5	01.0	00.5
							00.8	00.5				
N7	13/01/72	0024							00.4	00.5	00.4	00.5
		0031					00.8	00.5				
N7	13/01/72	0130							00.8	00.5	00.7	00.5
		0132					01.0	00.5				
N7	13/01/72	0230							01.2	00.5	00.8	00.5
		0232			01.8 (7.6m)	00.8	01.7	00.5				
N7	13/01/72	0330							01.6	00.8	01.4	00.8
		0332			02.9 (7.6m)	00.9	02.4	00.8				
N7	13/01/72	0400							02.0	00.7	01.8	00.6
		0402			03.5 (7.6m)	00.9	03.1	00.8				
N7	13/01/72	0430							03.6	00.8	03.1	00.7
		0432			03.8 (7.6m)	00.9	03.7	00.9				
N7	13/01/72	0530					10.0	01.5	04.7	00.8	02.6	00.5
		0533			12.2	01.7						

STA	DATE	TIME PST	12.2M 0/00 °C		9.1M 0/00 °C		6.1M 0/00 °C		3.0M 0/00 °C		SURF 0/00 °C	
N7	13/01/72	0600					16.0	02.2	06.6	00.9	04.6	00.7
		0603			17.6	02.3						
N7	13/01/72	0630					15.1	02.1	07.0	01.3	04.2	00.6
		0634			21.0	03.0						
N7	13/01/72	0700					14.4	01.9	04.2	00.6	02.9	00.6
		0703			23.9	03.3						
N7	13/01/72	0730					21.8	02.9	04.2	00.5	02.6	00.5
		0733			25.8	03.5						
N7	13/01/72	0800					23.6	03.4	07.1	01.1	02.5	00.5
		0803			27.0	03.8						
N7	13/01/72	0900					20.4	02.8	08.3	01.1	02.9	00.7
		0904			28.1	03.9						
N7	13/01/72	0930					22.6	03.1	03.2	00.9	03.2	00.8
		0933			28.0	04.2						
N7	13/01/72	1000					19.0	03.0	03.0	00.9	02.6	00.9
		1003			27.6	04.1						
N7	13/01/72	1030					25.2	03.6	02.6	01.0	02.3	01.0
		1033			28.8	04.4						
N7	13/01/72	1100					19.4	02.6	04.0	01.0	02.4	01.0
		1103			28.6	04.3						
N7	13/01/72	1130					25.4	03.0	04.1	01.1	02.6	01.1
		1133			29.5	04.3						
N7	13/01/72	1200					24.5	03.3	03.8	00.9	02.0	00.7
		1203			29.8	04.1						
N7	13/01/72	1230					24.8	03.7	06.5	01.0	01.8	00.8
		1233			29.3	04.4						
N7	13/01/72	1300					26.9	03.9	04.0	01.0	01.8	00.8
		1303			29.9	04.3						
TILB	15/01/72	0700					01.8	01.5	01.8	01.5	01.8	01.5
		0730					02.2	00.9	01.6	00.9	01.3	00.9
		0800					06.2	01.3	05.3	01.3	04.9	01.3
		0830					06.5	01.5	06.5	01.5	06.1	01.5
		0900					04.7	01.3	04.7	01.3	04.7	01.3

STA	DATE	TIME PST	12.2M 0/00	°C	9.1M 0/00	°C	6.1M 0/00	°C	3.0M 0/00	°C	SURF 0/00	°C
TILB	14/02/72	0630							00.0	00.8	00.0	00.8
	14/02/72	0633					00.0	00.8				
	14/02/72	0700							00.0	00.8	00.0	00.8
	14/02/72	0703					00.0	00.8				
	14/02/72	0730							00.0	00.8	00.0	00.8
	14/02/72	0733					00.0	00.8				
	14/02/72	0800							00.0	00.8	00.0	00.8
	14/02/72	0803					00.3	00.8				
	14/02/72	0830							00.0	00.8	00.0	00.8
	14/02/72	0833					00.7	00.8				
	14/02/72	0900							00.8	00.8	00.1	00.8
	14/02/72	0903					01.2	00.8				
	14/02/72	0930							01.8	01.0	00.0	00.8
	14/02/72	0933					02.1	01.0				
	14/02/72	1000							00.8	00.8	00.8	00.8
	14/02/72	1003					03.1	01.0				
	14/02/72	1030							00.2	00.8	00.2	00.8
	14/02/72	1033					01.6	00.8				
N7	14/02/72	2200							01.9	01.4	01.8	01.4
	14/02/72	2202					02.4	01.4				
	14/02/72	2230							01.5	01.3	01.2	01.3
	14/02/72	2232					01.7	01.3				
	14/02/72	2300							00.8	01.3	00.1	01.3
	14/02/72	2302					00.9	01.3				
	14/02/72	2330							00.3	01.2	00.5	01.2
	14/02/72	2332					00.6	01.2				
	15/02/72	0030							00.1	01.2	00.0	01.2
	15/02/72	0032					00.1	01.2				
	15/02/72	0100							00.0	01.2	00.0	01.2
	15/02/72	0102					00.0	01.2				
	15/02/72	0200							00.0	01.4	00.0	01.4
	15/02/72	0202					00.0	01.4				
	15/02/72	0300							00.0	01.4	00.0	01.4
	15/02/72	0302					00.0	01.4				
	15/02/72	0400							00.2	01.4	00.0	01.4
	15/02/72	0402					00.4	01.4				
	15/02/72	0500							02.6	01.6	02.5	01.6
	15/02/72	0503					03.1	01.6				

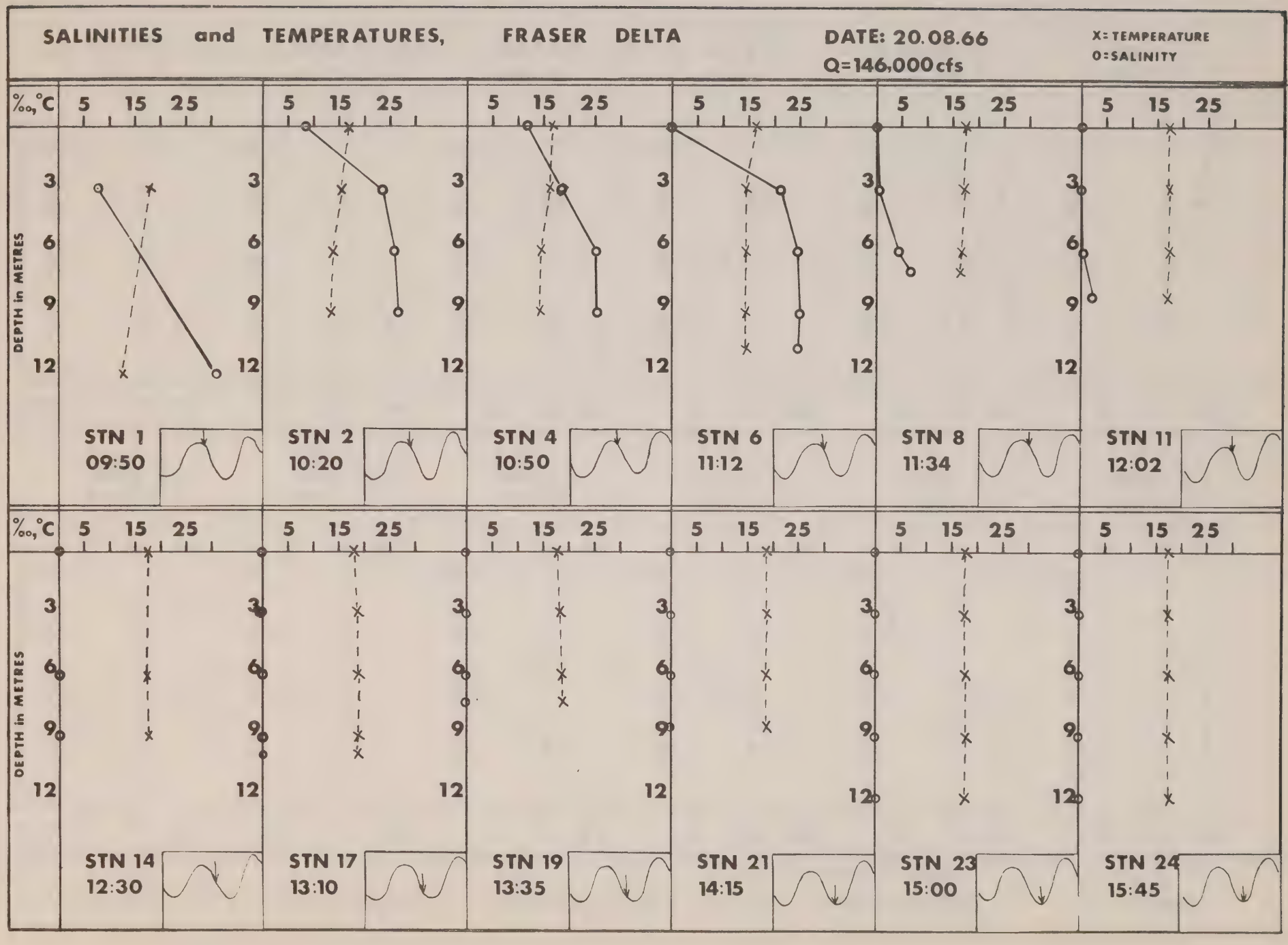
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	15/02/72	0530							03.8	01.8	03.2	01.8
	15/02/72	0533			04.9	01.8	04.5	01.8				
	15/02/72	0600							05.6	01.9	04.3	01.9
	15/02/72	0603			06.0	01.9	05.6	01.9				
	15/02/72	0630							06.4	02.2	05.5	02.2
	15/02/72	0633			07.0	02.2	06.9	02.2				
	15/02/72	0700							10.5	02.6	07.1	02.2
	15/02/72	0703			13.7	03.4	12.1	02.7				
	15/02/72	0730							07.9	02.5	07.3	02.5
	15/02/72	0733			17.1	03.6	13.8	03.1				
	15/02/72	0800							08.1	02.5	05.1	02.1
	15/02/72	0803			19.9	03.9	14.7	03.4				
	15/02/72	0830							07.6	02.5	05.3	02.2
	15/02/72	0833			20.0	03.9	17.8	03.6				
	15/02/72	0900							09.2	02.6	04.8	02.2
	15/02/72	0903			21.0 (7.6m)	04.1	19.6	03.9				
	15/02/72	1000							05.9	02.2	03.6	02.1
	15/02/72	1003					14.1	03.2				
	15/02/72	1100							03.4	02.0	03.1	02.0
	15/02/72	1102					05.9	02.3				
	15/02/72	1200							03.1	02.0	02.7	02.0
	15/02/72	1202					04.5	02.1				
	15/02/72	1300							01.8	02.0	01.4	02.0
	15/02/72	1303					05.5	02.3				
	15/02/72	1400							01.0	02.0	00.7	02.2
	15/02/72	1402					06.2	02.3				
	15/02/72	1500							02.9	02.0	06.4	02.0
	15/02/72	1502					08.4	02.3				
	15/02/72	1700							05.9	02.6	01.9	02.6
	15/02/72	1702					13.7	03.3				
	15/02/72	1800							04.5	02.2	01.2	02.0
	15/02/72	1803			17.9	03.9	13.6	03.1				
	15/02/72	1900							04.9	02.2	01.6	02.2
	15/02/72	1903			18.1	03.8	14.0	03.5				
	15/02/72	2000							02.8	01.9	00.6	01.8
	15/02/72	2002					08.3	02.5				
	15/02/72	2100							01.5	02.0	00.9	02.0
	15/02/72	2102					05.9	02.2				

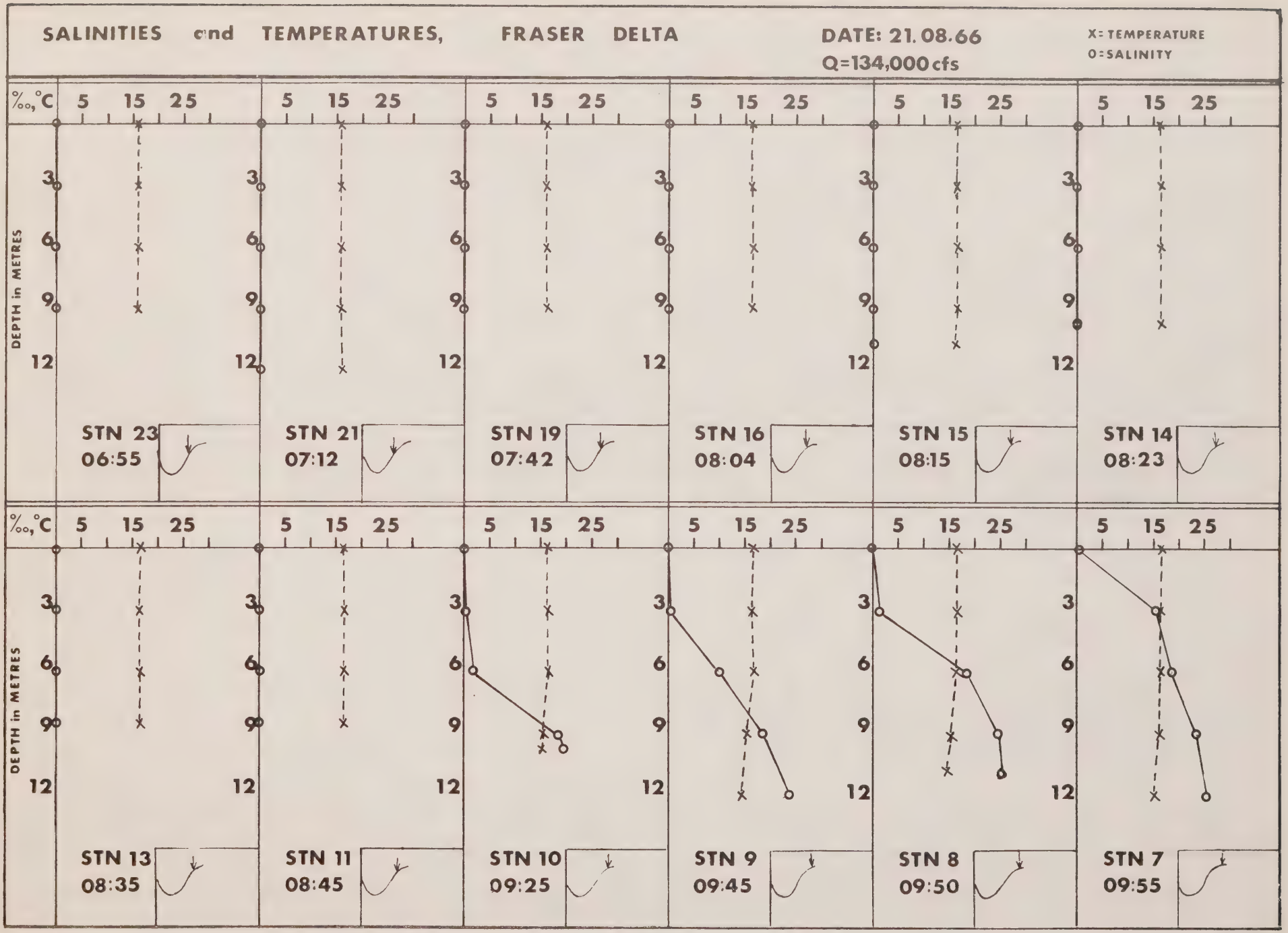
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RR	16/02/72	0830							00.0	02.5	00.0	02.5
		0833			00.0	02.5	00.0	02.5				
		0900							00.0	02.1	00.0	02.5
		0903			00.0	02.2	00.0	02.1				
		0930							00.0	02.8	00.0	03.3
		0933			00.0	03.5	00.0	02.8				
		1000							00.0	02.2	00.0	02.2
		1003			00.0	02.2	00.0	02.2				

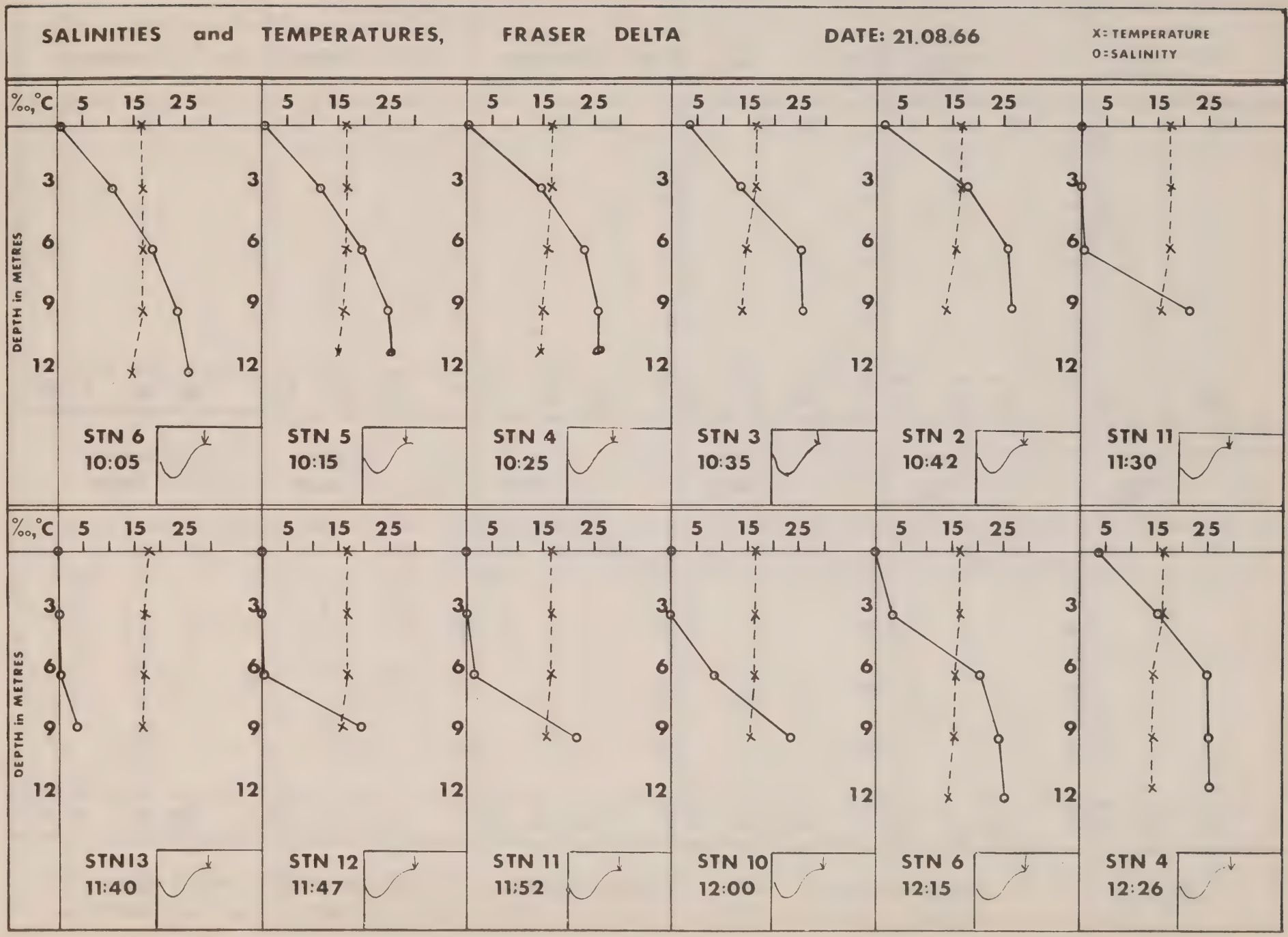
PROFILES OF

TABULATED DATA

1966 - 1973


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12
STN 1
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STN 2
10:20
STN 4
10:50
STN 6
11:12
STN 8
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12:30
STN 17
13:10
STN 19
13:35
STN 21
14:15
STN 23
15:00
STN 24
15:45


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 21.08.66
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O= SALINITY
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DEPTH in METRES
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12
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06:55
STN 21
07:12
STN 19
07:42
STN 16
08:04
STN 15
08:15
STN 14
08:23
STN 13
08:35
STN 11
08:45
STN 10
09:25
STN 9
09:45
STN 8
09:50
STN 7
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SALINITIES and TEMPERATURES, FRASER DELTA
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O=SALINITY
‰,°C
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DEPTH in METRES
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9
12
STN 6
10:05
STN 5
10:15
STN 4
10:25
STN 3
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STN 2
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11:30
STN13
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STN 12
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STN 4
12:26

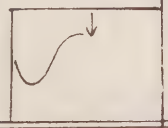
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X = TEMPERATURE
O = SALINITY

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DEPTH in METRES 3 6 9 12

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STN 1
12:50



STN

STN

STN

STN

‰, °C 5 15 25

DEPTH in METRES 3 6 9 12

STN

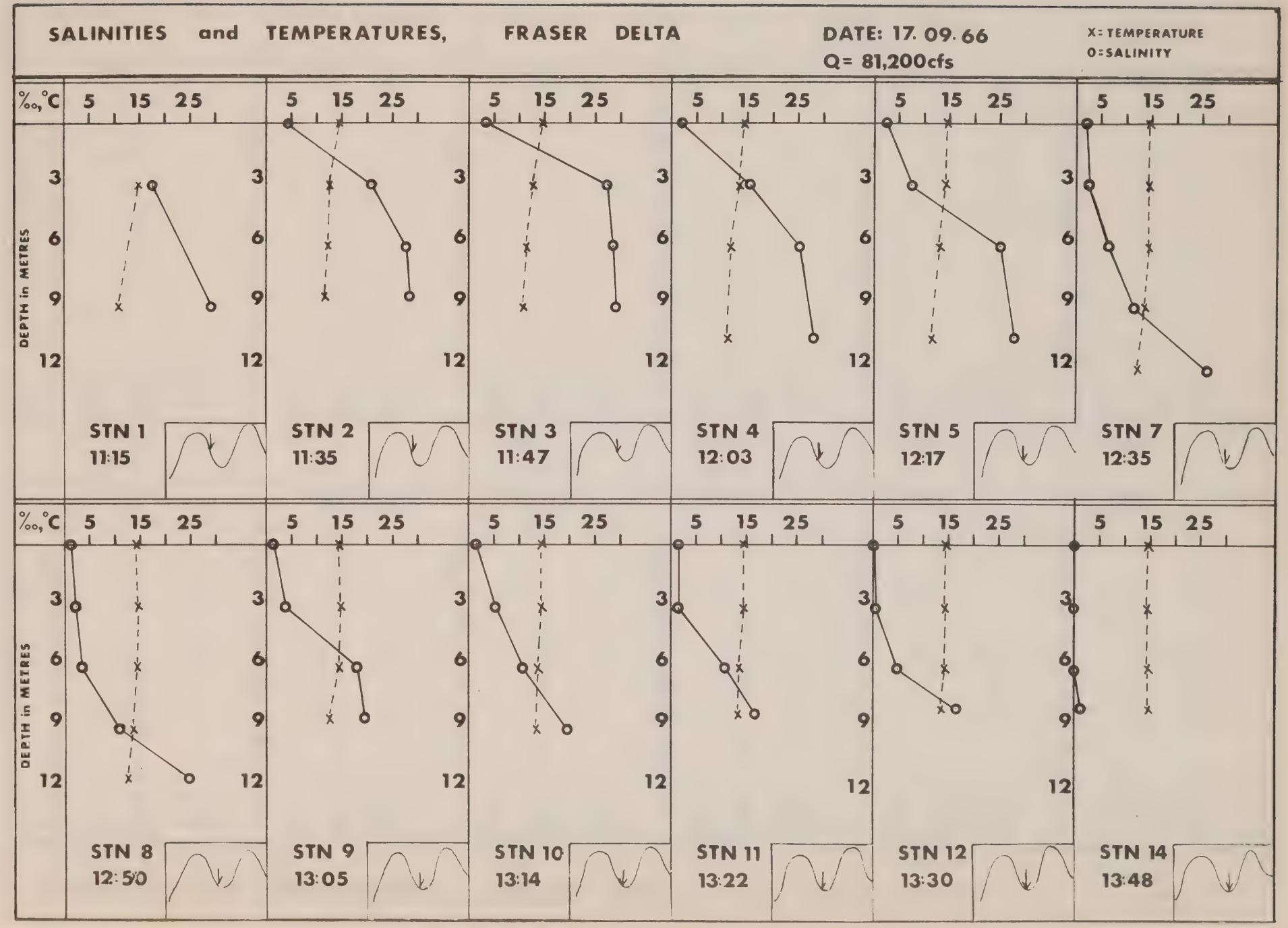
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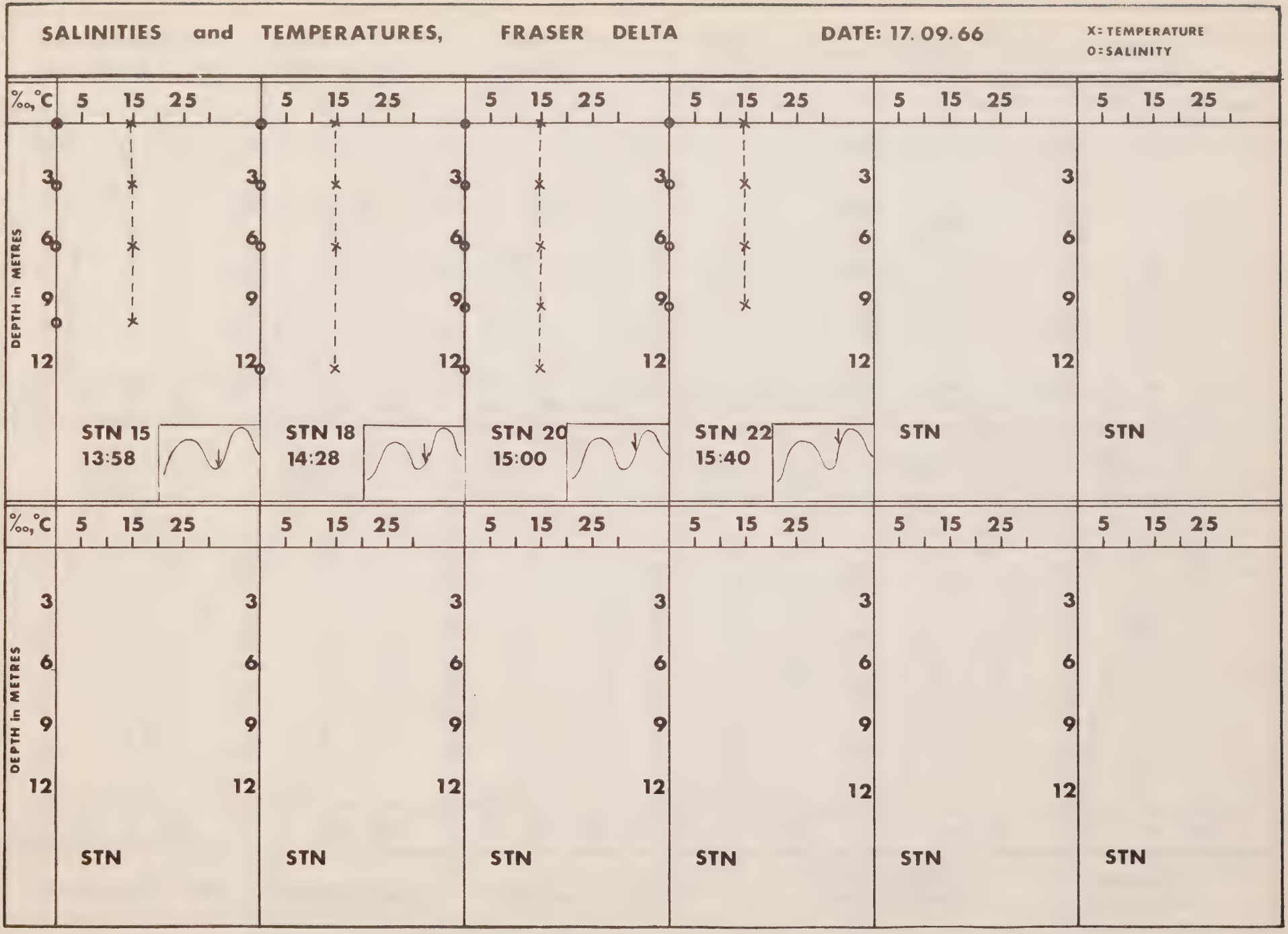
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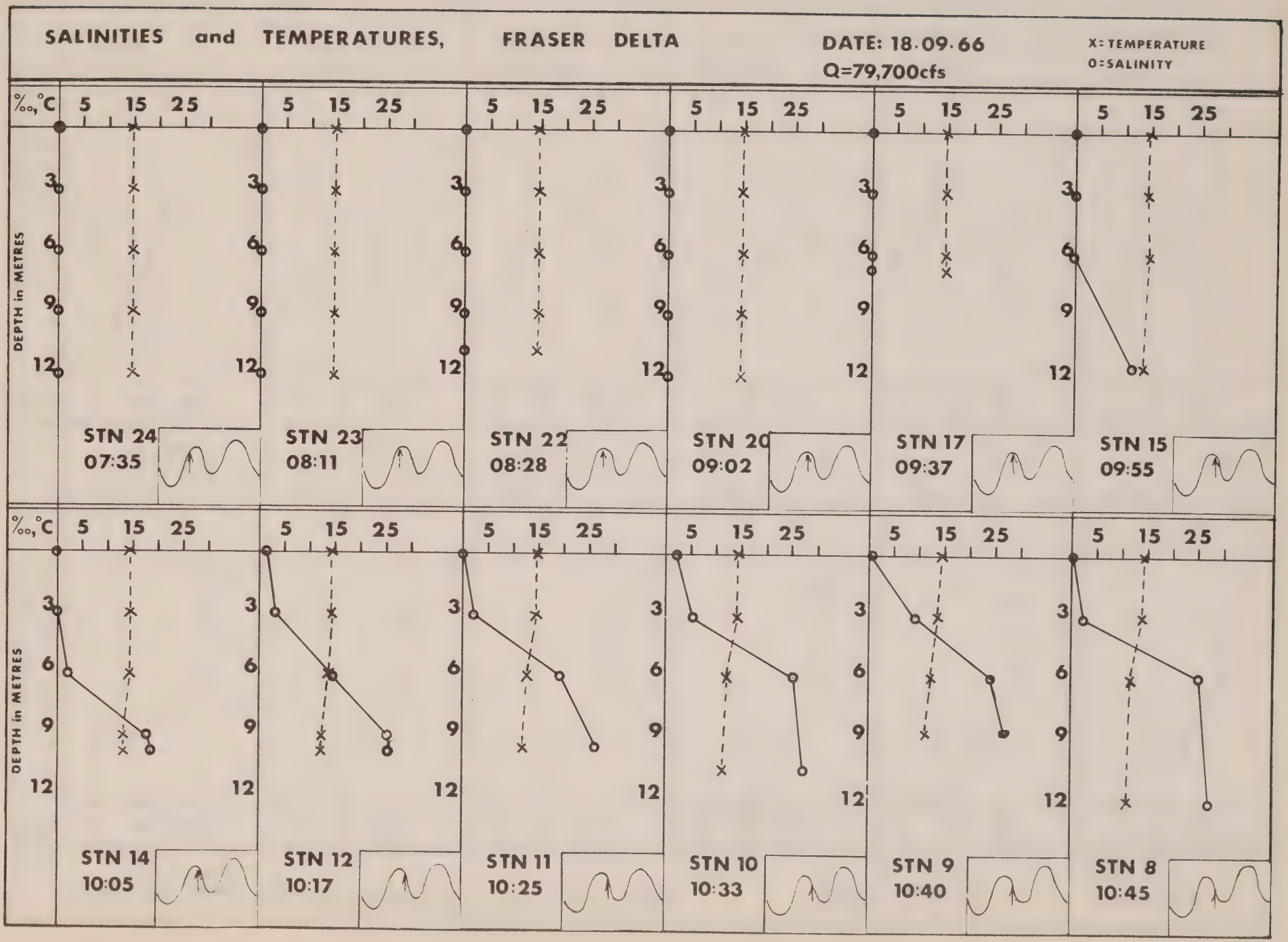
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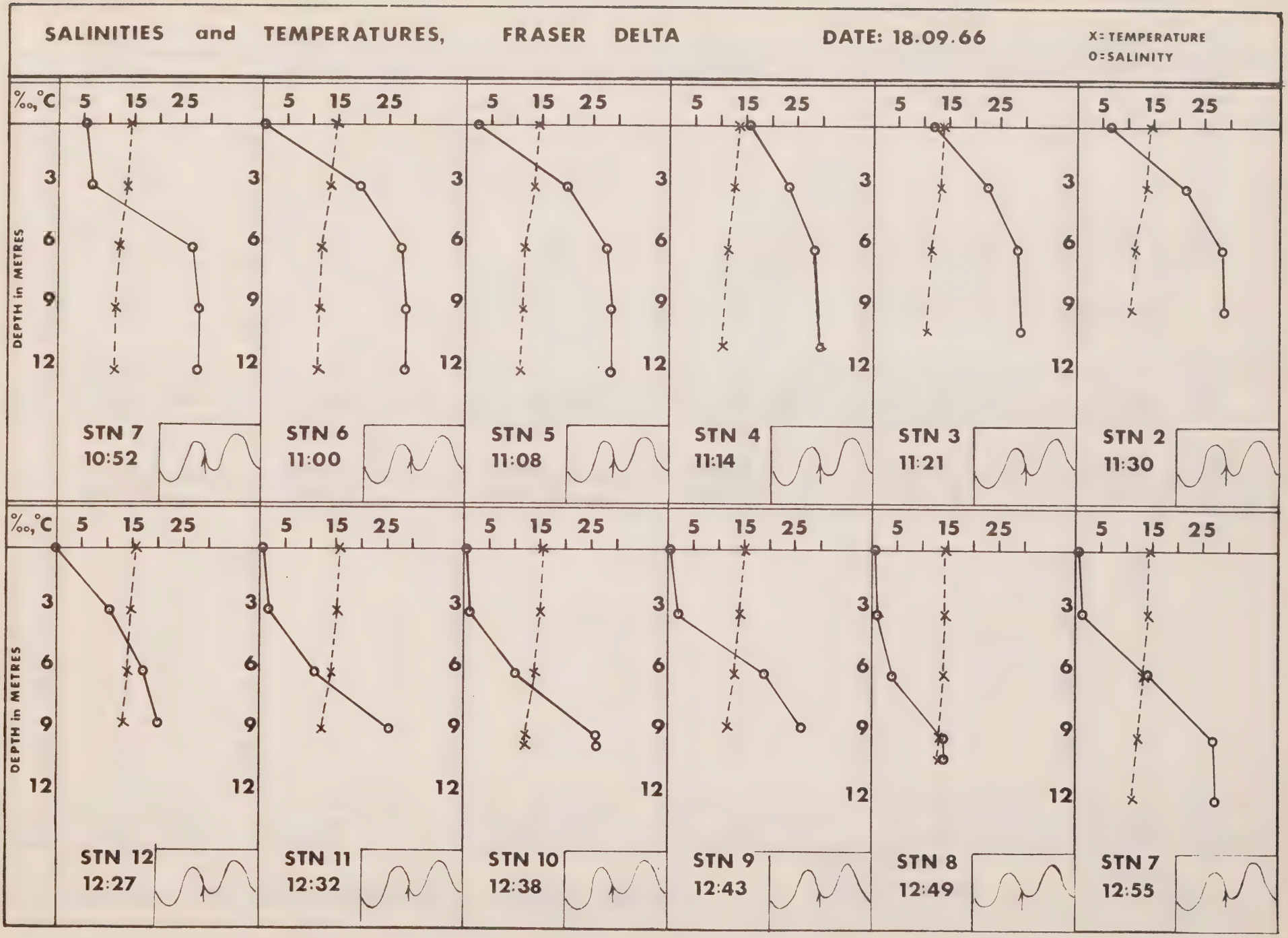
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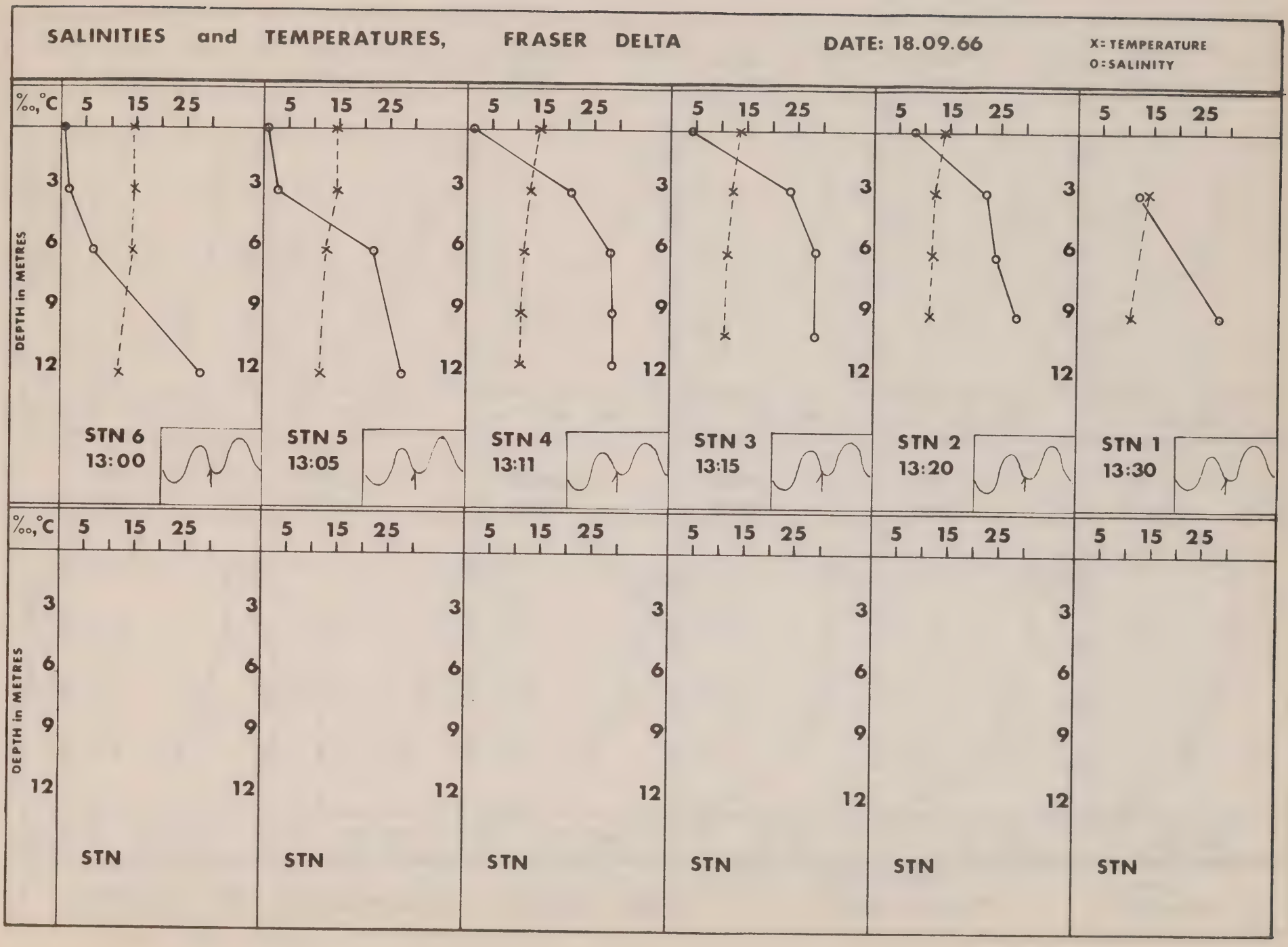
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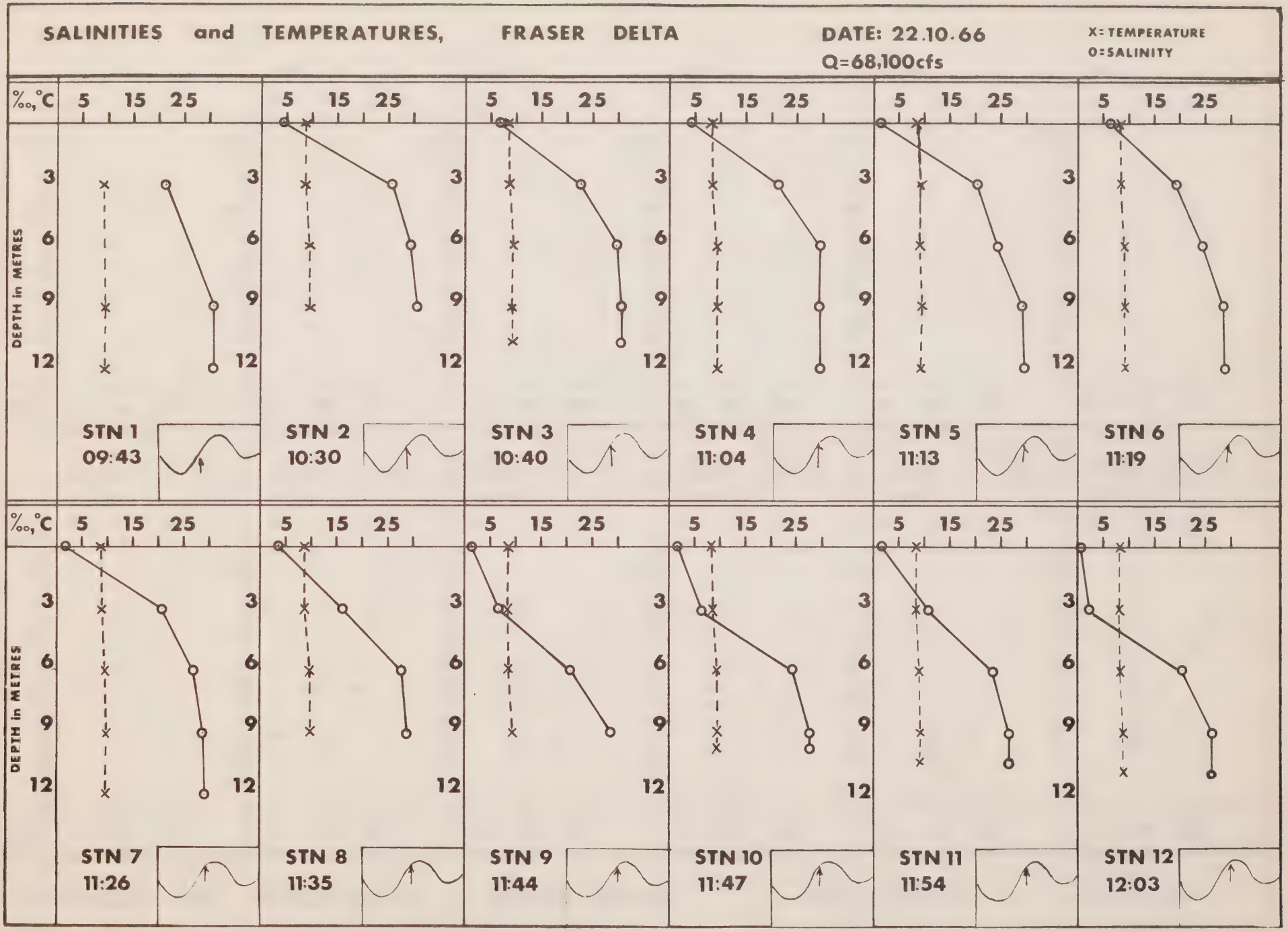

SALINITIES and TEMPERATURES, FRASER DELTA
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12
STN 1
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STN 2
11:35
STN 3
11:47
STN 4
12:03
STN 5
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13:30
STN 14
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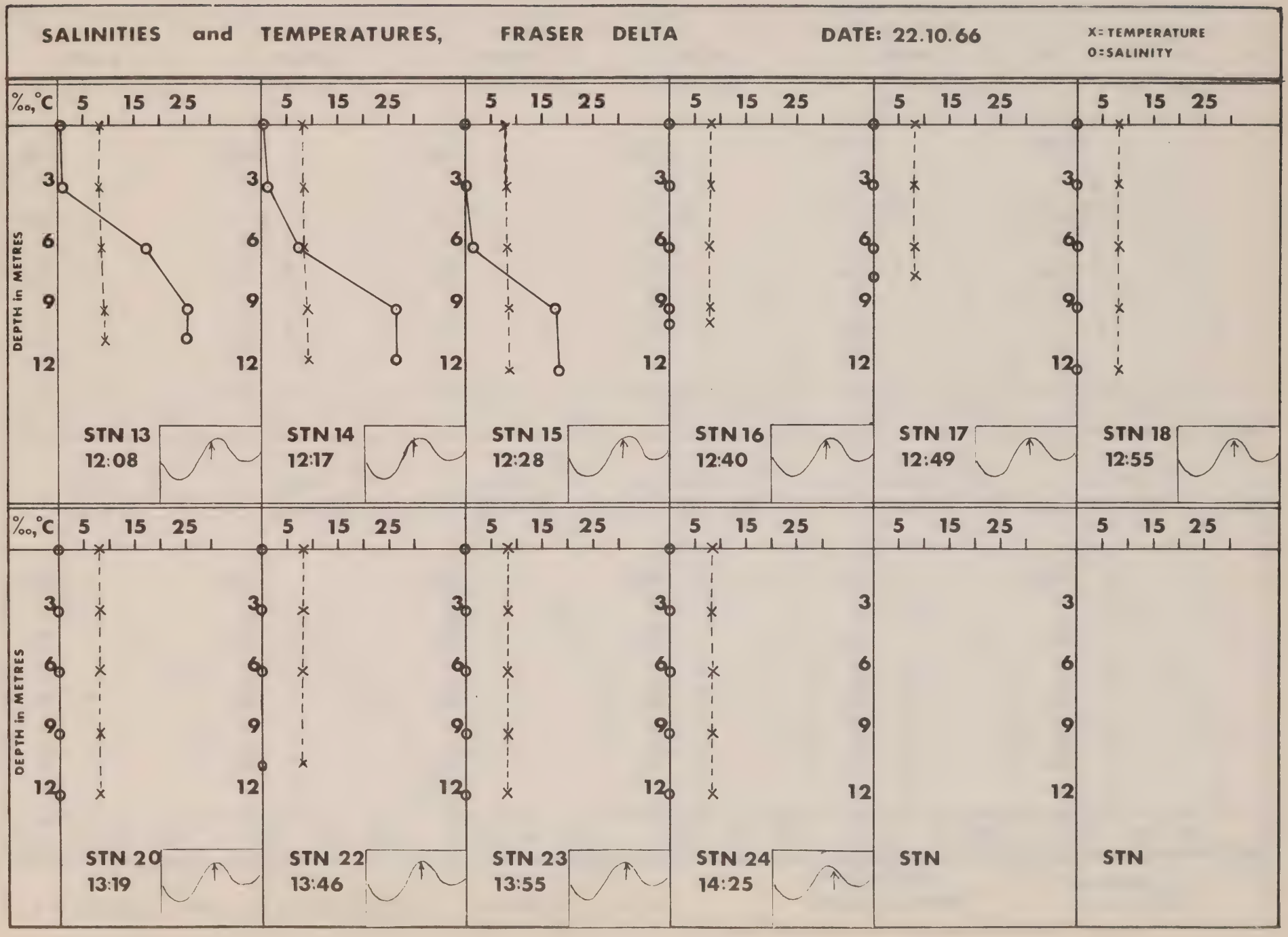

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 17. 09. 66
X = TEMPERATURE
O = SALINITY
‰, °C
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DEPTH in METRES
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12
STN 15
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14:28
STN 20
15:00
STN 22
15:40
STN

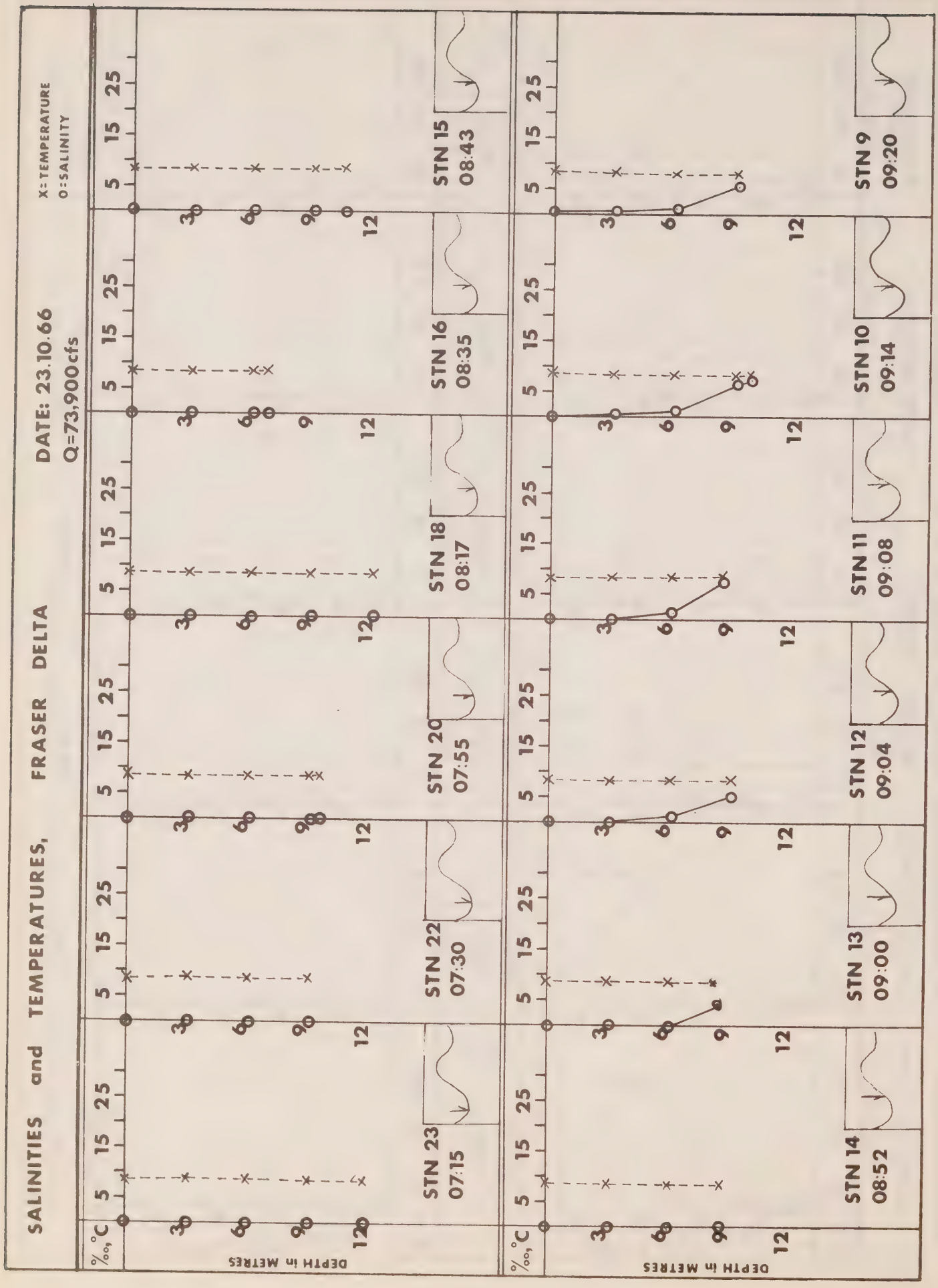

SALINITIES and TEMPERATURES, FRASER DELTA
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O=SALINITY
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DEPTH in METRES
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6
9
12
STN 24
07:35
STN 23
08:11
STN 22
08:28
STN 20
09:02
STN 17
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STN 8
10:45

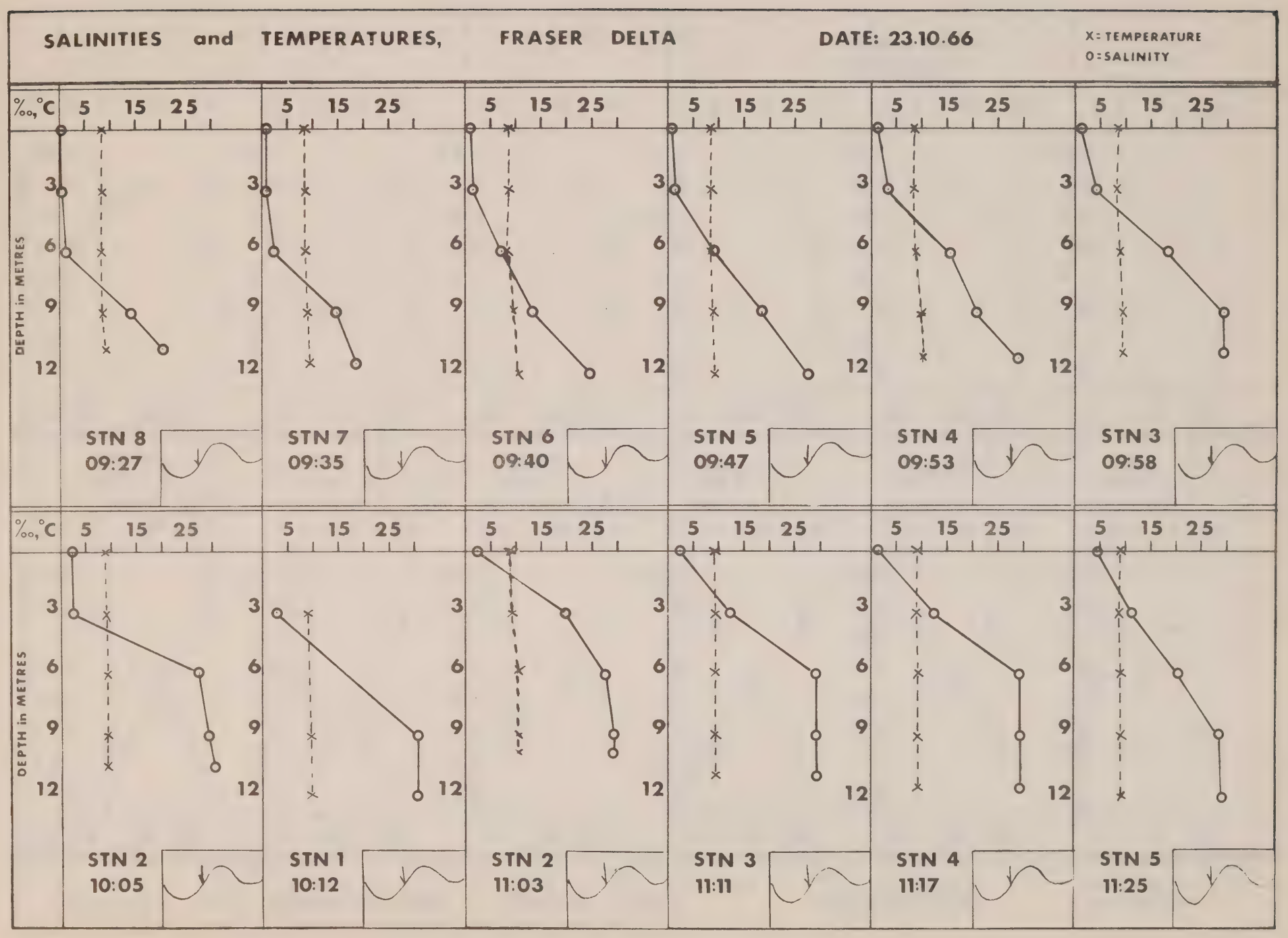

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 18.09.66
X = TEMPERATURE
O = SALINITY
‰, °C
5 15 25
DEPTH in METRES
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6
9
12
STN 7
10:52
STN 6
11:00
STN 5
11:08
STN 4
11:14
STN 3
11:21
STN 2
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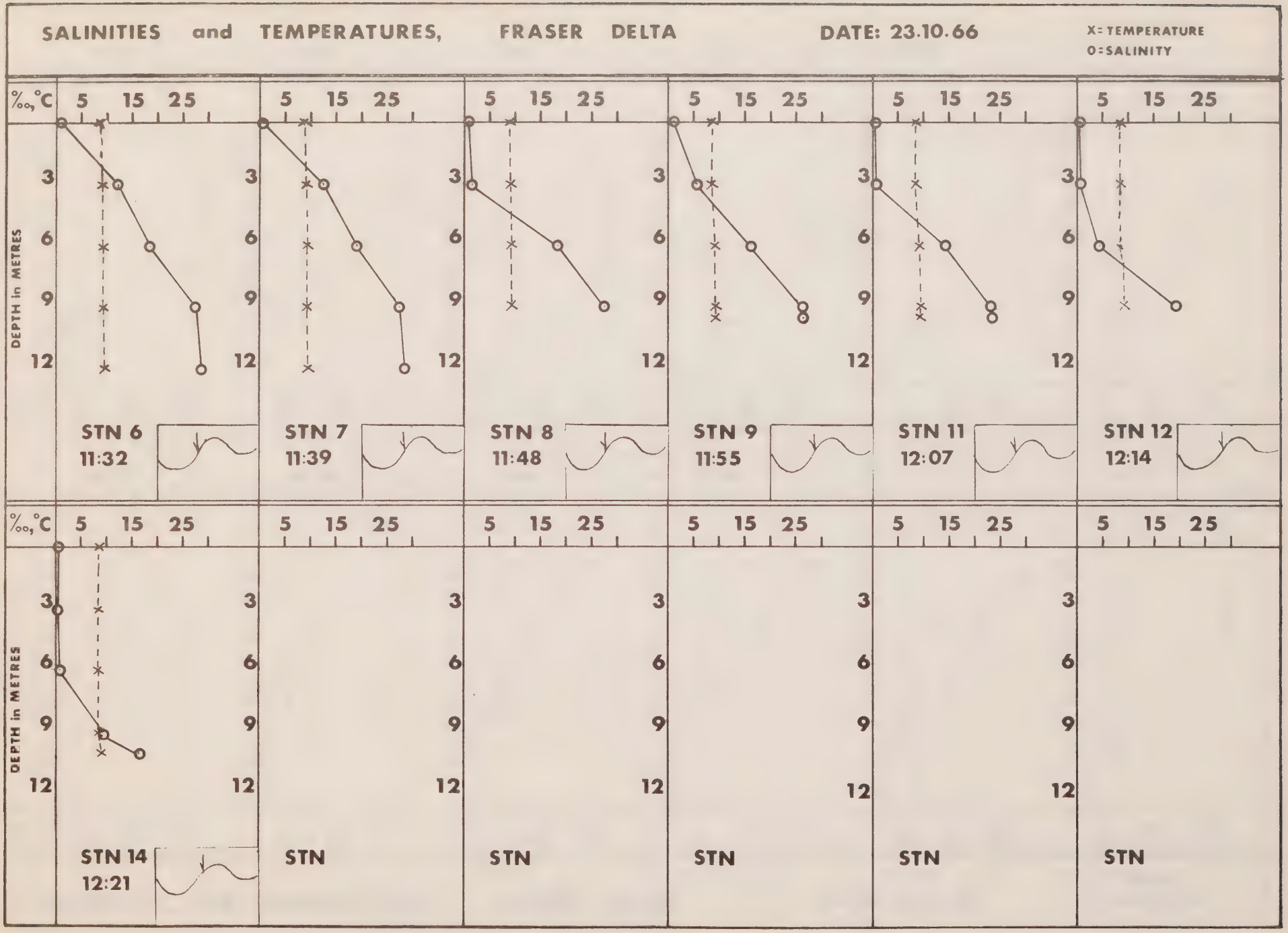

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 18.09.66
X = TEMPERATURE
O = SALINITY
‰, °C
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DEPTH in METRES
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6
9
12
STN 6
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STN 4
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STN 3
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STN 2
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STN 1
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STN

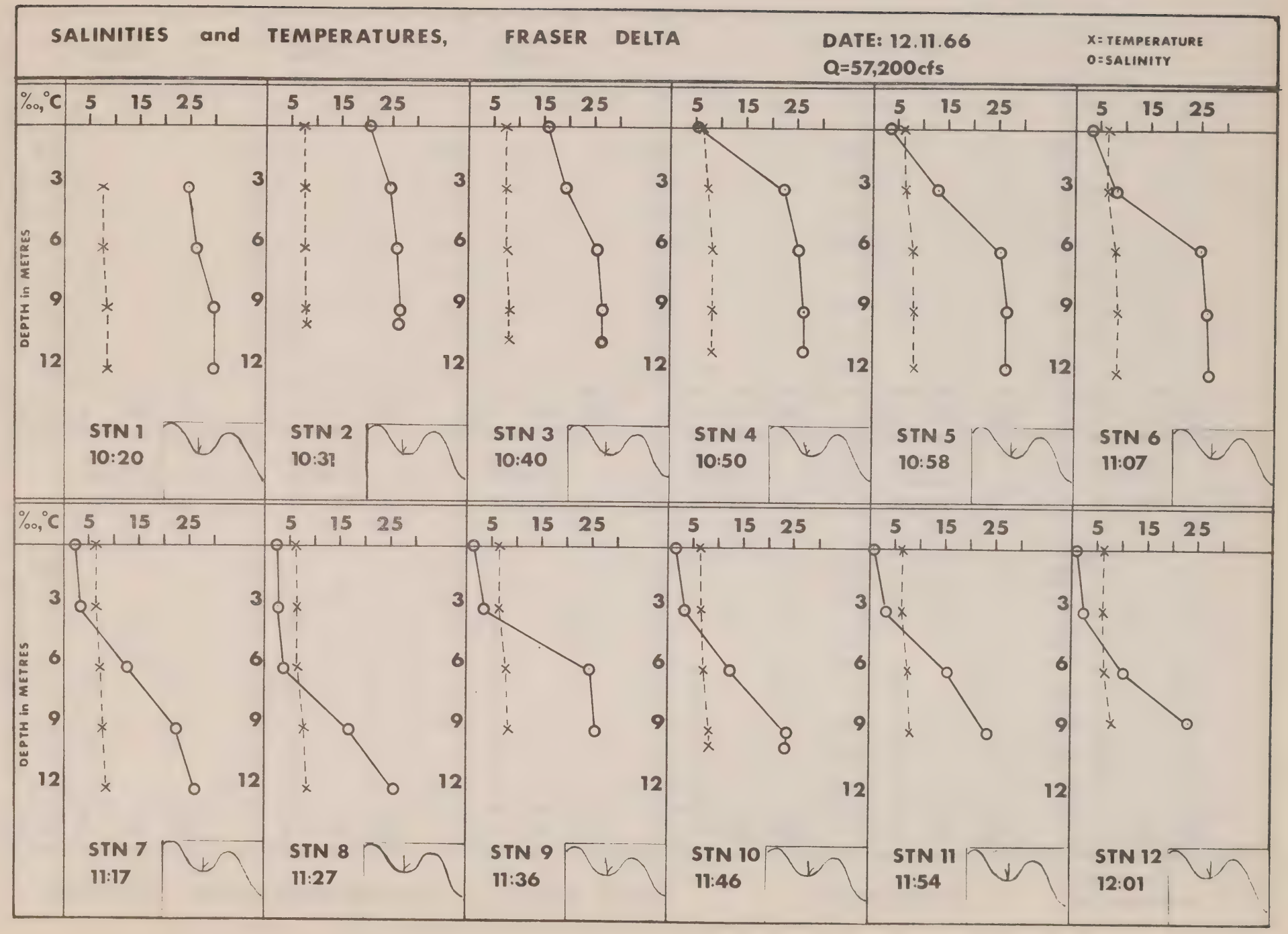

SALINITIES and TEMPERATURES, FRASER DELTA
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O=SALINITY
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DEPTH in METRES
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6
9
12
STN 1
09:43
STN 2
10:30
STN 3
10:40
STN 4
11:04
STN 5
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STN 12
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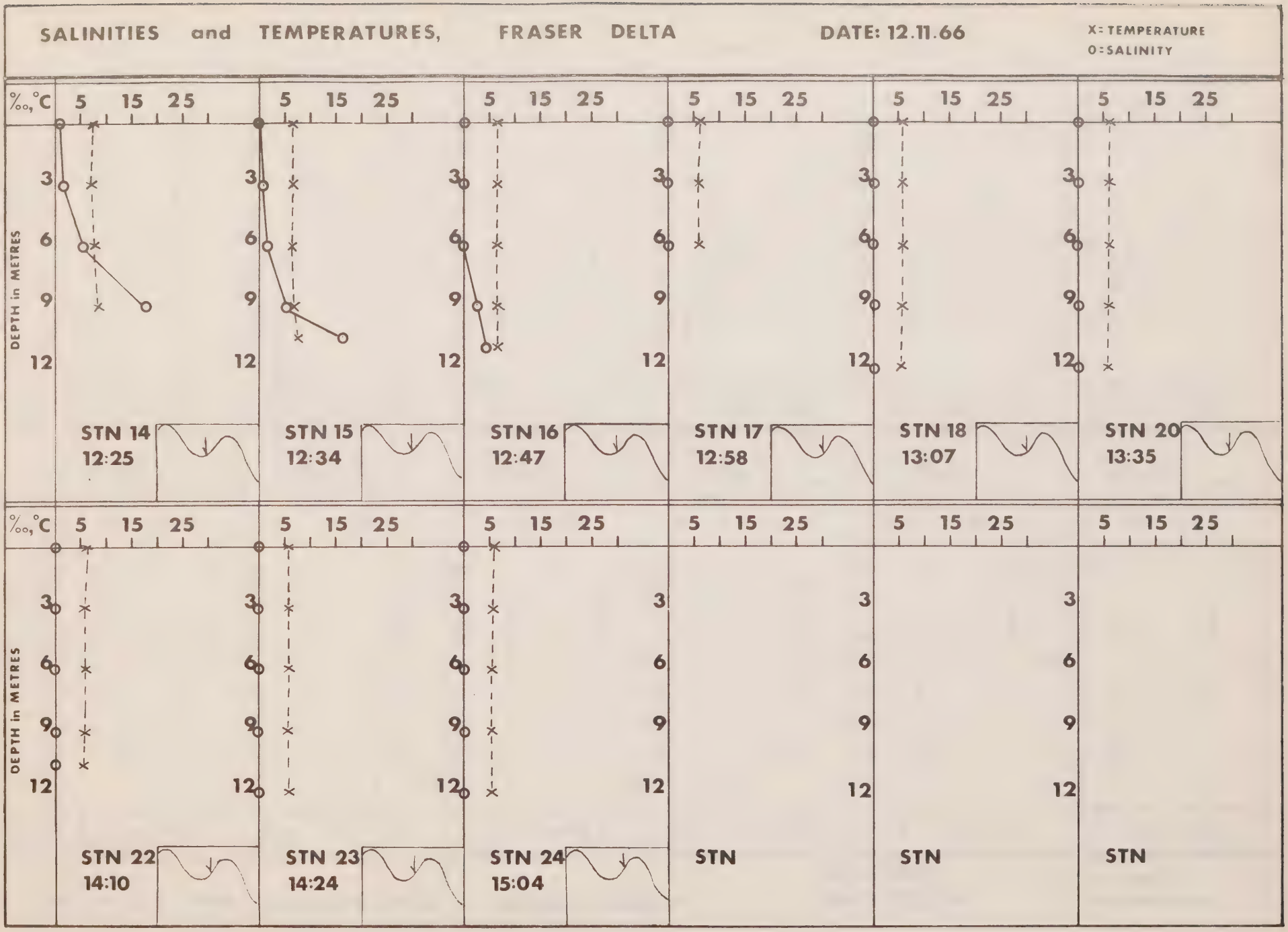

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 22.10.66
X= TEMPERATURE
O=SALINITY
‰, °C
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DEPTH in METRES
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6
9
12
STN 13
12:08
STN 14
12:17
STN 15
12:28
STN 16
12:40
STN 17
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STN 18
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13:19
STN 22
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STN 24
14:25
STN
STN

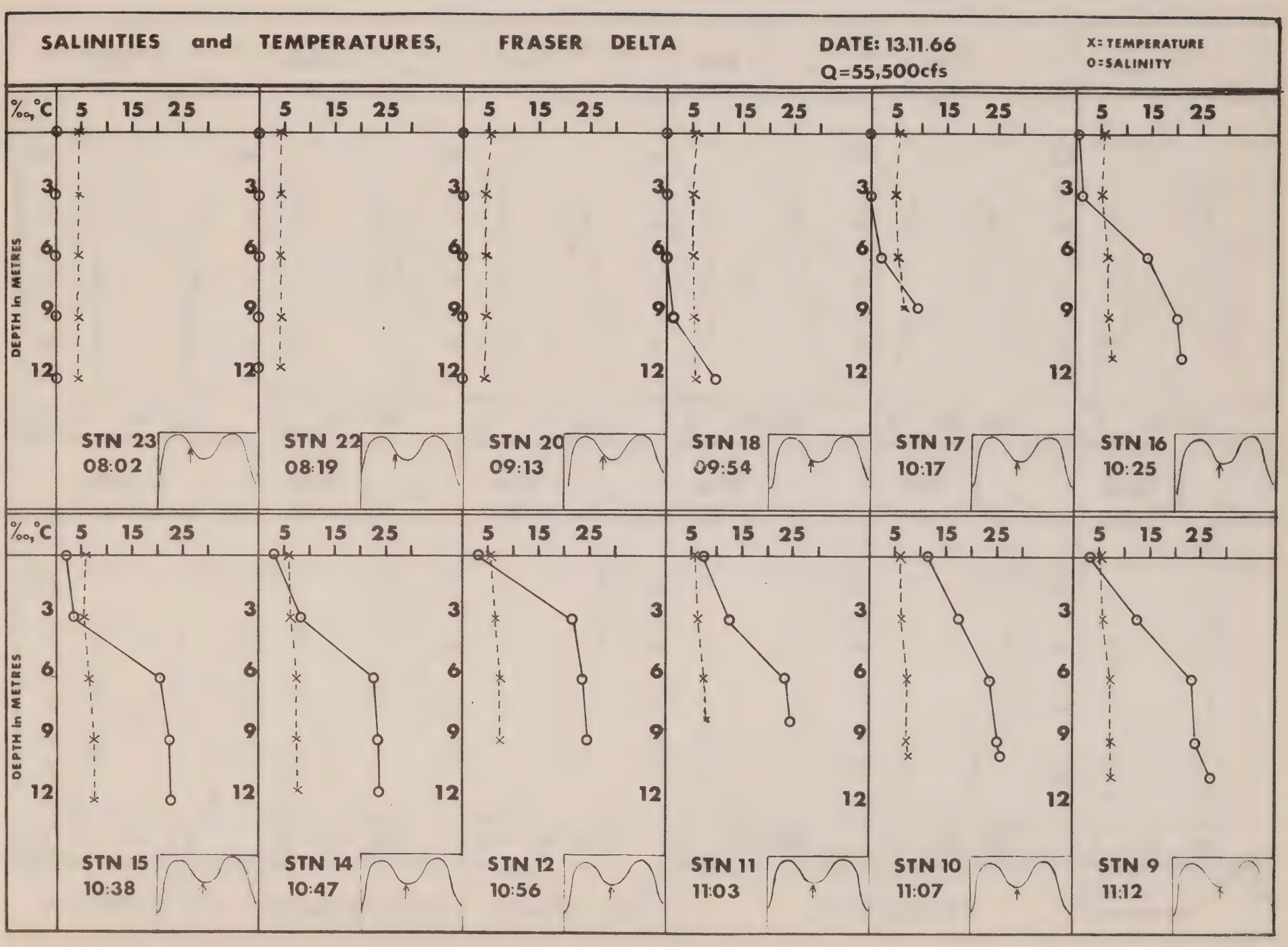

SALINITIES and TEMPERATURES, FRASER DELTA
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O: SALINITY
‰, °C
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3 6 9 12
DEPTH in METRES
STN 23 07:15
STN 22 07:30
STN 20 07:55
STN 18 08:17
STN 16 08:35
STN 15 08:43
STN 14 08:52
STN 13 09:00
STN 12 09:04
STN 11 09:08
STN 10 09:14
STN 9 09:20

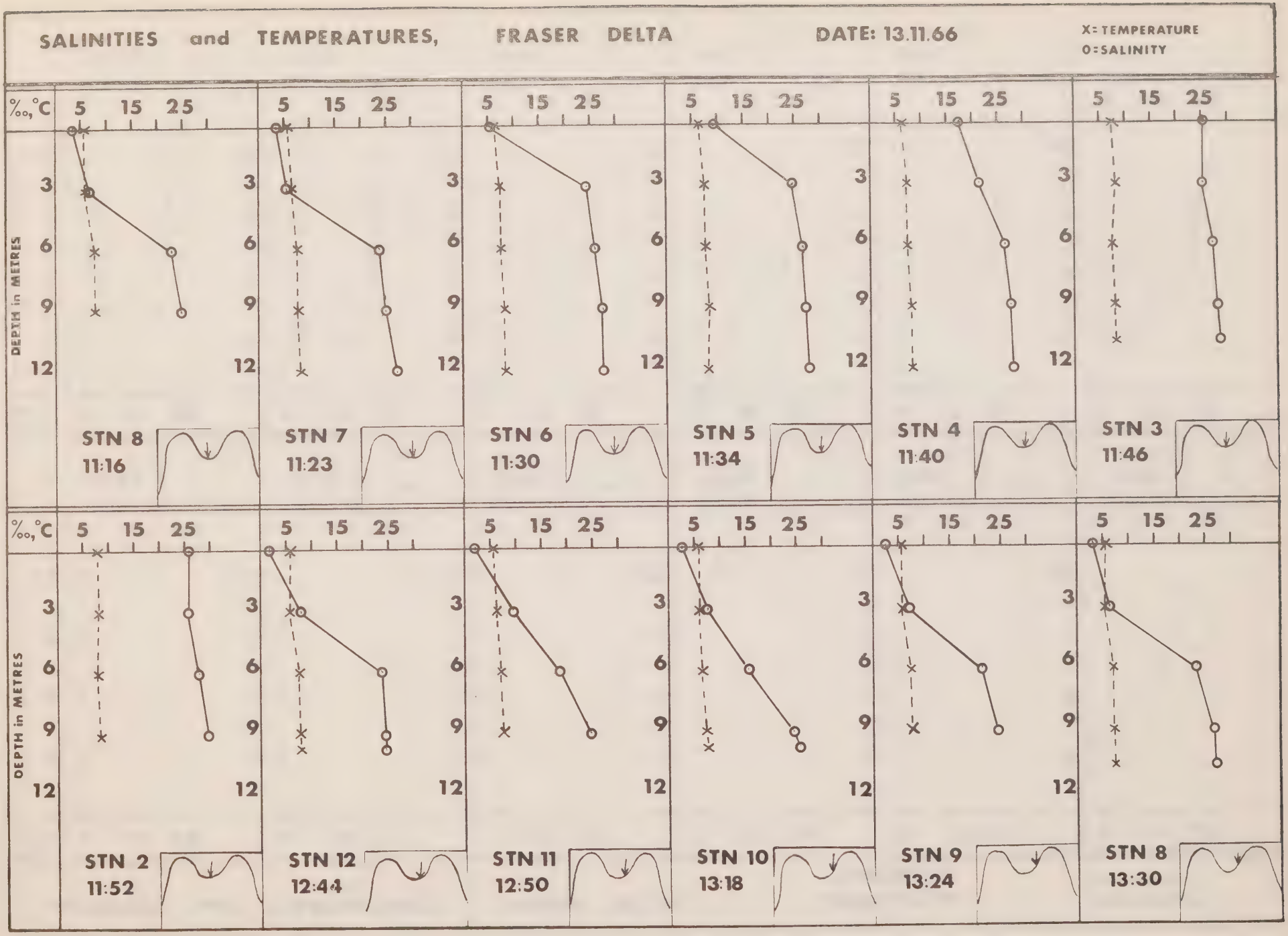

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 23.10.66
X = TEMPERATURE
O = SALINITY
‰, °C
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DEPTH in METRES
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6
9
12
STN 8
09:27
STN 7
09:35
STN 6
09:40
STN 5
09:47
STN 4
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09:58
STN 2
10:05
STN 1
10:12
STN 2
11:03
STN 3
11:11
STN 4
11:17
STN 5
11:25

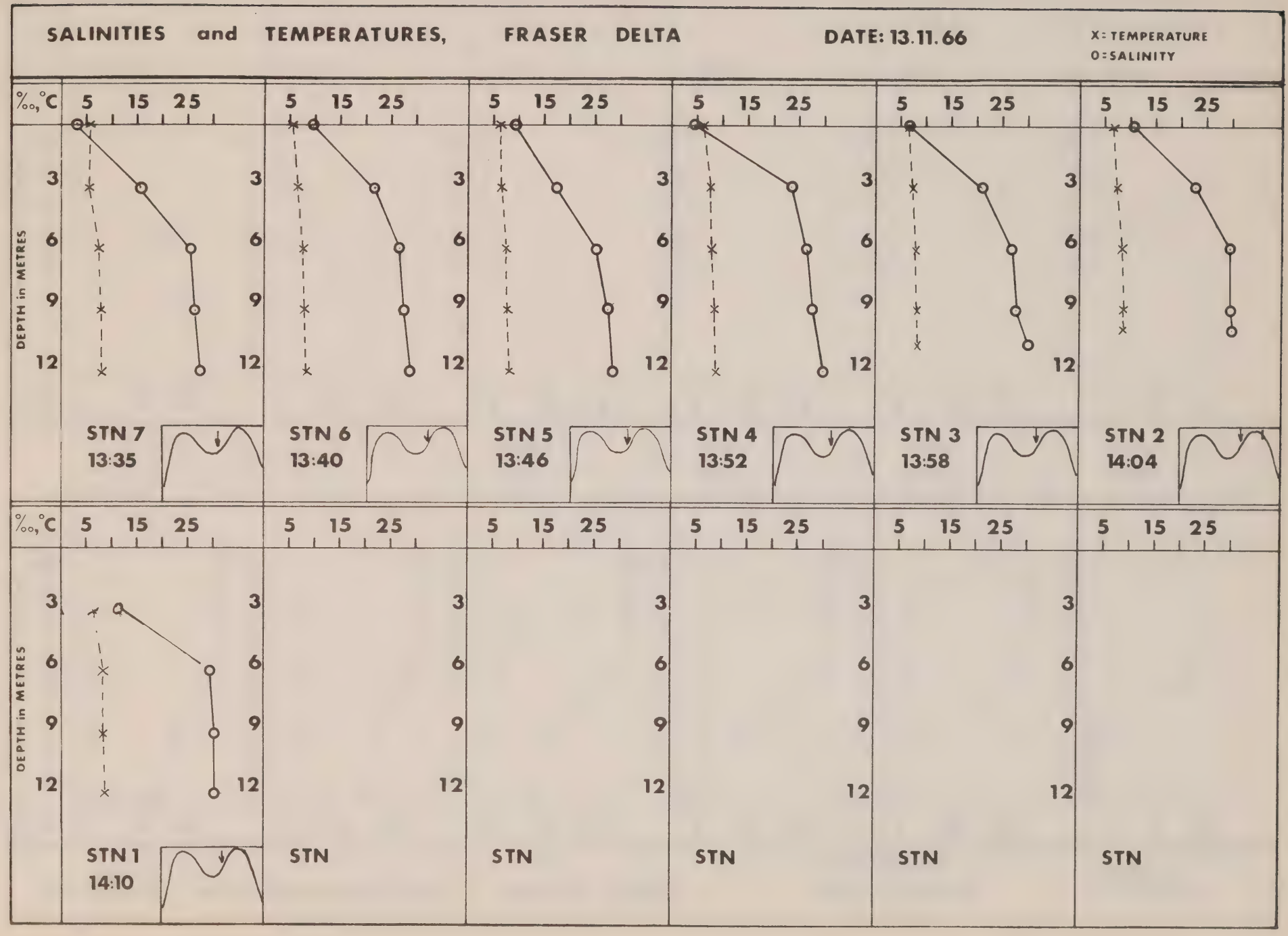

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 23.10.66
X = TEMPERATURE
O = SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 6
11:32
STN 7
11:39
STN 8
11:48
STN 9
11:55
STN 11
12:07
STN 12
12:14
STN 14
12:21
STN
STN
STN
STN
STN

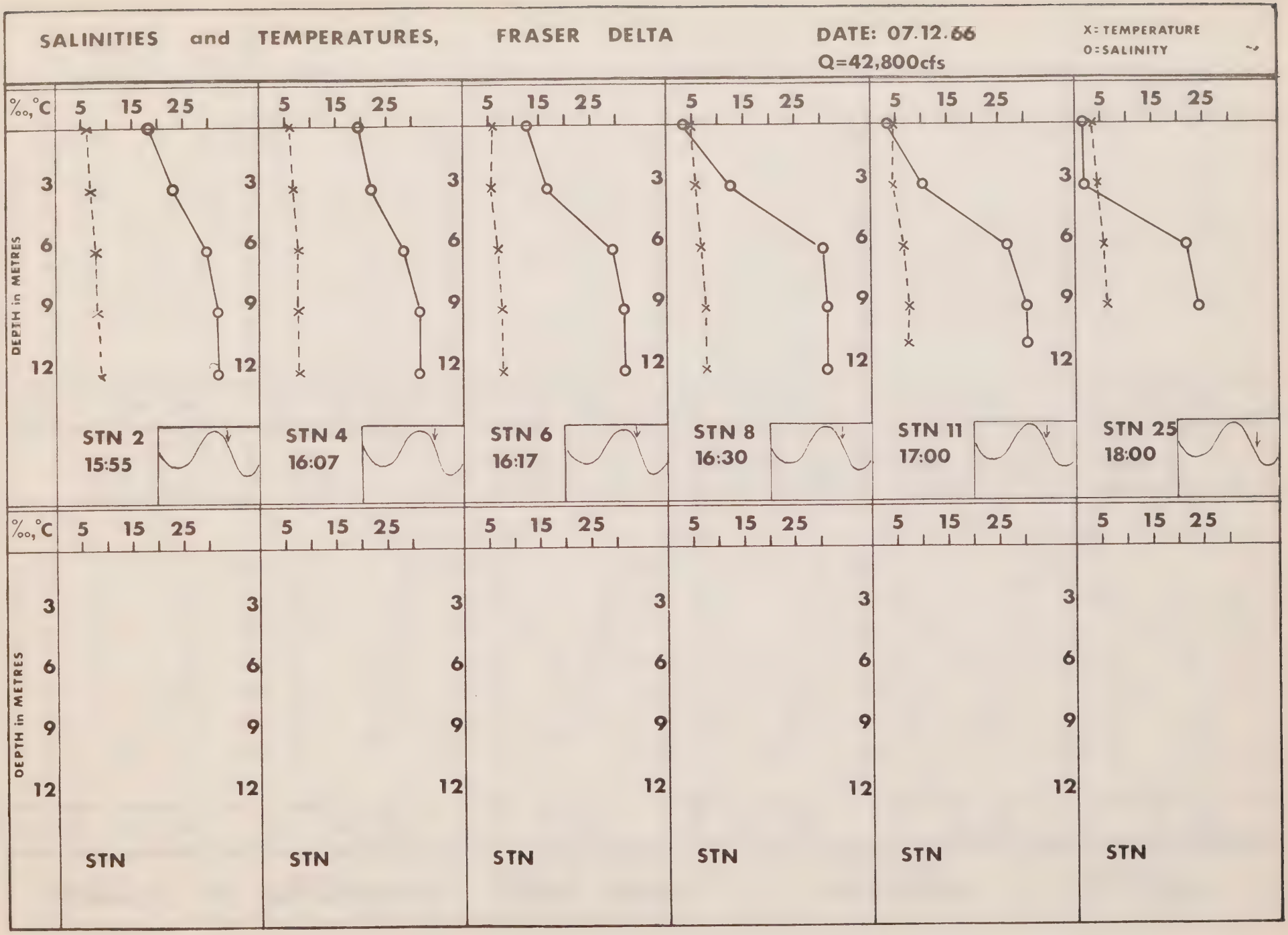

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 12.11.66
Q=57,200cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 1
10:20
STN 2
10:31
STN 3
10:40
STN 4
10:50
STN 5
10:58
STN 6
11:07
STN 7
11:17
STN 8
11:27
STN 9
11:36
STN 10
11:46
STN 11
11:54
STN 12
12:01

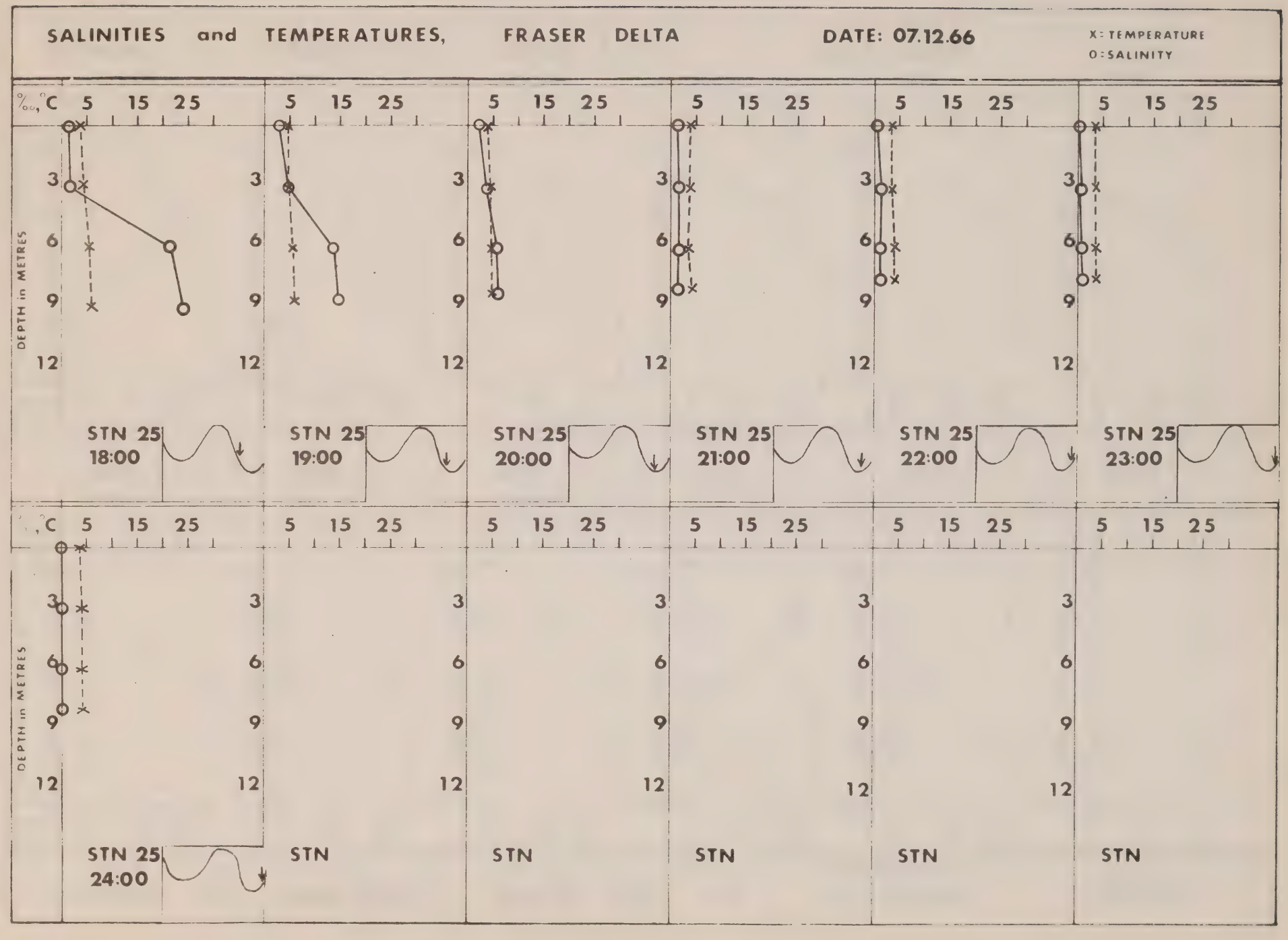

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 12.11.66
X = TEMPERATURE
O = SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 14
12:25
STN 15
12:34
STN 16
12:47
STN 17
12:58
STN 18
13:07
STN 20
13:35
STN 22
14:10
STN 23
14:24
STN 24
15:04
STN
STN
STN

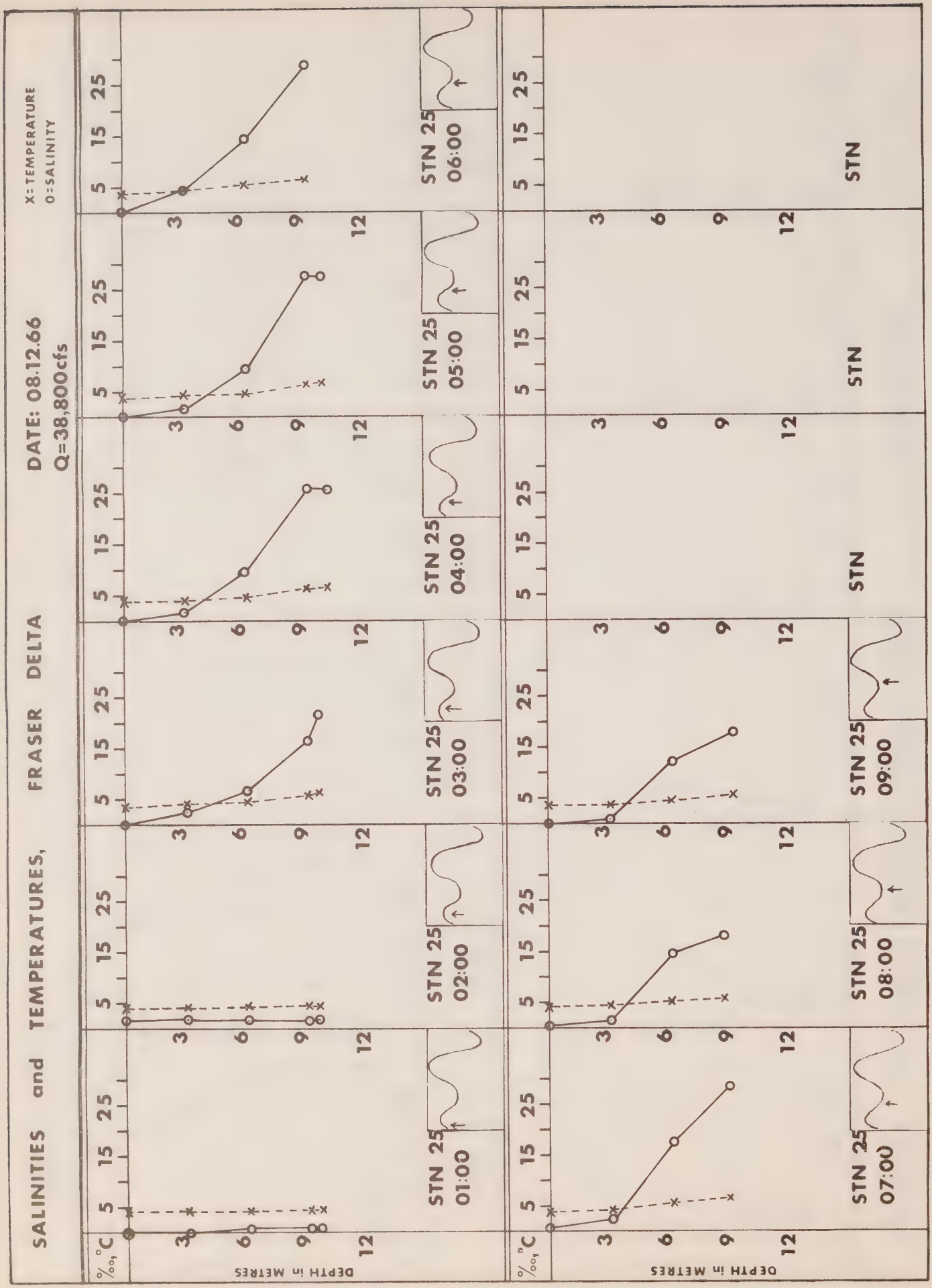

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 13.11.66
Q=55,500cfs
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 23
08:02
STN 22
08:19
STN 20
09:13
STN 18
09:54
STN 17
10:17
STN 16
10:25
STN 15
10:38
STN 14
10:47
STN 12
10:56
STN 11
11:03
STN 10
11:07
STN 9
11:12

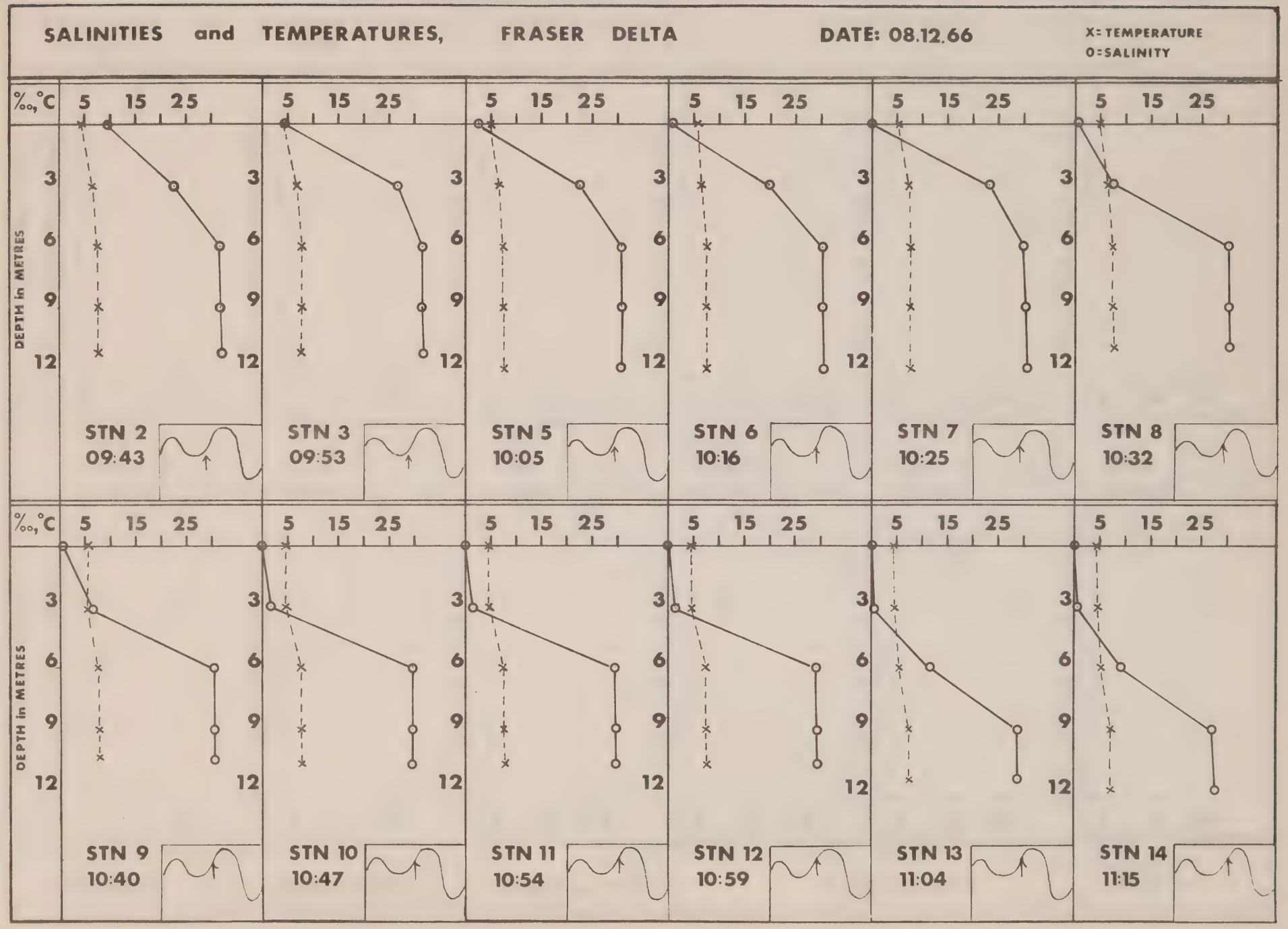

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 13.11.66
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 8
11:16
STN 7
11:23
STN 6
11:30
STN 5
11:34
STN 4
11:40
STN 3
11:46
STN 2
11:52
STN 12
12:44
STN 11
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13:24
STN 8
13:30

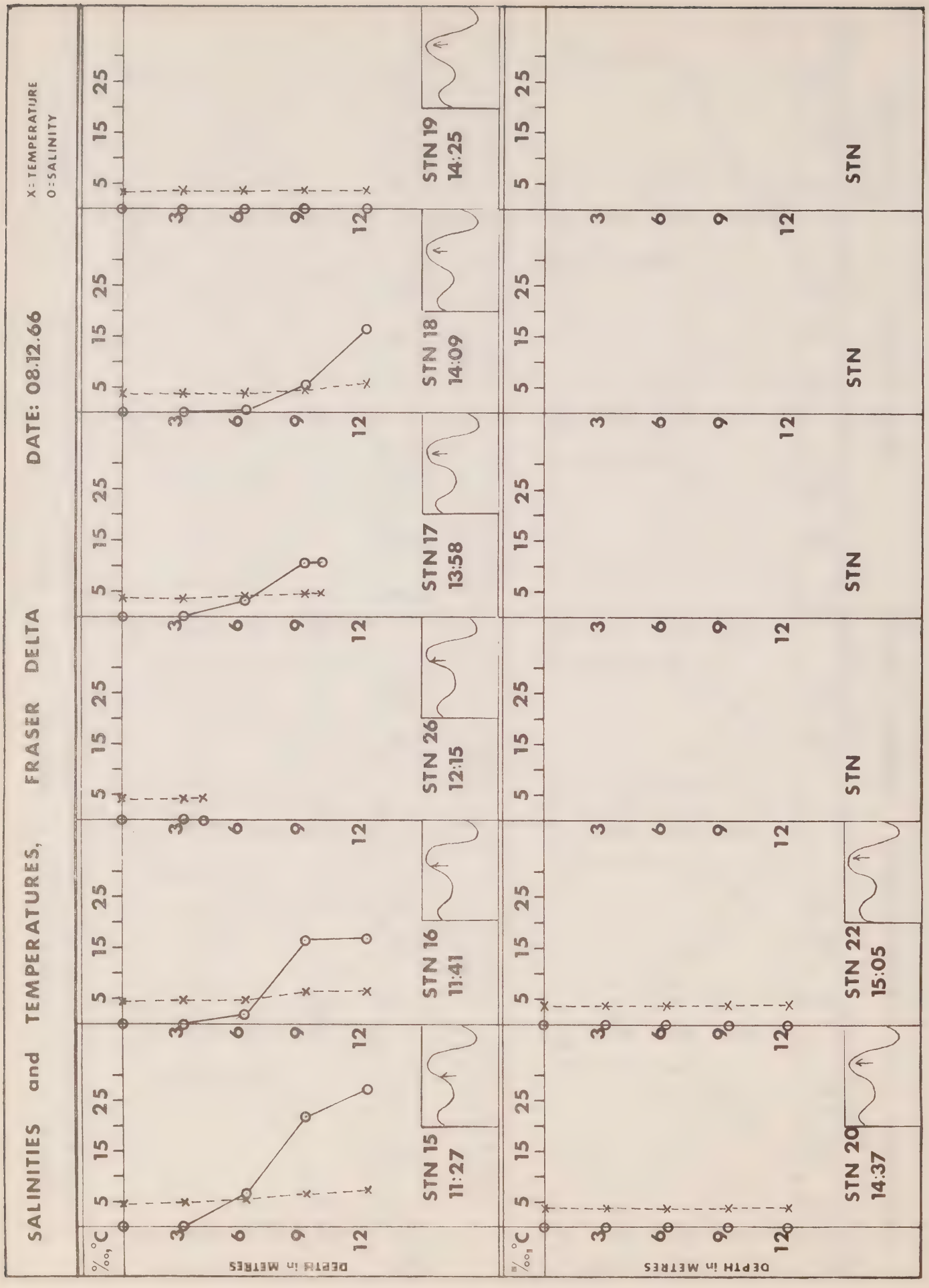

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 13.11.66
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 7
13:35
STN 6
13:40
STN 5
13:46
STN 4
13:52
STN 3
13:58
STN 2
14:04
STN 1
14:10
STN
STN
STN
STN
STN

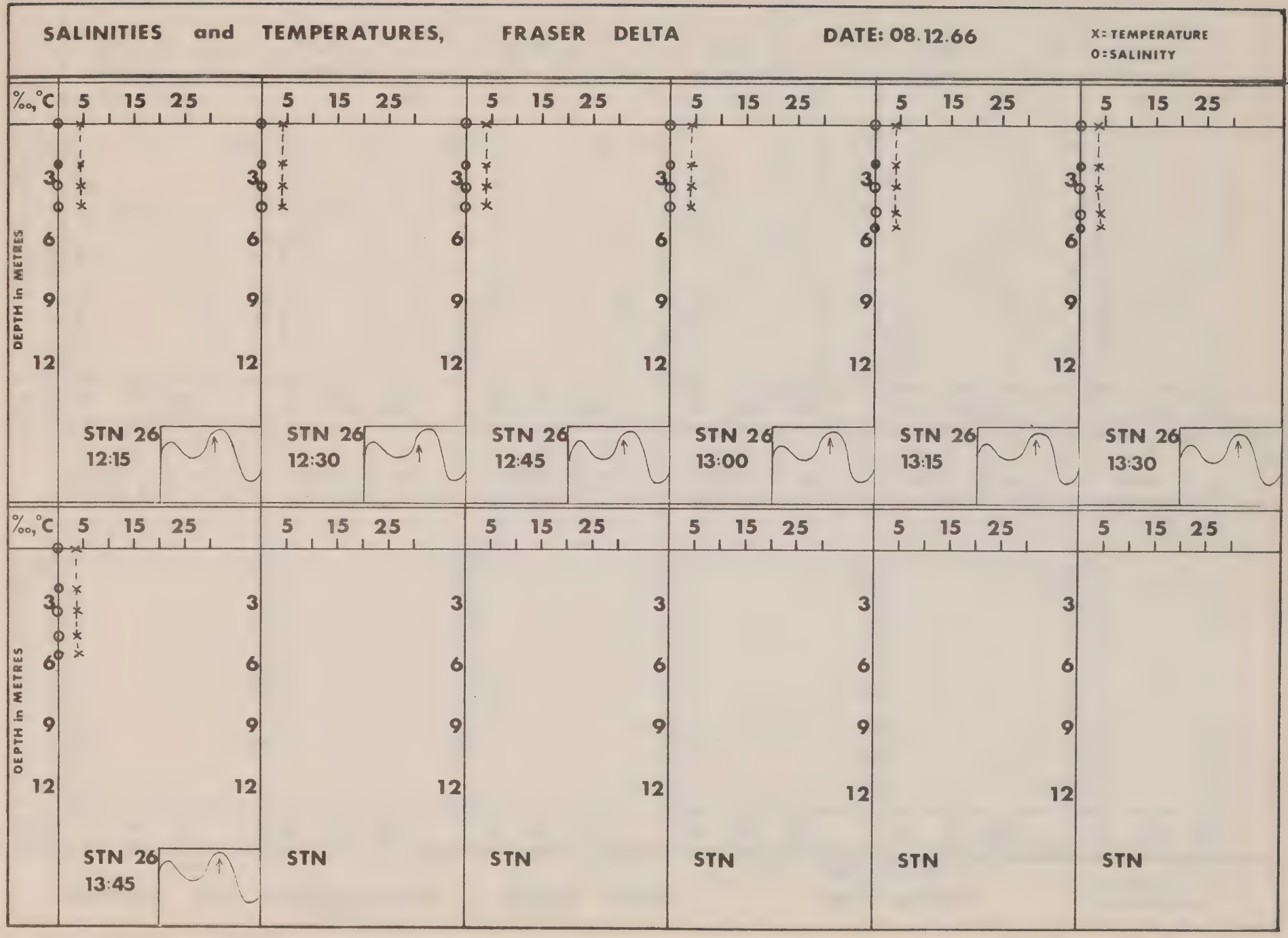

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 07.12.66
Q=42,800cfs
X: TEMPERATURE
O: SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 2
15:55
STN 4
16:07
STN 6
16:17
STN 8
16:30
STN 11
17:00
STN 25
18:00
STN

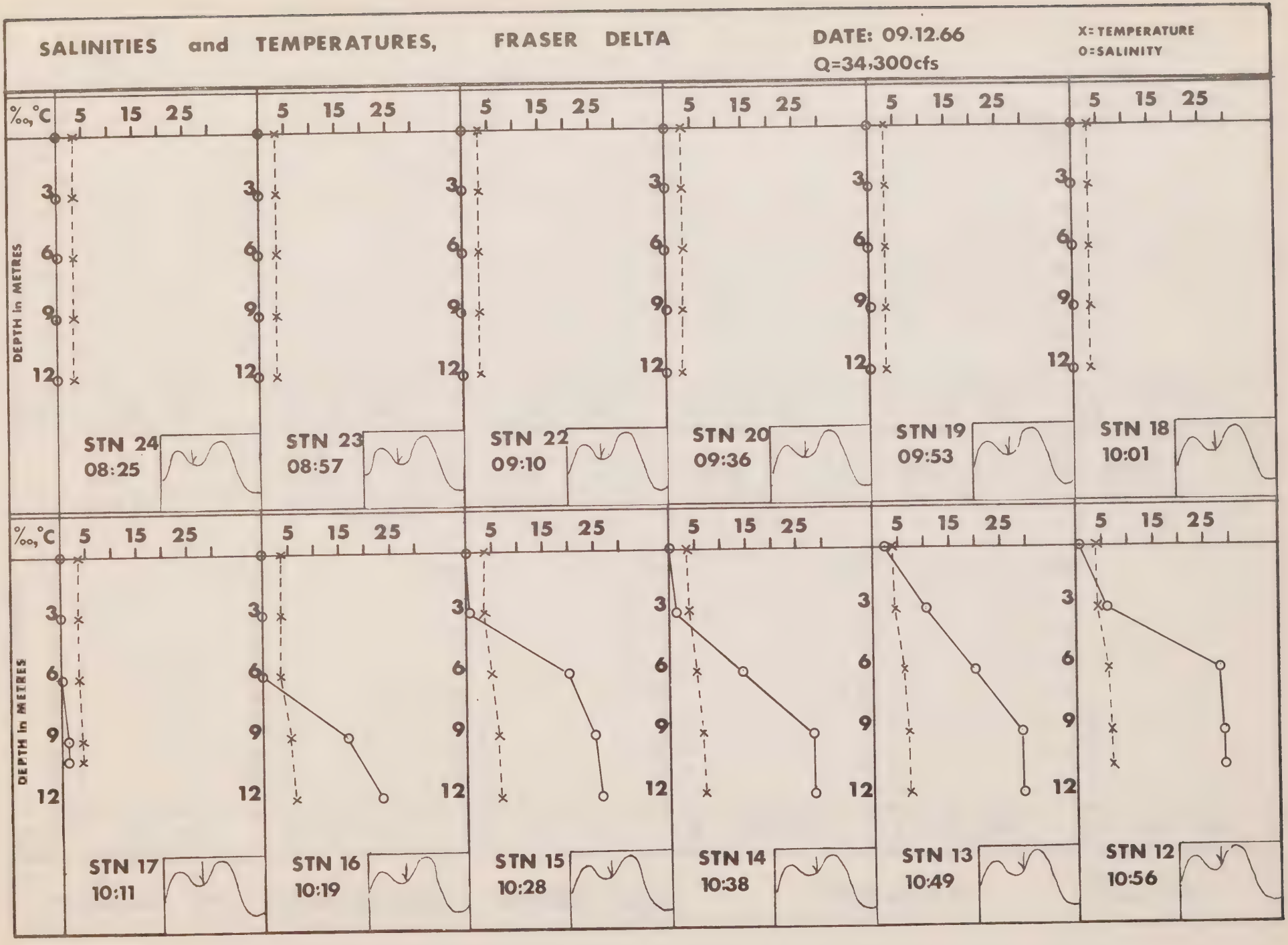

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 07.12.66
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 25
18:00
STN 25
19:00
STN 25
20:00
STN 25
21:00
STN 25
22:00
STN 25
23:00
STN 25
24:00
STN
STN
STN
STN
STN

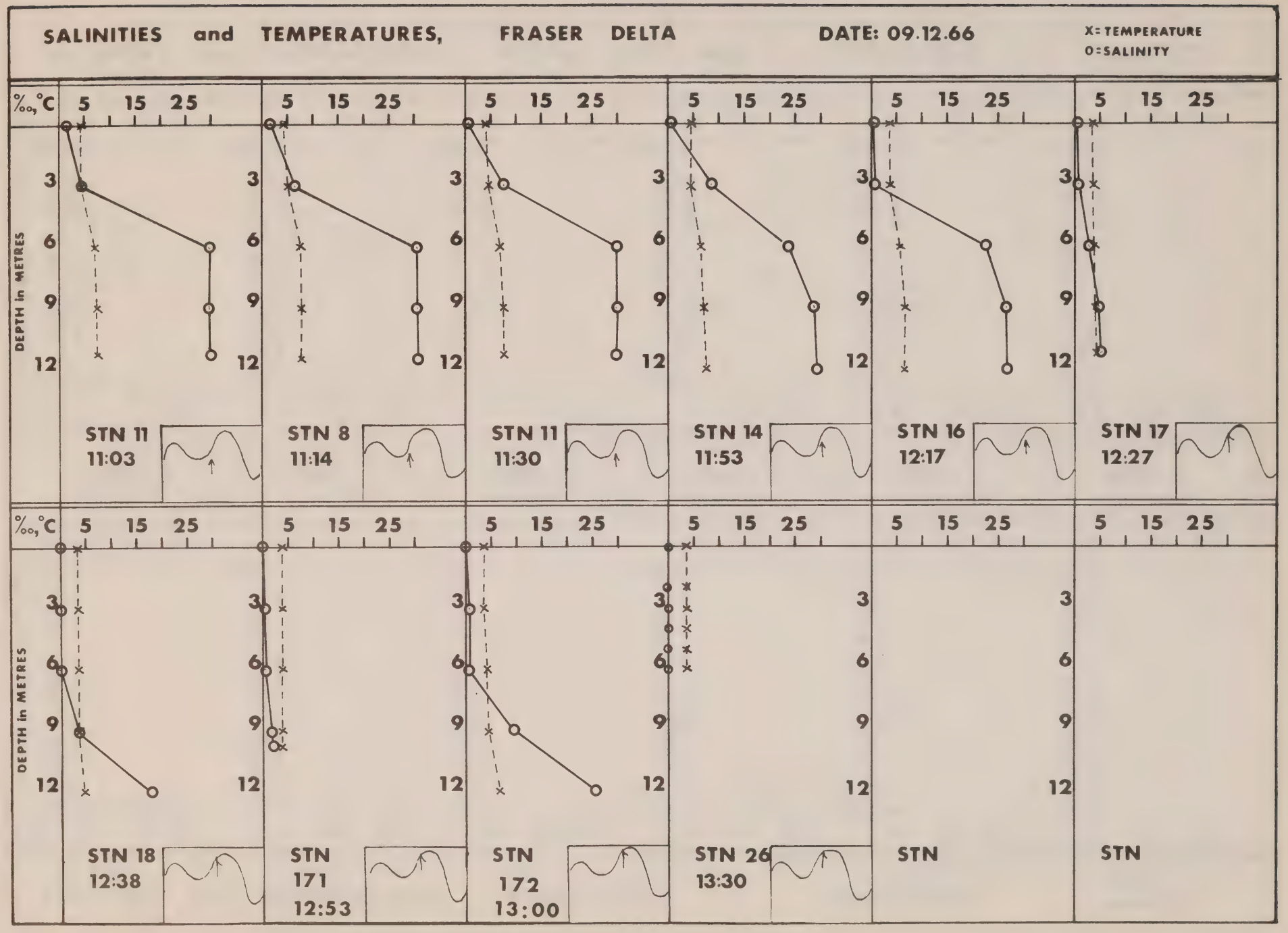

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 08.12.66
Q=38,800cfs
X: TEMPERATURE
O: SALINITY
‰ °C
DEPTH in METRES
STN 25 01:00
STN 25 02:00
STN 25 03:00
STN 25 04:00
STN 25 05:00
STN 25 06:00
STN 25 07:00
STN 25 08:00
STN 25 09:00
STN
STN
STN

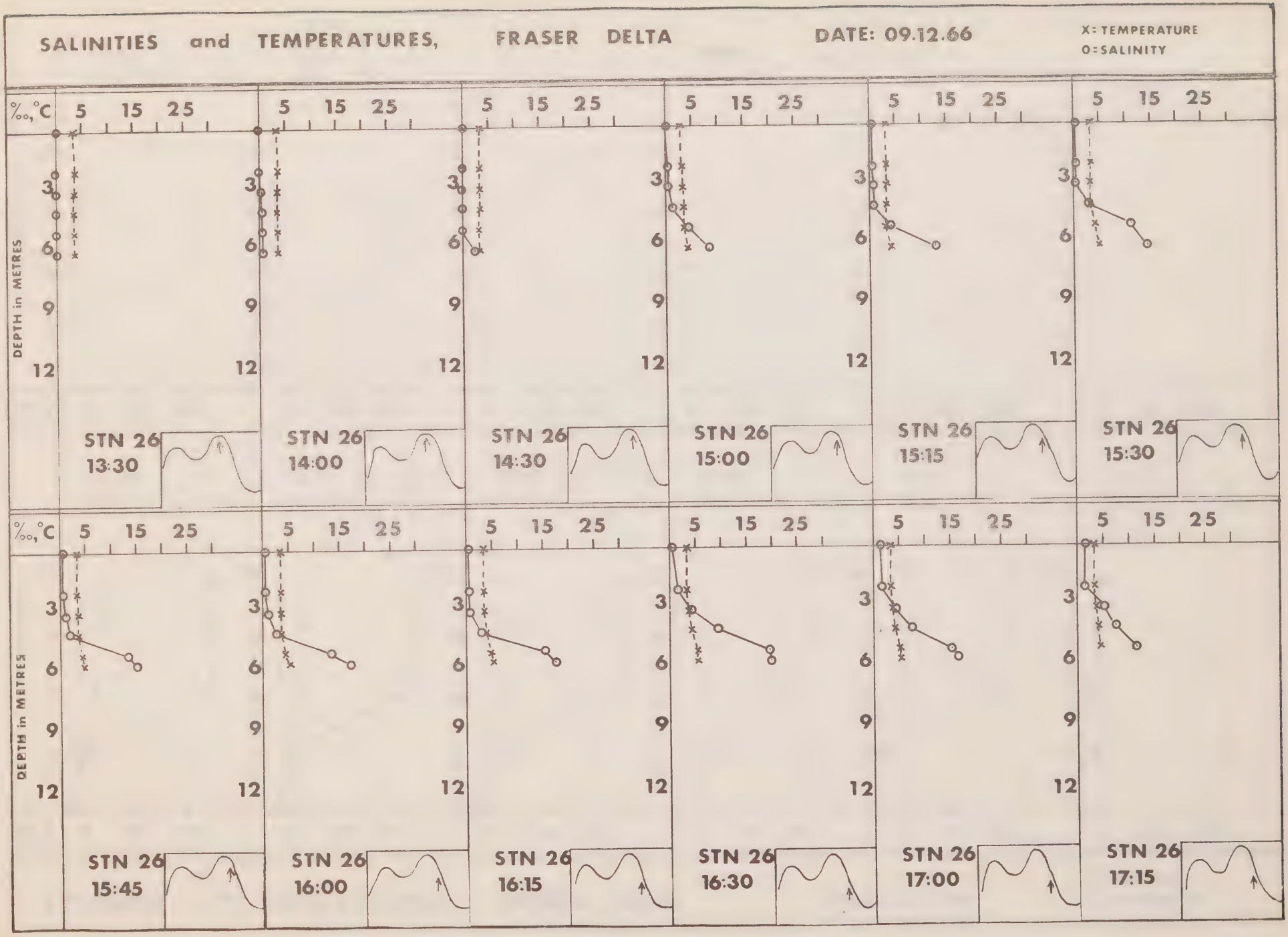

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 08.12.66
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 2
09:43
STN 3
09:53
STN 5
10:05
STN 6
10:16
STN 7
10:25
STN 8
10:32
STN 9
10:40
STN 10
10:47
STN 11
10:54
STN 12
10:59
STN 13
11:04
STN 14
11:15

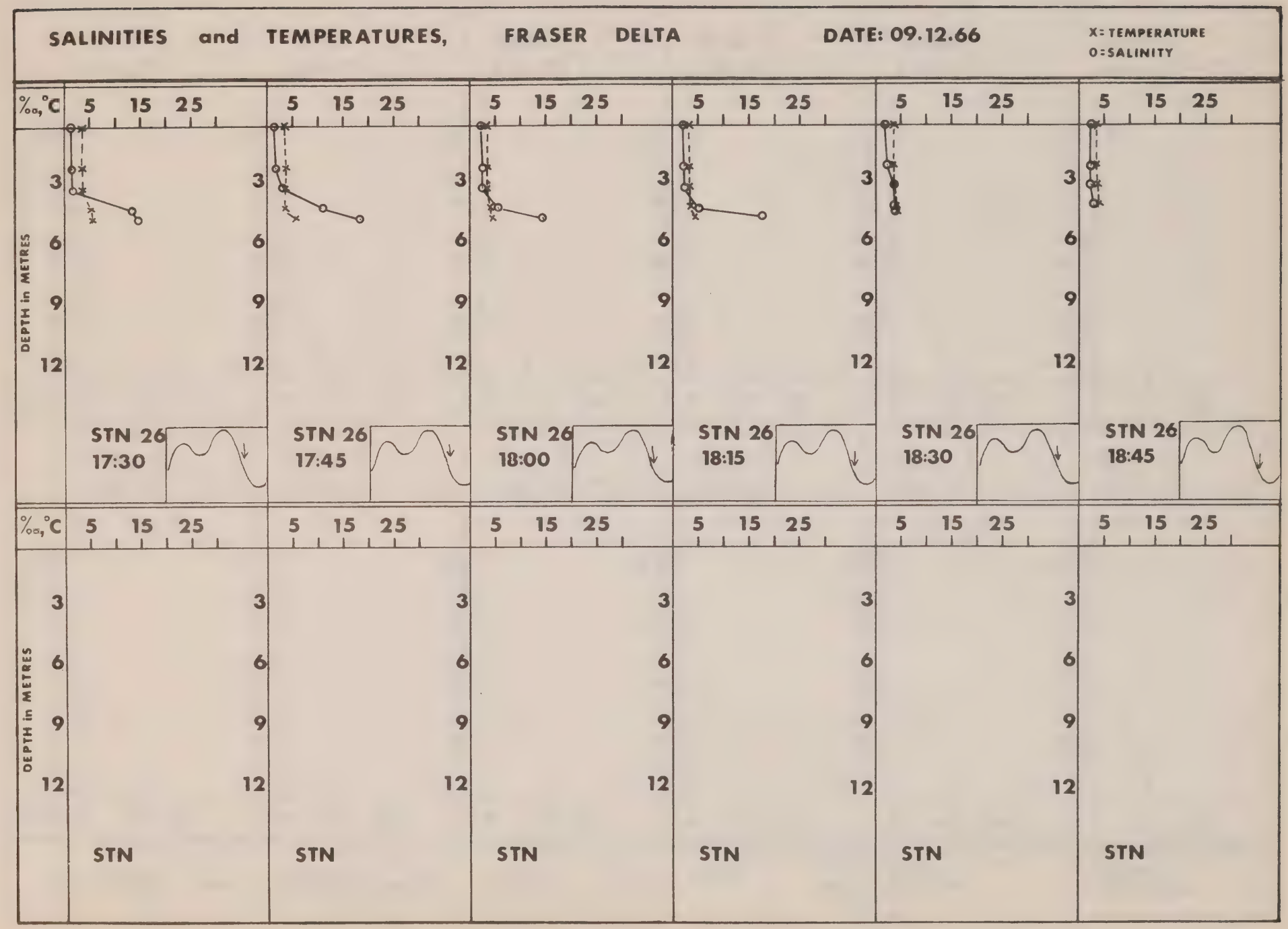

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 08.12.66
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
3 6 9 12
DEPTH in METRES
STN 15 11:27
STN 16 11:41
STN 26 12:15
STN 17 13:58
STN 18 14:09
STN 19 14:25
STN 20 14:37
STN 22 15:05
STN

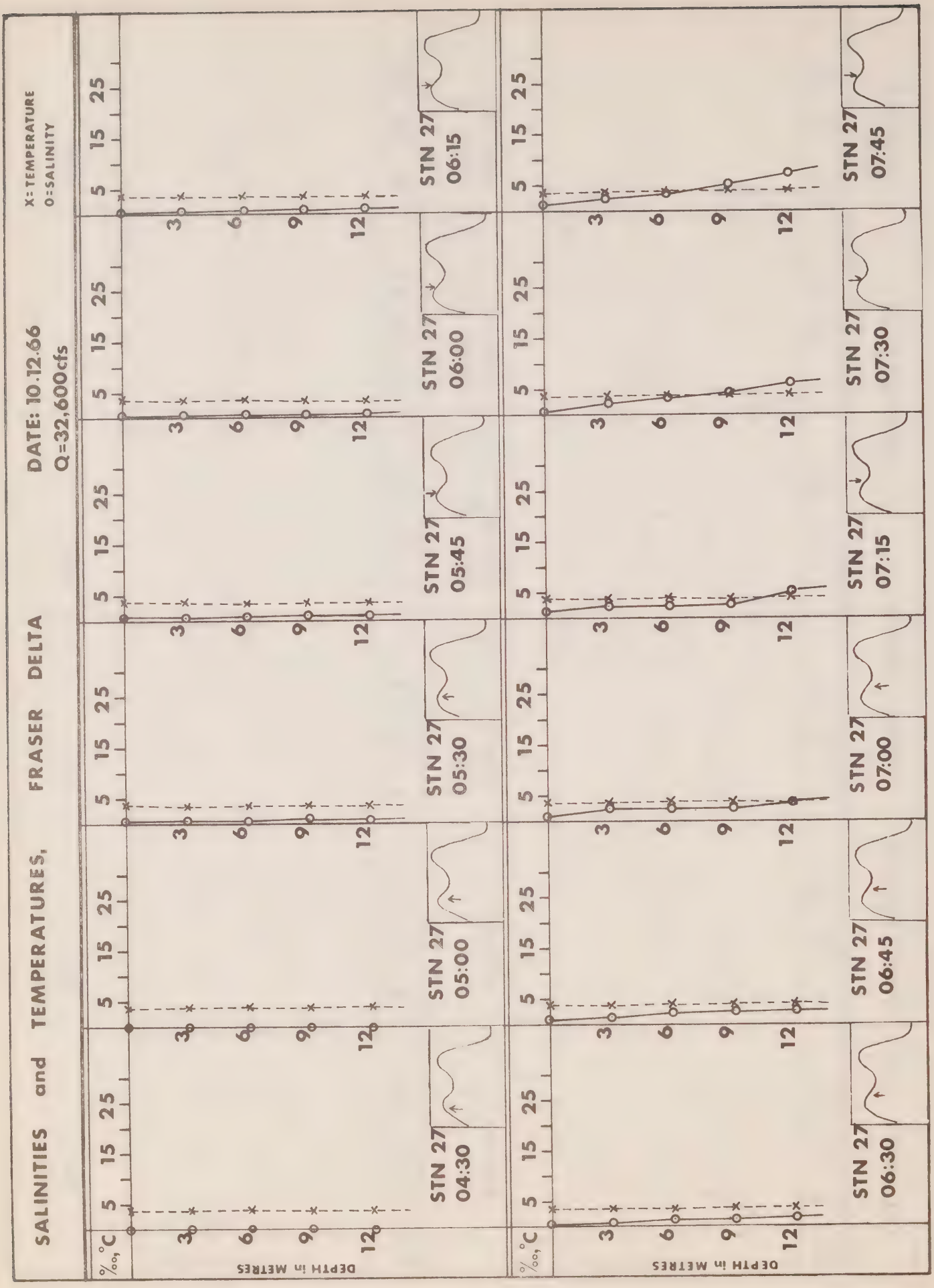

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 08.12.66
X = TEMPERATURE
O = SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 26
12:15
STN 26
12:30
STN 26
12:45
STN 26
13:00
STN 26
13:15
STN 26
13:30
STN 26
13:45
STN
STN
STN
STN
STN

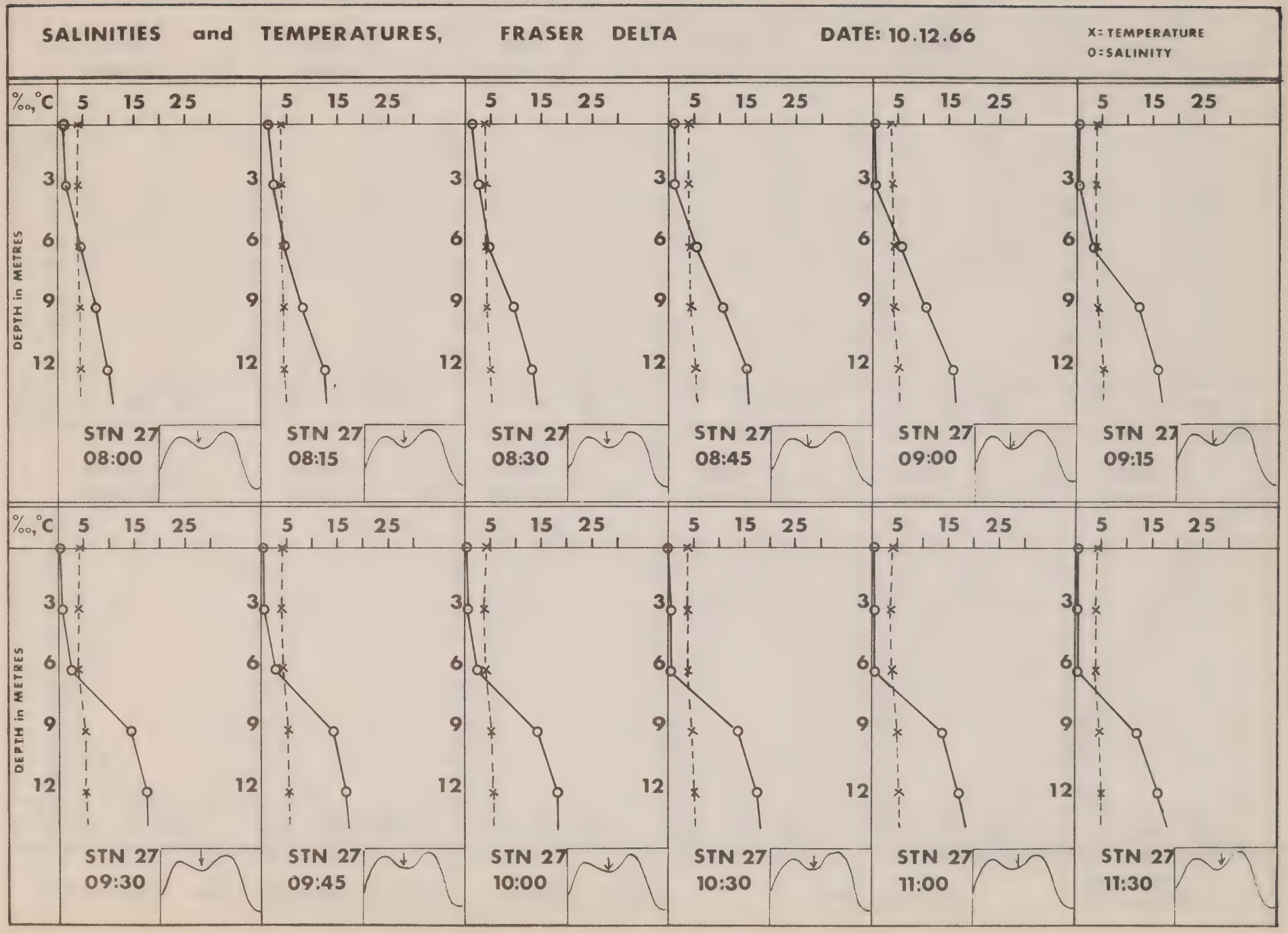

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 09.12.66
Q=34,300cfs
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 24
08:25
STN 23
08:57
STN 22
09:10
STN 20
09:36
STN 19
09:53
STN 18
10:01
STN 17
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10:19
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10:28
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STN 13
10:49
STN 12
10:56

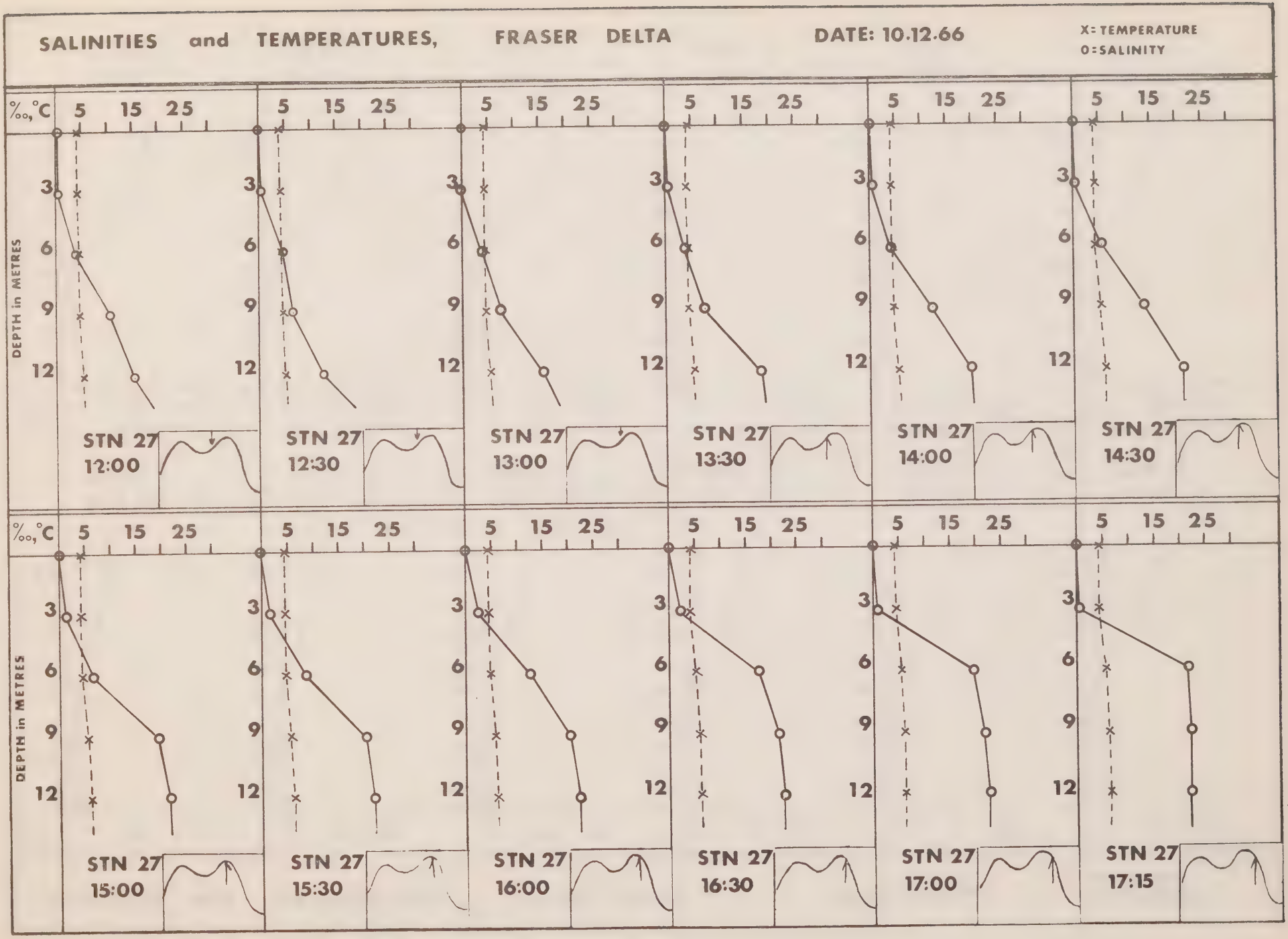

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 09.12.66
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 11
11:03
STN 8
11:14
STN 11
11:30
STN 14
11:53
STN 16
12:17
STN 17
12:27
STN 18
12:38
STN
171
12:53
STN
172
13:00
STN 26
13:30
STN
STN

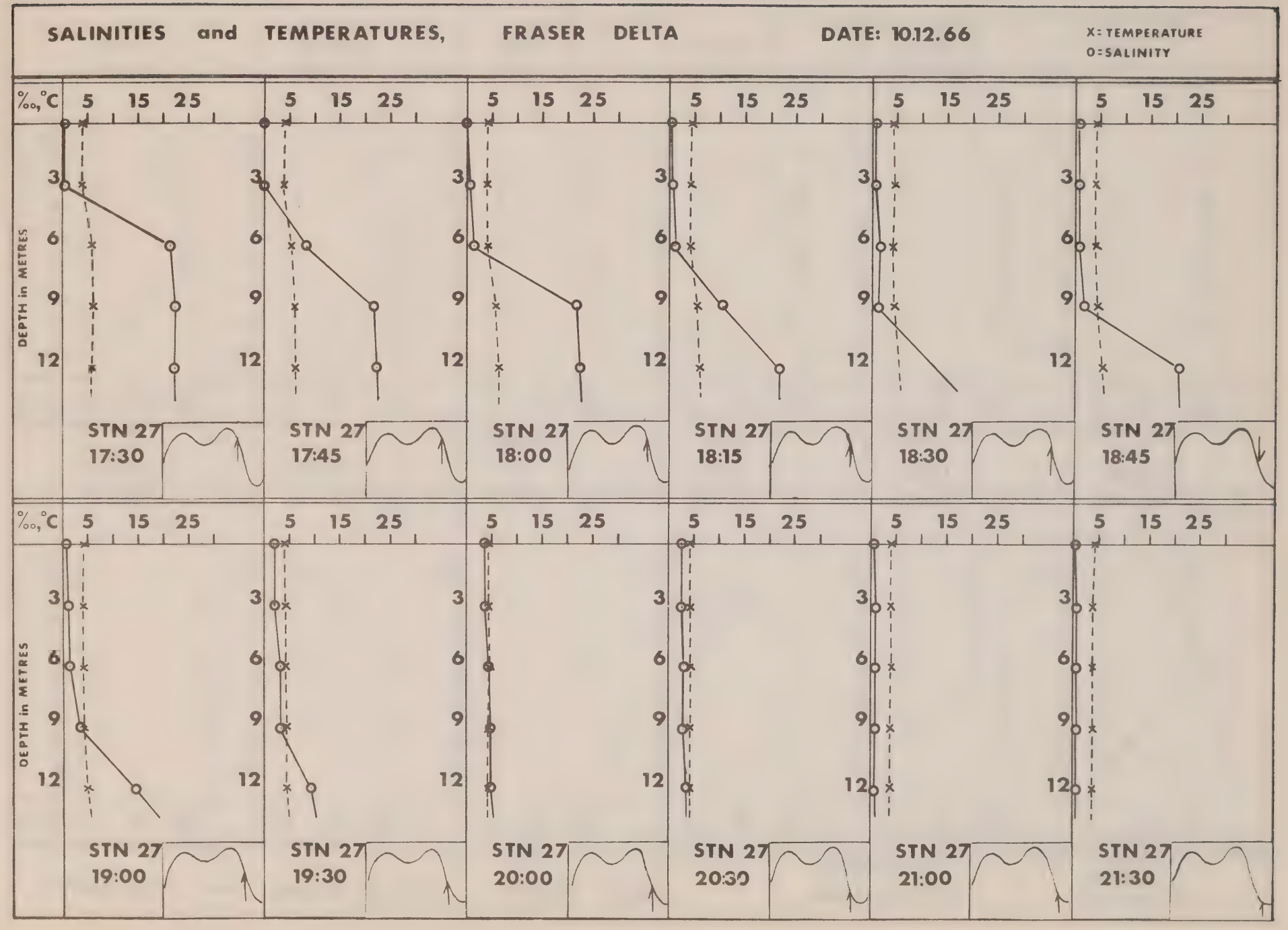

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 09.12.66
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 26 13:30
STN 26 14:00
STN 26 14:30
STN 26 15:00
STN 26 15:15
STN 26 15:30
STN 26 15:45
STN 26 16:00
STN 26 16:15
STN 26 16:30
STN 26 17:00
STN 26 17:15

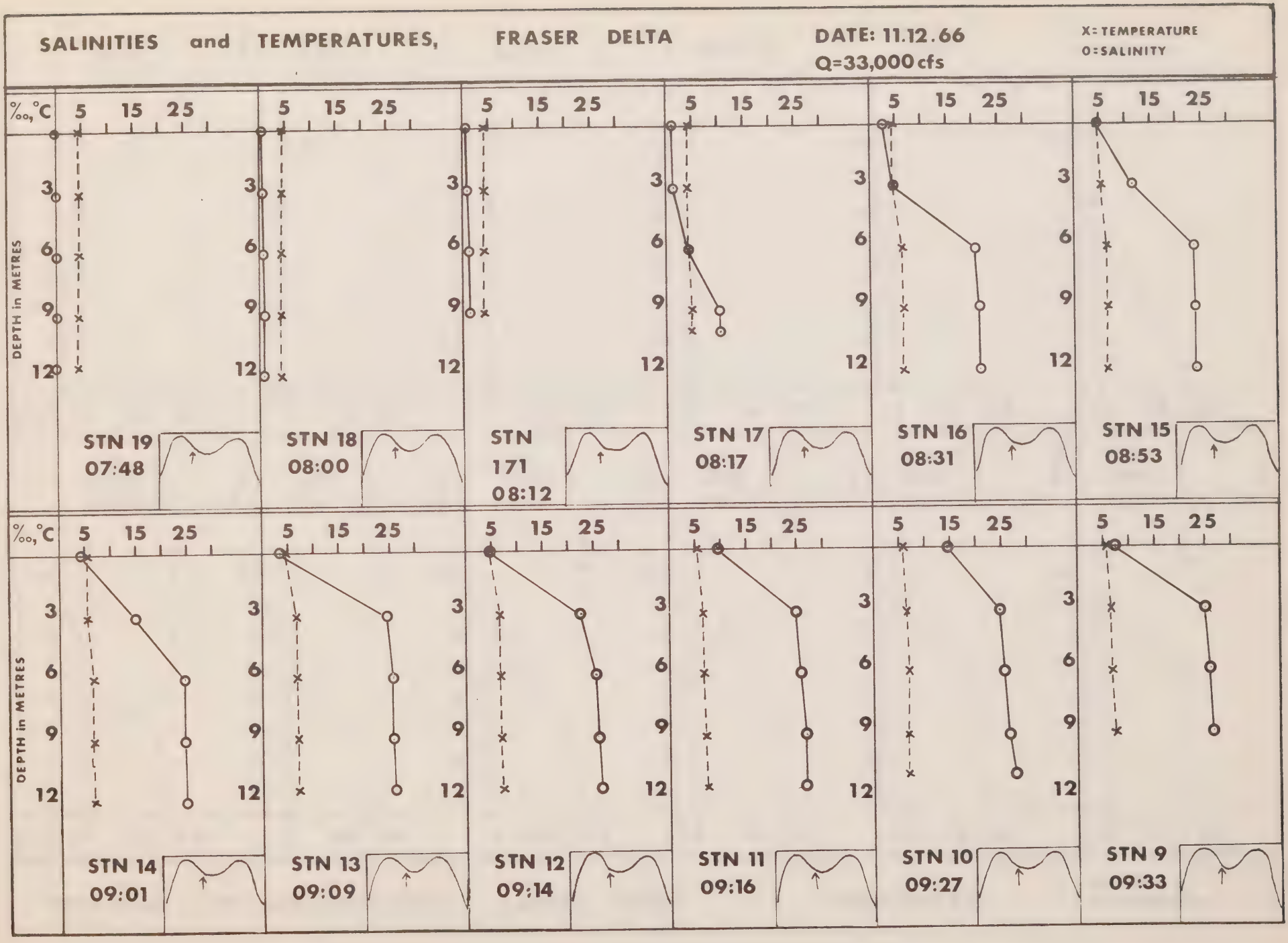

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 09.12.66
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 26
17:30
STN 26
17:45
STN 26
18:00
STN 26
18:15
STN 26
18:30
STN 26
18:45
STN

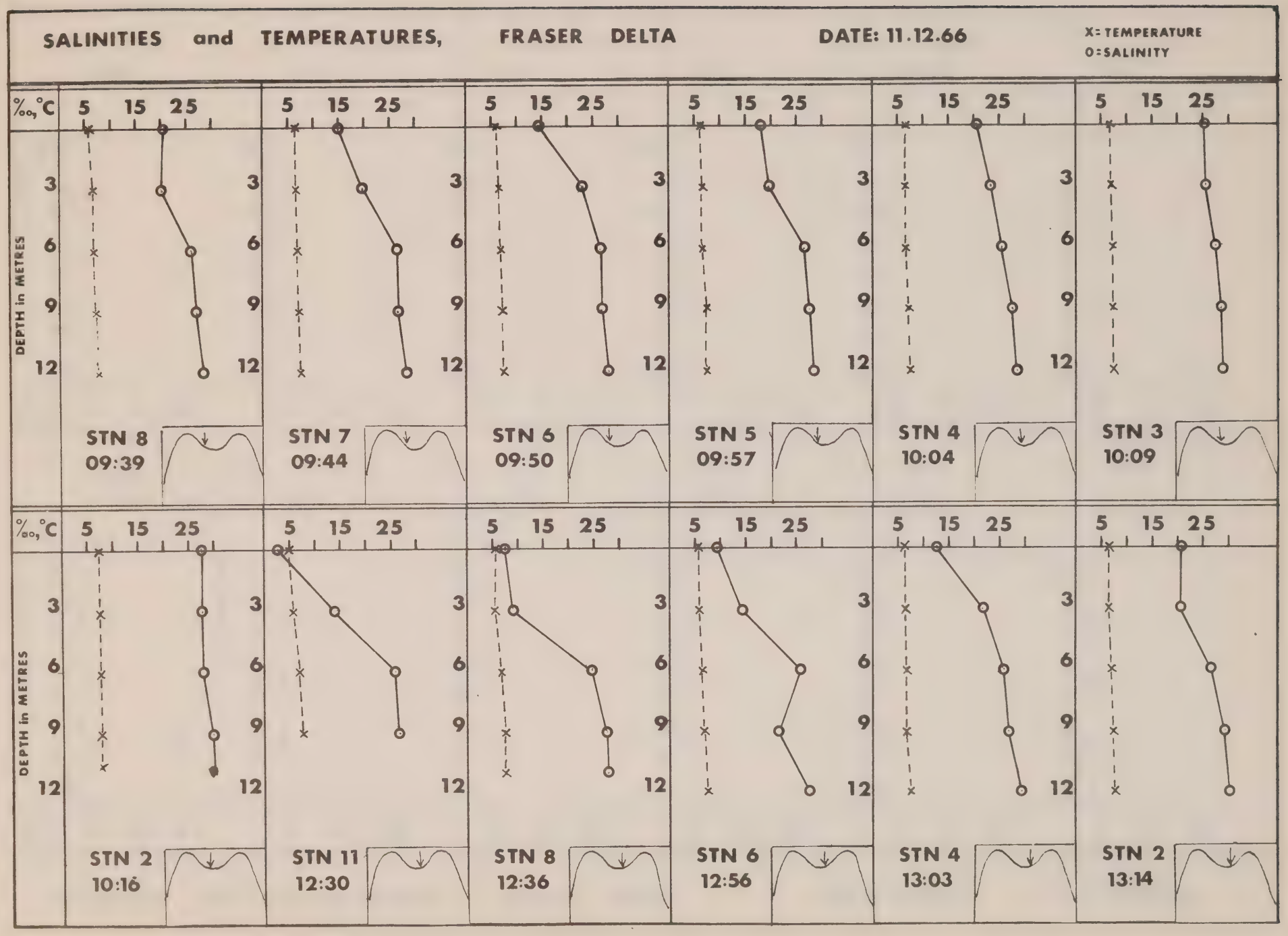

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 10.12.66
Q=32,600cfs
X=TEMPERATURE
O=SALINITY
‰, °C
DEPTH in METRES
STN 27 04:30
STN 27 05:00
STN 27 05:30
STN 27 05:45
STN 27 06:00
STN 27 06:15
STN 27 06:30
STN 27 06:45
STN 27 07:00
STN 27 07:15
STN 27 07:30
STN 27 07:45


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 10.12.66
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 27
08:00
STN 27
08:15
STN 27
08:30
STN 27
08:45
STN 27
09:00
STN 27
09:15
STN 27
09:30
STN 27
09:45
STN 27
10:00
STN 27
10:30
STN 27
11:00
STN 27
11:30


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 10.12.66
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 27
12:00
STN 27
12:30
STN 27
13:00
STN 27
13:30
STN 27
14:00
STN 27
14:30
STN 27
15:00
STN 27
15:30
STN 27
16:00
STN 27
16:30
STN 27
17:00
STN 27
17:15


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 10.12.66
X = TEMPERATURE
O = SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 27
17:30
STN 27
17:45
STN 27
18:00
STN 27
18:15
STN 27
18:30
STN 27
18:45
STN 27
19:00
STN 27
19:30
STN 27
20:00
STN 27
20:30
STN 27
21:00
STN 27
21:30


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 11.12.66
Q=33,000 cfs
X= TEMPERATURE
O= SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 19
07:48
STN 18
08:00
STN
171
08:12
STN 17
08:17
STN 16
08:31
STN 15
08:53
STN 14
09:01
STN 13
09:09
STN 12
09:14
STN 11
09:16
STN 10
09:27
STN 9
09:33


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 11.12.66
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 8 09:39
STN 7 09:44
STN 6 09:50
STN 5 09:57
STN 4 10:04
STN 3 10:09
STN 2 10:16
STN 11 12:30
STN 8 12:36
STN 6 12:56
STN 4 13:03
STN 2 13:14

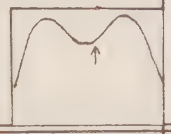
SALINITIES and TEMPERATURES, FRASER DELTA DATE: 11.12.66

X = TEMPERATURE
O = SALINITY

‰, °C 5 15 25

DEPTH in METRES 3 6 9 12

STN 1
13:20



STN

STN

STN

STN

STN

‰, °C 5 15 25

DEPTH in METRES 3 6 9 12

STN

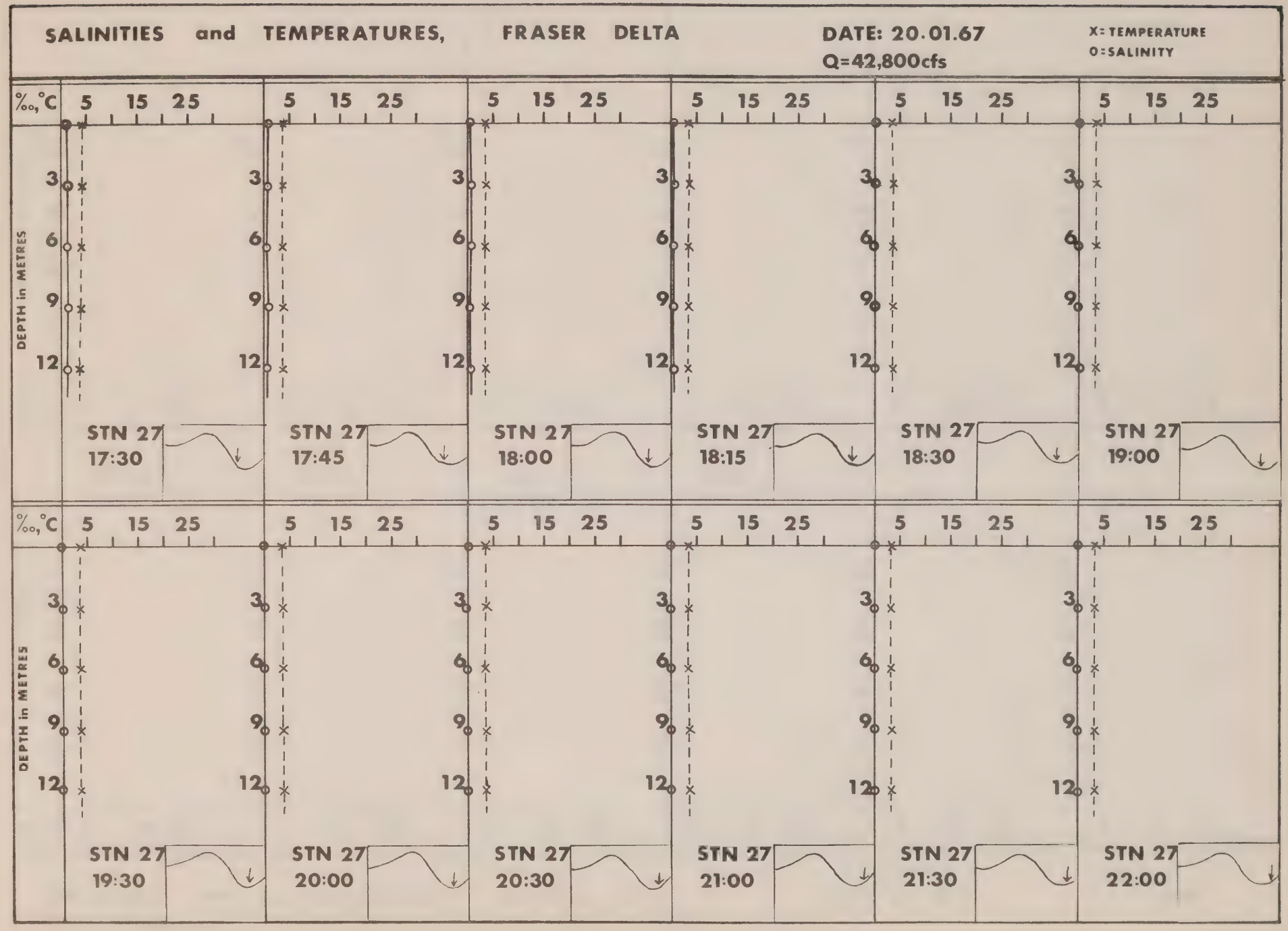
STN

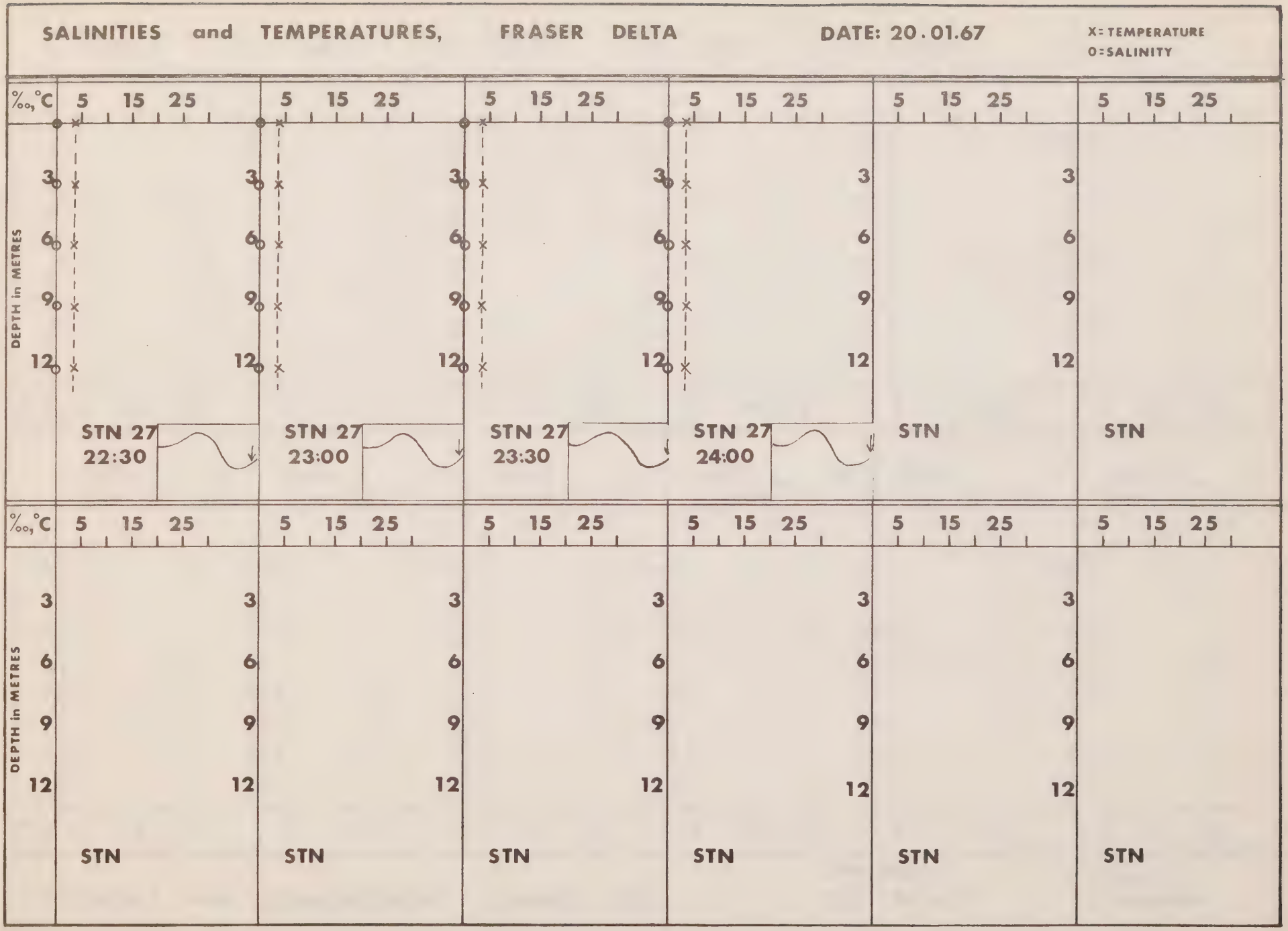
STN

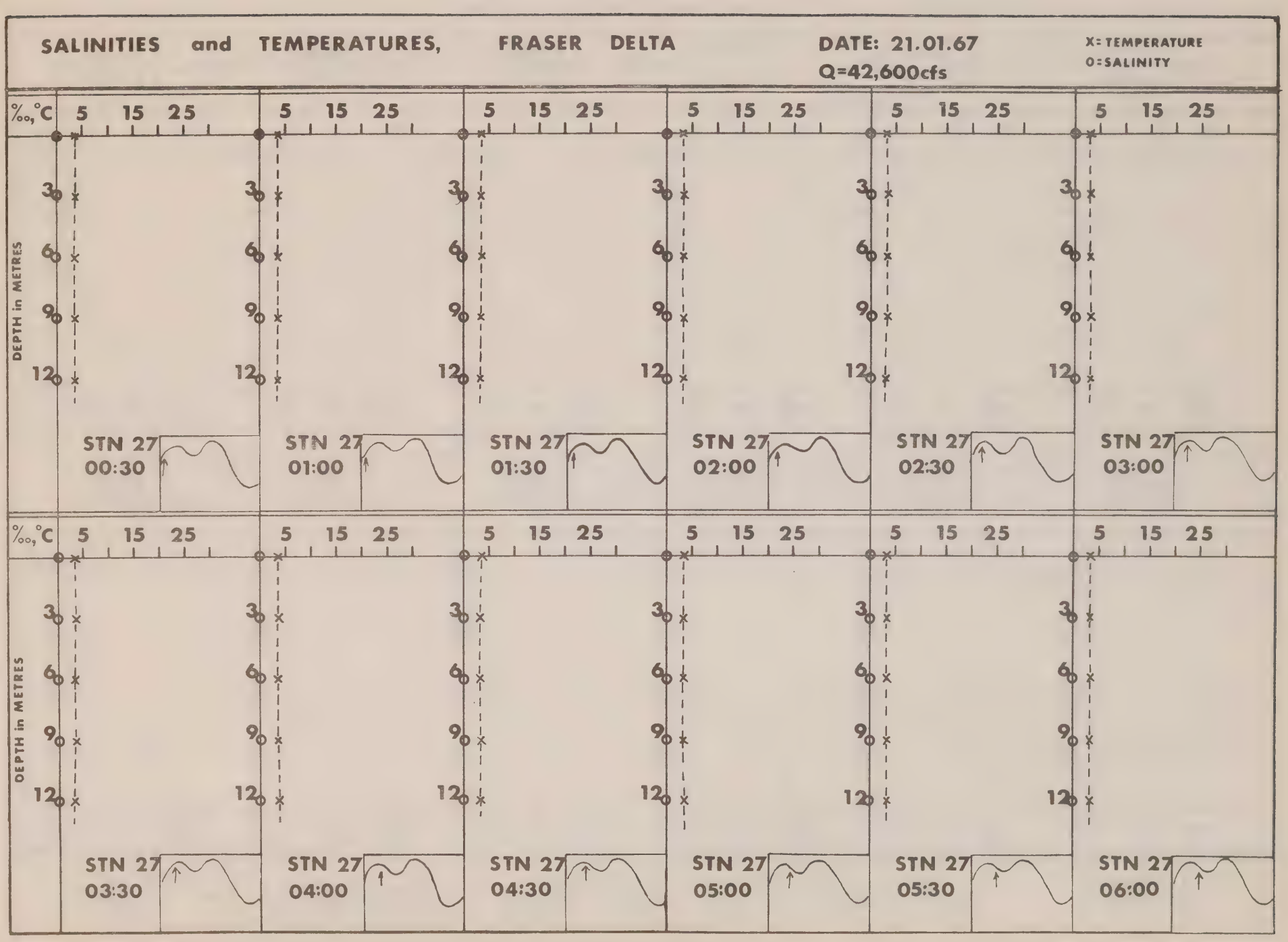
STN

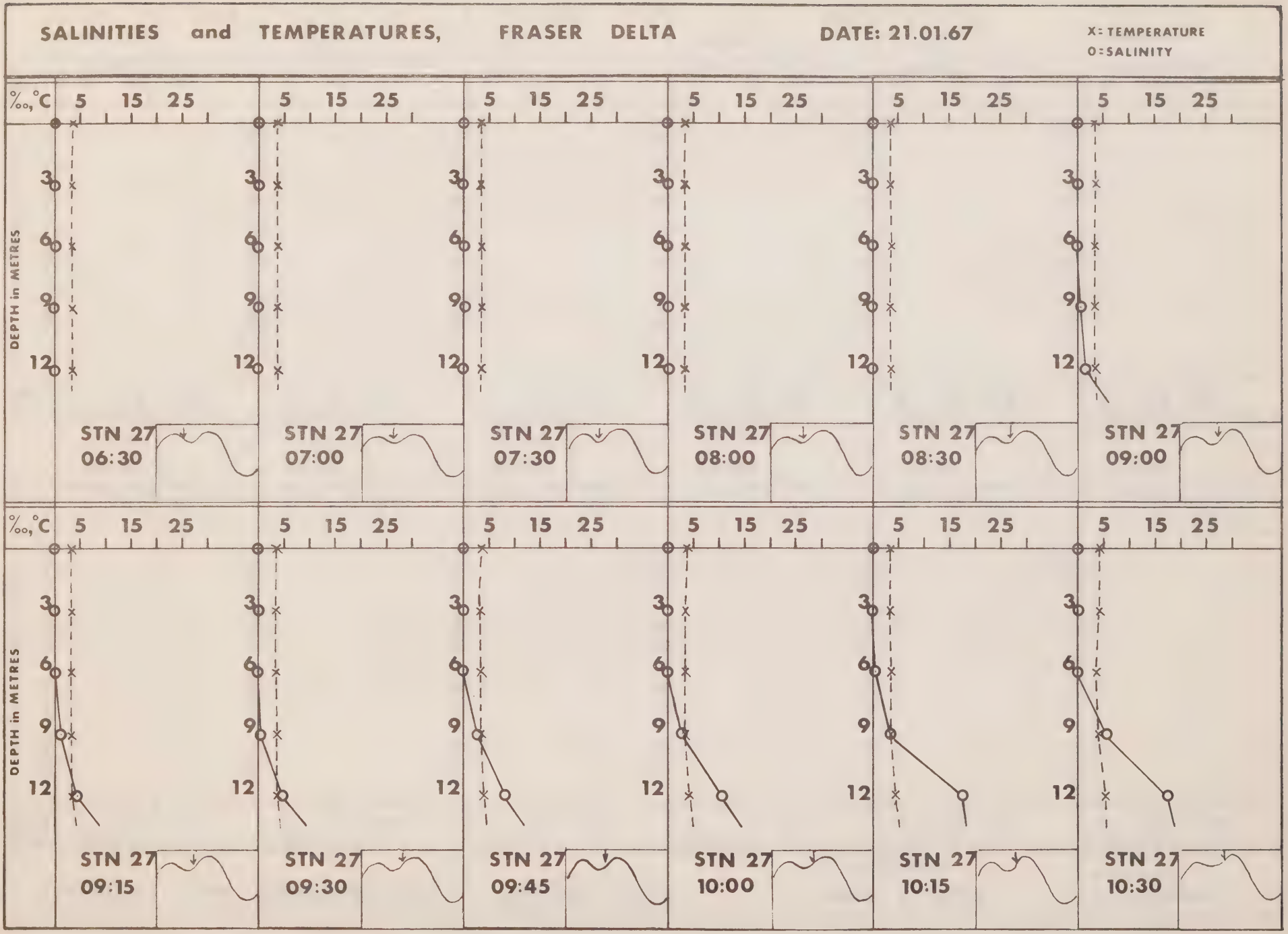
STN

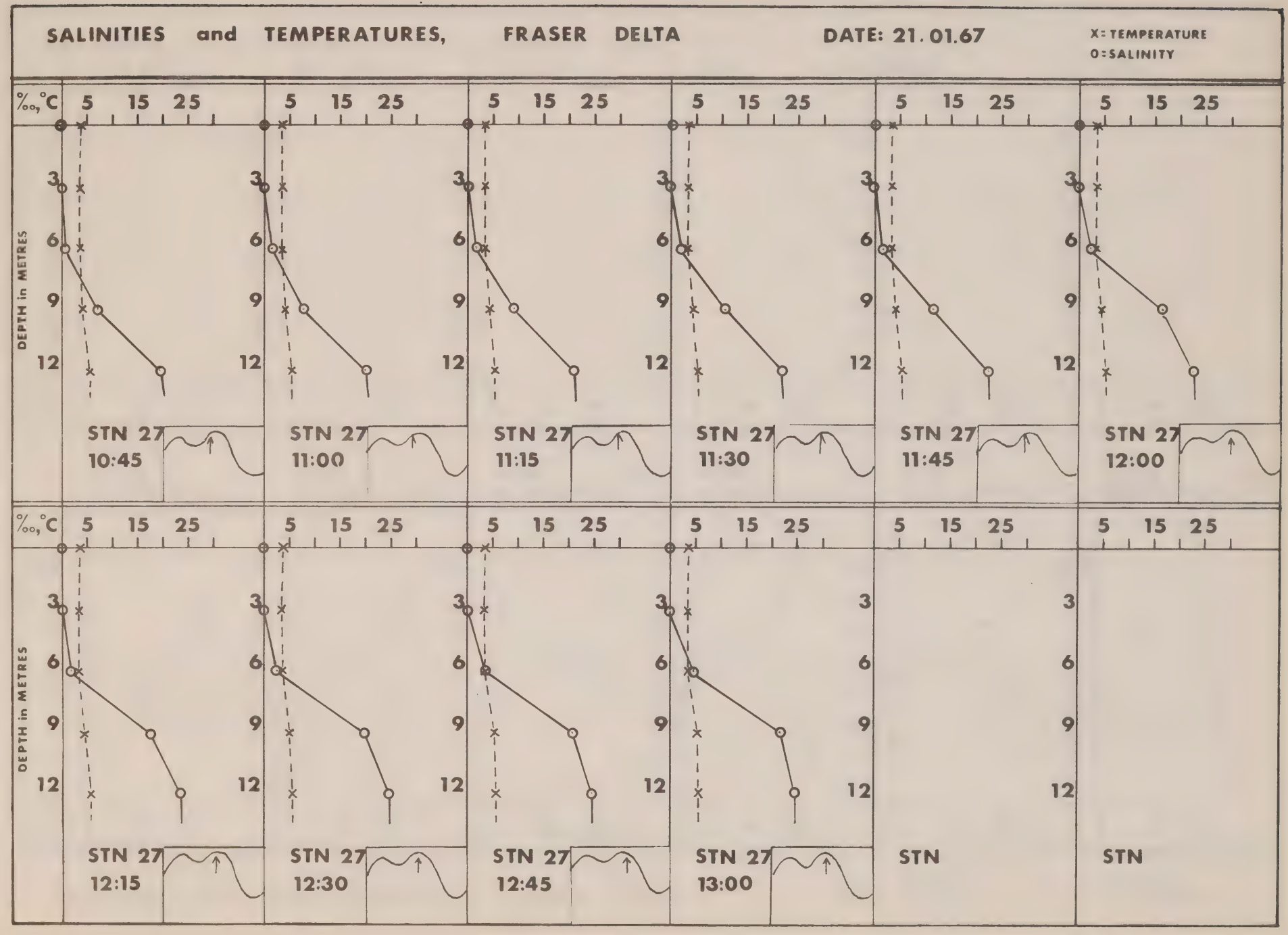
STN

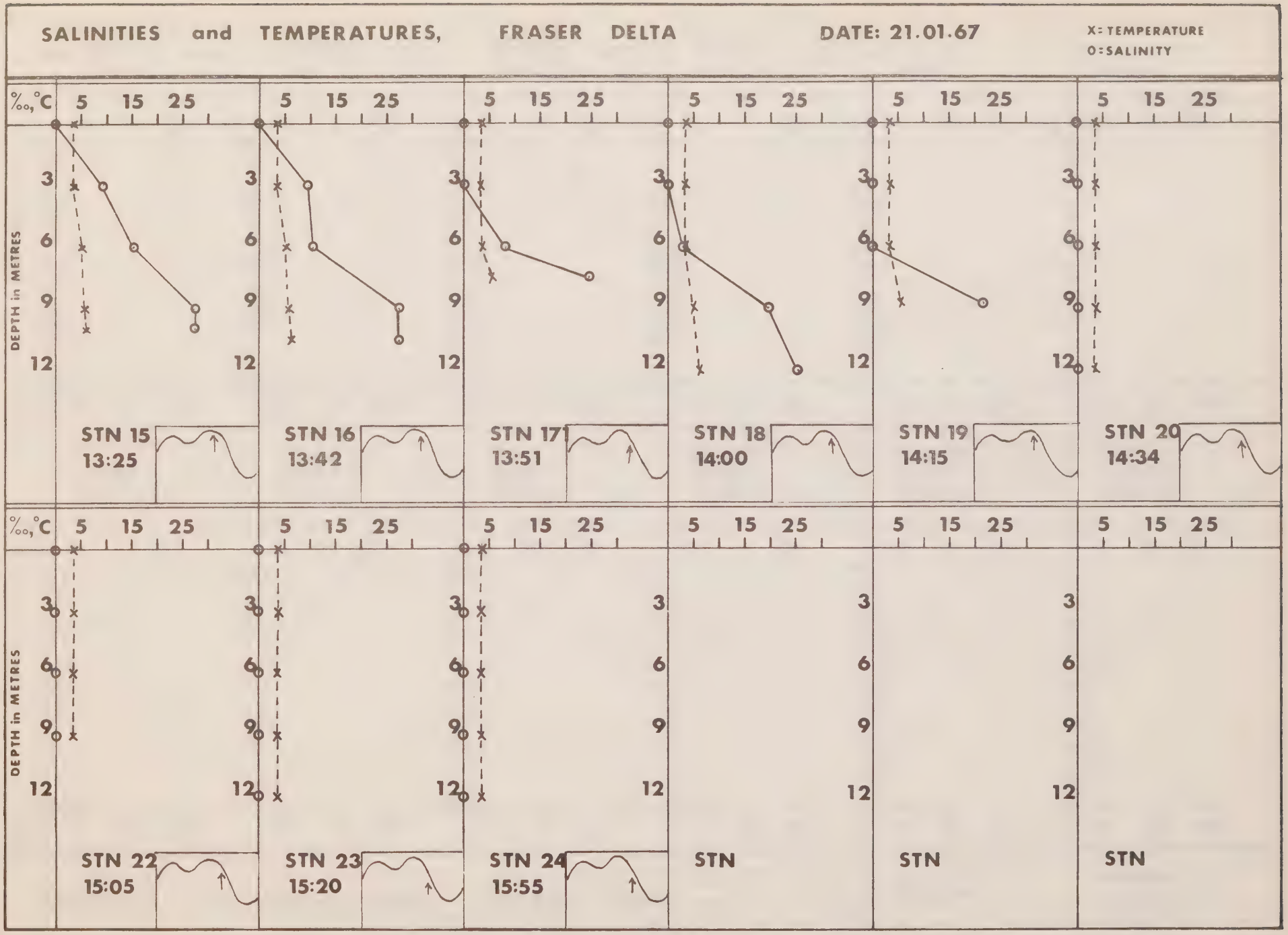

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 20.01.67
Q=42,800cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 27
17:30
STN 27
17:45
STN 27
18:00
STN 27
18:15
STN 27
18:30
STN 27
19:00
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21:30
STN 27
22:00

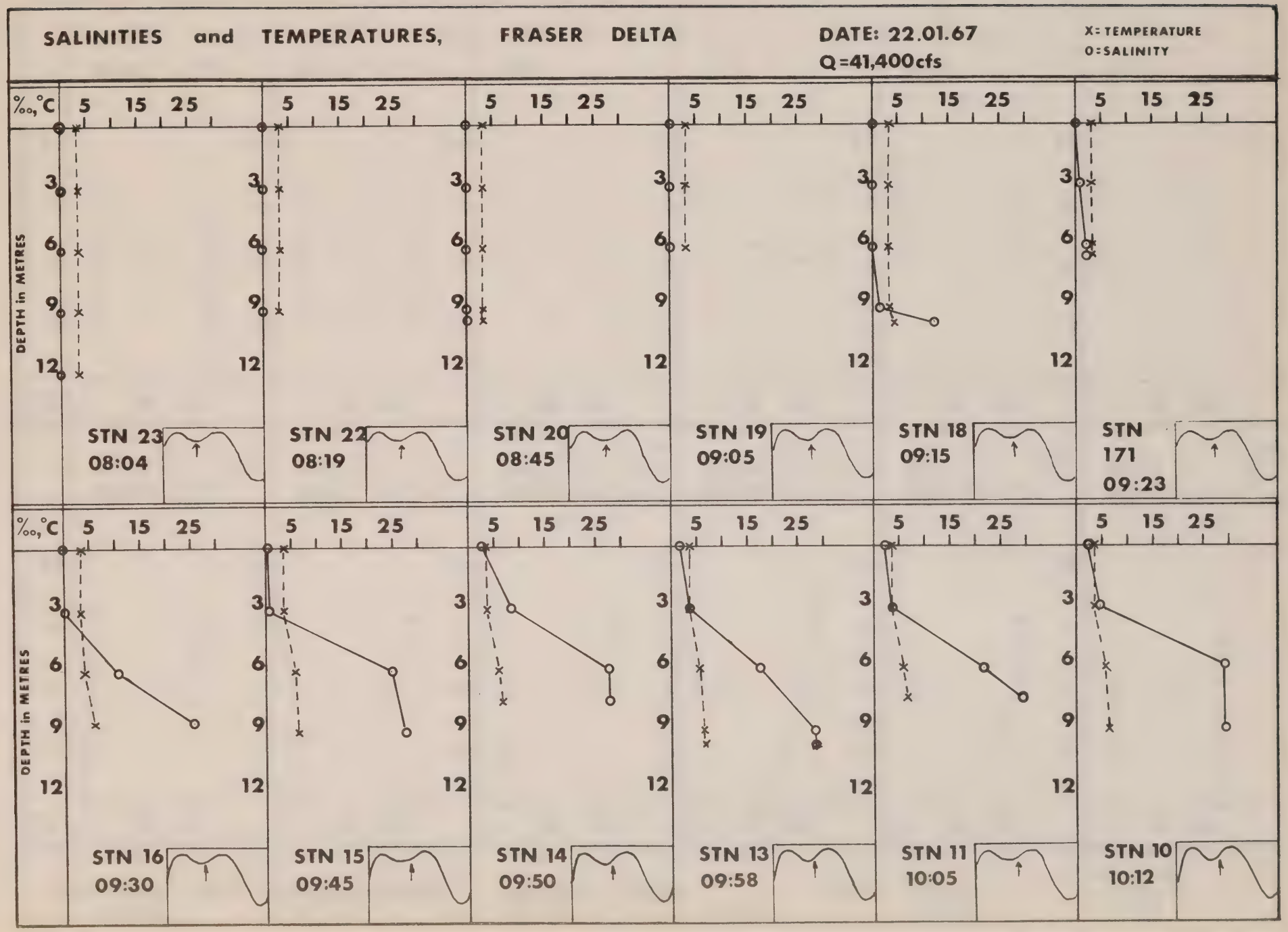

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 20.01.67
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 27
22:30
STN 27
23:00
STN 27
23:30
STN 27
24:00
STN
STN
STN
STN
STN
STN
STN
STN
STN
STN

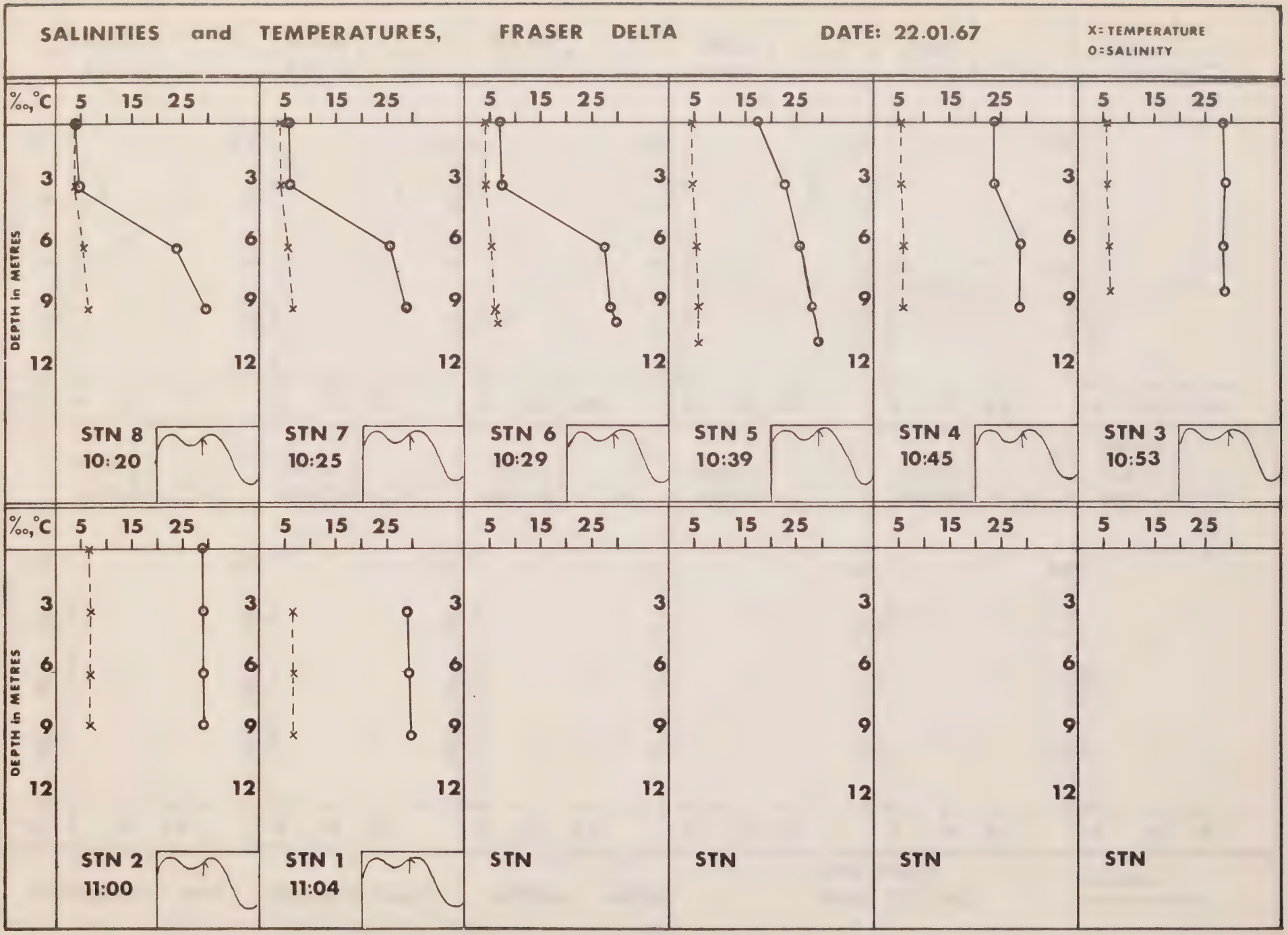

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 21.01.67
Q=42,600cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 27
00:30
STN 27
01:00
STN 27
01:30
STN 27
02:00
STN 27
02:30
STN 27
03:00
STN 27
03:30
STN 27
04:00
STN 27
04:30
STN 27
05:00
STN 27
05:30
STN 27
06:00

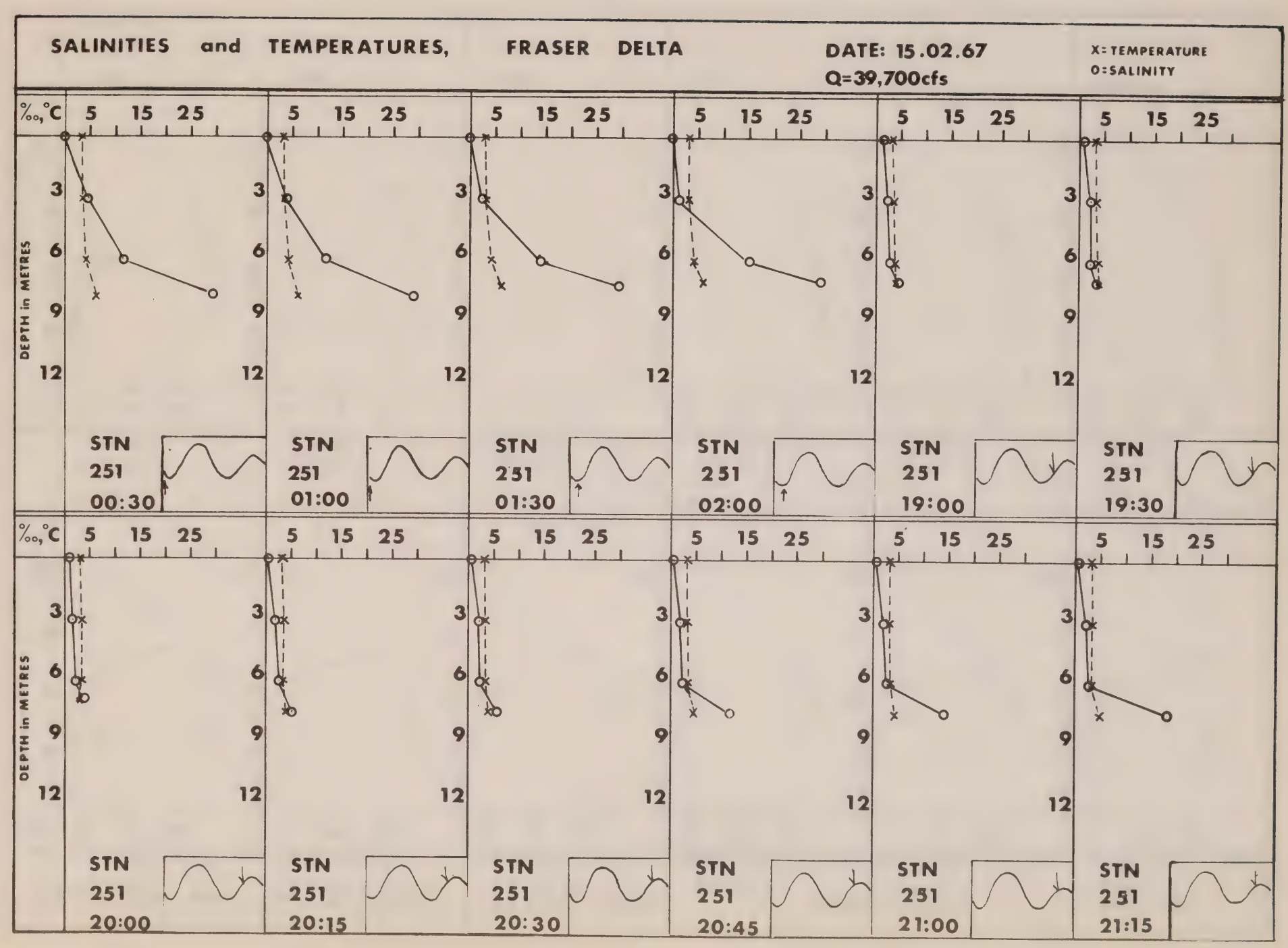

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 21.01.67
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 27
06:30
STN 27
07:00
STN 27
07:30
STN 27
08:00
STN 27
08:30
STN 27
09:00
STN 27
09:15
STN 27
09:30
STN 27
09:45
STN 27
10:00
STN 27
10:15
STN 27
10:30

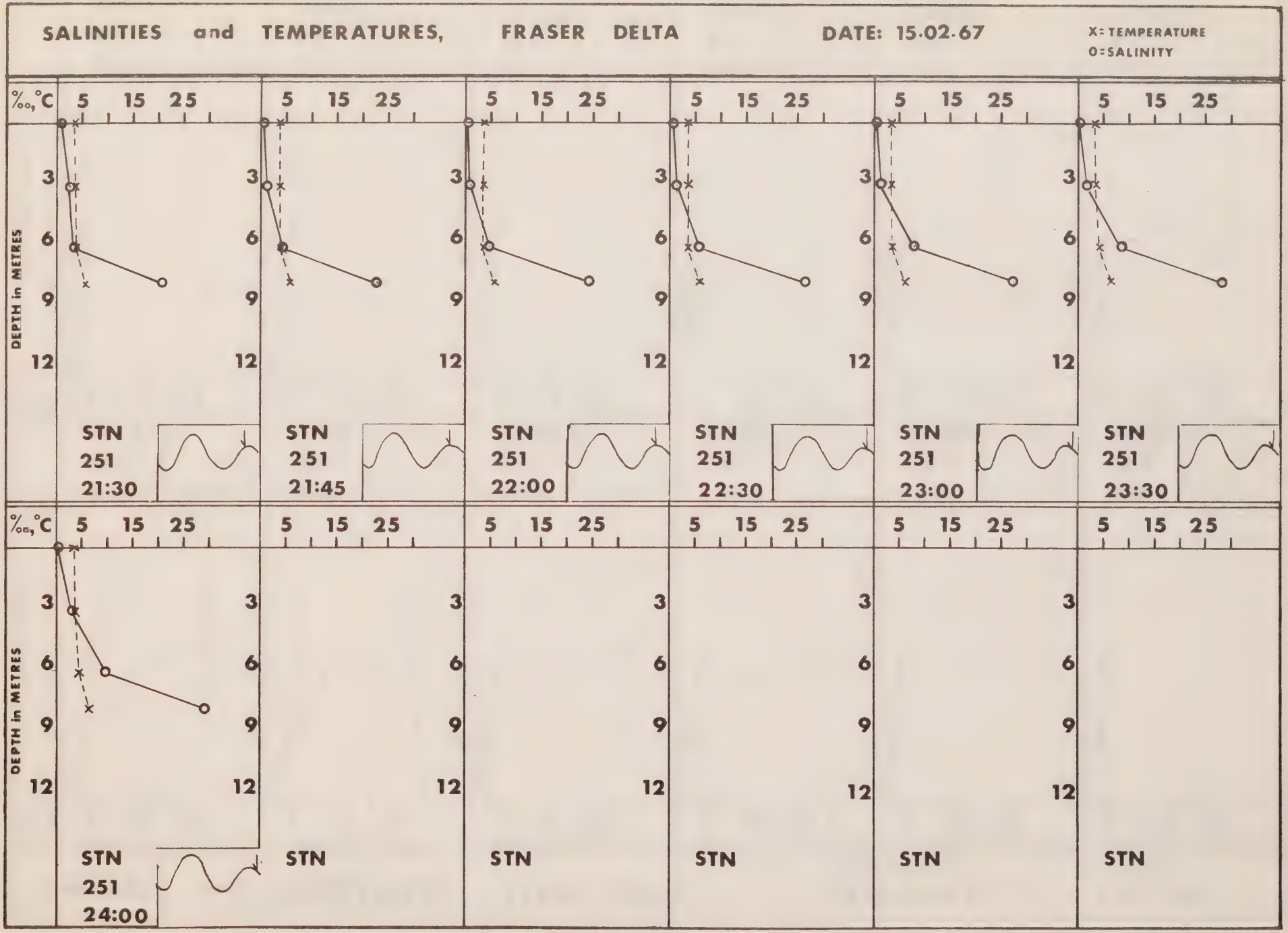

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 21.01.67
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 27
10:45
STN 27
11:00
STN 27
11:15
STN 27
11:30
STN 27
11:45
STN 27
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STN 27
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STN 27
12:30
STN 27
12:45
STN 27
13:00
STN
STN

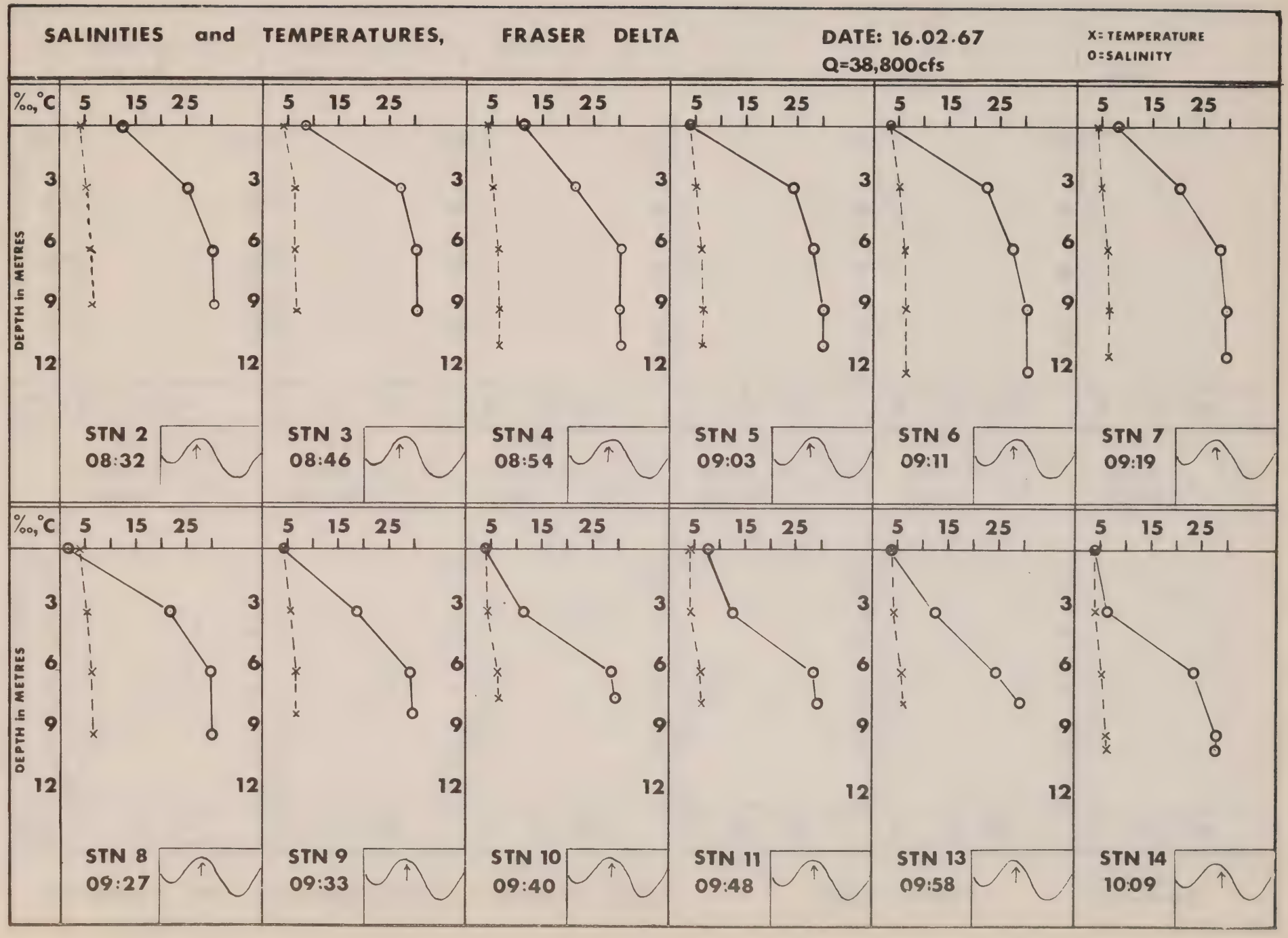

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 21.01.67
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 15
13:25
STN 16
13:42
STN 17
13:51
STN 18
14:00
STN 19
14:15
STN 20
14:34
STN 22
15:05
STN 23
15:20
STN 24
15:55
STN
STN
STN

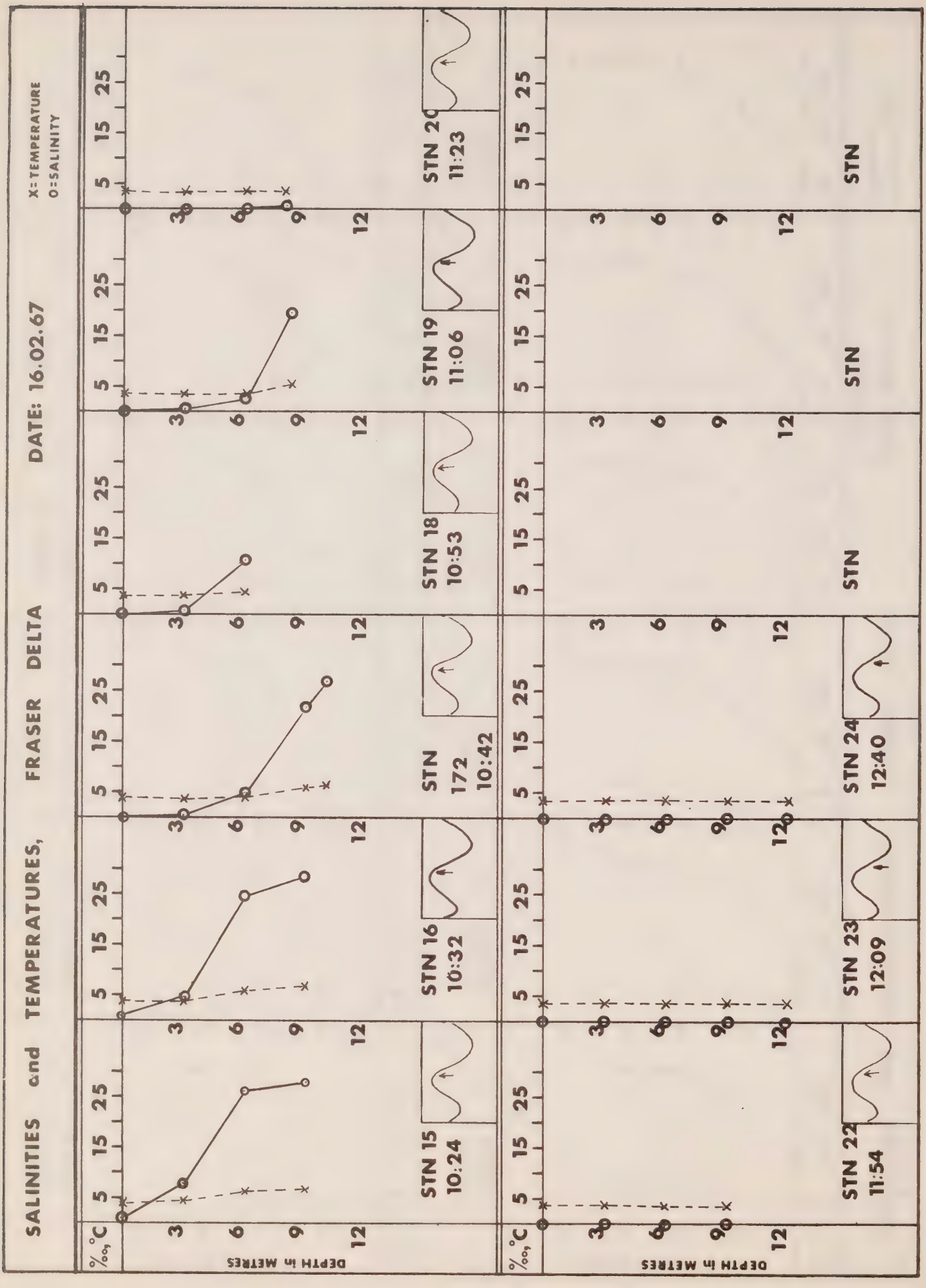

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 22.01.67
Q=41,400cfs
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O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 23
08:04
STN 22
08:19
STN 20
08:45
STN 19
09:05
STN 18
09:15
STN
171
09:23
STN 16
09:30
STN 15
09:45
STN 14
09:50
STN 13
09:58
STN 11
10:05
STN 10
10:12

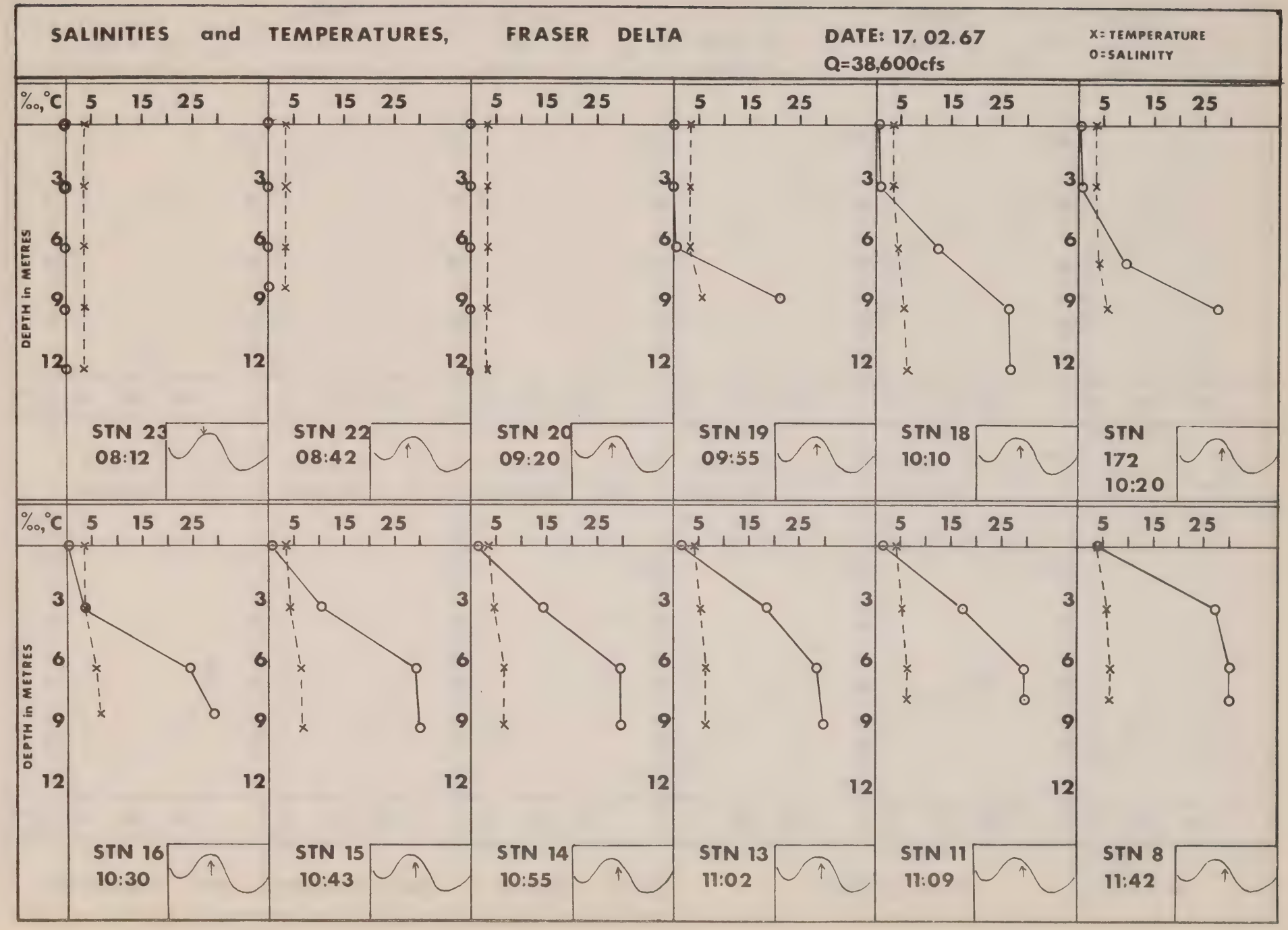

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 22.01.67
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 8
10:20
STN 7
10:25
STN 6
10:29
STN 5
10:39
STN 4
10:45
STN 3
10:53
STN 2
11:00
STN 1
11:04
STN
STN
STN
STN

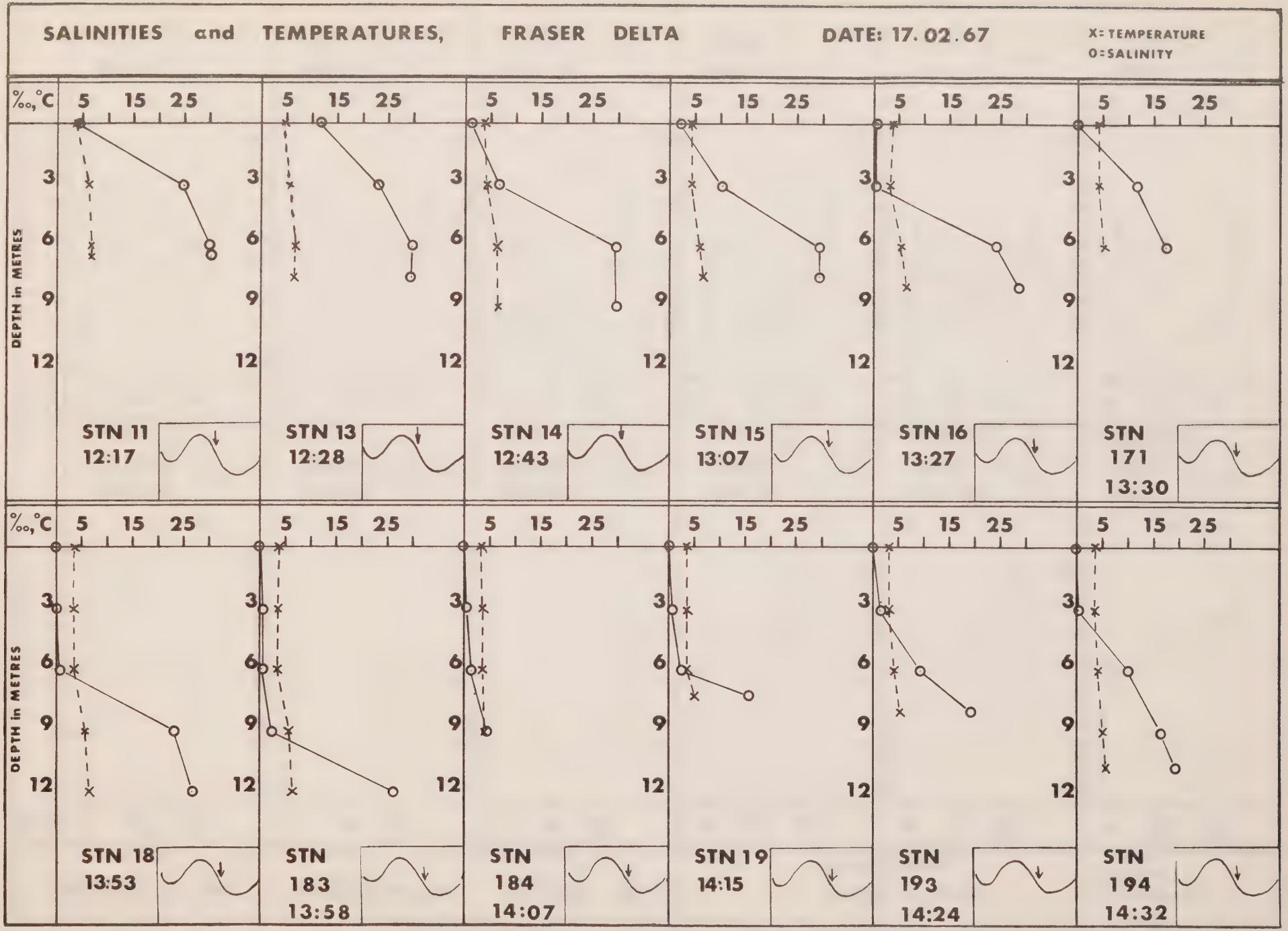

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 15.02.67
Q=39,700cfs
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 251 00:30
STN 251 01:00
STN 251 01:30
STN 251 02:00
STN 251 19:00
STN 251 19:30
STN 251 20:00
STN 251 20:15
STN 251 20:30
STN 251 20:45
STN 251 21:00
STN 251 21:15


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 15.02.67
X = TEMPERATURE
O = SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 251 21:30
STN 251 21:45
STN 251 22:00
STN 251 22:30
STN 251 23:00
STN 251 23:30
STN 251 24:00
STN


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 16.02.67
Q=38,800cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 2
08:32
STN 3
08:46
STN 4
08:54
STN 5
09:03
STN 6
09:11
STN 7
09:19
STN 8
09:27
STN 9
09:33
STN 10
09:40
STN 11
09:48
STN 13
09:58
STN 14
10:09


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 16.02.67
X=TEMPERATURE
O=SALINITY
‰, °C
5 15 25
3 6 9 12
DEPTH in METRES
STN 15
10:24
STN 16
10:32
STN
172
10:42
STN 18
10:53
STN 19
11:06
STN 20
11:23
STN 22
11:54
STN 23
12:09
STN 24
12:40
STN


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 17. 02. 67
Q=38,600cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 23
08:12
STN 22
08:42
STN 20
09:20
STN 19
09:55
STN 18
10:10
STN
172
10:20
STN 16
10:30
STN 15
10:43
STN 14
10:55
STN 13
11:02
STN 11
11:09
STN 8
11:42


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 17.02.67
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 11
12:17
STN 13
12:28
STN 14
12:43
STN 15
13:07
STN 16
13:27
STN
171
13:30
STN 18
13:53
STN
183
13:58
STN
184
14:07
STN 19
14:15
STN
193
14:24
STN
194
14:32

SALINITIES and TEMPERATURES, FRASER DELTA DATE: 17.02.67

X = TEMPERATURE
O = SALINITY

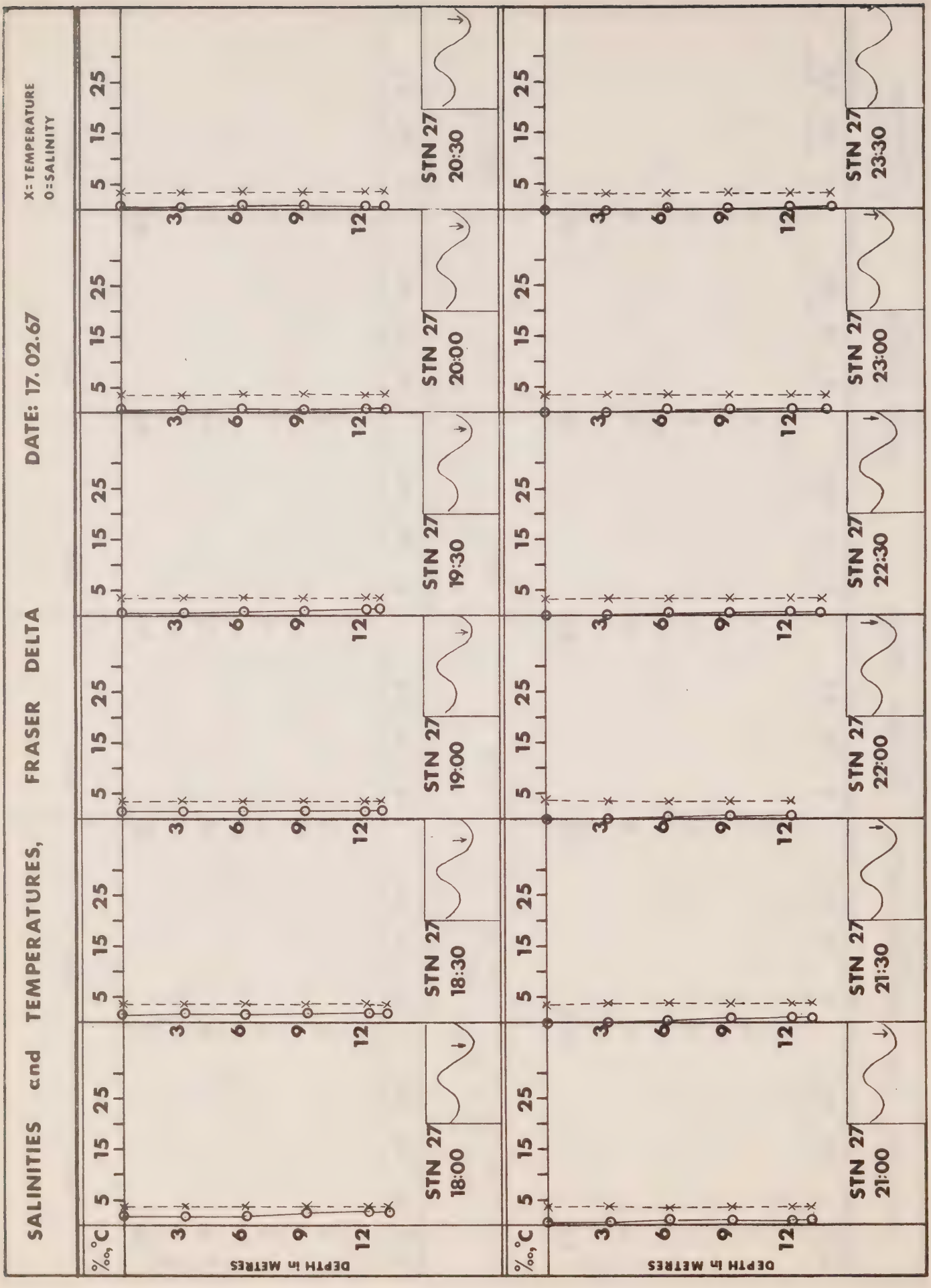
‰, °C 5 15 25

DEPTH in METRES 3 6 9 12

STN 19.5
14:42

STN 20
14:52

STN


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 17.02.67
X=TEMPERATURE
O=SALINITY
‰, °C
5 15 25
3 6 9 12
DEPTH in METRES
STN 27 18:00
STN 27 18:30
STN 27 19:00
STN 27 19:30
STN 27 20:00
STN 27 20:30
STN 27 21:00
STN 27 21:30
STN 27 22:00
STN 27 22:30
STN 27 23:00
STN 27 23:30

SALINITIES and TEMPERATURES, FRASER DELTA DATE: 17.02.67

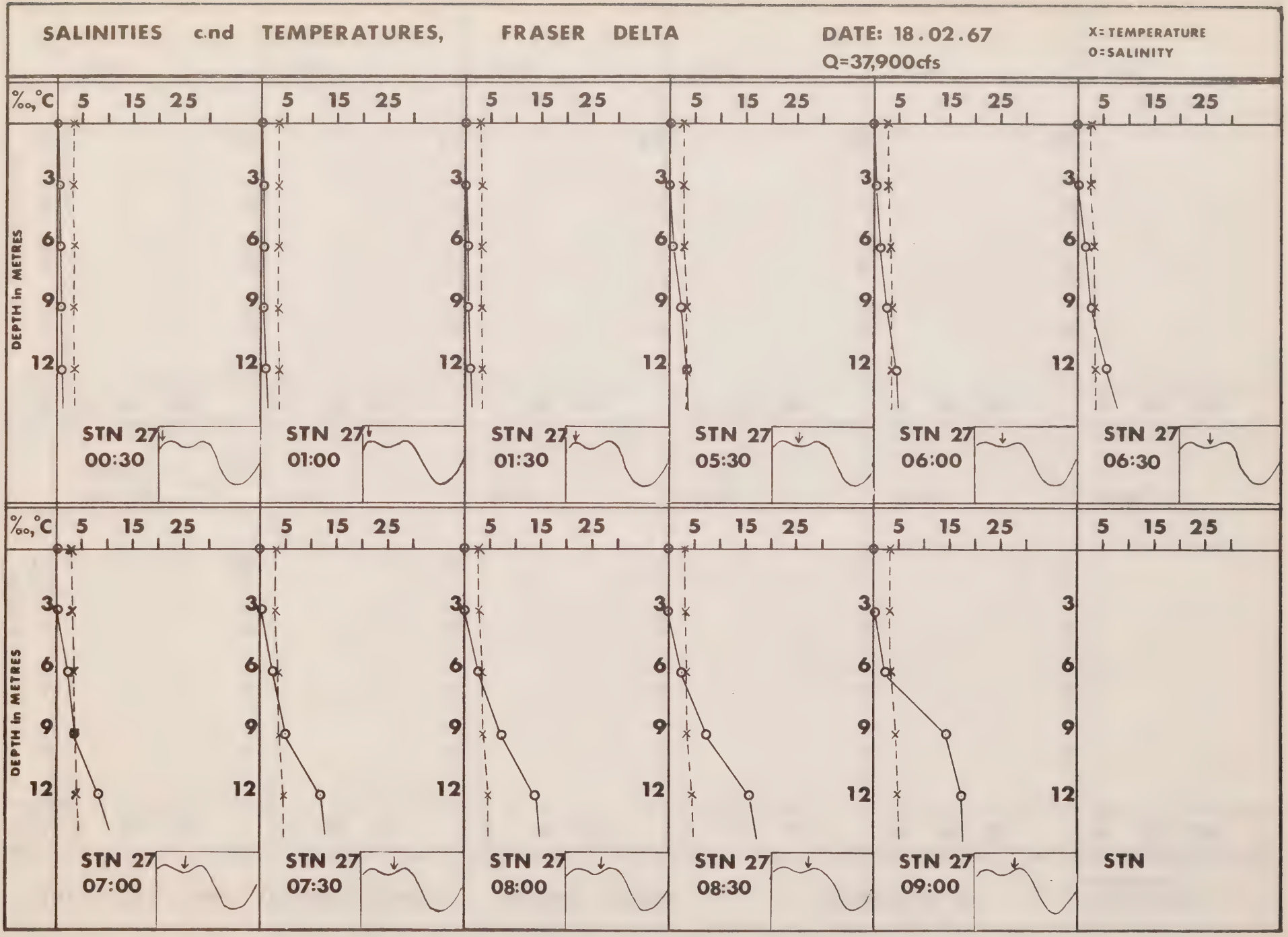
X = TEMPERATURE
O = SALINITY

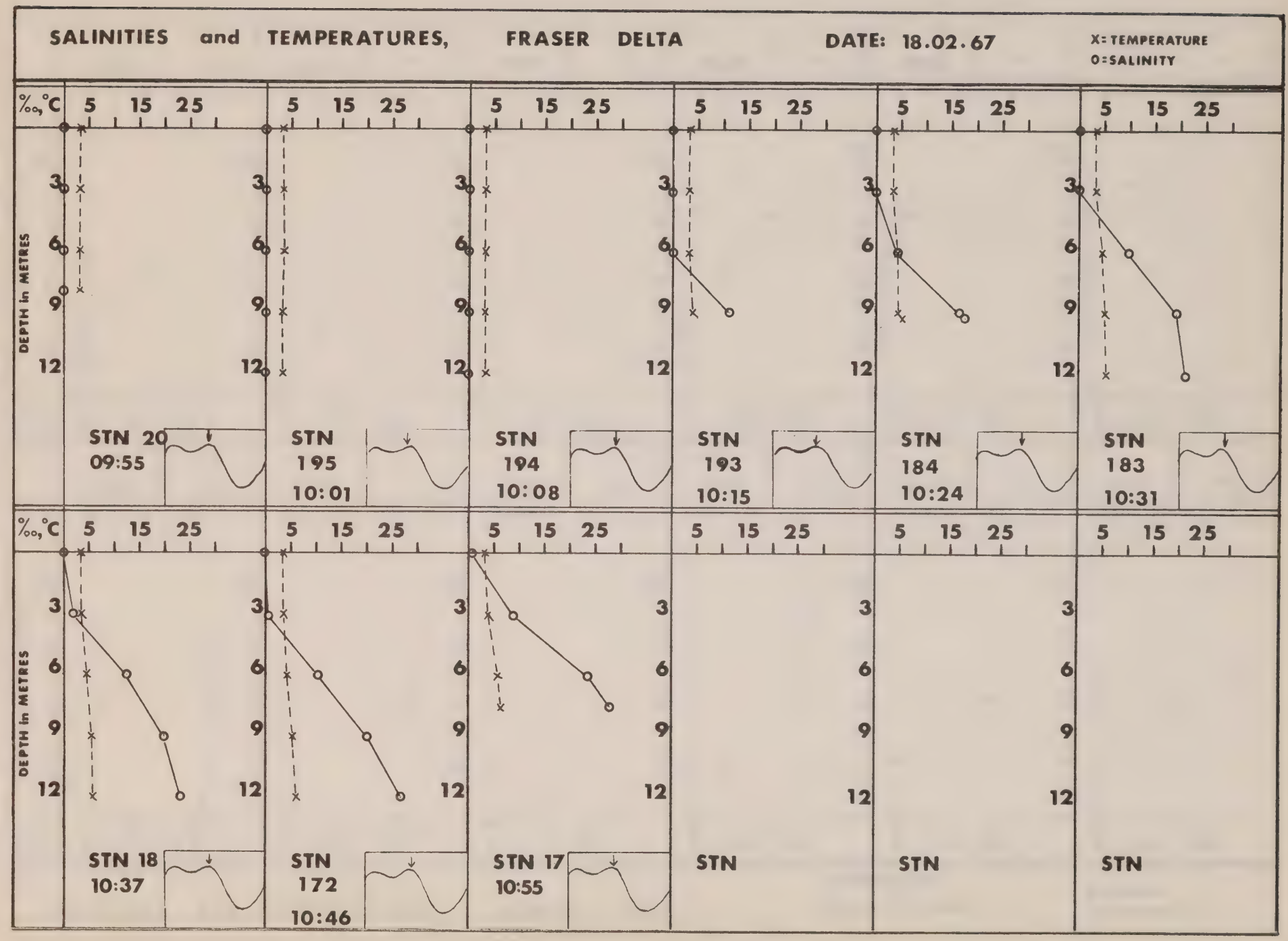
‰, °C 5 15 25

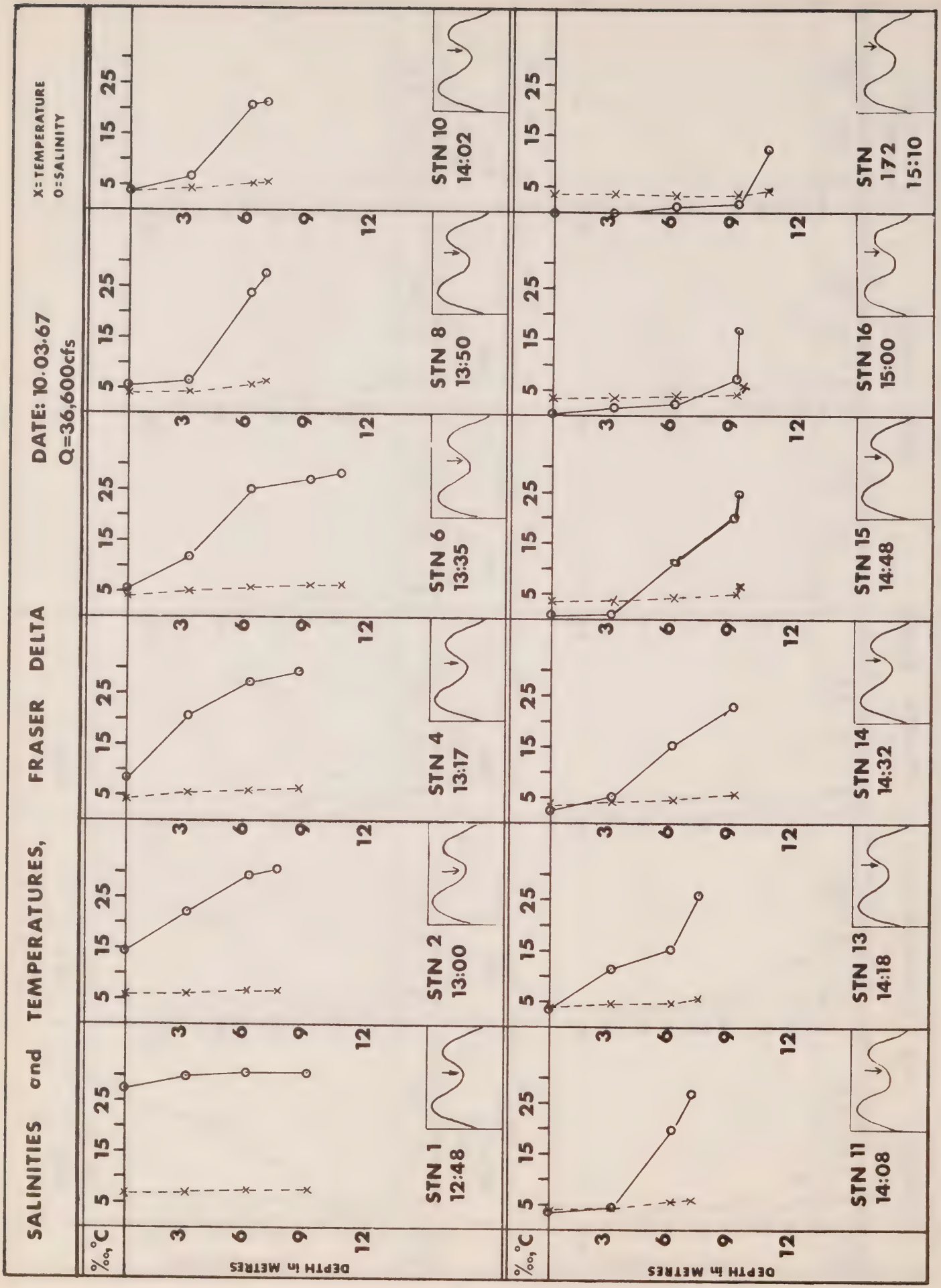
DEPTH in METRES 3 6 9 12

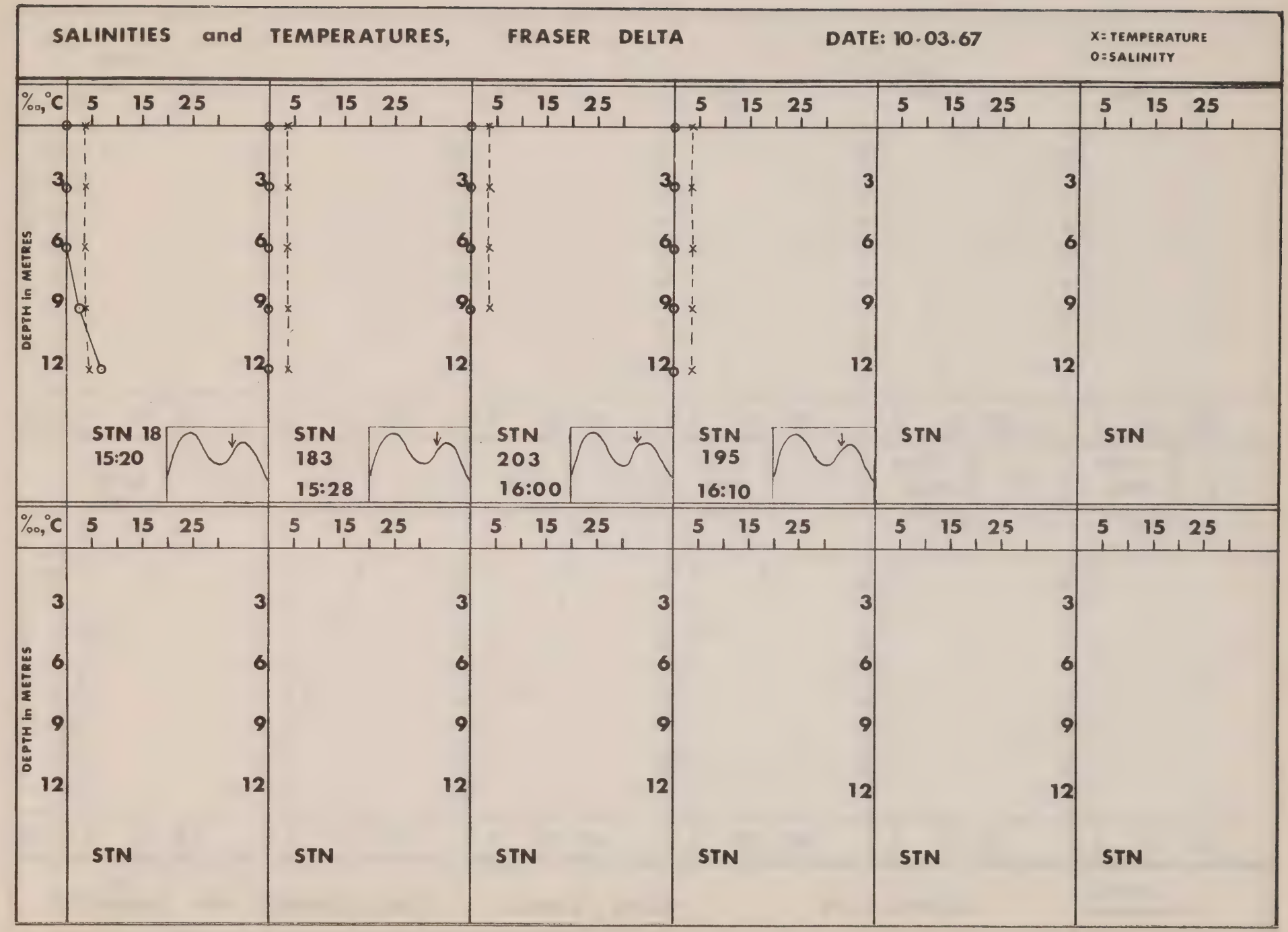
STN 27
24:00

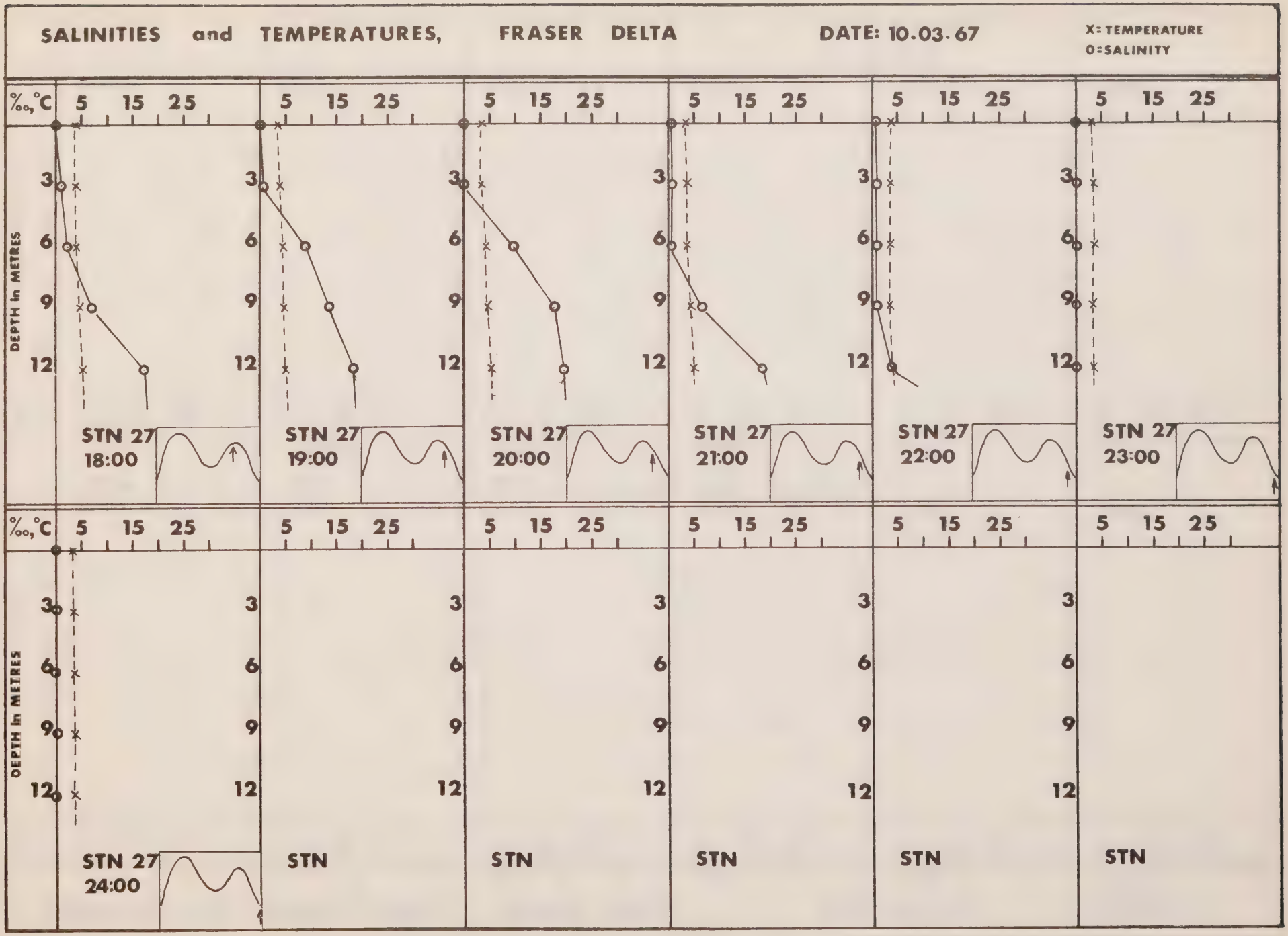
STN

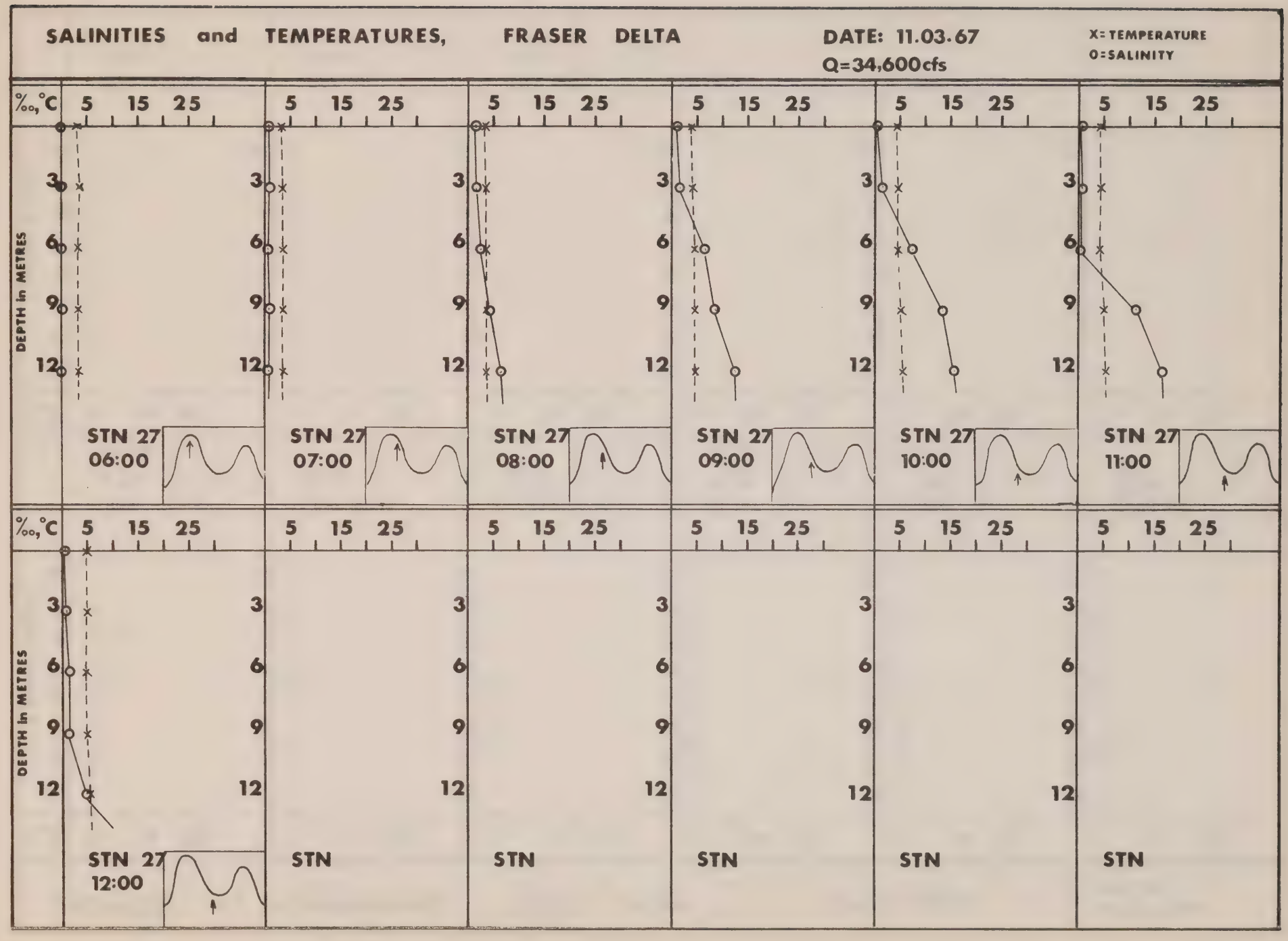

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 18.02.67
Q=37,900cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 27
00:30
STN 27
01:00
STN 27
01:30
STN 27
05:30
STN 27
06:00
STN 27
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STN 27
09:00
STN

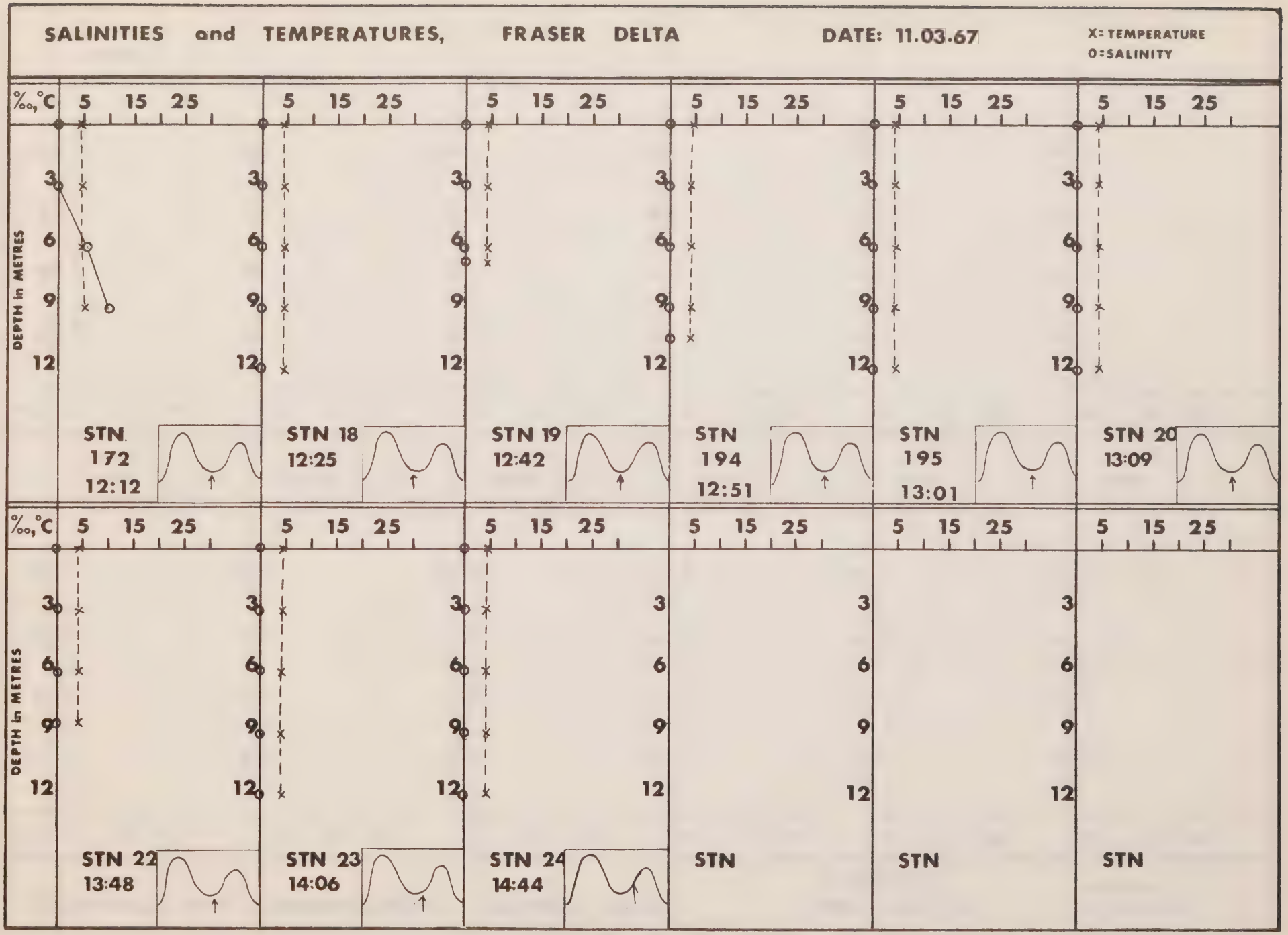

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 18.02.67
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 20
09:55
STN
195
10:01
STN
194
10:08
STN
193
10:15
STN
184
10:24
STN
183
10:31
STN 18
10:37
STN
172
10:46
STN 17
10:55
STN
STN
STN

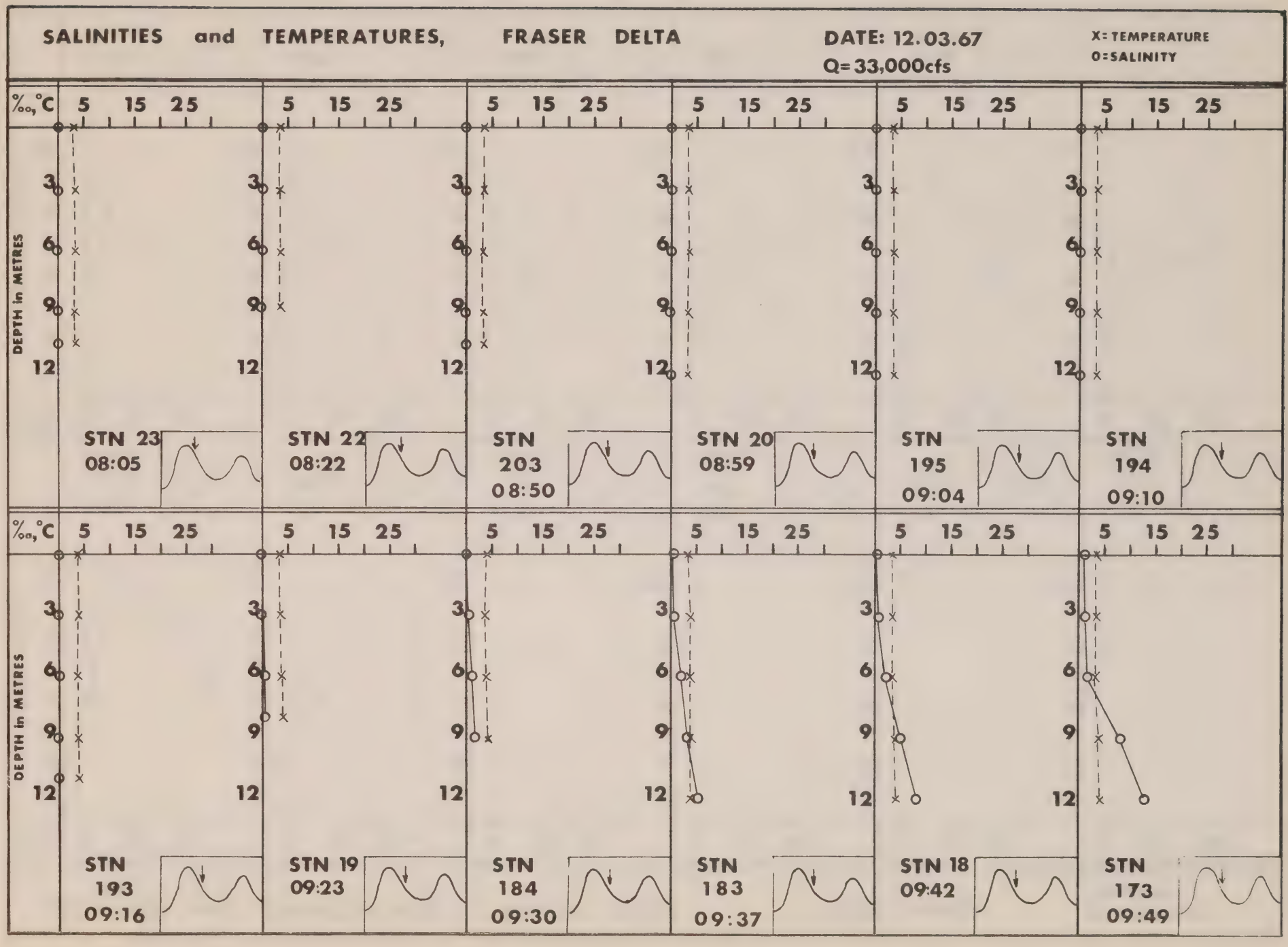

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 10.03.67
Q=36,600cfs
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
3 6 9 12
DEPTH in METRES
STN 1 12:48
STN 2 13:00
STN 4 13:17
STN 6 13:35
STN 8 13:50
STN 10 14:02
STN 11 14:08
STN 13 14:18
STN 14 14:32
STN 15 14:48
STN 16 15:00
STN 172 15:10

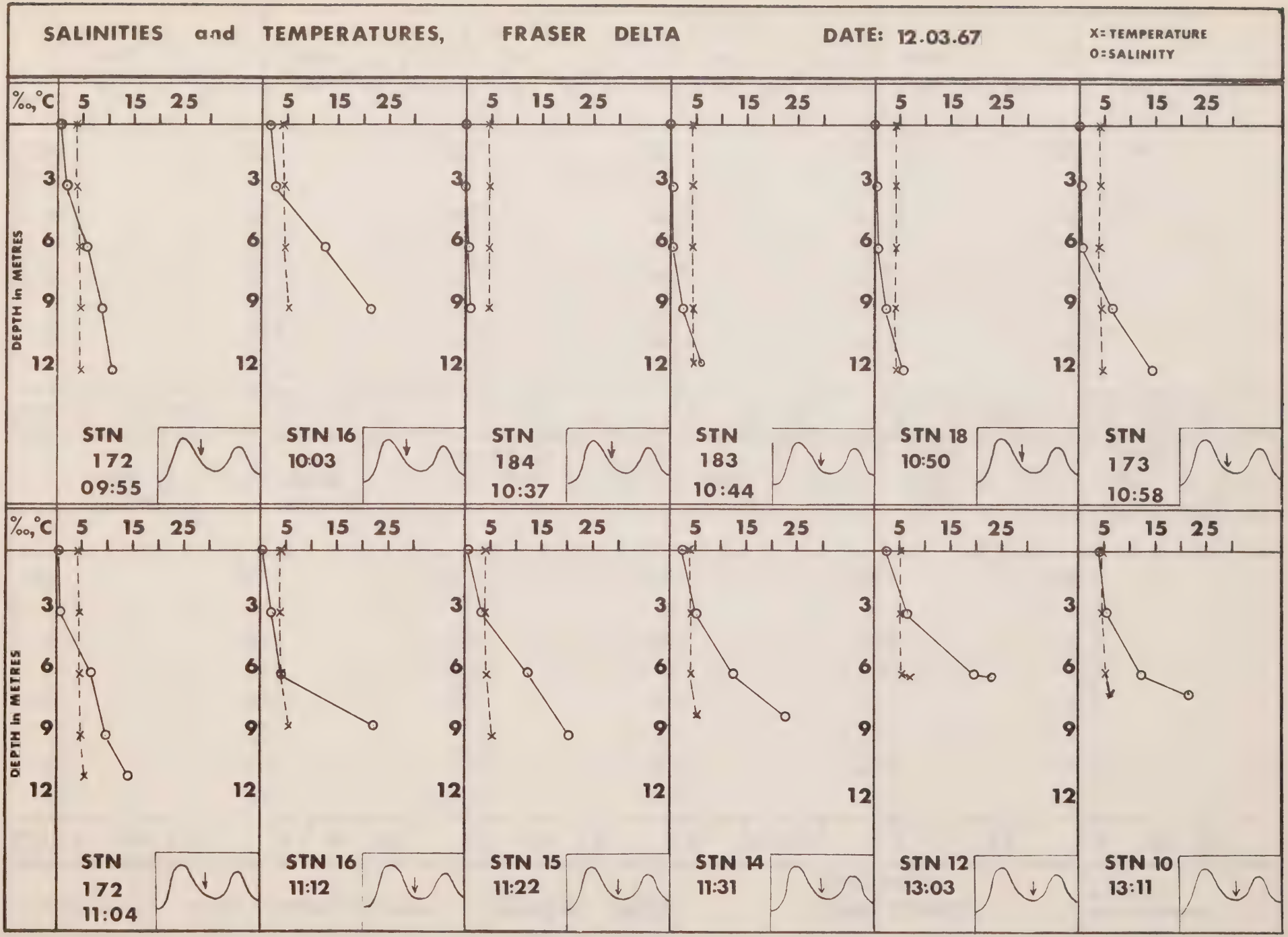

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 10·03·67
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 18
15:20
STN
183
15:28
STN
203
16:00
STN
195
16:10
STN
STN
STN
STN
STN
STN
STN
STN
STN
STN
STN
STN

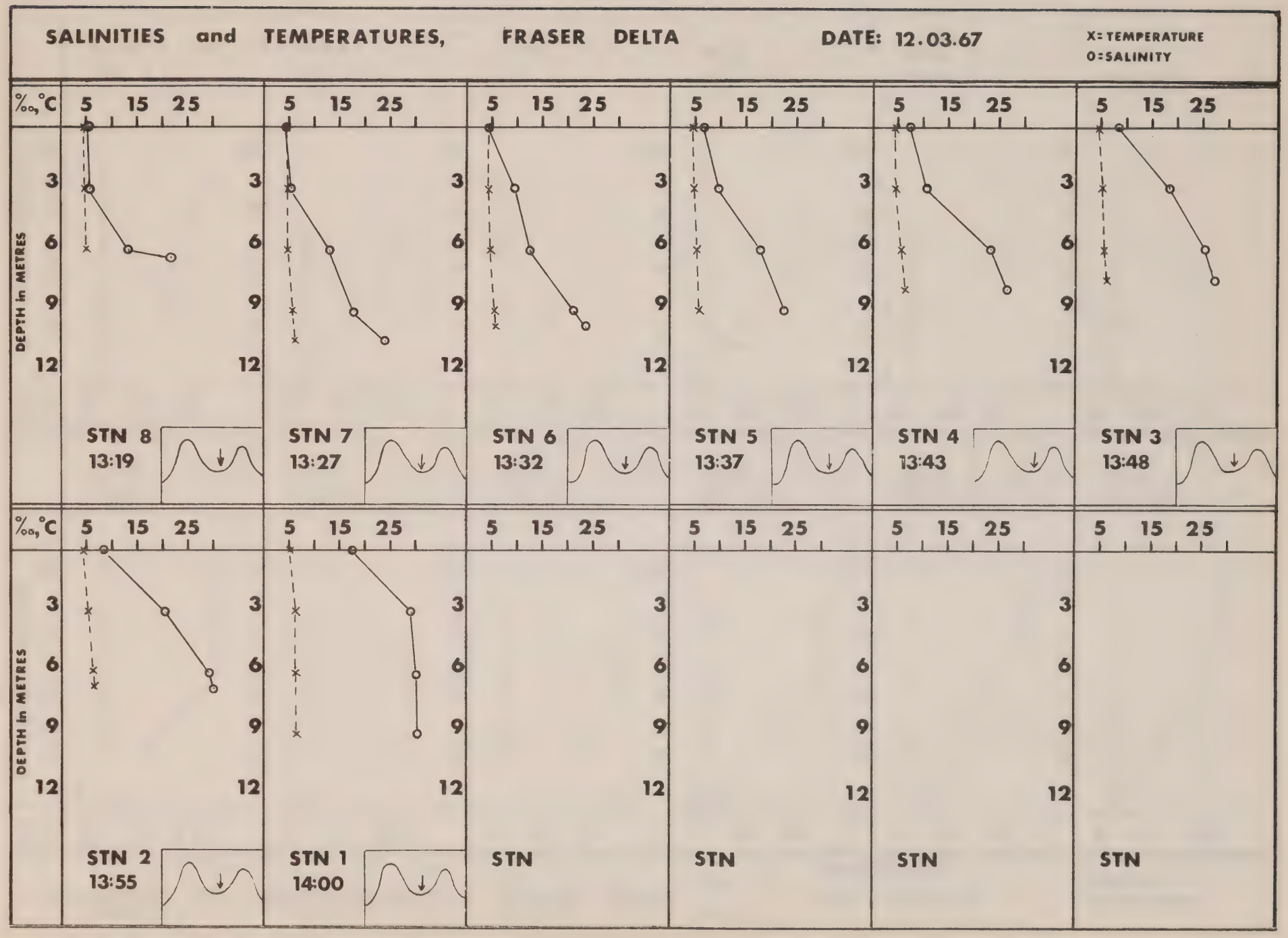

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 10.03.67
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 27
18:00
STN 27
19:00
STN 27
20:00
STN 27
21:00
STN 27
22:00
STN 27
23:00
STN 27
24:00
STN
STN
STN
STN
STN

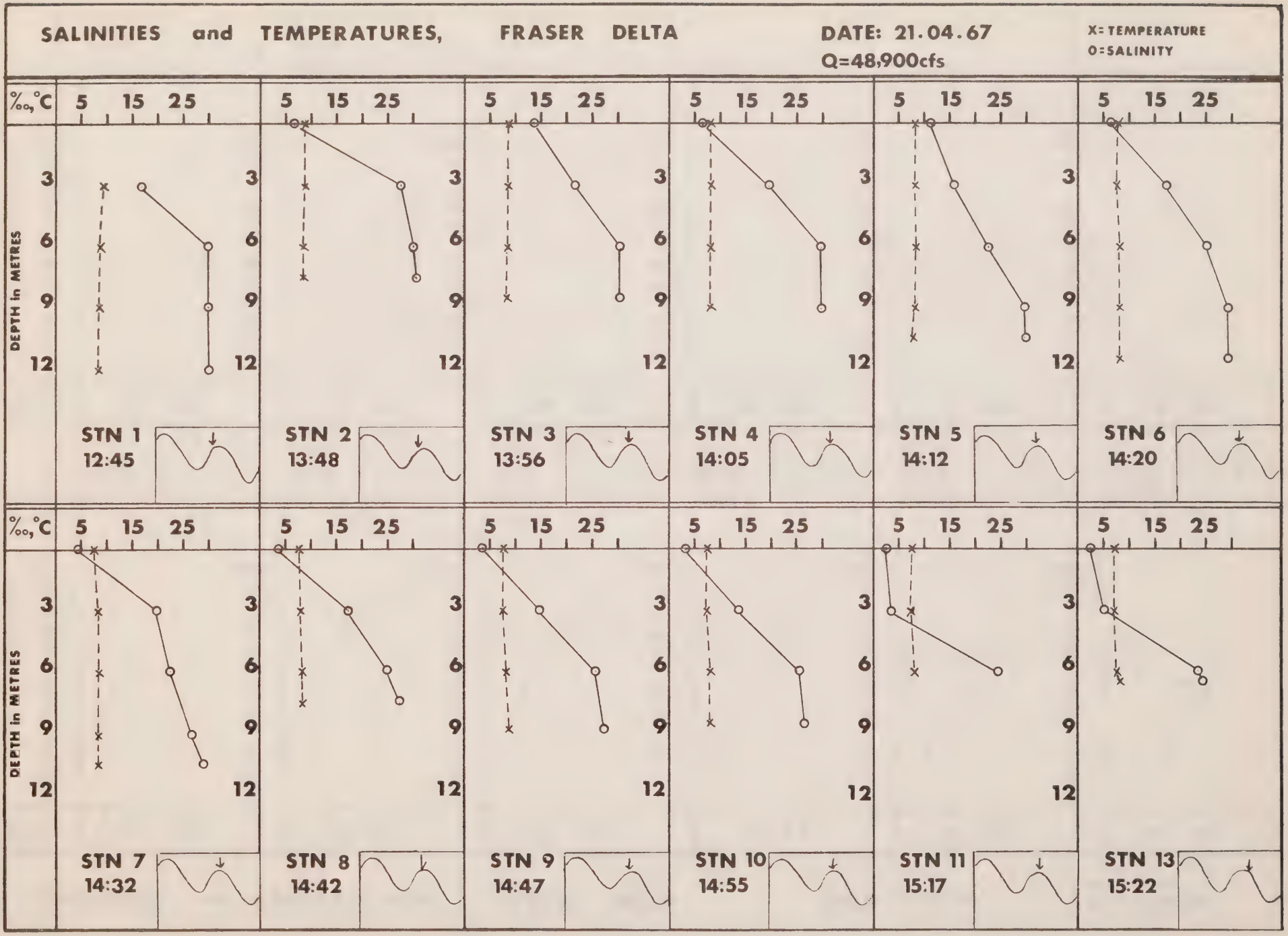

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 11.03.67
Q=34,600cfs
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 27
06:00
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STN 27
08:00
STN 27
09:00
STN 27
10:00
STN 27
11:00
STN 27
12:00
STN
STN
STN
STN
STN

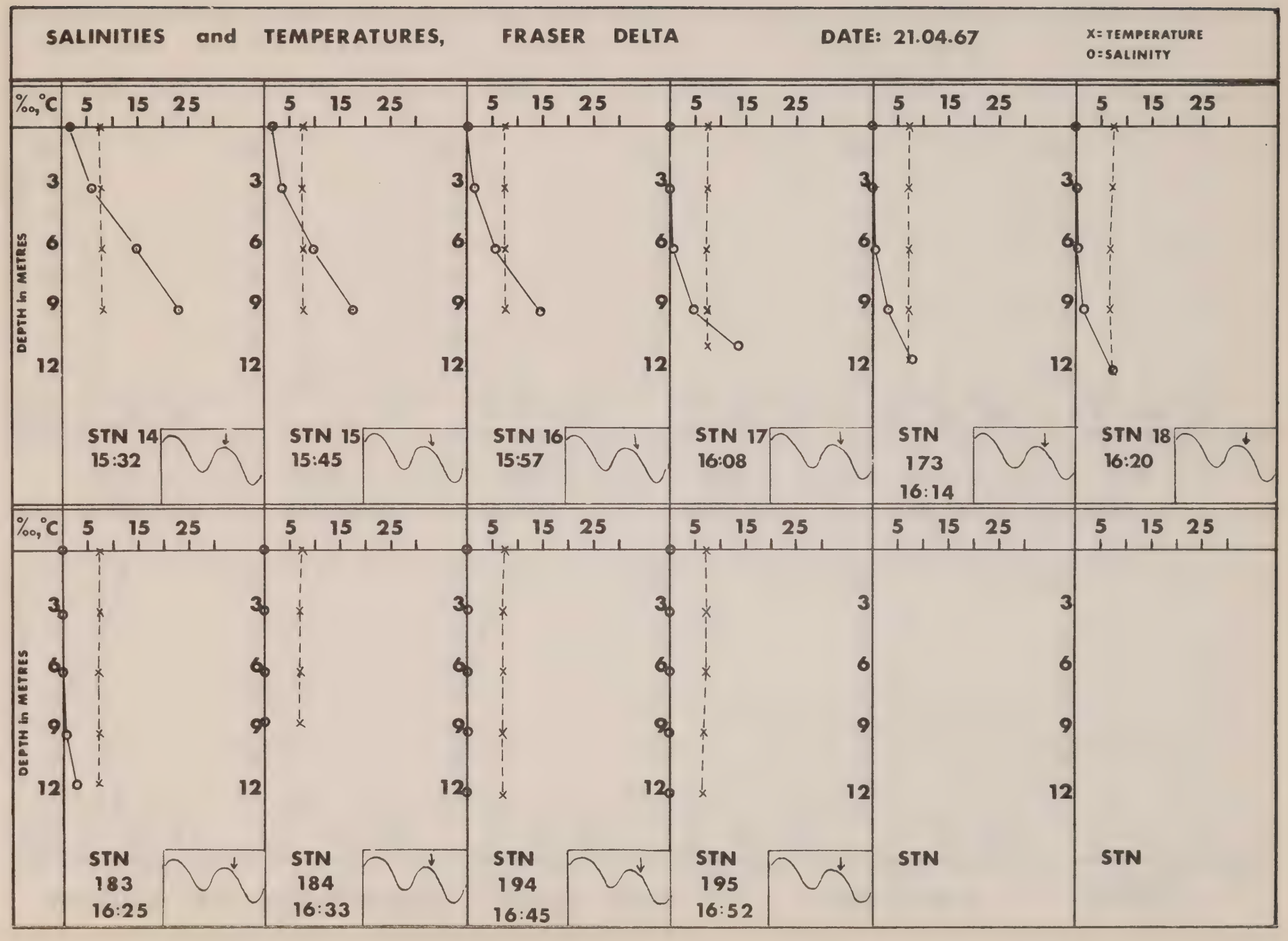

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 11.03.67
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 172
12:12
STN 18
12:25
STN 19
12:42
STN 194
12:51
STN 195
13:01
STN 20
13:09
STN 22
13:48
STN 23
14:06
STN 24
14:44
STN
STN
STN

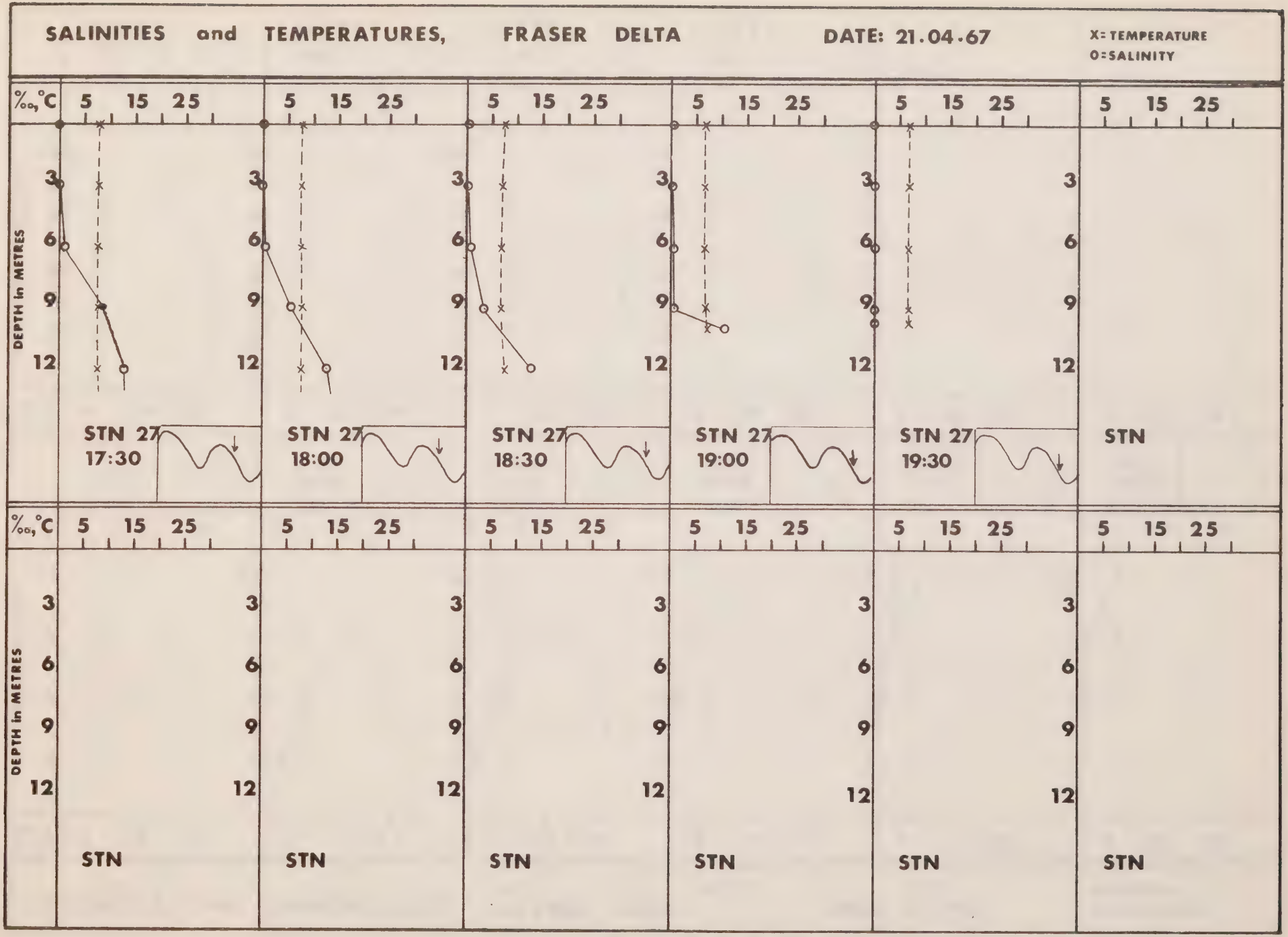

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 12.03.67
Q= 33,000cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 23
08:05
STN 22
08:22
STN
203
08:50
STN 20
08:59
STN
195
09:04
STN
194
09:10
STN
193
09:16
STN 19
09:23
STN
184
09:30
STN
183
09:37
STN 18
09:42
STN
173
09:49

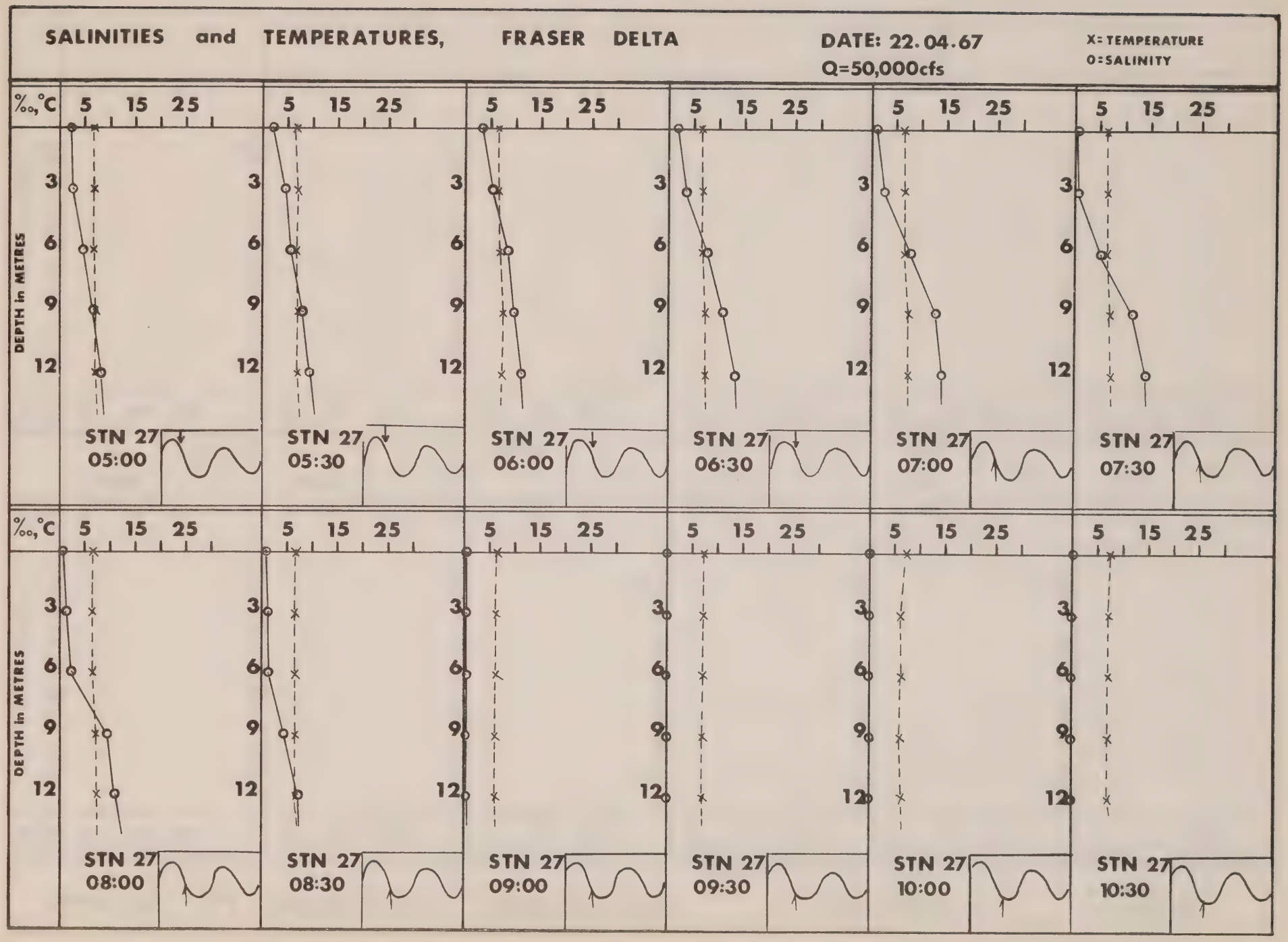

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 12.03.67
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 172 09:55
STN 16 10:03
STN 184 10:37
STN 183 10:44
STN 18 10:50
STN 173 10:58
STN 172 11:04
STN 16 11:12
STN 15 11:22
STN 14 11:31
STN 12 13:03
STN 10 13:11


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 12.03.67
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 8
13:19
STN 7
13:27
STN 6
13:32
STN 5
13:37
STN 4
13:43
STN 3
13:48
STN 2
13:55
STN 1
14:00
STN
STN
STN
STN


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 21.04.67
Q=48,900cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 1
12:45
STN 2
13:48
STN 3
13:56
STN 4
14:05
STN 5
14:12
STN 6
14:20
STN 7
14:32
STN 8
14:42
STN 9
14:47
STN 10
14:55
STN 11
15:17
STN 13
15:22


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 21.04.67
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 14
15:32
STN 15
15:45
STN 16
15:57
STN 17
16:08
STN
173
16:14
STN 18
16:20
STN
183
16:25
STN
184
16:33
STN
194
16:45
STN
195
16:52
STN
STN


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 21.04.67
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 27
17:30
STN 27
18:00
STN 27
18:30
STN 27
19:00
STN 27
19:30
STN
STN
STN
STN
STN
STN


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 22.04.67
Q=50,000cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 27
05:00
STN 27
05:30
STN 27
06:00
STN 27
06:30
STN 27
07:00
STN 27
07:30
STN 27
08:00
STN 27
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STN 27
09:00
STN 27
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STN 27
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STN 27
10:30

SALINITIES and TEMPERATURES, FRASER DELTA DATE: 22.04.67

X = TEMPERATURE
O = SALINITY

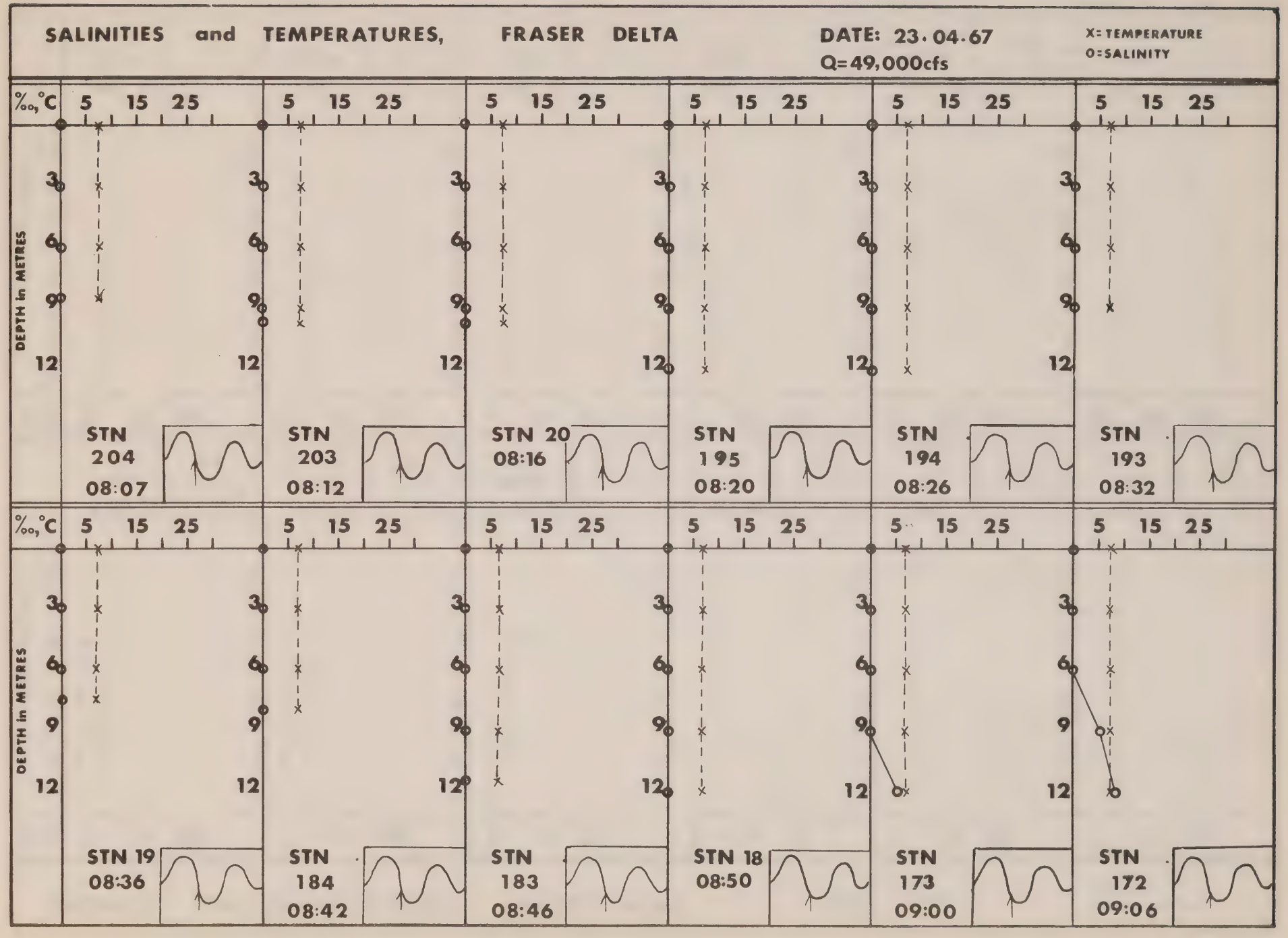
‰, °C 5 15 25

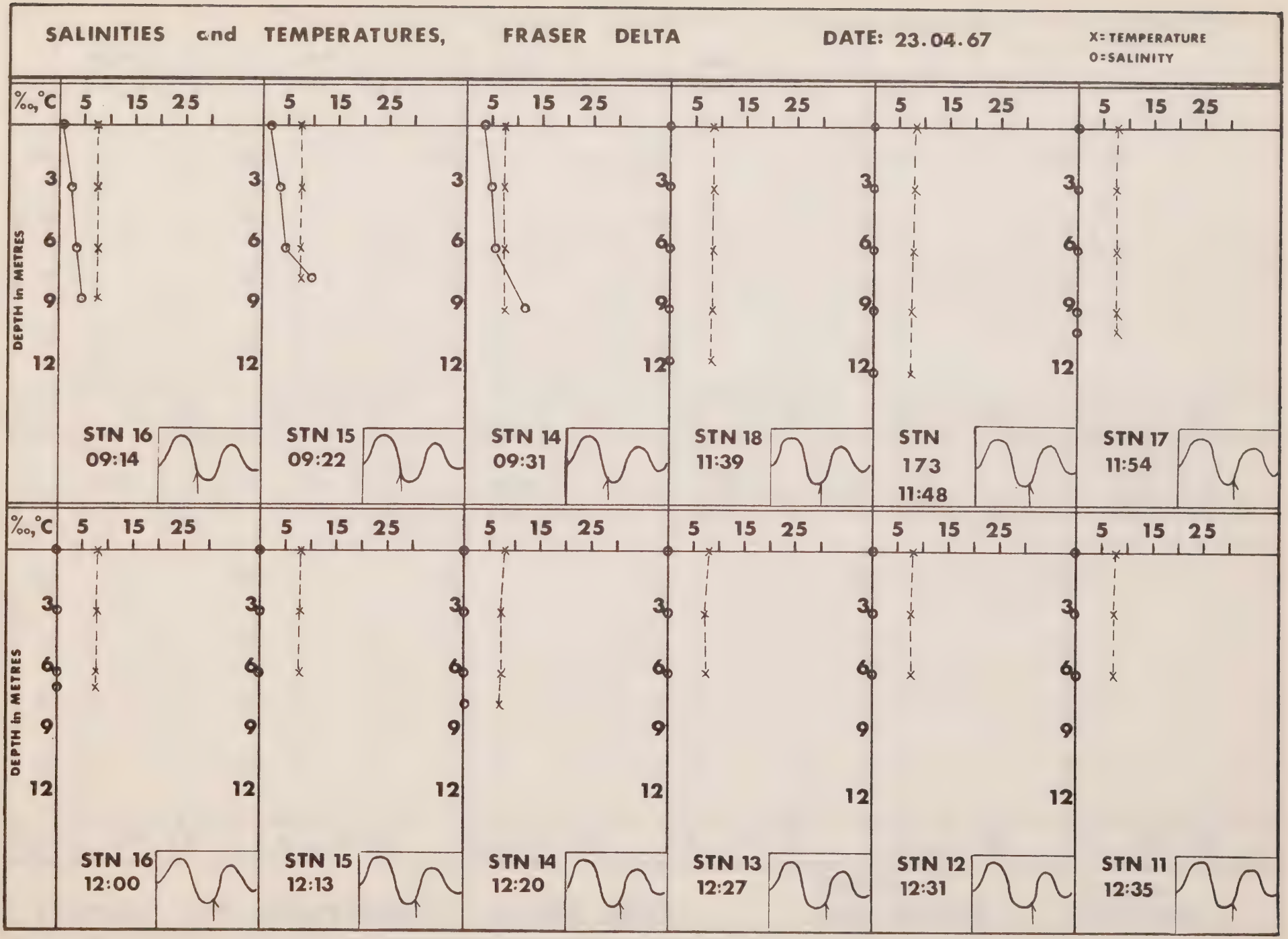
DEPTH in METRES 3 6 9 12

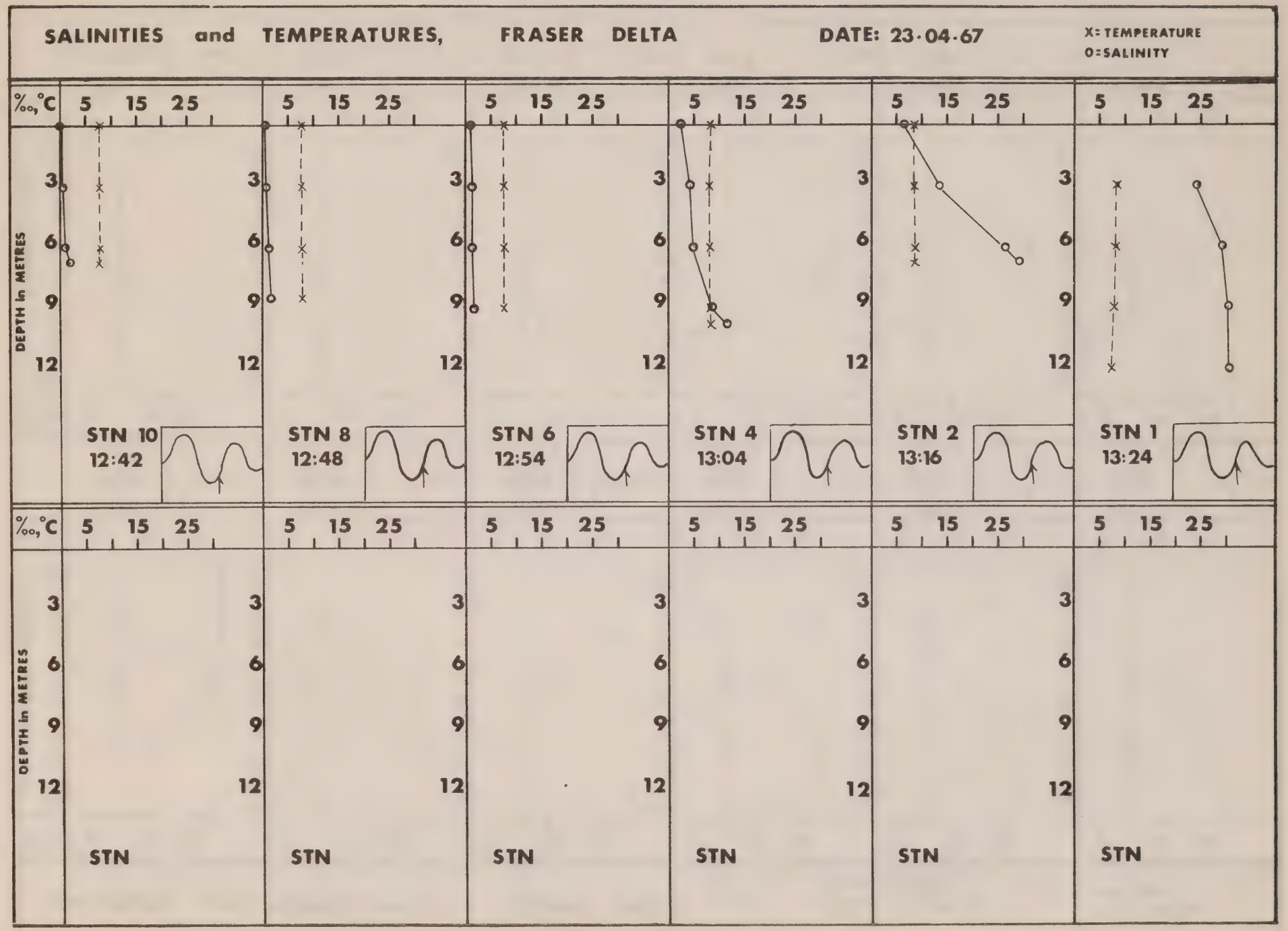
STN 27 11:00

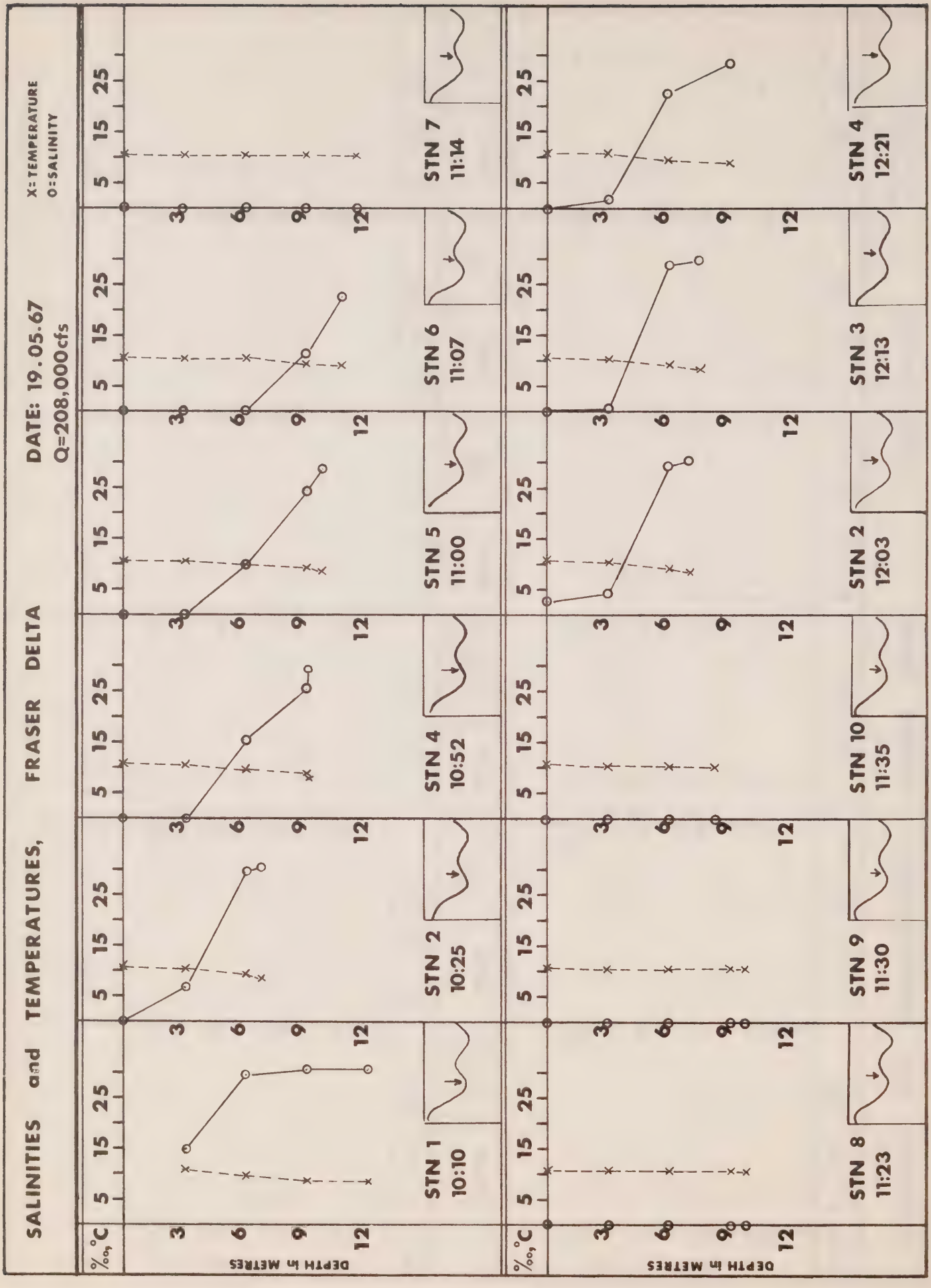
STN 27 11:30

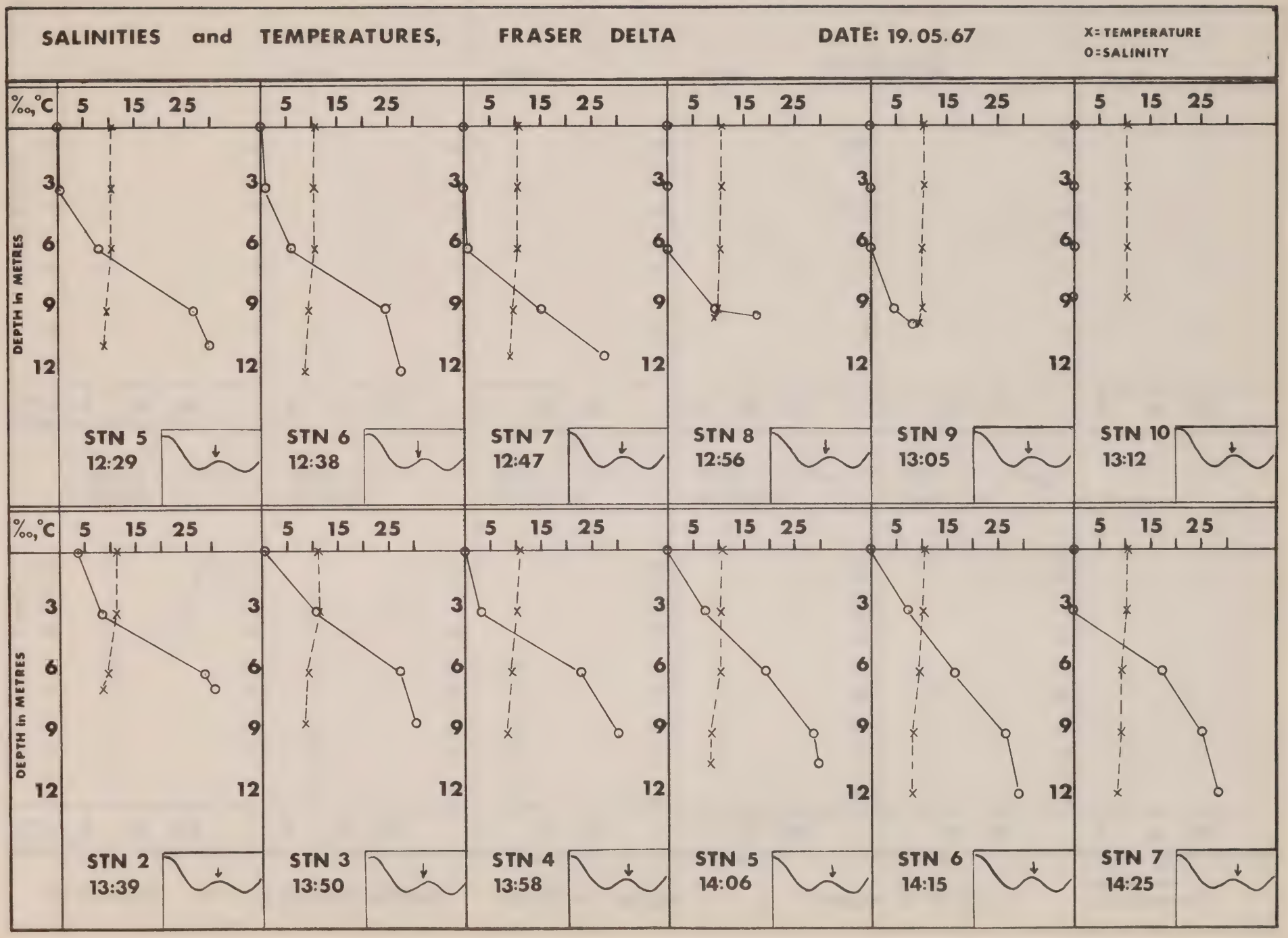
STN

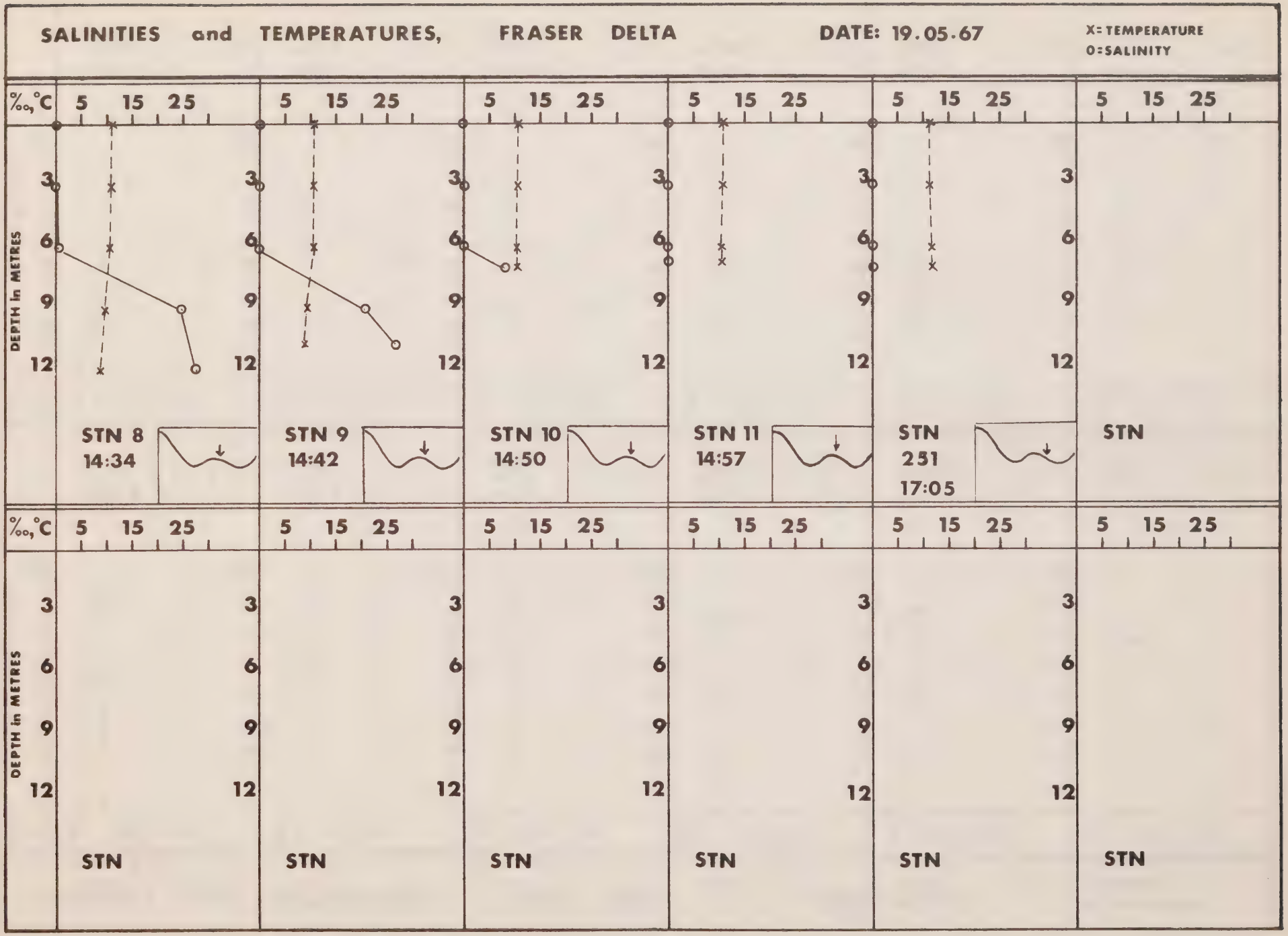

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 23.04.67
Q=49,000cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 204 08:07
STN 203 08:12
STN 20 08:16
STN 195 08:20
STN 194 08:26
STN 193 08:32
STN 19 08:36
STN 184 08:42
STN 183 08:46
STN 18 08:50
STN 173 09:00
STN 172 09:06

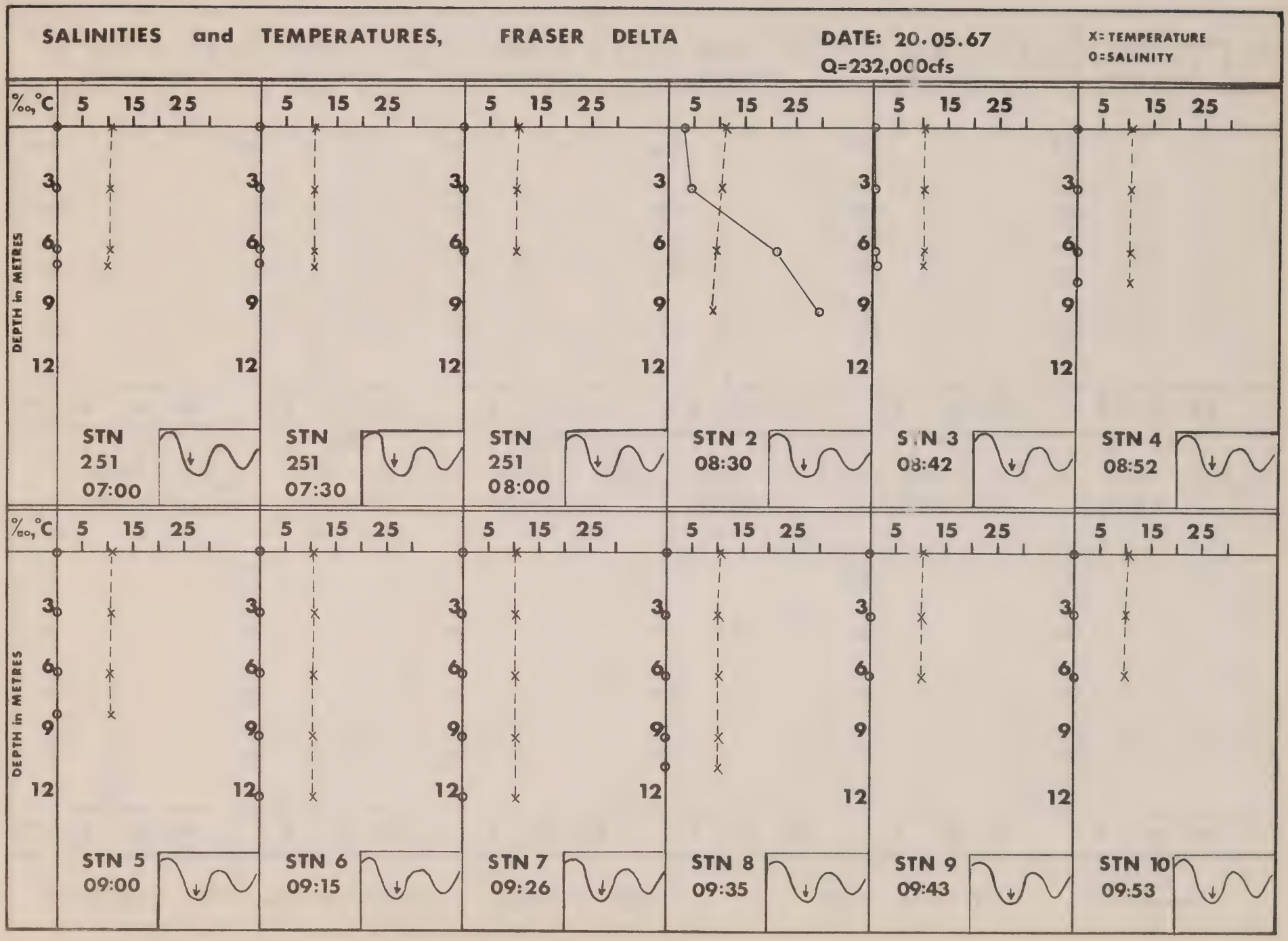

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 23.04.67
X = TEMPERATURE
O = SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 16
09:14
STN 15
09:22
STN 14
09:31
STN 18
11:39
STN
173
11:48
STN 17
11:54
STN 16
12:00
STN 15
12:13
STN 14
12:20
STN 13
12:27
STN 12
12:31
STN 11
12:35

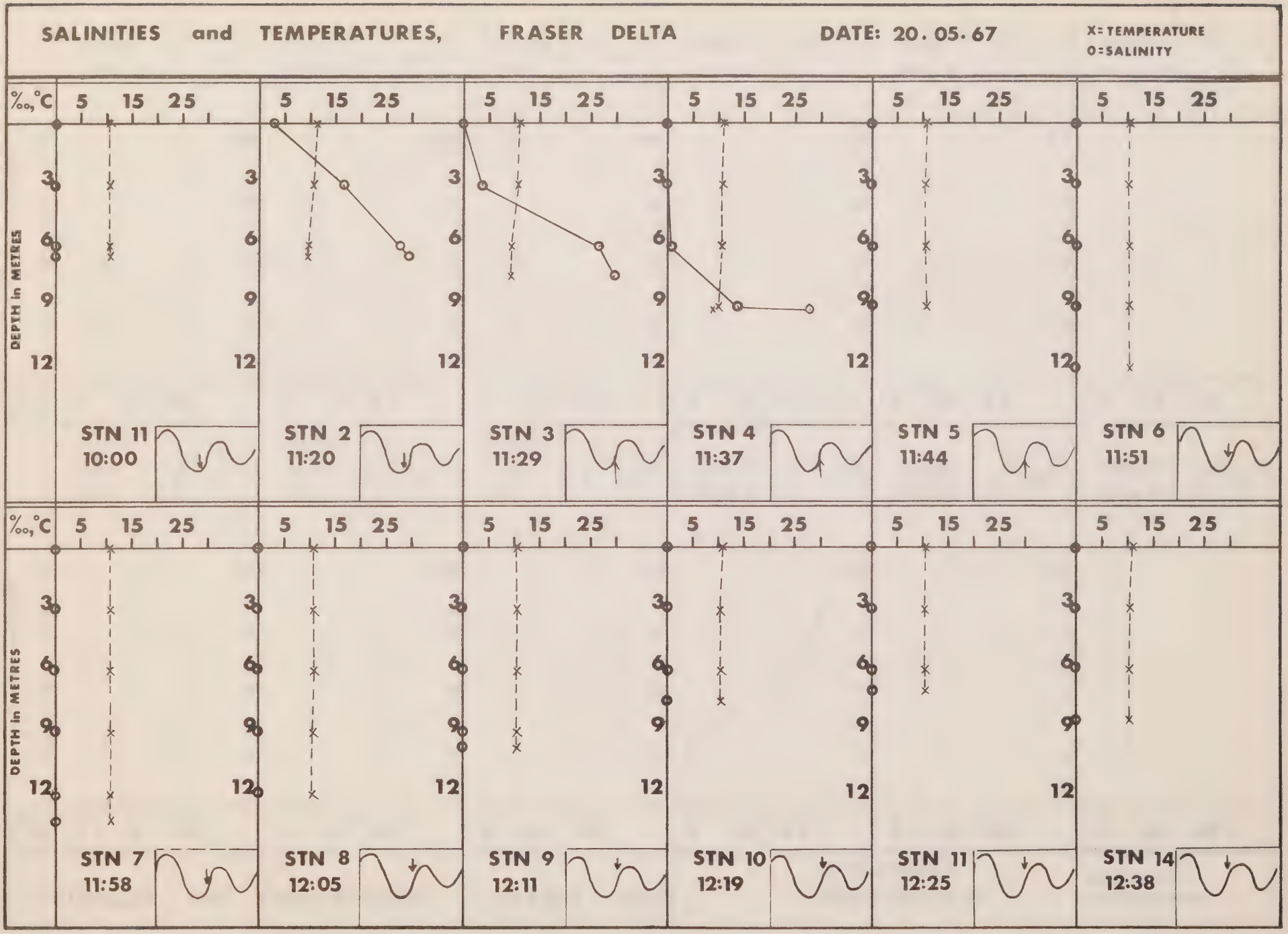

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 23·04·67
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 10
12:42
STN 8
12:48
STN 6
12:54
STN 4
13:04
STN 2
13:16
STN 1
13:24
STN

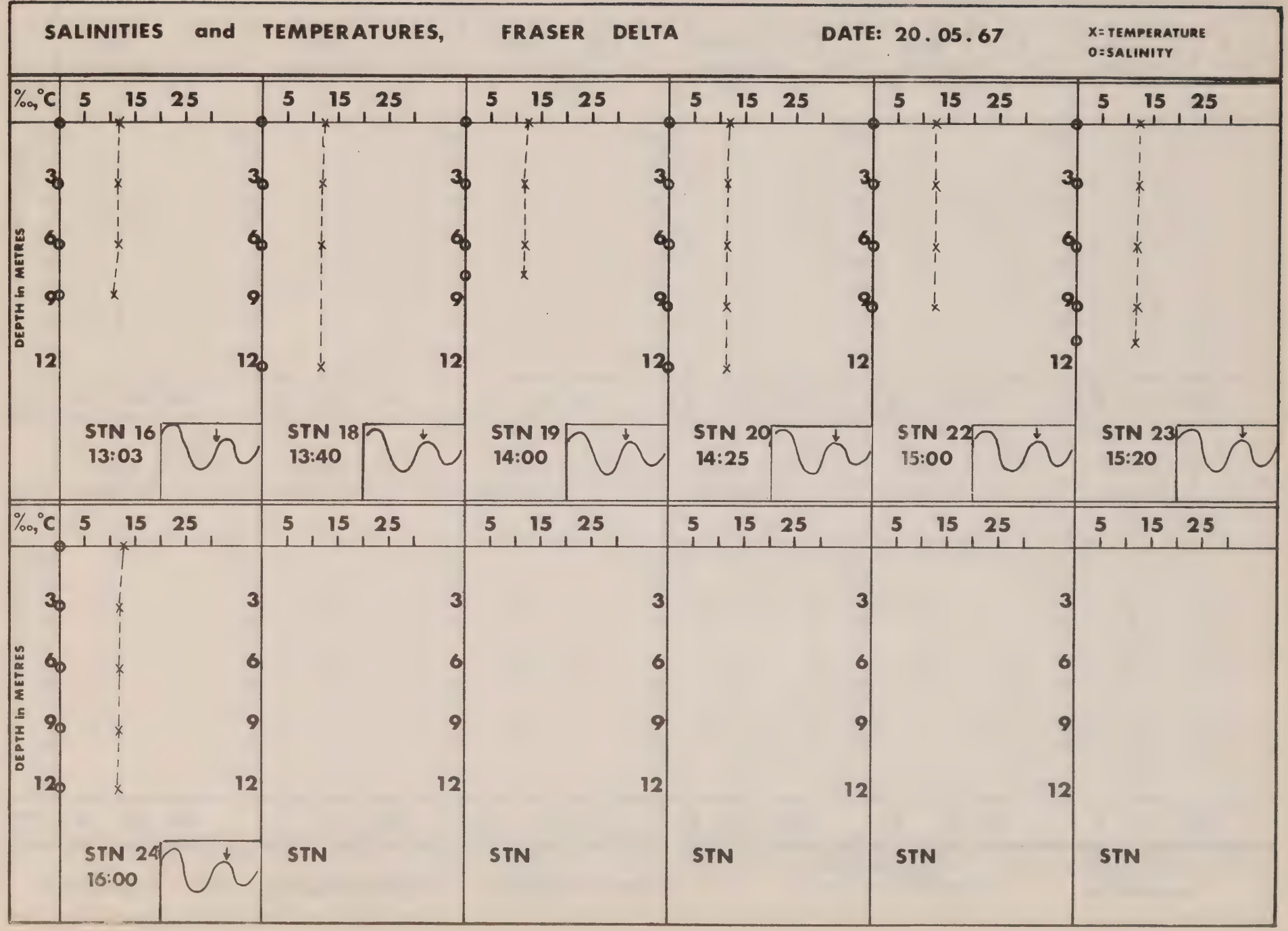

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 19.05.67
Q=208,000cfs
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3 6 9 12
STN 1 10:10
STN 2 10:25
STN 4 10:52
STN 5 11:00
STN 6 11:07
STN 7 11:14
STN 8 11:23
STN 9 11:30
STN 10 11:35
STN 2 12:03
STN 3 12:13
STN 4 12:21

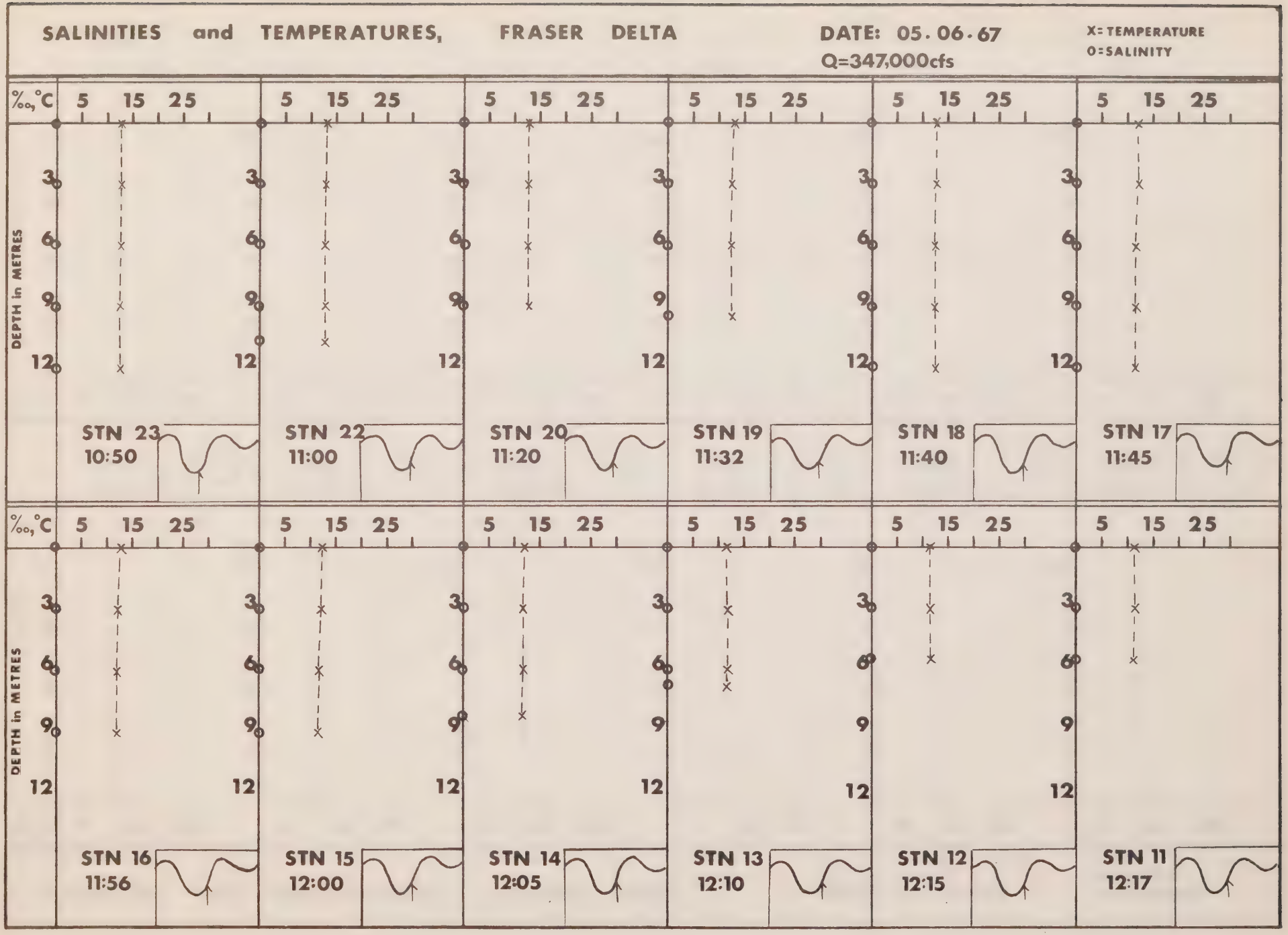

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 19.05.67
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 5
12:29
STN 6
12:38
STN 7
12:47
STN 8
12:56
STN 9
13:05
STN 10
13:12
STN 2
13:39
STN 3
13:50
STN 4
13:58
STN 5
14:06
STN 6
14:15
STN 7
14:25

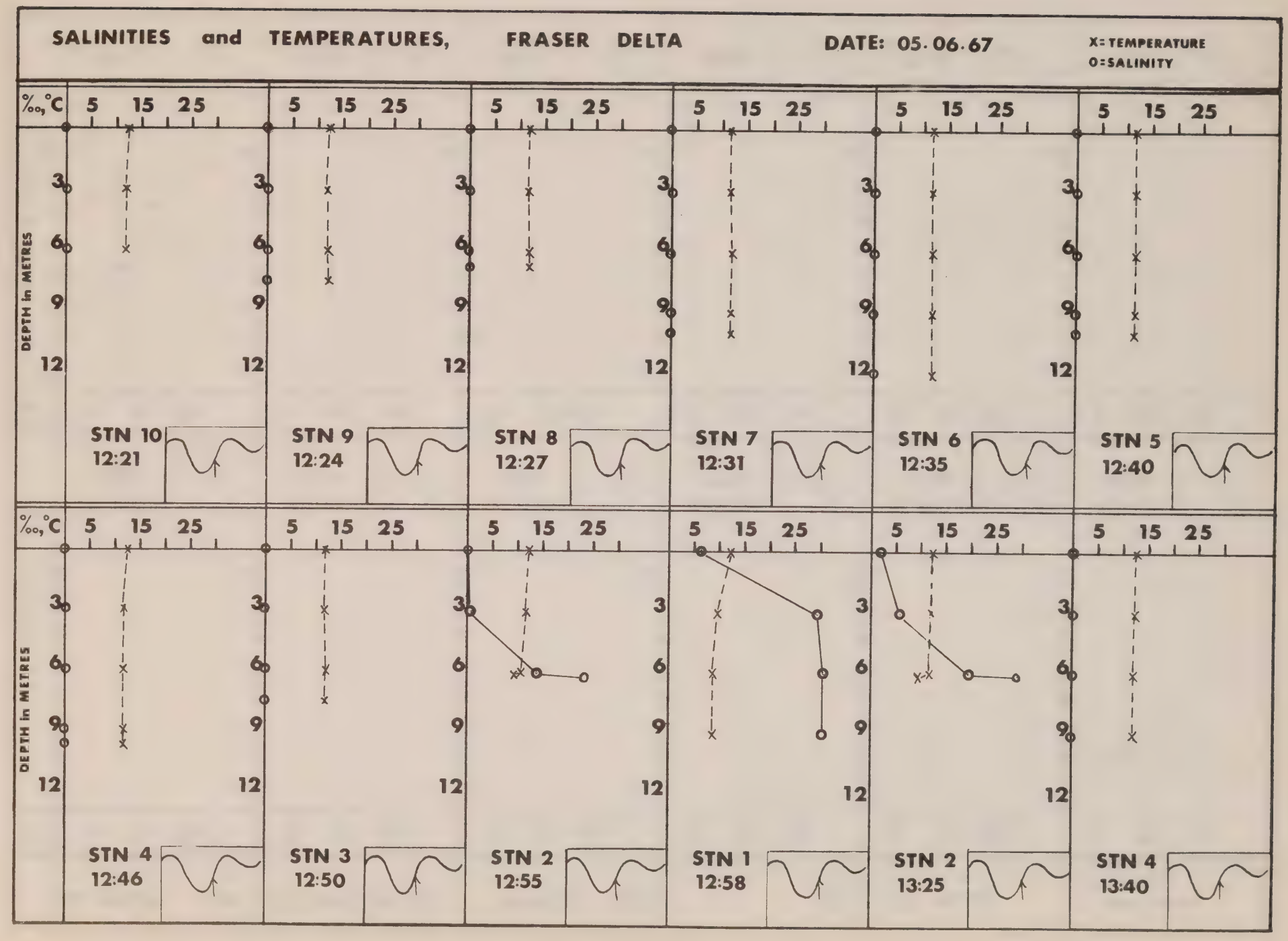

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 19.05.67
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 8
14:34
STN 9
14:42
STN 10
14:50
STN 11
14:57
STN
251
17:05
STN

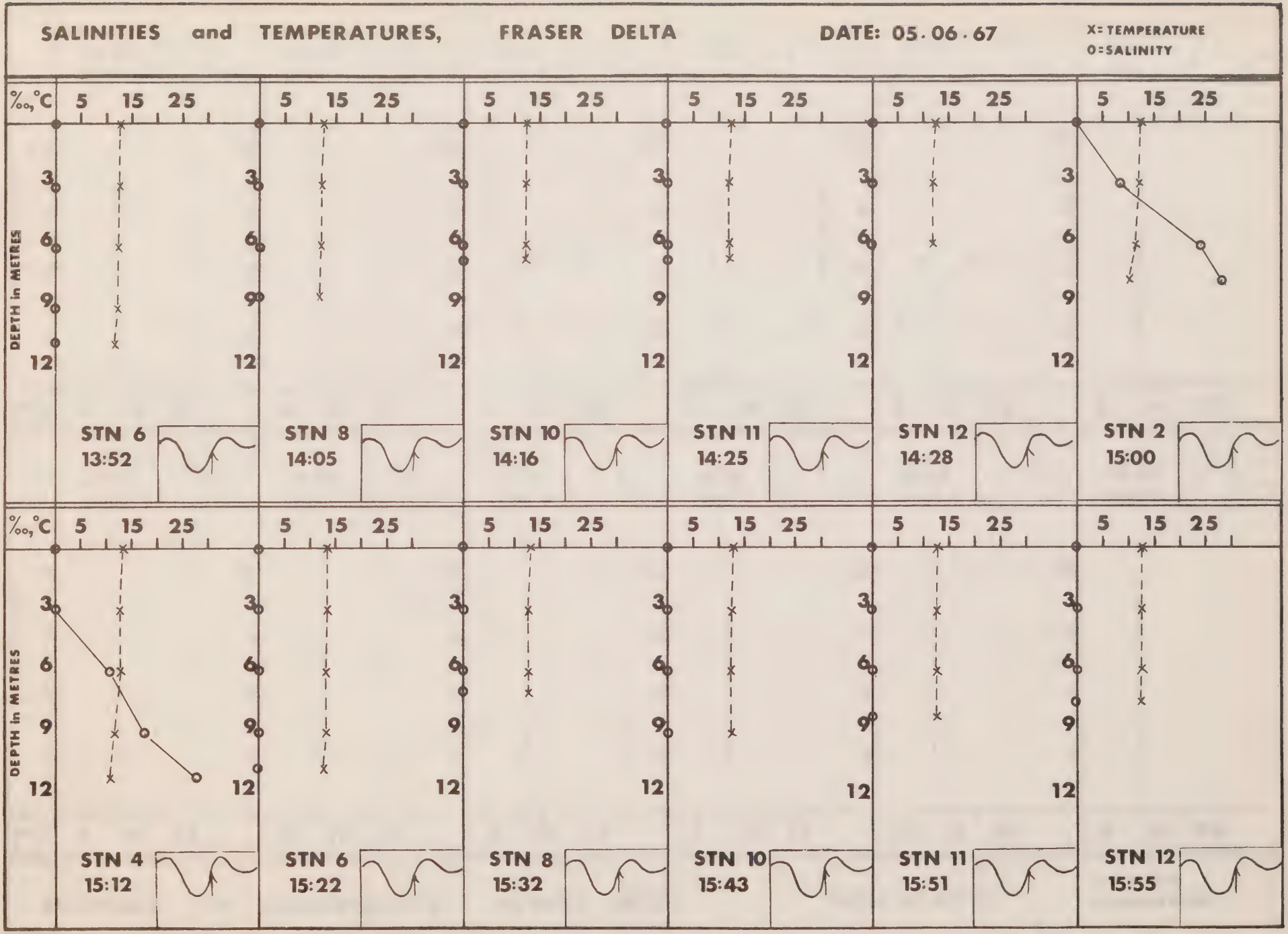

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 20.05.67
Q=232,000cfs
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 251 07:00
STN 251 07:30
STN 251 08:00
STN 2 08:30
STN 3 08:42
STN 4 08:52
STN 5 09:00
STN 6 09:15
STN 7 09:26
STN 8 09:35
STN 9 09:43
STN 10 09:53


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 20.05.67
X = TEMPERATURE
O = SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 11
10:00
STN 2
11:20
STN 3
11:29
STN 4
11:37
STN 5
11:44
STN 6
11:51
STN 7
11:58
STN 8
12:05
STN 9
12:11
STN 10
12:19
STN 11
12:25
STN 14
12:38


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 20.05.67
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 16
13:03
STN 18
13:40
STN 19
14:00
STN 20
14:25
STN 22
15:00
STN 23
15:20
STN 24
16:00
STN

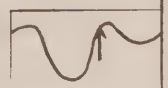

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 05.06.67
Q=347,000cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 23
10:50
STN 22
11:00
STN 20
11:20
STN 19
11:32
STN 18
11:40
STN 17
11:45
STN 16
11:56
STN 15
12:00
STN 14
12:05
STN 13
12:10
STN 12
12:15
STN 11
12:17

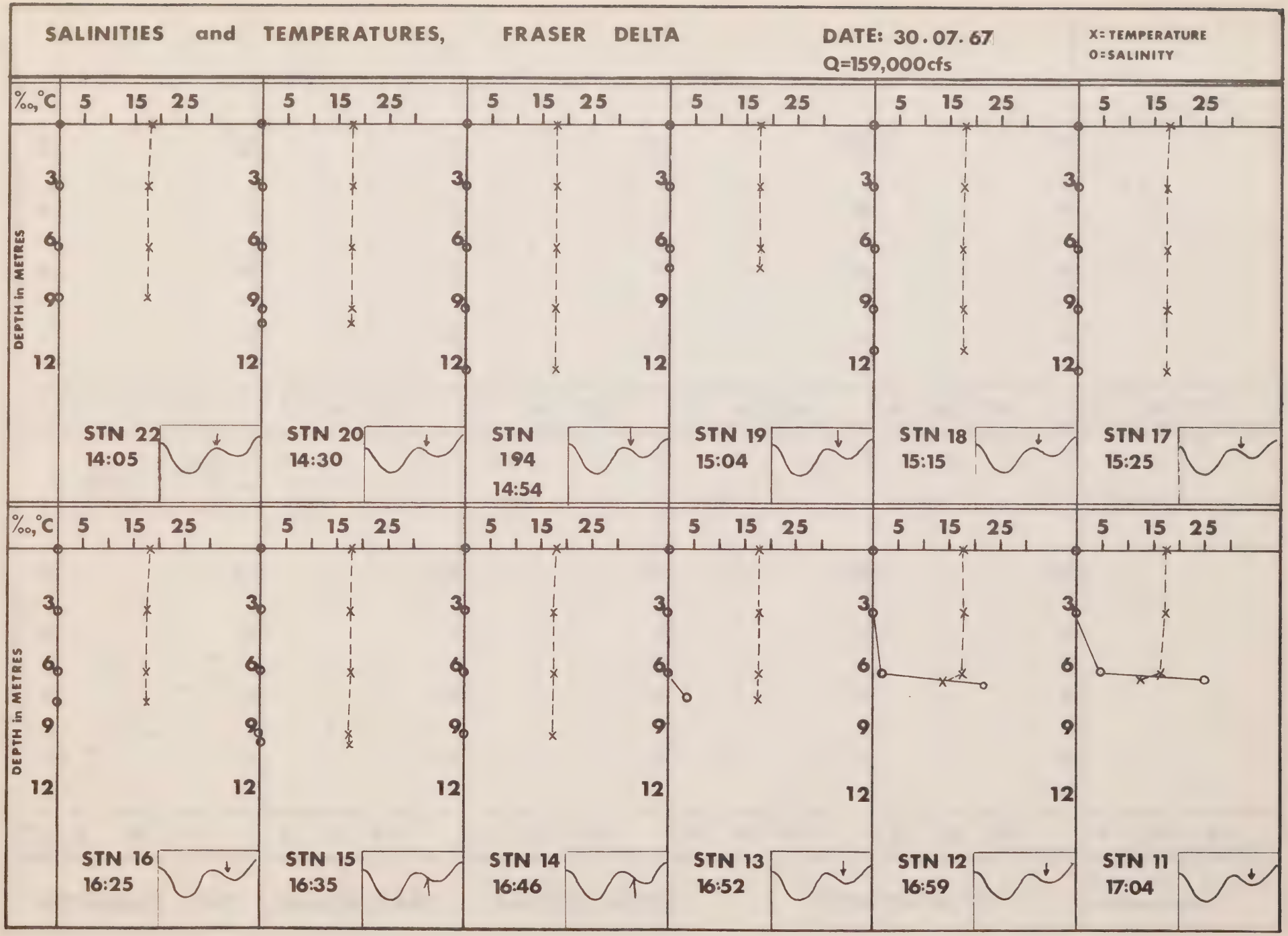

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 05.06.67
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 10
12:21
STN 9
12:24
STN 8
12:27
STN 7
12:31
STN 6
12:35
STN 5
12:40
STN 4
12:46
STN 3
12:50
STN 2
12:55
STN 1
12:58
STN 2
13:25
STN 4
13:40

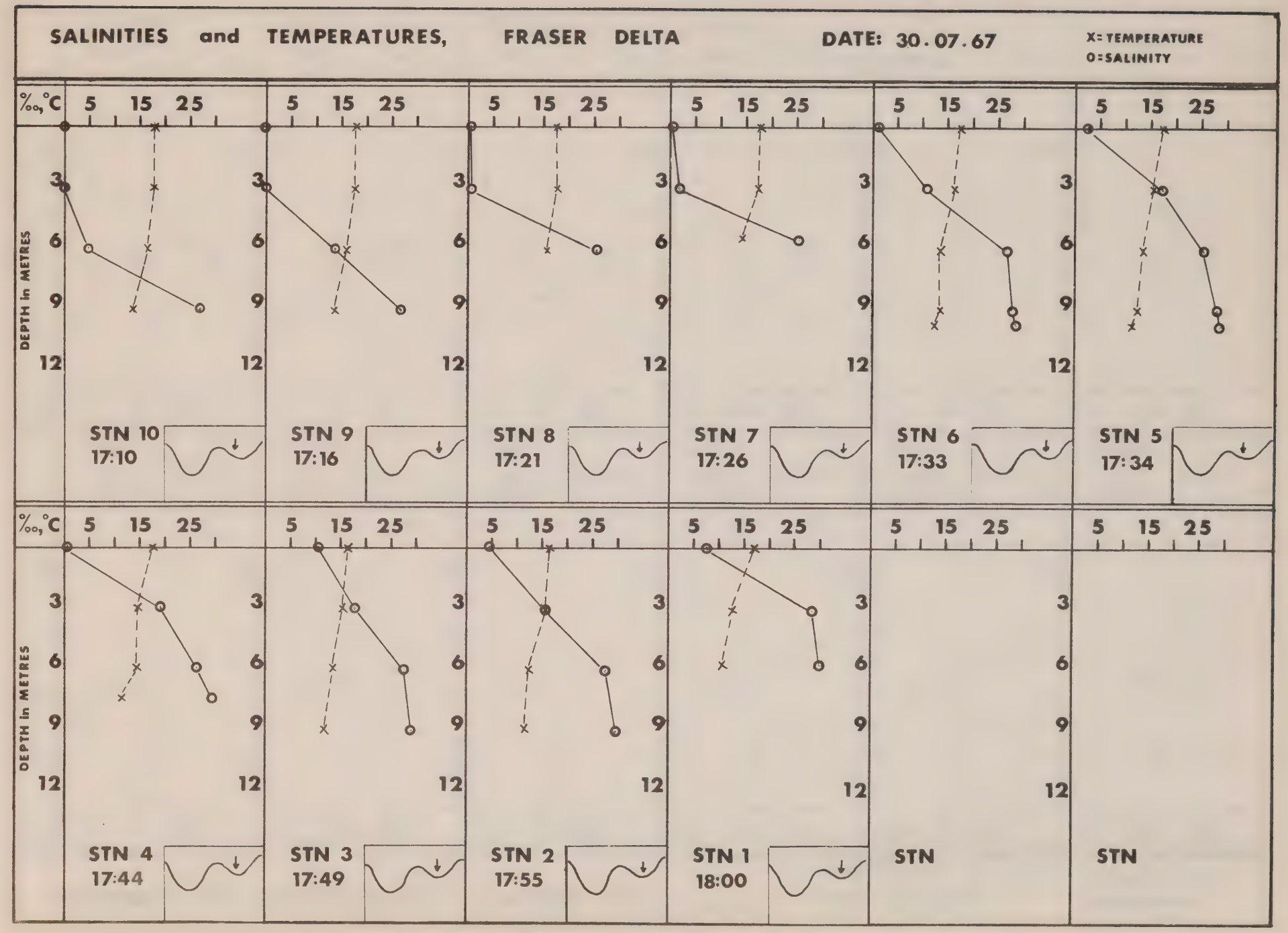

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 05.06.67
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 6
13:52
STN 8
14:05
STN 10
14:16
STN 11
14:25
STN 12
14:28
STN 2
15:00
STN 4
15:12
STN 6
15:22
STN 8
15:32
STN 10
15:43
STN 11
15:51
STN 12
15:55

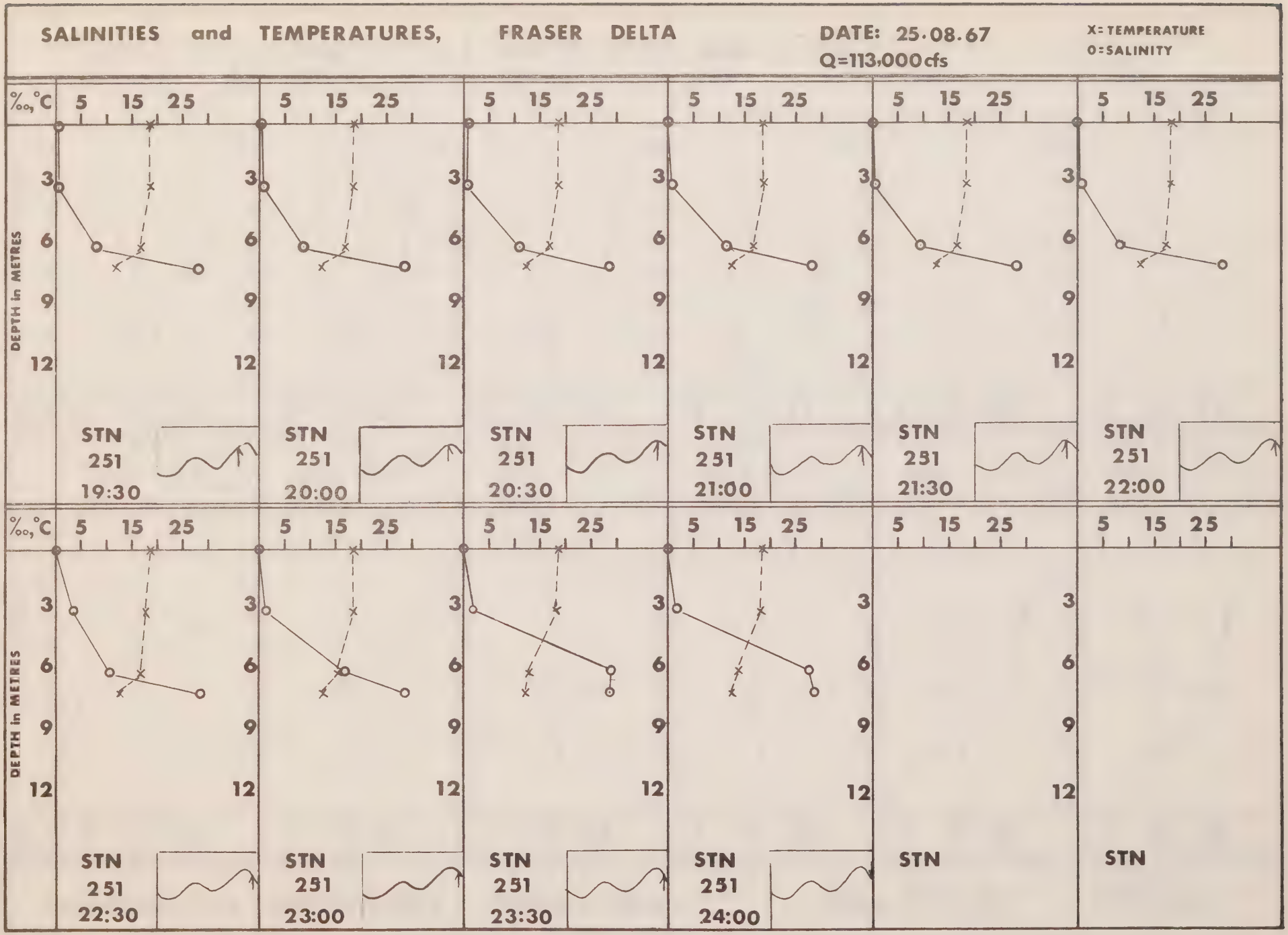
SALINITIES and TEMPERATURES, FRASER DELTA **DATE: 05 · 06 · 67**

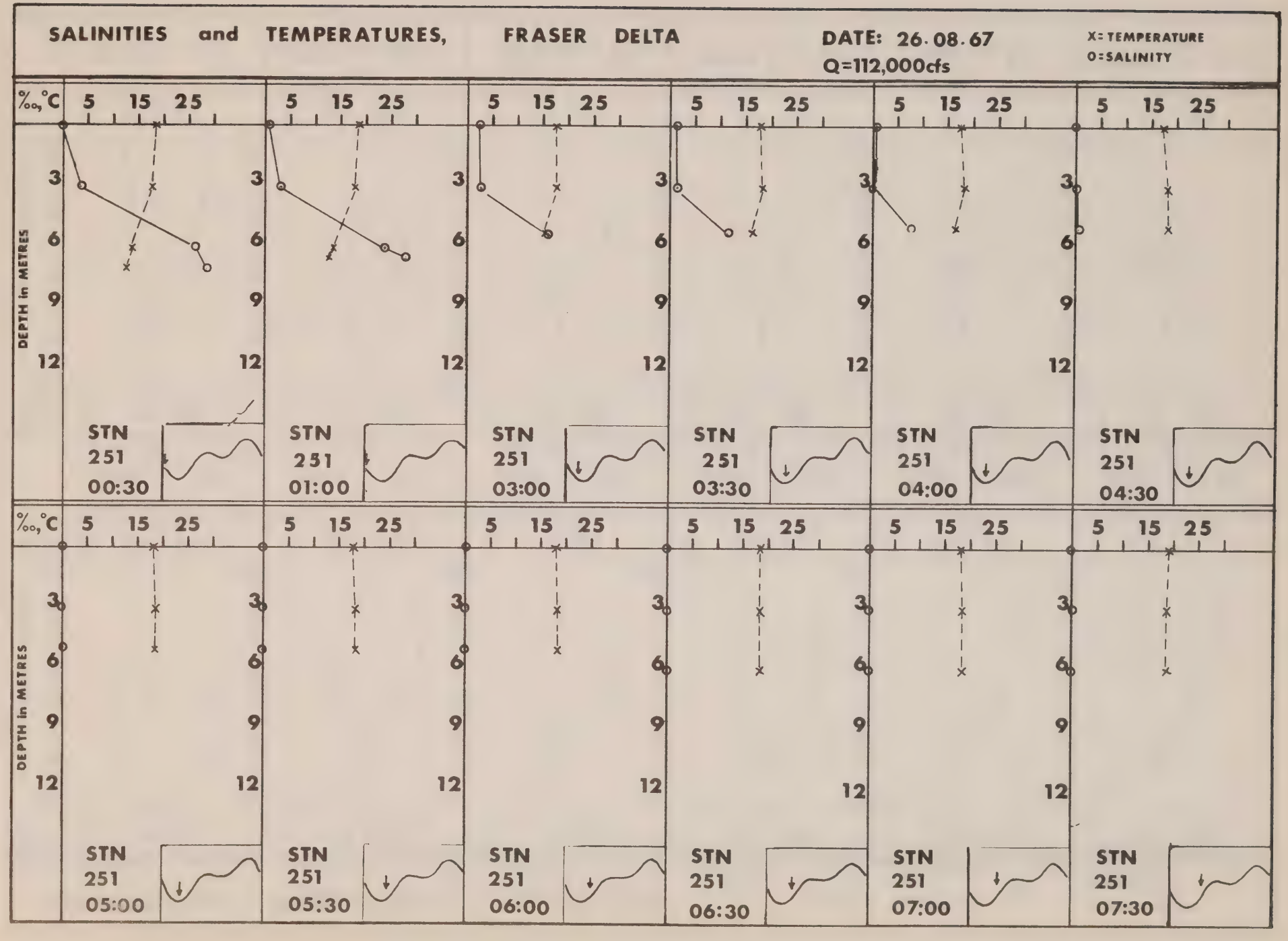
X = TEMPERATURE
O = SALINITY

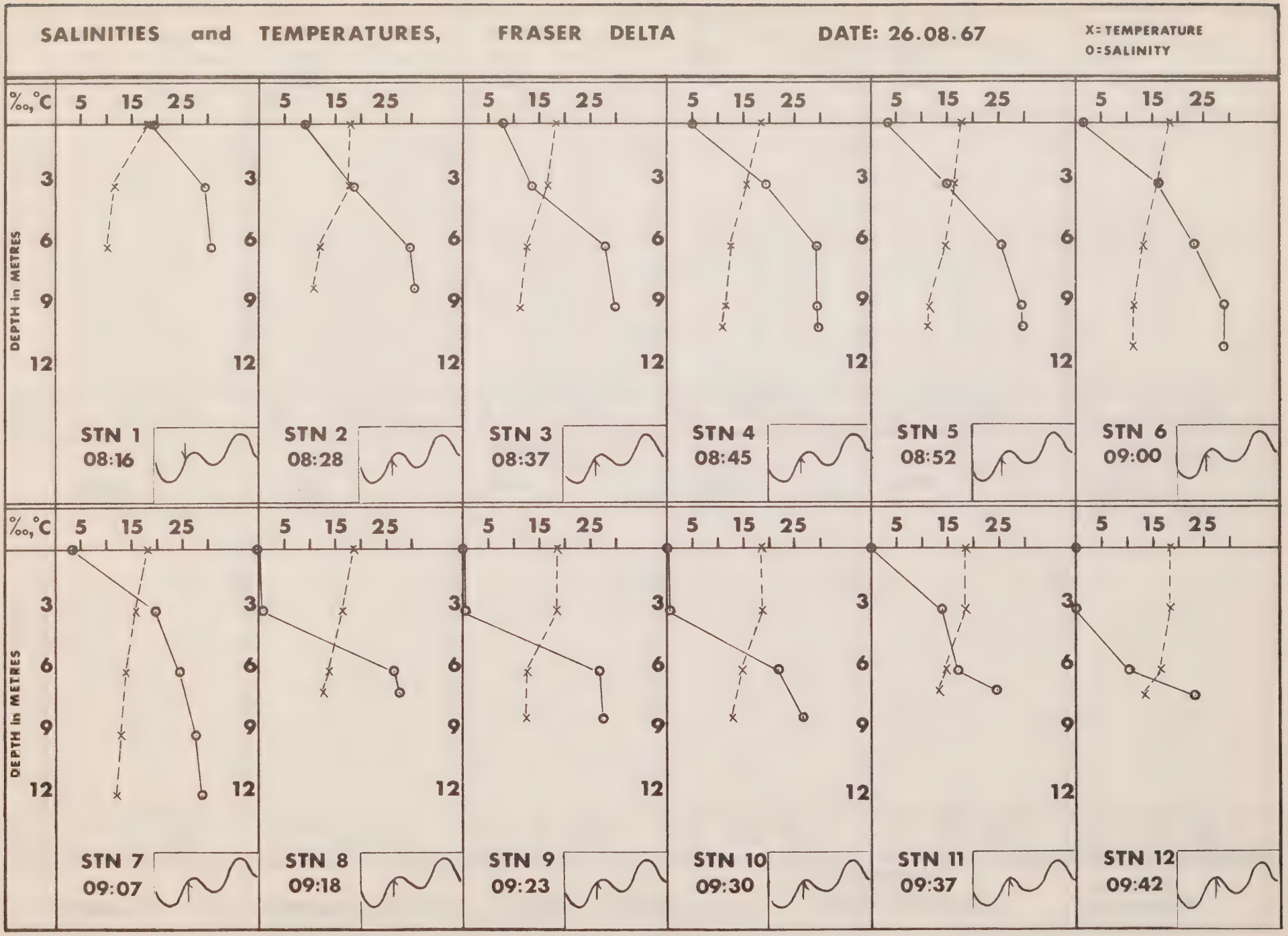
‰, °C	5 15 25	5 15 25	5 15 25	5 15 25	5 15 25	5 15 25
DEPTH in METRES	3 6 9 12	3 6 9 12	3 6 9 12	3 6 9 12	3 6 9 12	3 6 9 12
	STN 2 16:47 	STN	STN	STN	STN	STN
‰, °C	5 15 25	5 15 25	5 15 25	5 15 25	5 15 25	5 15 25
DEPTH in METRES	3 6 9 12	3 6 9 12	3 6 9 12	3 6 9 12	3 6 9 12	3 6 9 12
	STN	STN	STN	STN	STN	STN

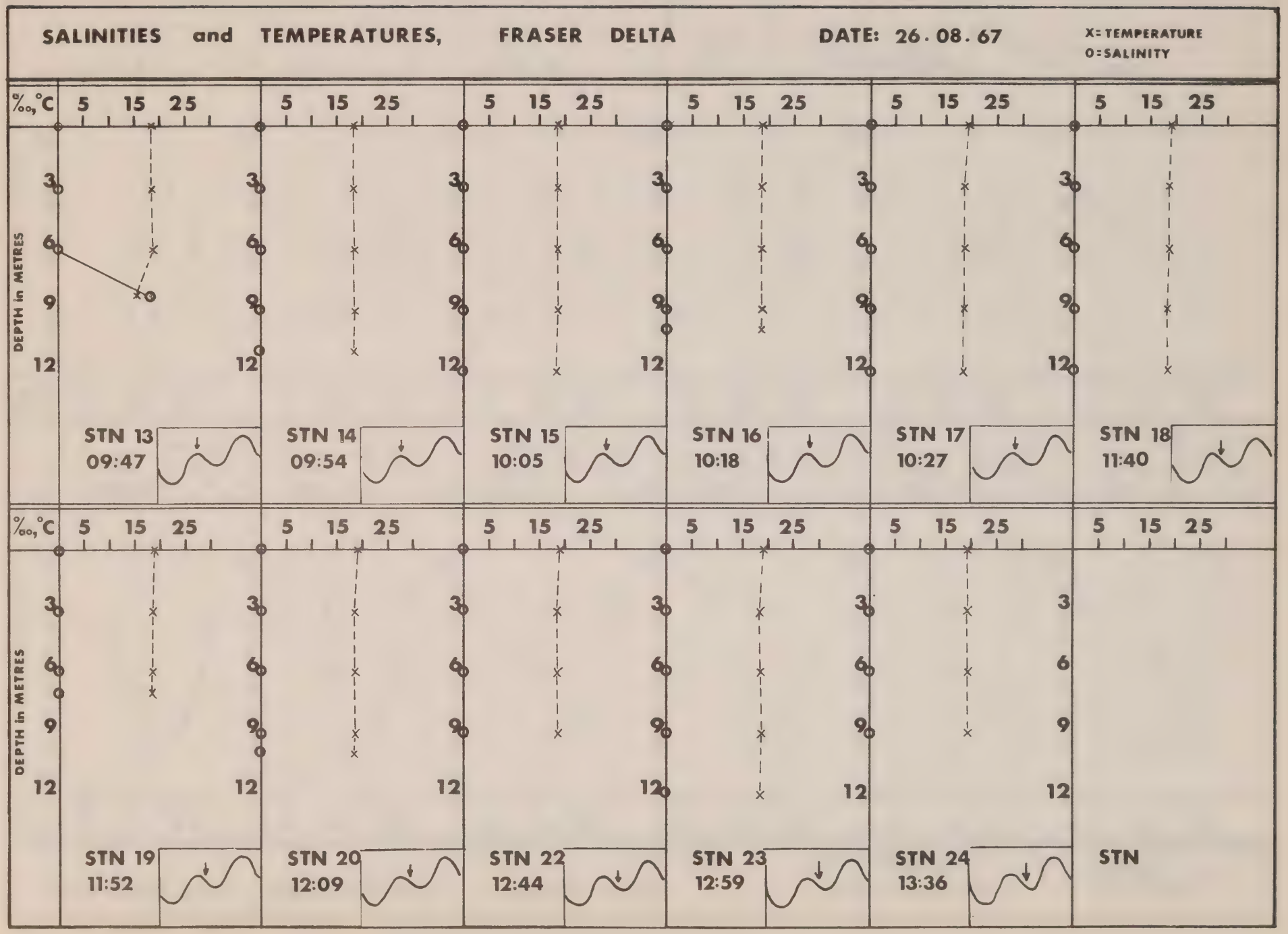

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 30.07.67
Q=159,000cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 22
14:05
STN 20
14:30
STN
194
14:54
STN 19
15:04
STN 18
15:15
STN 17
15:25
STN 16
16:25
STN 15
16:35
STN 14
16:46
STN 13
16:52
STN 12
16:59
STN 11
17:04

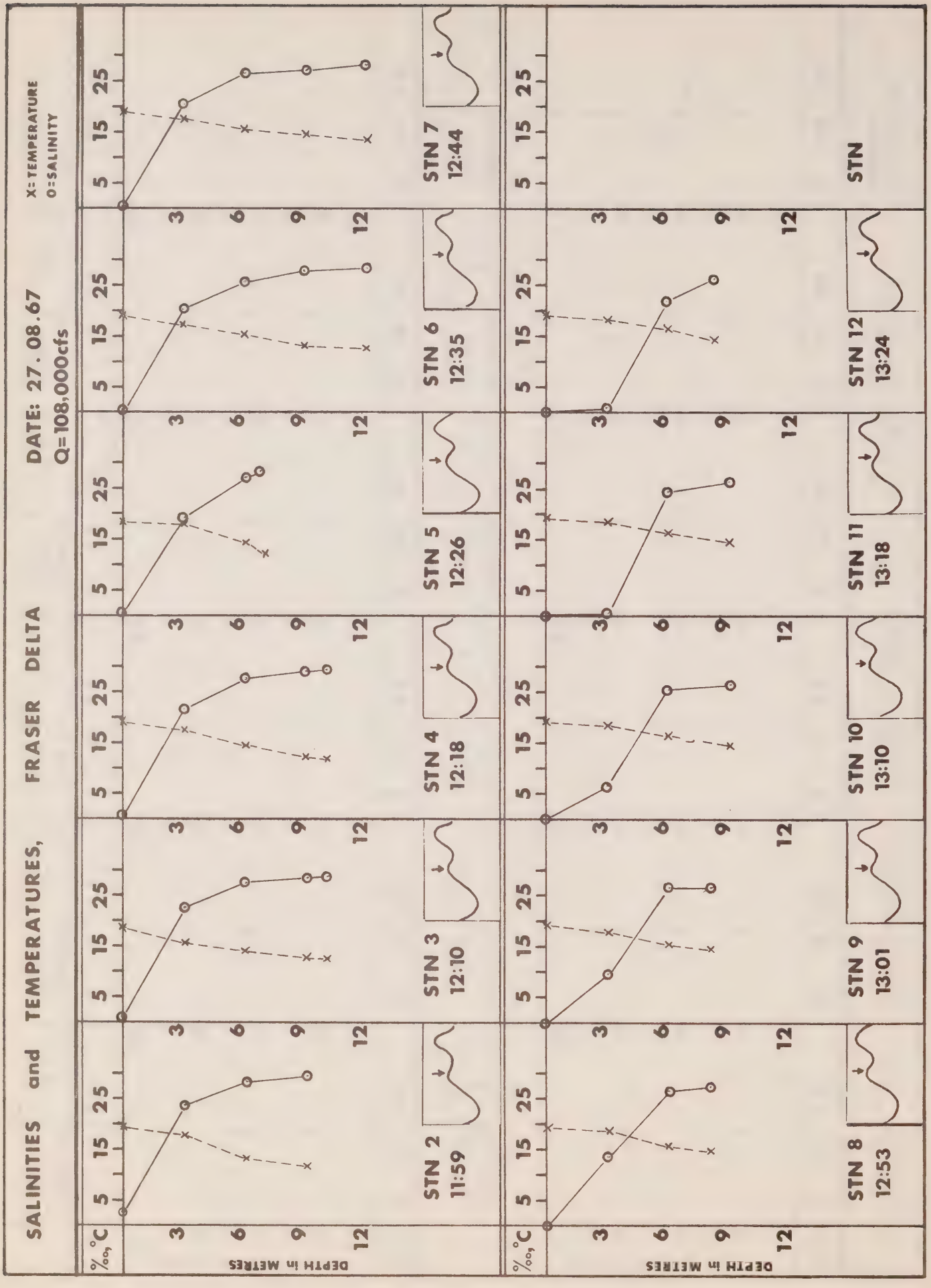

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 30.07.67
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 10
17:10
STN 9
17:16
STN 8
17:21
STN 7
17:26
STN 6
17:33
STN 5
17:34
STN 4
17:44
STN 3
17:49
STN 2
17:55
STN 1
18:00
STN
STN

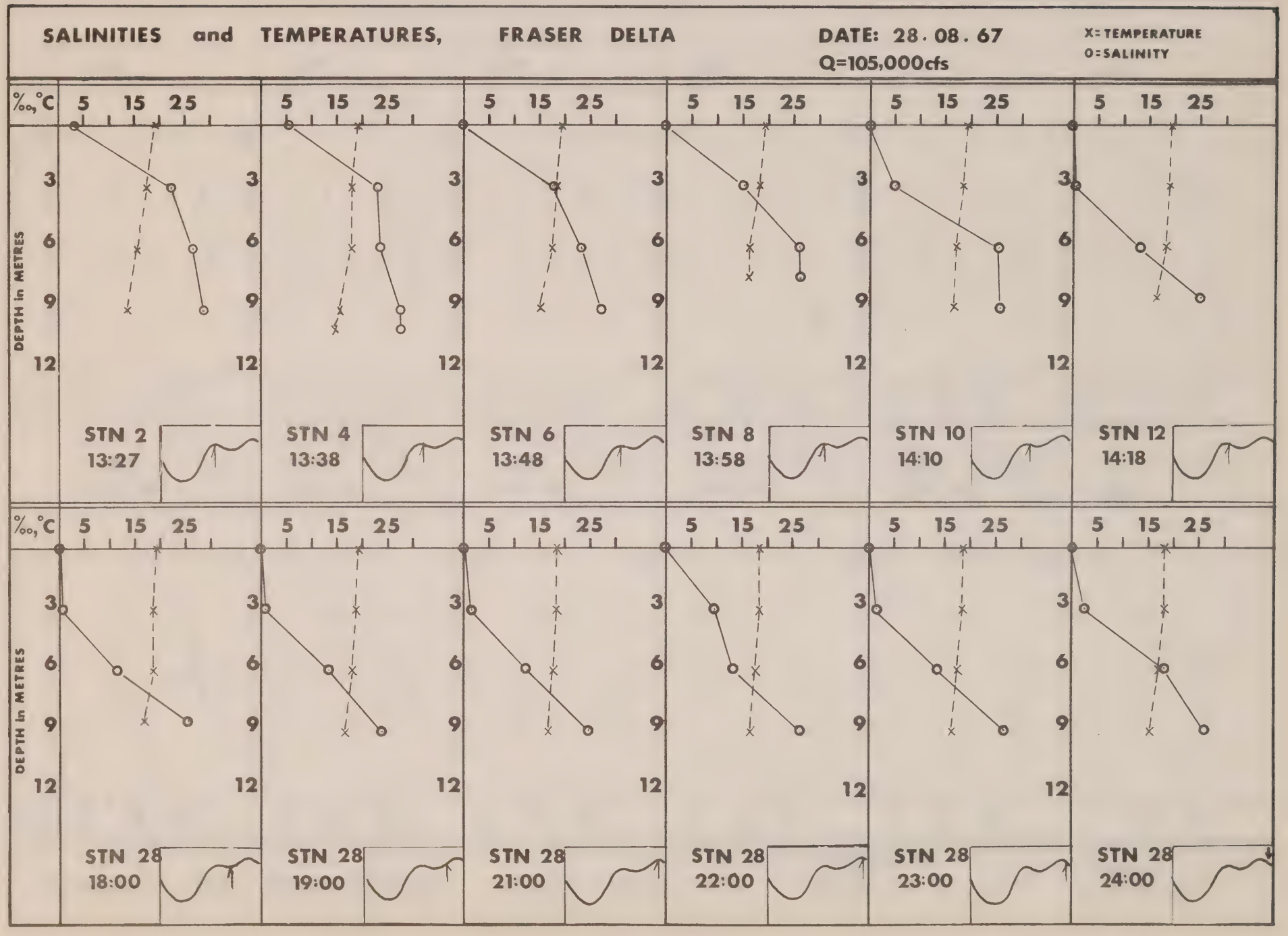

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 25.08.67
Q=113,000cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 251 19:30
STN 251 20:00
STN 251 20:30
STN 251 21:00
STN 251 21:30
STN 251 22:00
STN 251 22:30
STN 251 23:00
STN 251 23:30
STN 251 24:00
STN
STN

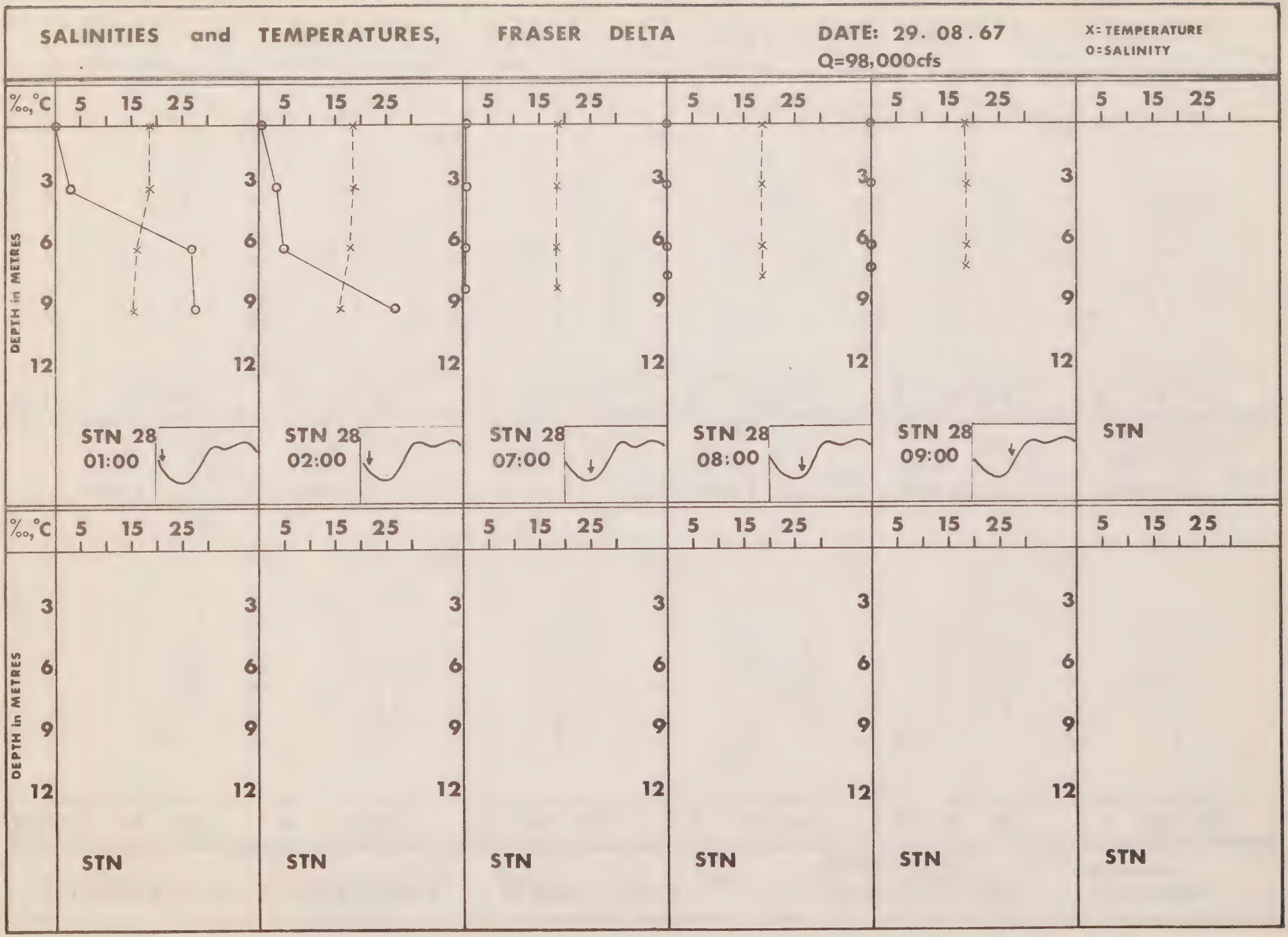

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 26.08.67
Q=112,000cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 251 00:30
STN 251 01:00
STN 251 03:00
STN 251 03:30
STN 251 04:00
STN 251 04:30
STN 251 05:00
STN 251 05:30
STN 251 06:00
STN 251 06:30
STN 251 07:00
STN 251 07:30

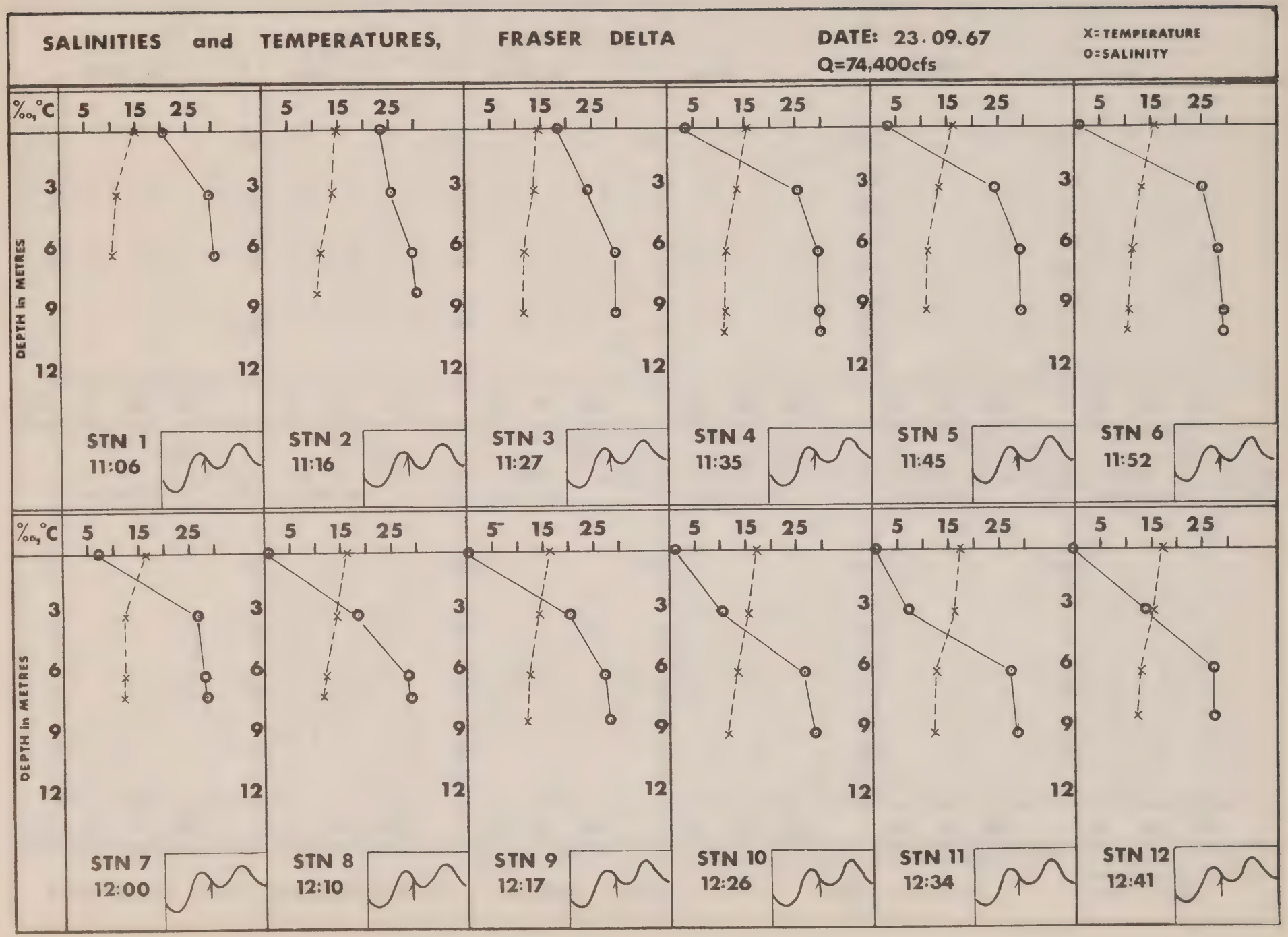

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 26.08.67
X = TEMPERATURE
O = SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 1
08:16
STN 2
08:28
STN 3
08:37
STN 4
08:45
STN 5
08:52
STN 6
09:00
STN 7
09:07
STN 8
09:18
STN 9
09:23
STN 10
09:30
STN 11
09:37
STN 12
09:42

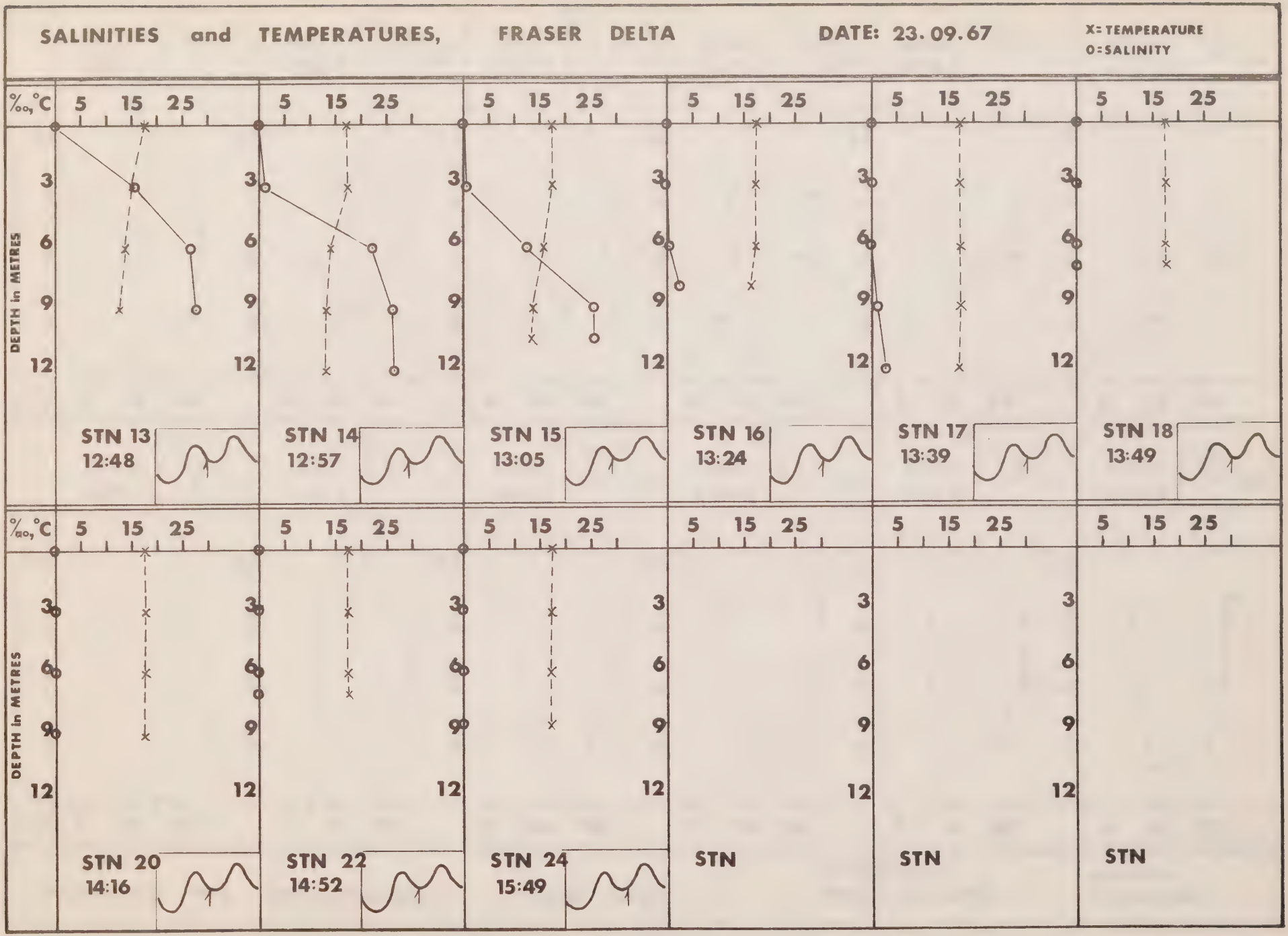

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 26.08.67
X=TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 13
09:47
STN 14
09:54
STN 15
10:05
STN 16
10:18
STN 17
10:27
STN 18
11:40
STN 19
11:52
STN 20
12:09
STN 22
12:44
STN 23
12:59
STN 24
13:36
STN

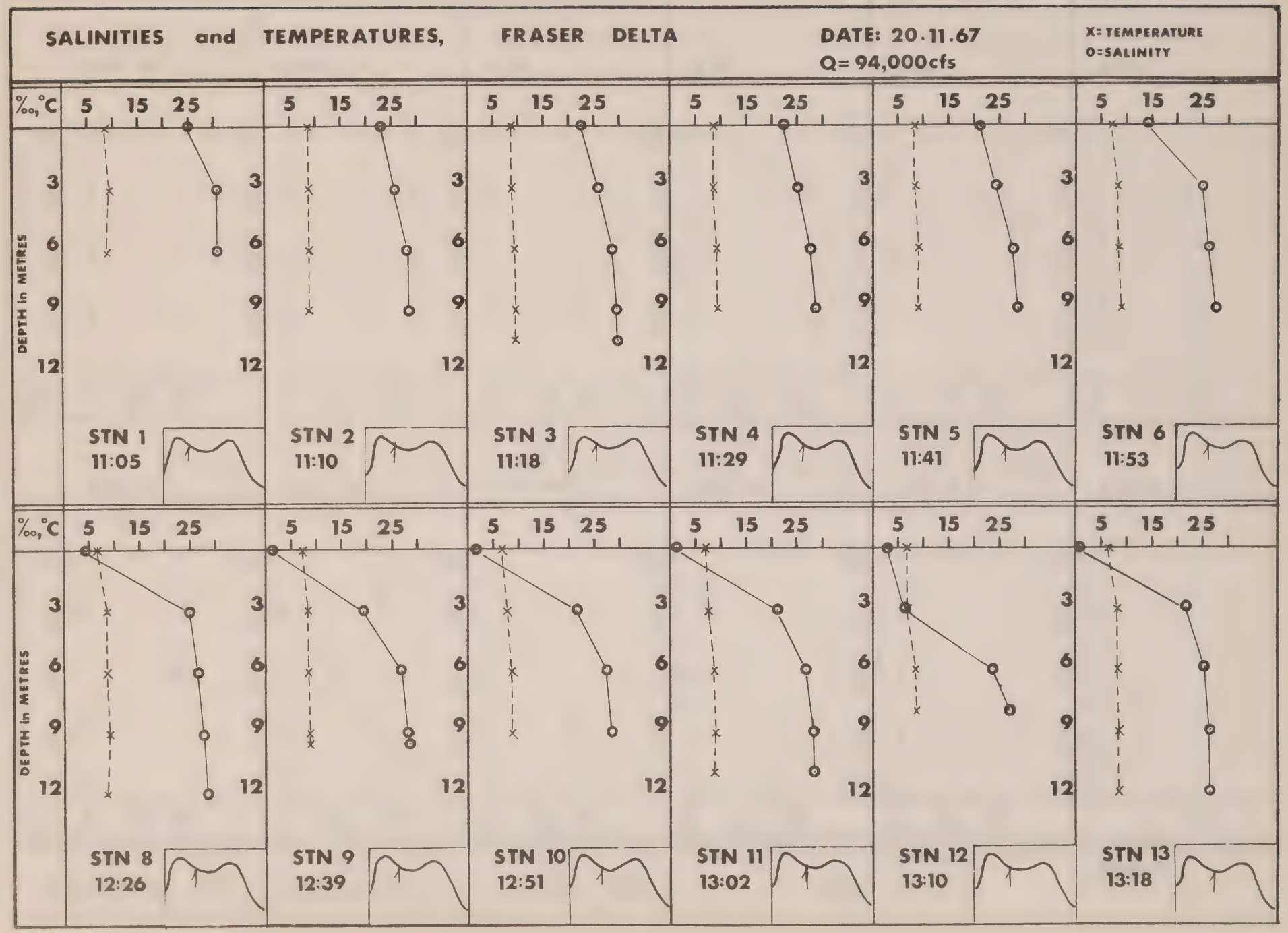

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 27.08.67
Q=108,000cfs
X=TEMPERATURE
O=SALINITY
‰, °C
DEPTH in METRES
STN 2 11:59
STN 3 12:10
STN 4 12:18
STN 5 12:26
STN 6 12:35
STN 7 12:44
STN 8 12:53
STN 9 13:01
STN 10 13:10
STN 11 13:18
STN 12 13:24
STN

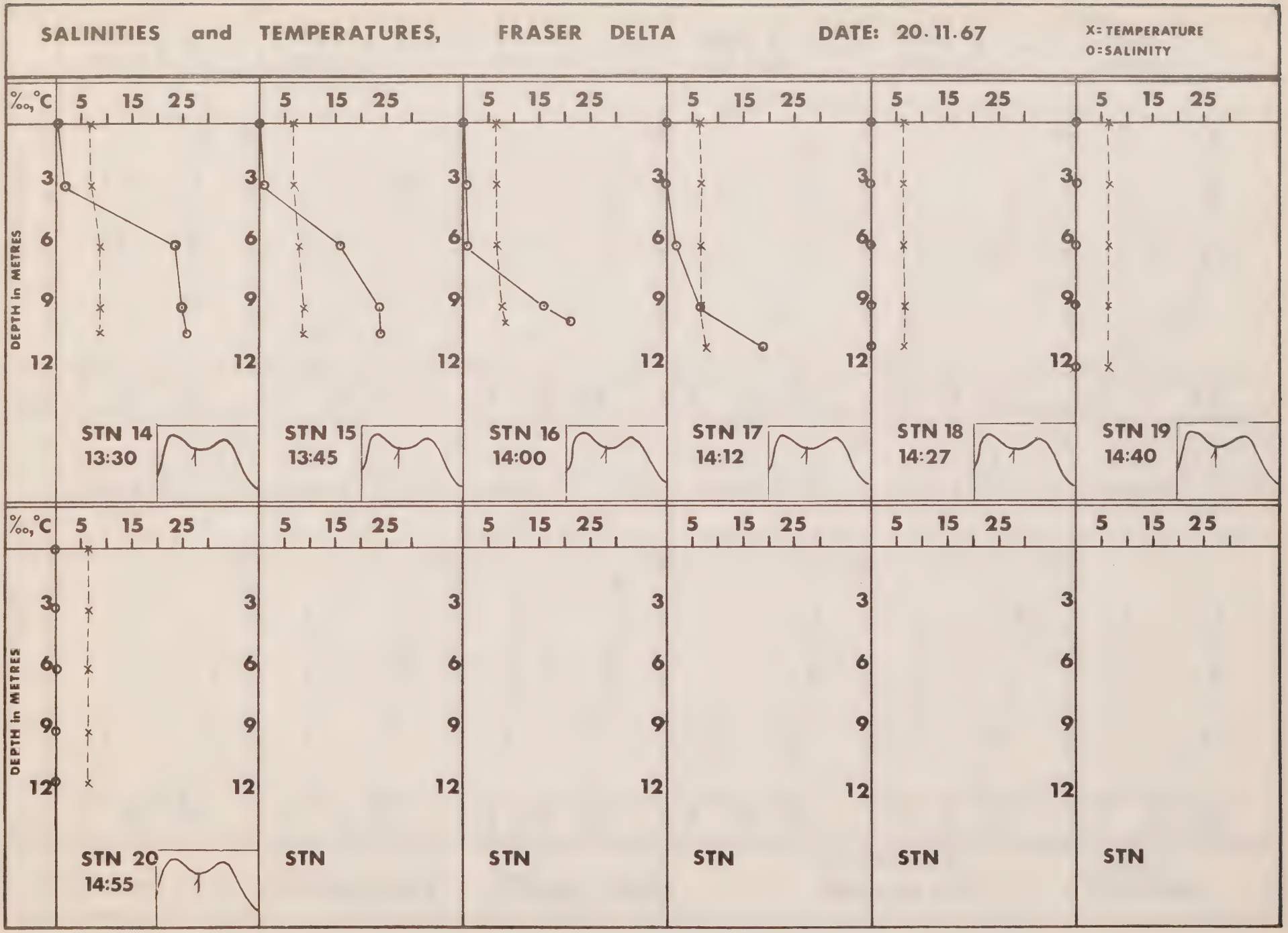

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 28.08.67
Q=105,000cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 2
13:27
STN 4
13:38
STN 6
13:48
STN 8
13:58
STN 10
14:10
STN 12
14:18
STN 28
18:00
STN 28
19:00
STN 28
21:00
STN 28
22:00
STN 28
23:00
STN 28
24:00

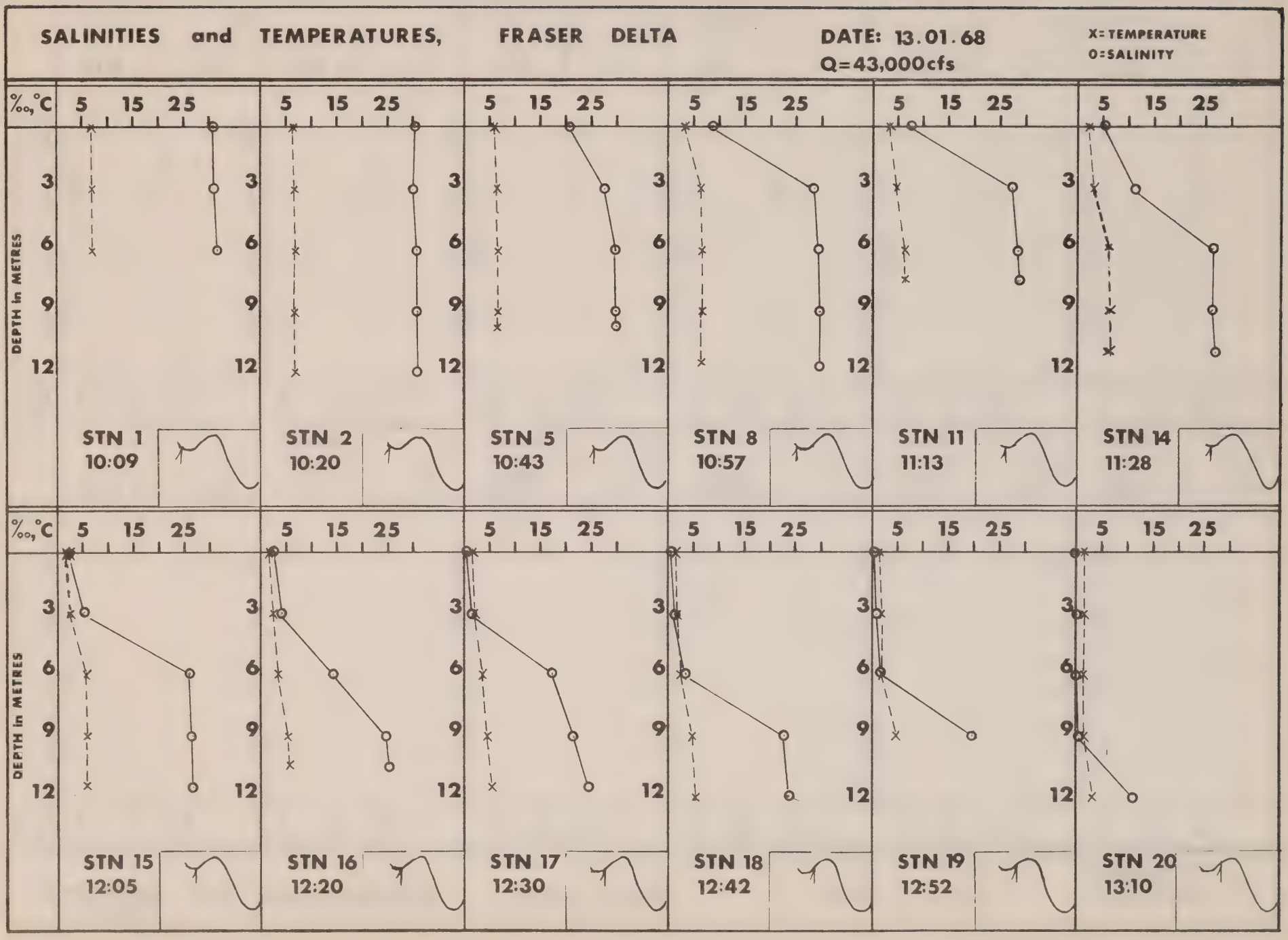

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 29. 08. 67
Q=98,000cfs
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 28
01:00
STN 28
02:00
STN 28
07:00
STN 28
08:00
STN 28
09:00
STN

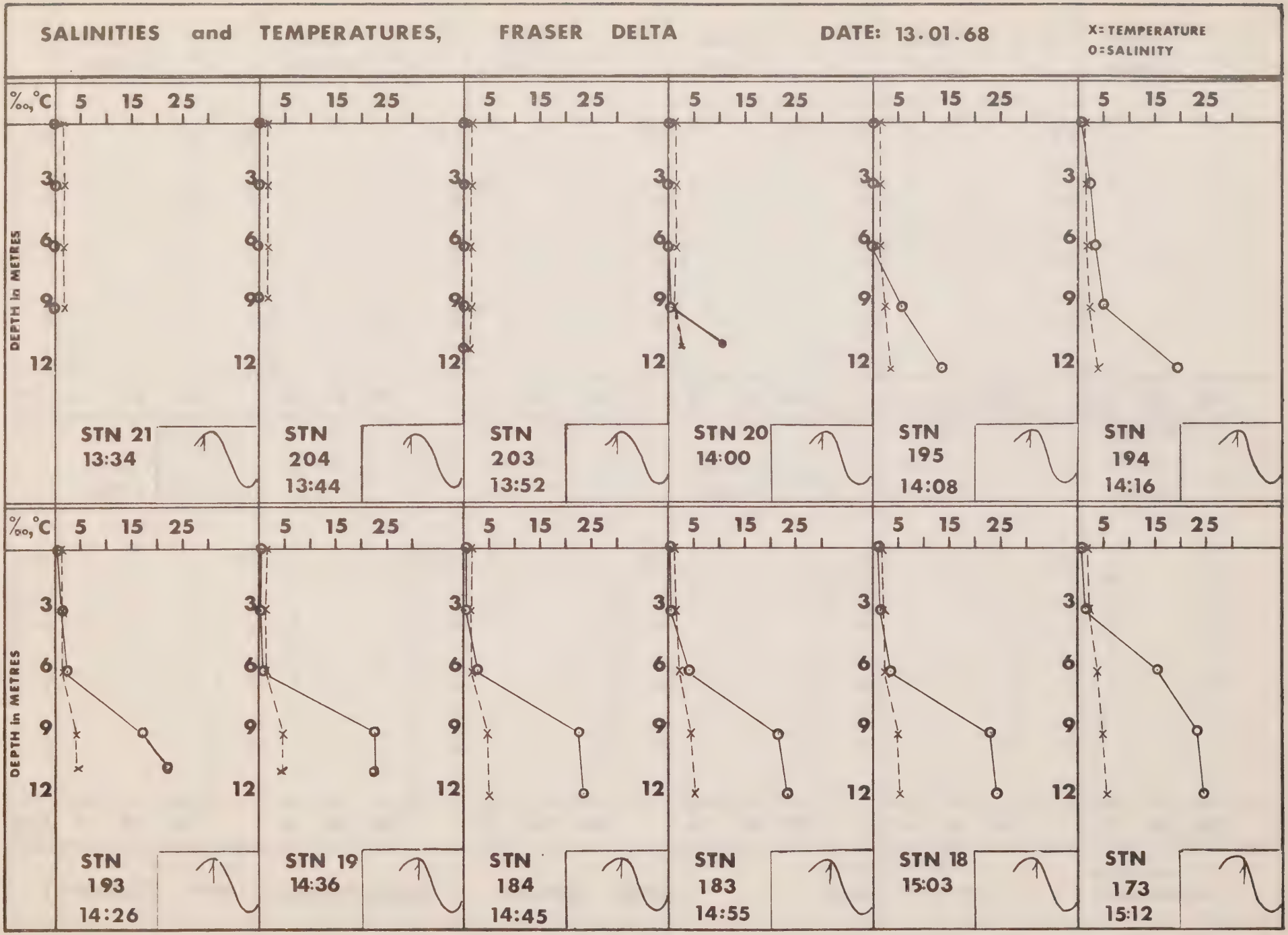

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 23.09.67
Q=74,400cfs
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 1
11:06
STN 2
11:16
STN 3
11:27
STN 4
11:35
STN 5
11:45
STN 6
11:52
STN 7
12:00
STN 8
12:10
STN 9
12:17
STN 10
12:26
STN 11
12:34
STN 12
12:41

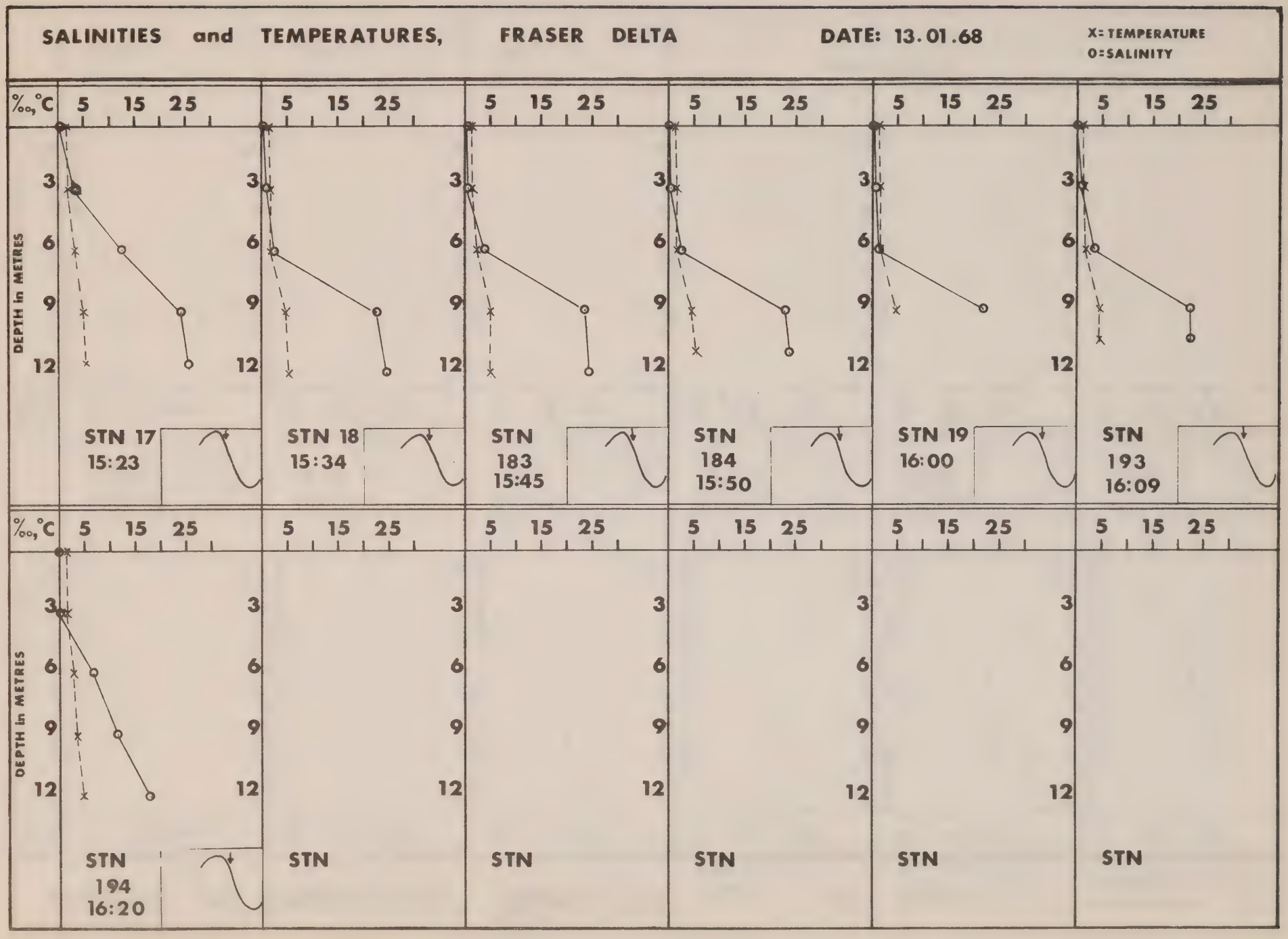

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 23.09.67
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 13
12:48
STN 14
12:57
STN 15
13:05
STN 16
13:24
STN 17
13:39
STN 18
13:49
STN 20
14:16
STN 22
14:52
STN 24
15:49
STN
STN
STN

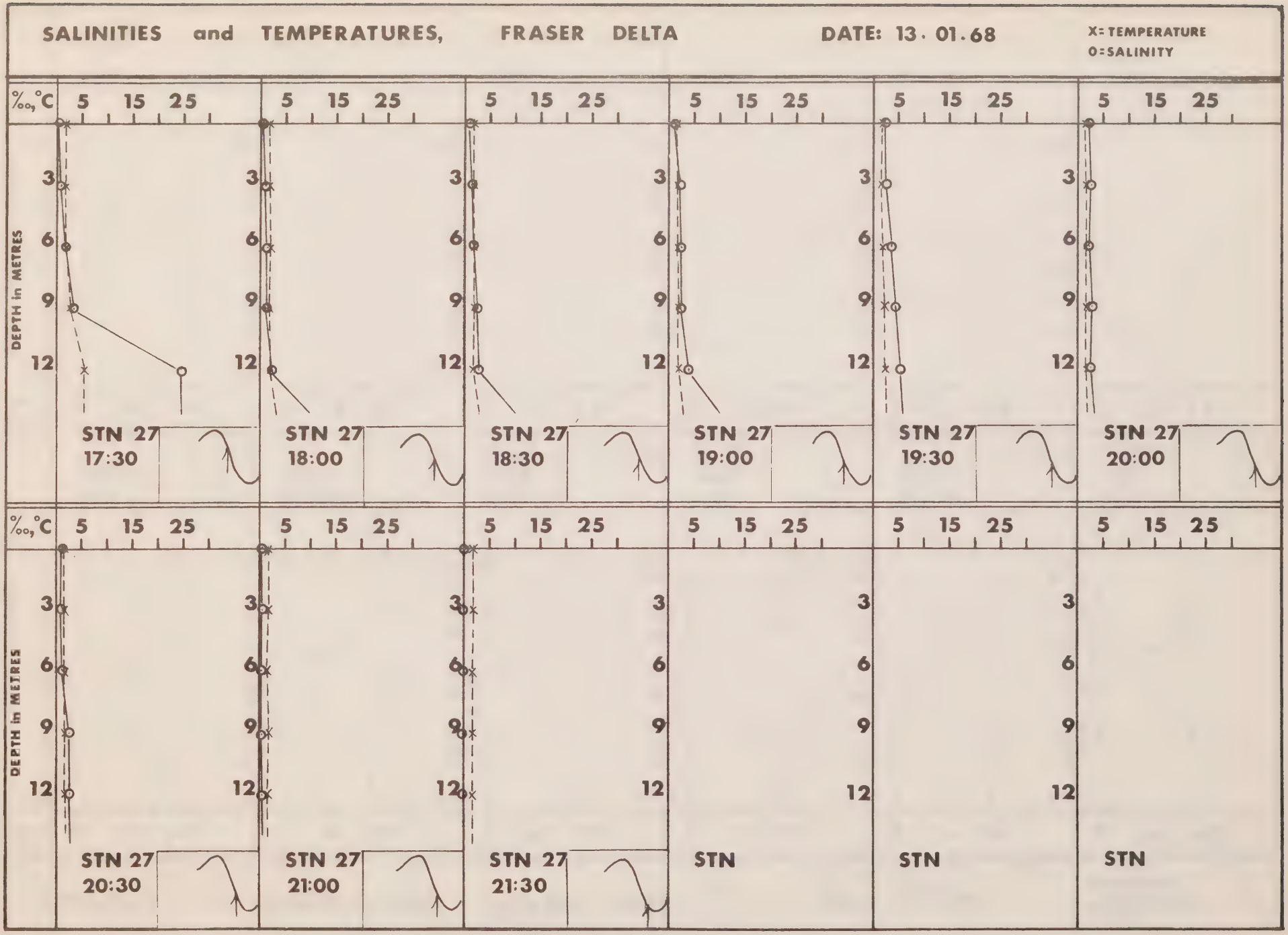

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 20.11.67
Q= 94,000cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 1
11:05
STN 2
11:10
STN 3
11:18
STN 4
11:29
STN 5
11:41
STN 6
11:53
STN 8
12:26
STN 9
12:39
STN 10
12:51
STN 11
13:02
STN 12
13:10
STN 13
13:18

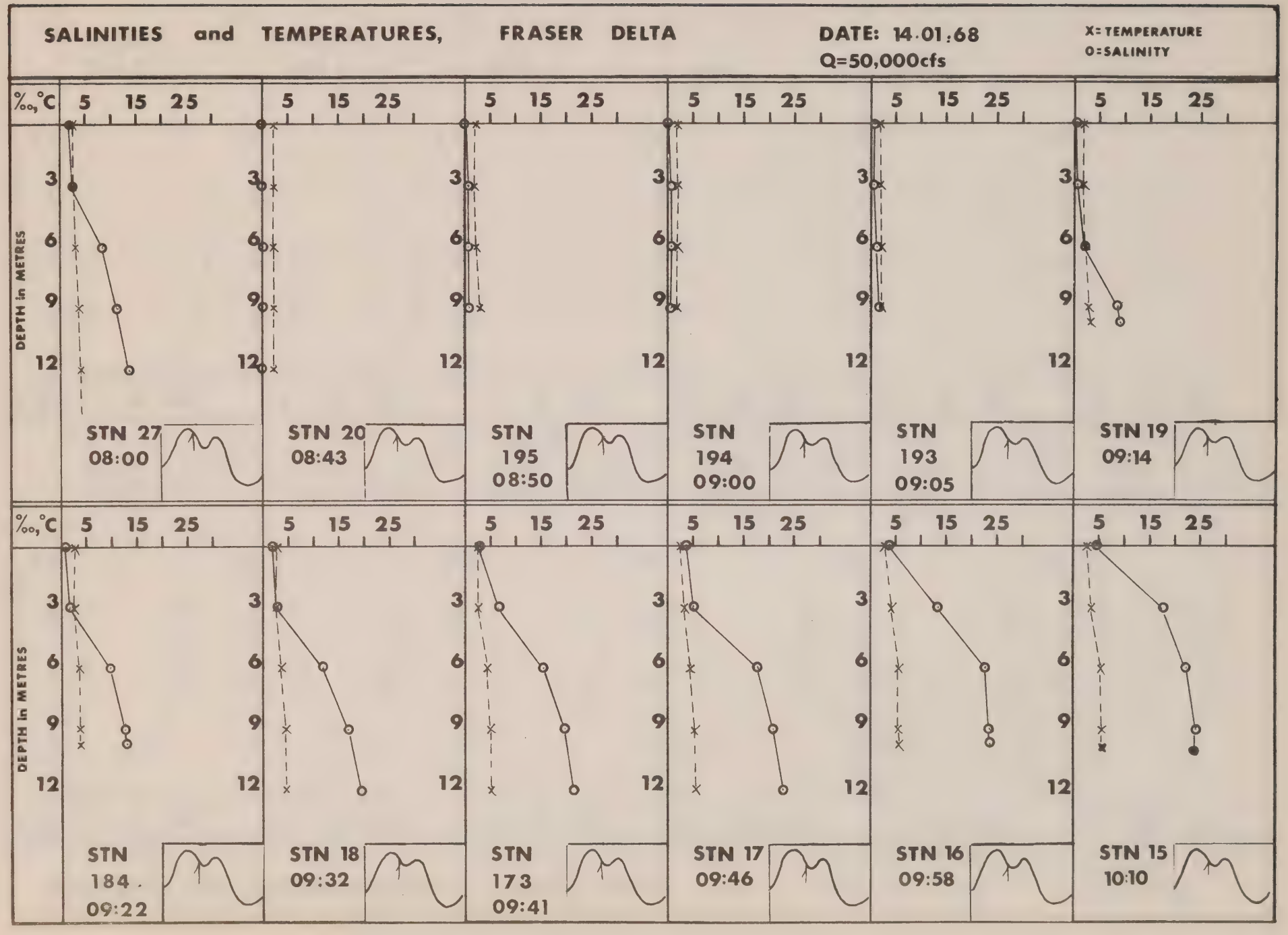

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 20.11.67
X = TEMPERATURE
O = SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 14
13:30
STN 15
13:45
STN 16
14:00
STN 17
14:12
STN 18
14:27
STN 19
14:40
STN 20
14:55
STN
STN
STN
STN
STN


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 13.01.68
Q=43,000cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 1
10:09
STN 2
10:20
STN 5
10:43
STN 8
10:57
STN 11
11:13
STN 14
11:28
STN 15
12:05
STN 16
12:20
STN 17
12:30
STN 18
12:42
STN 19
12:52
STN 20
13:10


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 13.01.68
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 21
13:34
STN
204
13:44
STN
203
13:52
STN 20
14:00
STN
195
14:08
STN
194
14:16
STN
193
14:26
STN 19
14:36
STN
184
14:45
STN
183
14:55
STN 18
15:03
STN
173
15:12

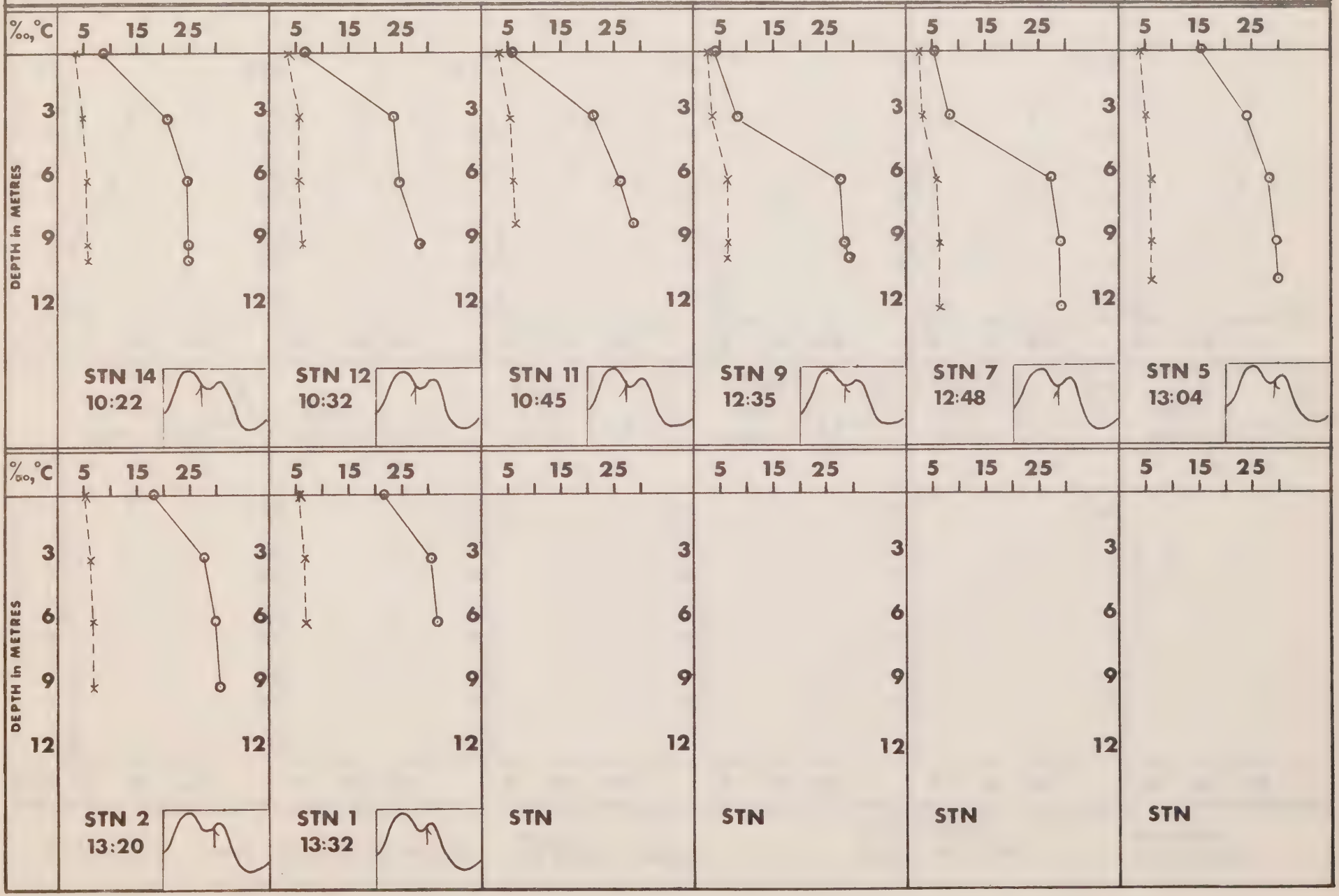

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 13.01.68
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 17
15:23
STN 18
15:34
STN
183
15:45
STN
184
15:50
STN 19
16:00
STN
193
16:09
STN
194
16:20
STN
STN
STN
STN
STN

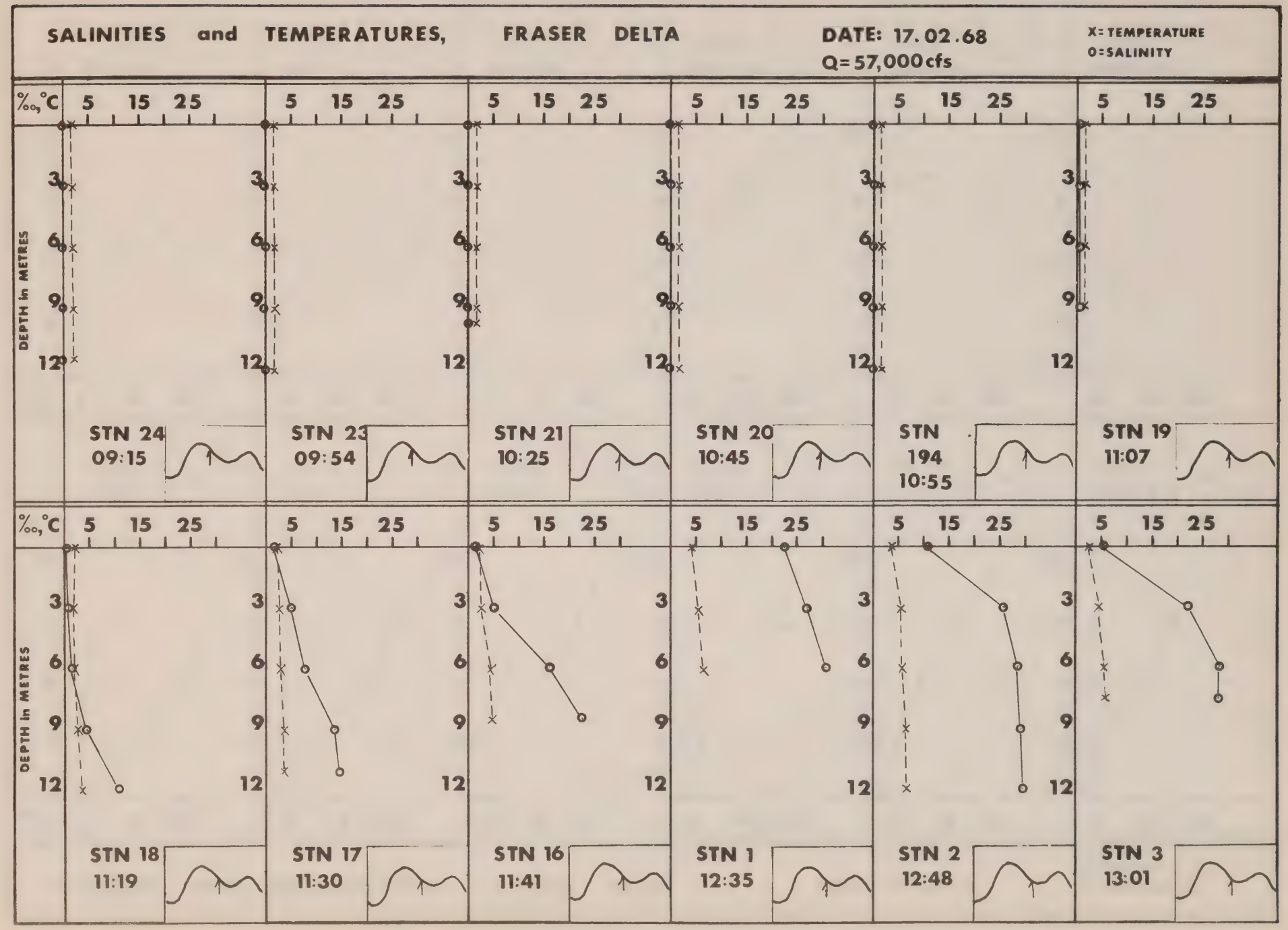

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 13 · 01 · 68
X = TEMPERATURE
O = SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 27
17:30
STN 27
18:00
STN 27
18:30
STN 27
19:00
STN 27
19:30
STN 27
20:00
STN 27
20:30
STN 27
21:00
STN 27
21:30
STN
STN
STN

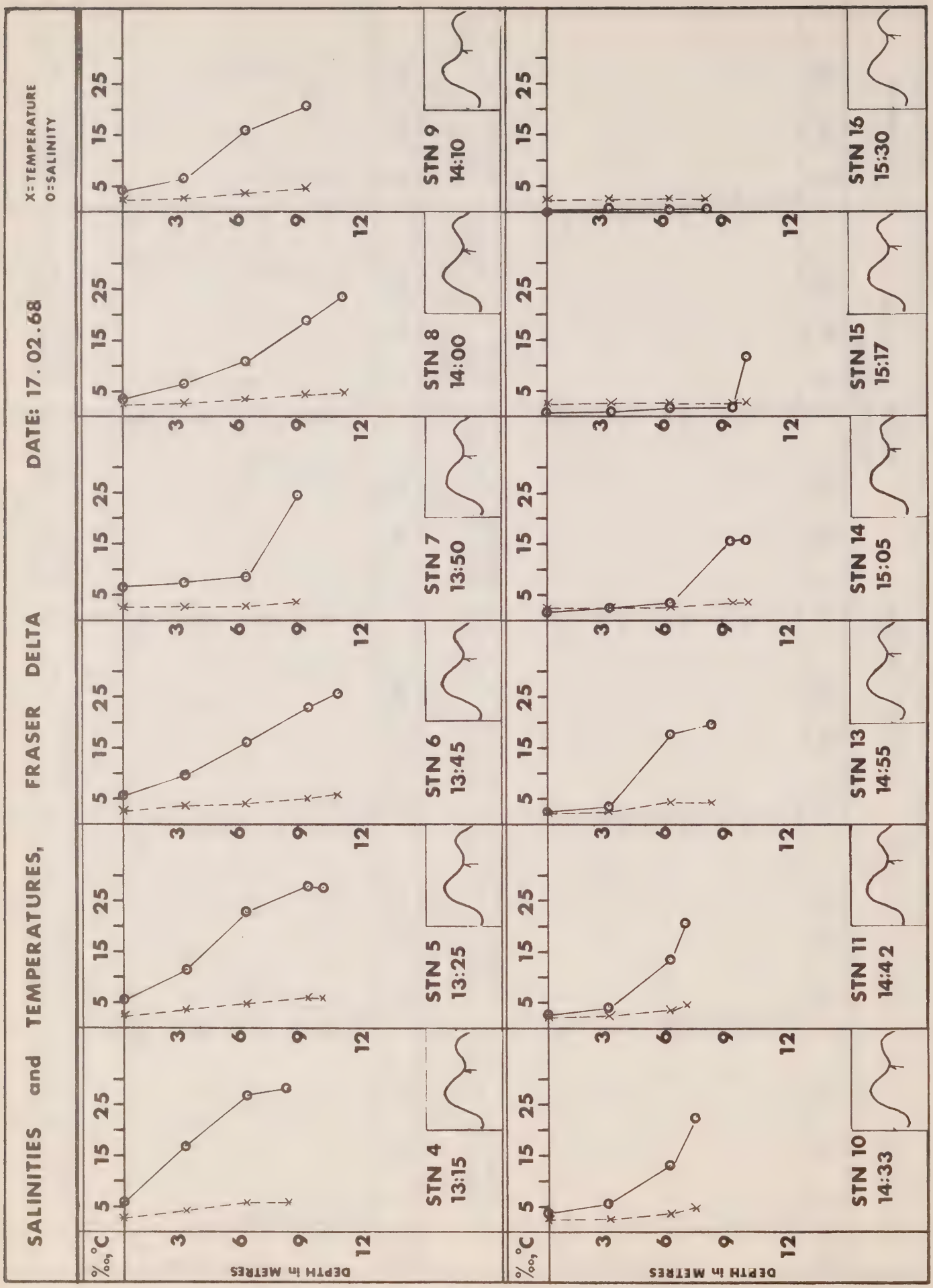

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 14.01.68
Q=50,000cfs
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 27
08:00
STN 20
08:43
STN
195
08:50
STN
194
09:00
STN
193
09:05
STN 19
09:14
STN
184
09:22
STN 18
09:32
STN
173
09:41
STN 17
09:46
STN 16
09:58
STN 15
10:10

SALINITIES and TEMPERATURES, FRASER DELTA DATE: 14 · 01 · 68

X = TEMPERATURE
O = SALINITY




SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 17.02.68
Q=57,000cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 24
09:15
STN 23
09:54
STN 21
10:25
STN 20
10:45
STN
194
10:55
STN 19
11:07
STN 18
11:19
STN 17
11:30
STN 16
11:41
STN 1
12:35
STN 2
12:48
STN 3
13:01


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 17.02.68
X=TEMPERATURE
O=SALINITY
‰, °C
DEPTH in METRES
STN 4 13:15
STN 5 13:25
STN 6 13:45
STN 7 13:50
STN 8 14:00
STN 9 14:10
STN 10 14:33
STN 11 14:42
STN 13 14:55
STN 14 15:05
STN 15 15:17
STN 16 15:30

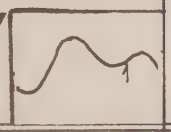
SALINITIES and TEMPERATURES, FRASER DELTA DATE: 17.02.68

X: TEMPERATURE
O: SALINITY

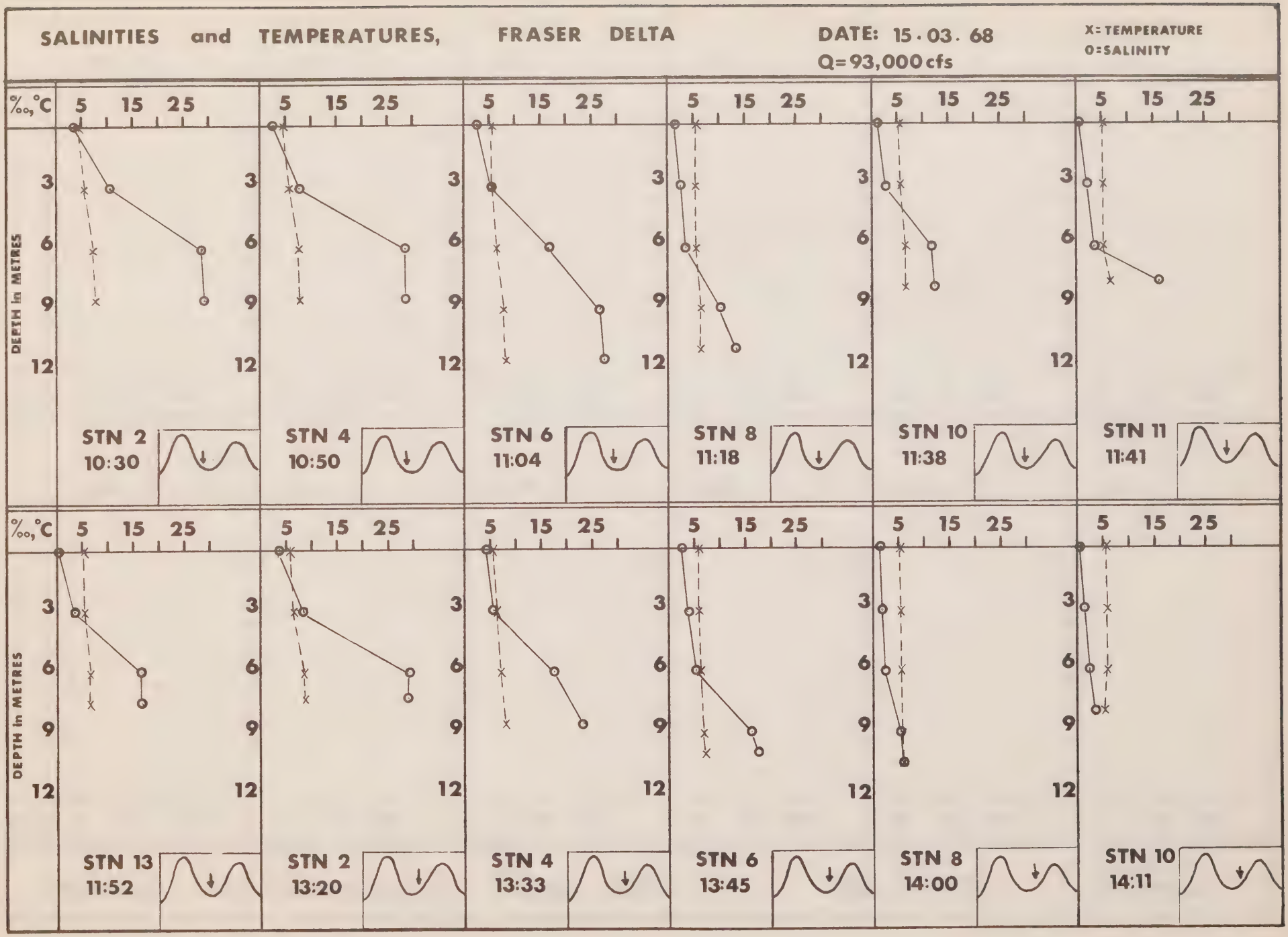
‰, °C 5 15 25

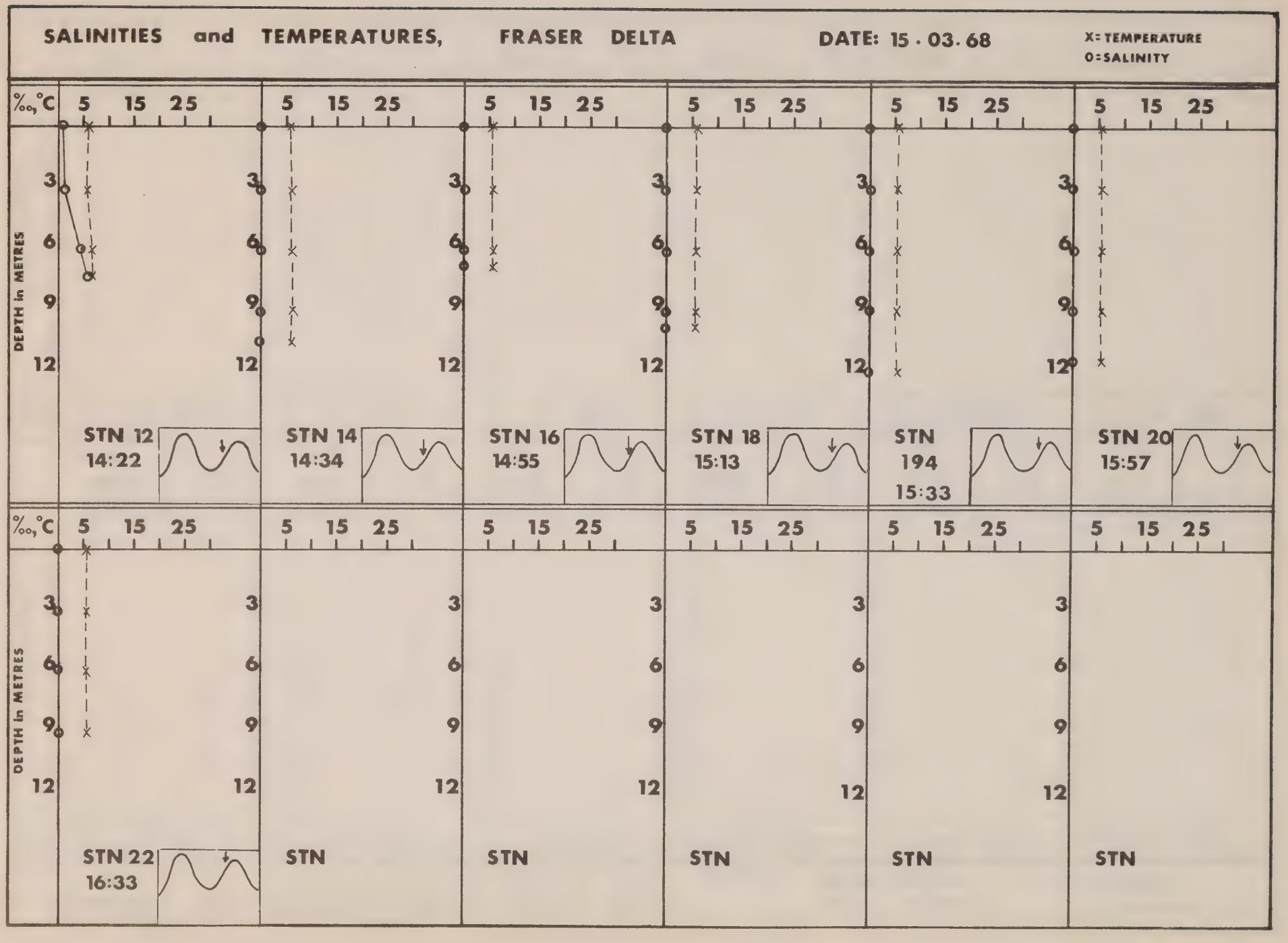
DEPTH in METRES 3 6 9 12

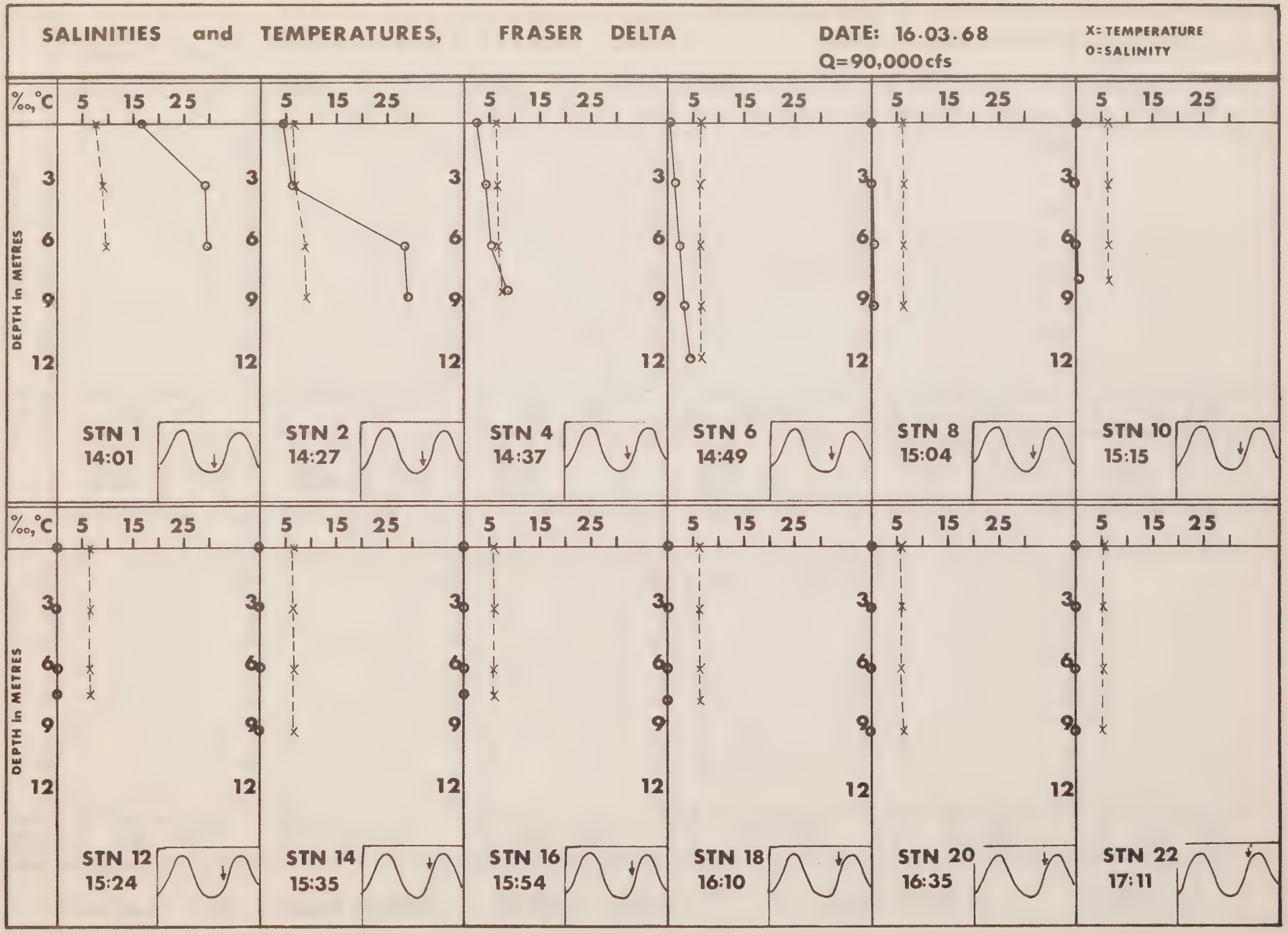
STN 17
15:42

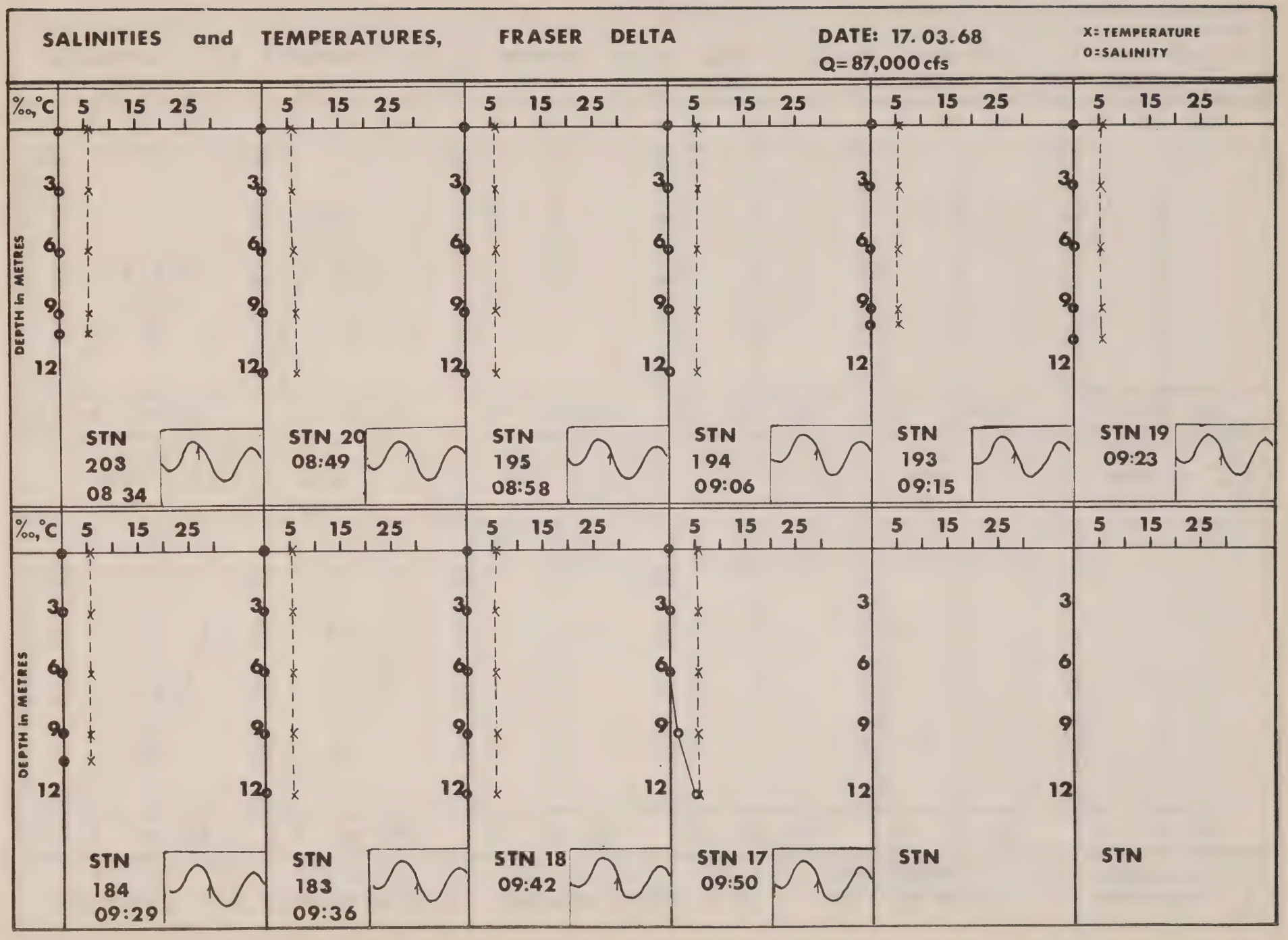


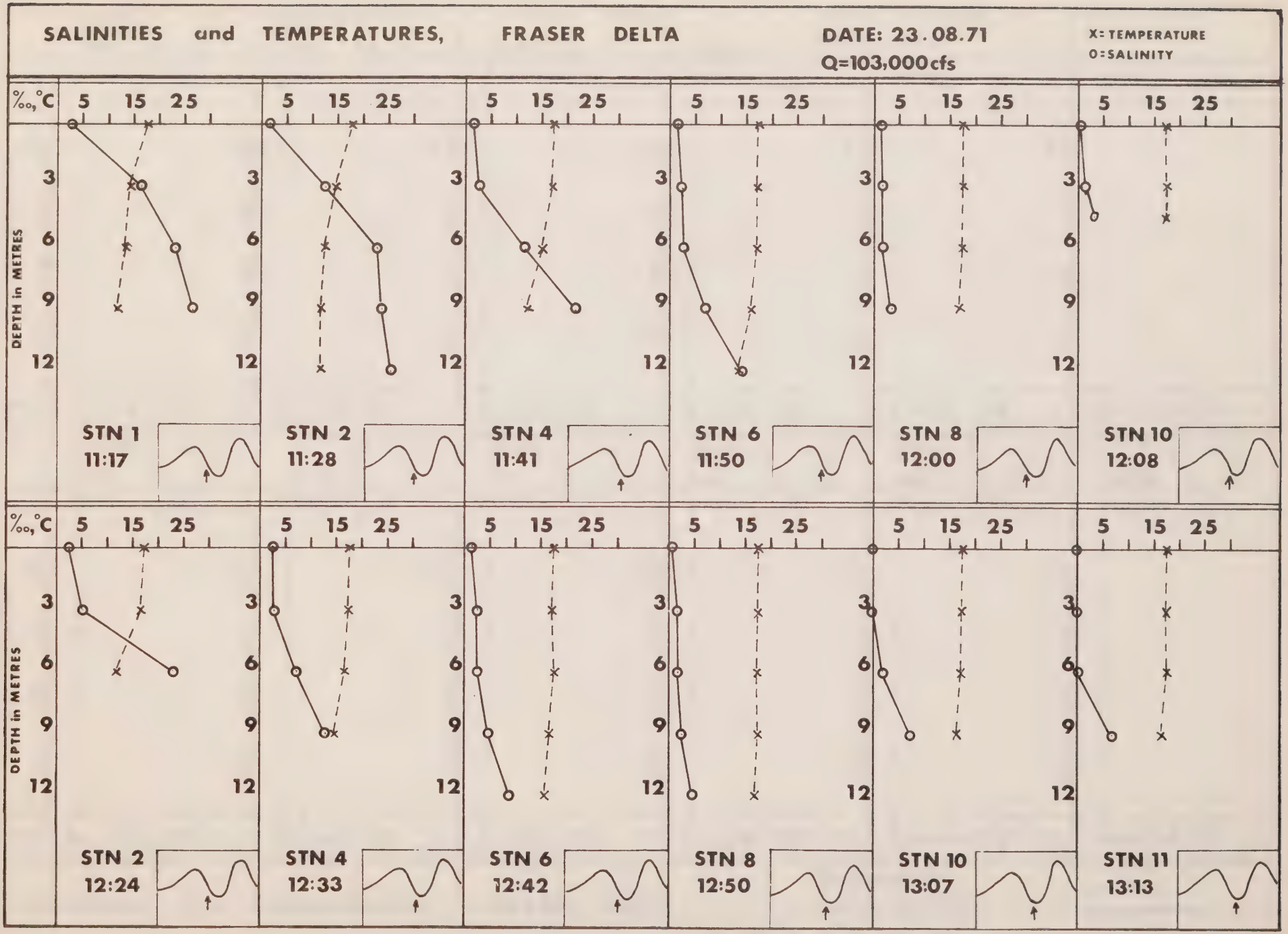
STN

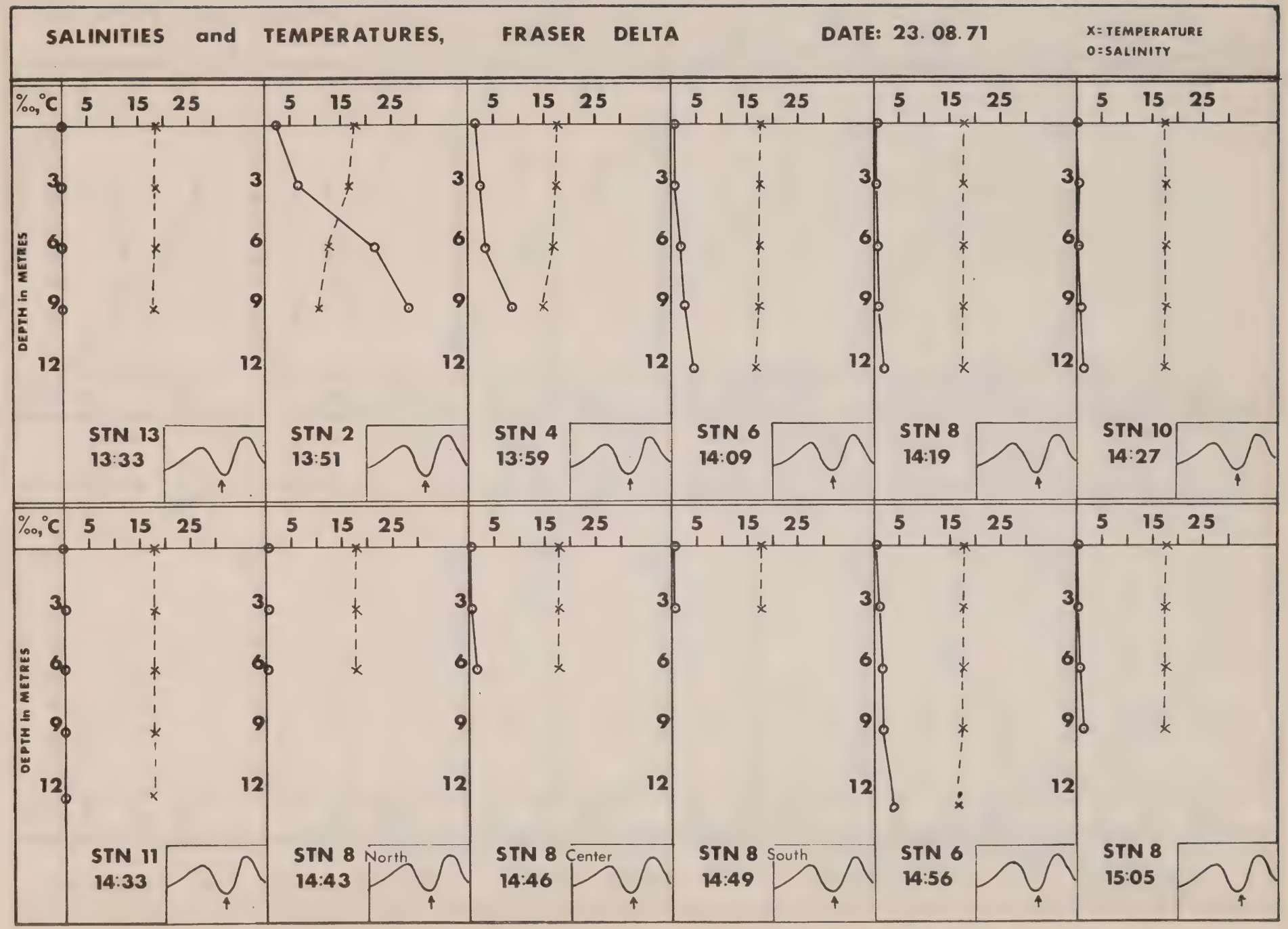

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 15 · 03 · 68
Q = 93,000 cfs
X = TEMPERATURE
O = SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 2
10:30
STN 4
10:50
STN 6
11:04
STN 8
11:18
STN 10
11:38
STN 11
11:41
STN 13
11:52
STN 2
13:20
STN 4
13:33
STN 6
13:45
STN 8
14:00
STN 10
14:11

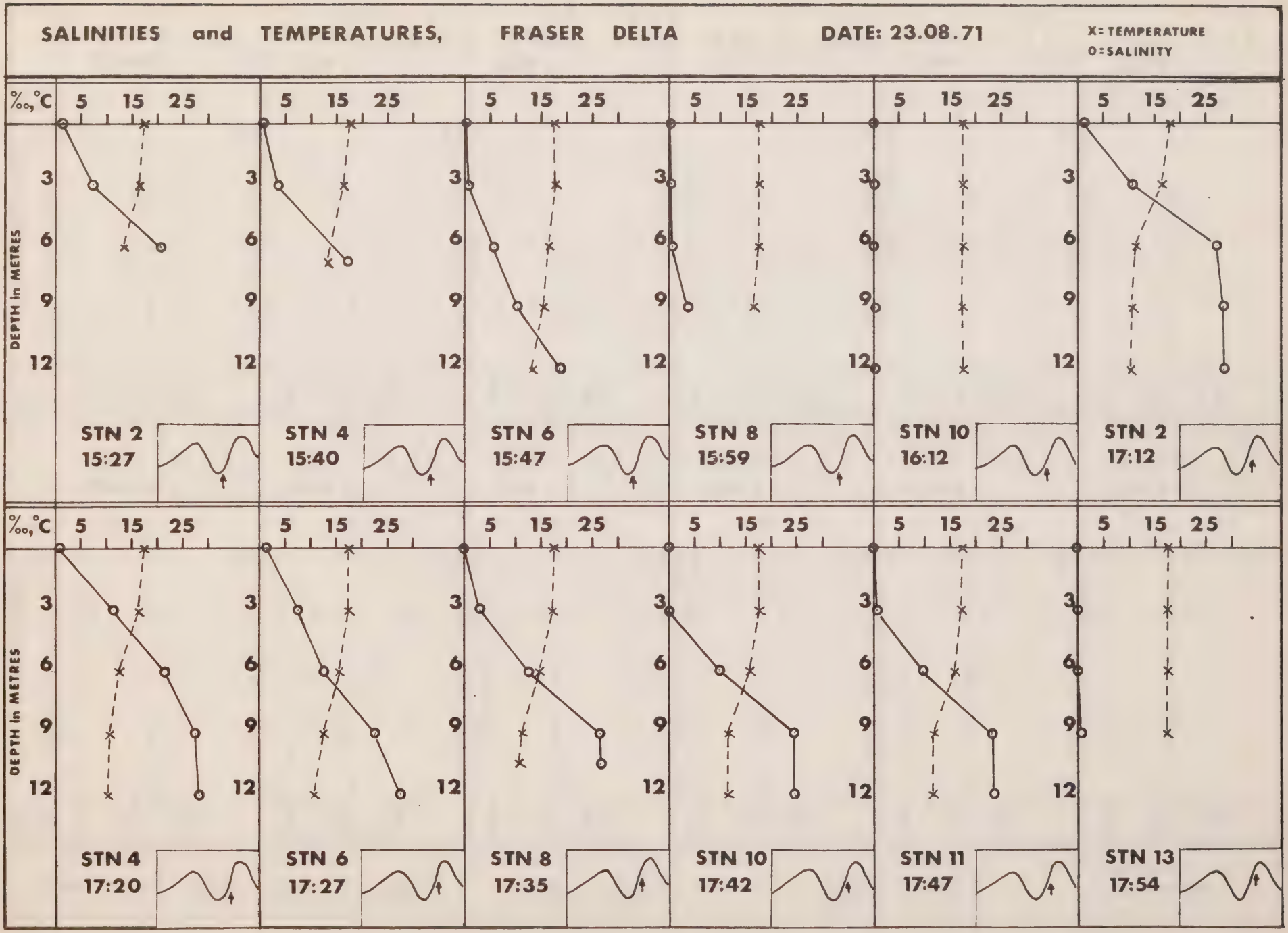

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 15 . 03. 68
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 12
14:22
STN 14
14:34
STN 16
14:55
STN 18
15:13
STN
194
15:33
STN 20
15:57
STN 22
16:33
STN
STN
STN
STN
STN

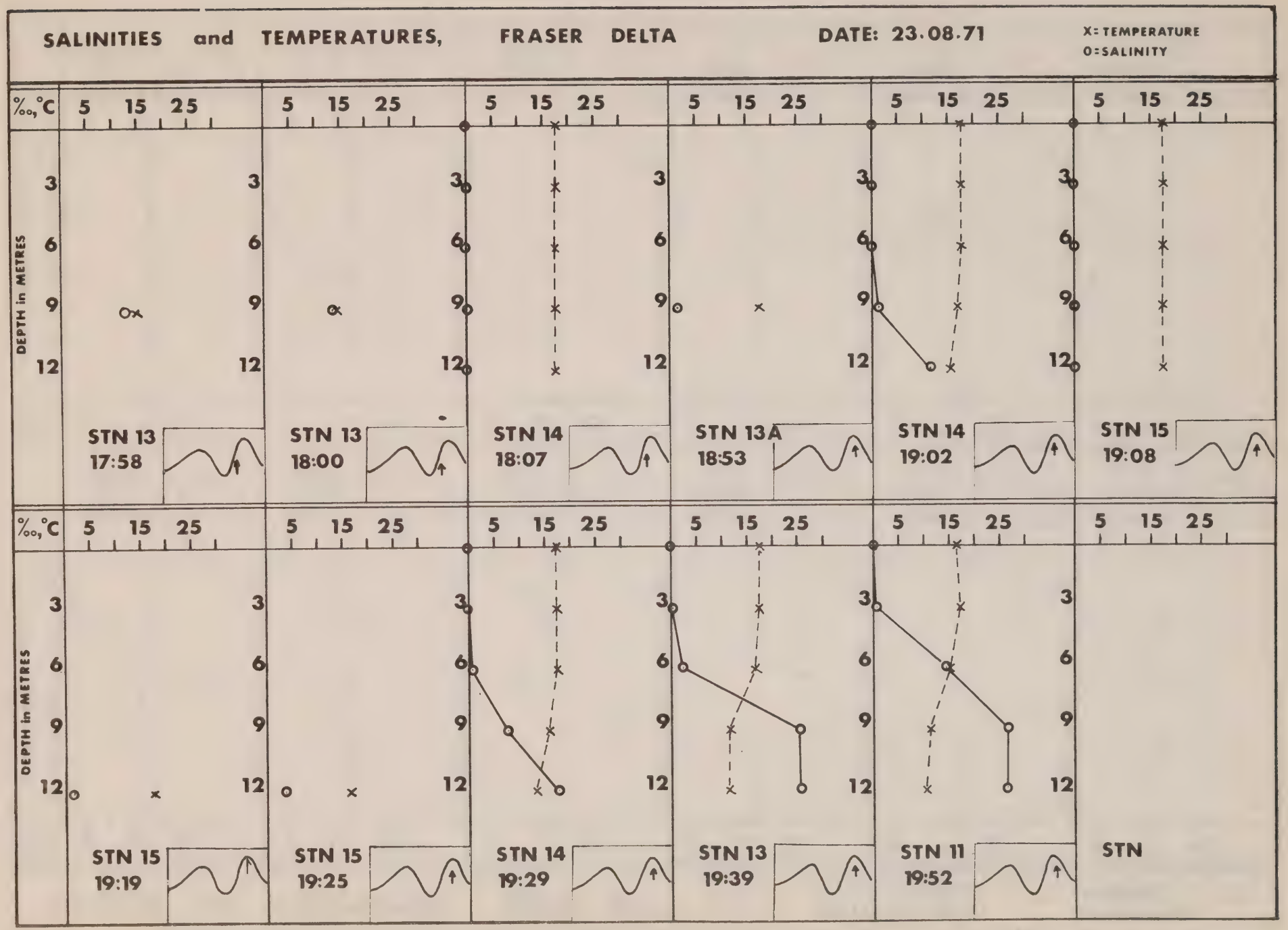

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 16.03.68
Q=90,000 cfs
X= TEMPERATURE
O= SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 1
14:01
STN 2
14:27
STN 4
14:37
STN 6
14:49
STN 8
15:04
STN 10
15:15
STN 12
15:24
STN 14
15:35
STN 16
15:54
STN 18
16:10
STN 20
16:35
STN 22
17:11

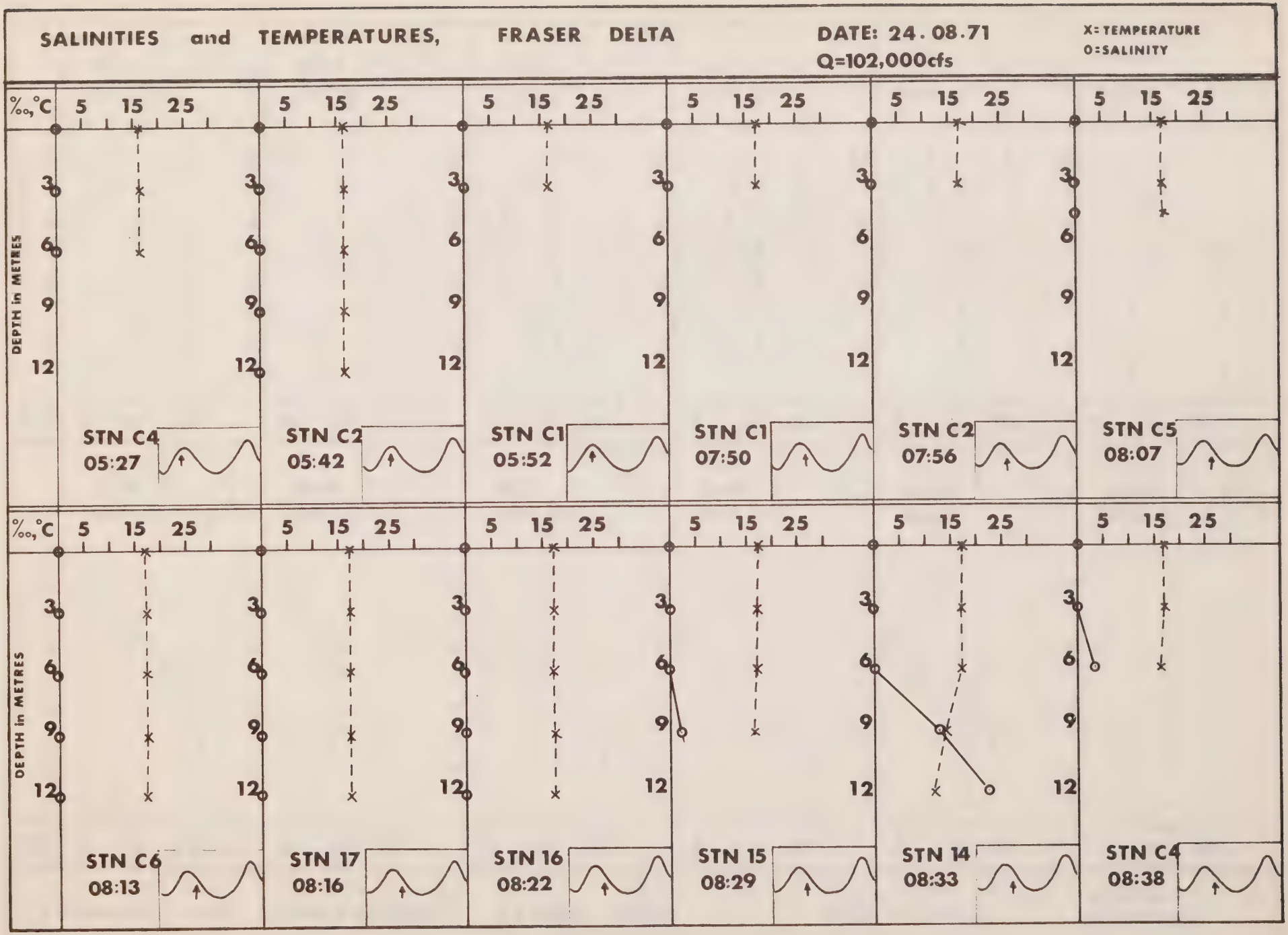

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 17.03.68
Q=87,000 cfs
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 203 08 34
STN 20 08:49
STN 195 08:58
STN 194 09:06
STN 193 09:15
STN 19 09:23
STN 184 09:29
STN 183 09:36
STN 18 09:42
STN 17 09:50
STN
STN

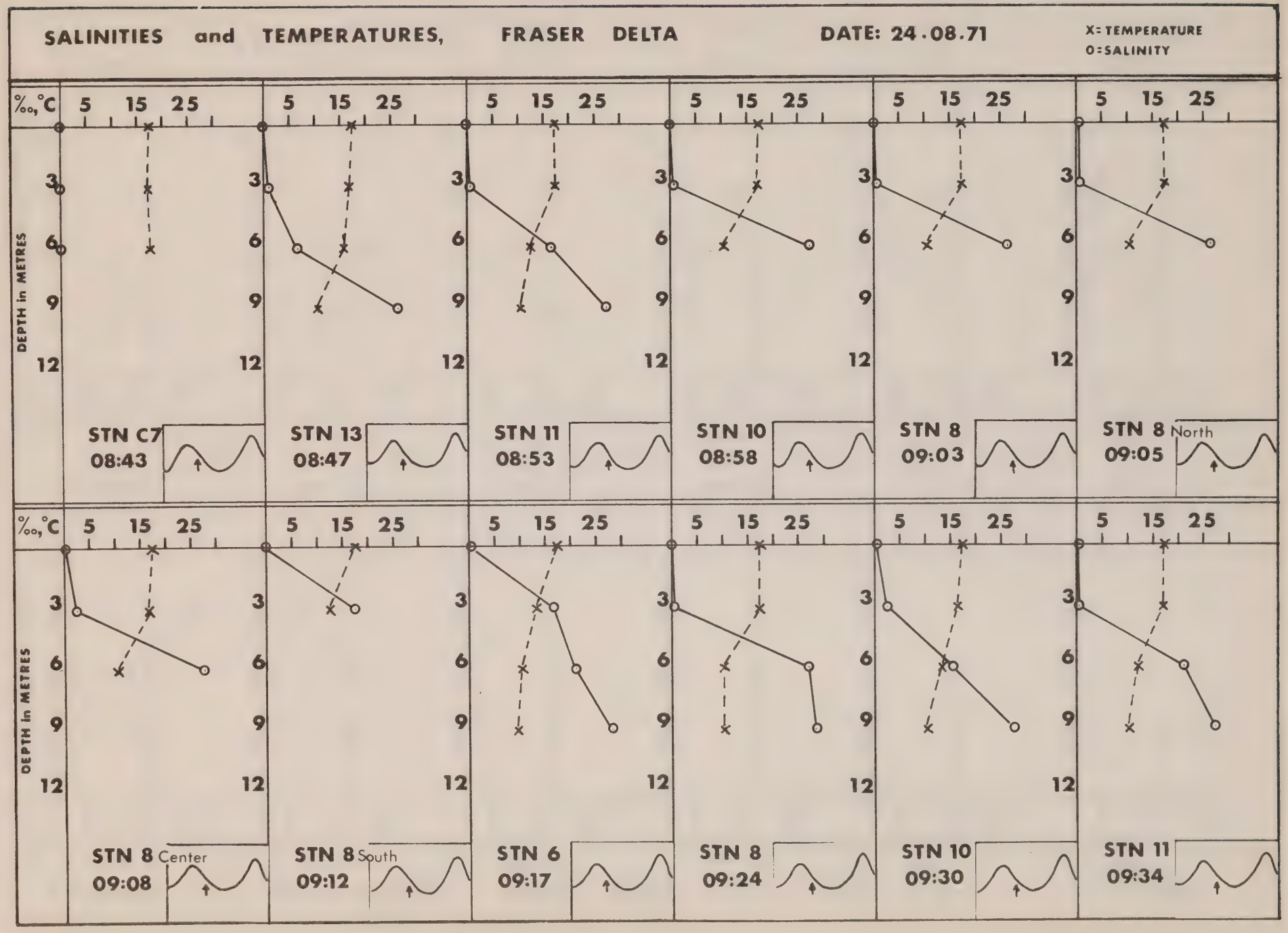

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 23.08.71
Q=103,000cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 1
11:17
STN 2
11:28
STN 4
11:41
STN 6
11:50
STN 8
12:00
STN 10
12:08
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STN 4
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13:07
STN 11
13:13

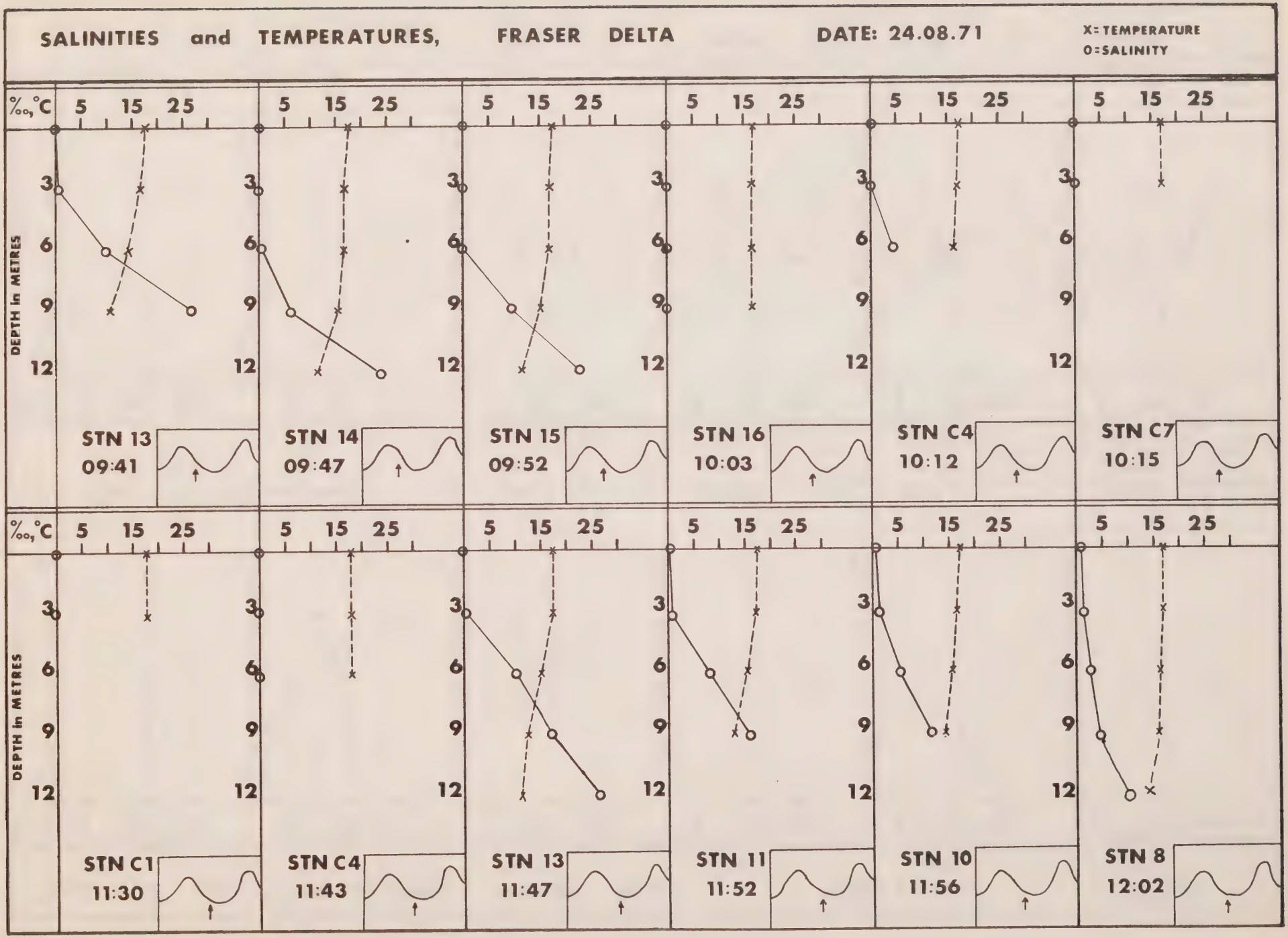

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 23. 08. 71
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 13
13:33
STN 2
13:51
STN 4
13:59
STN 6
14:09
STN 8
14:19
STN 10
14:27
STN 11
14:33
STN 8 North
14:43
STN 8 Center
14:46
STN 8 South
14:49
STN 6
14:56
STN 8
15:05

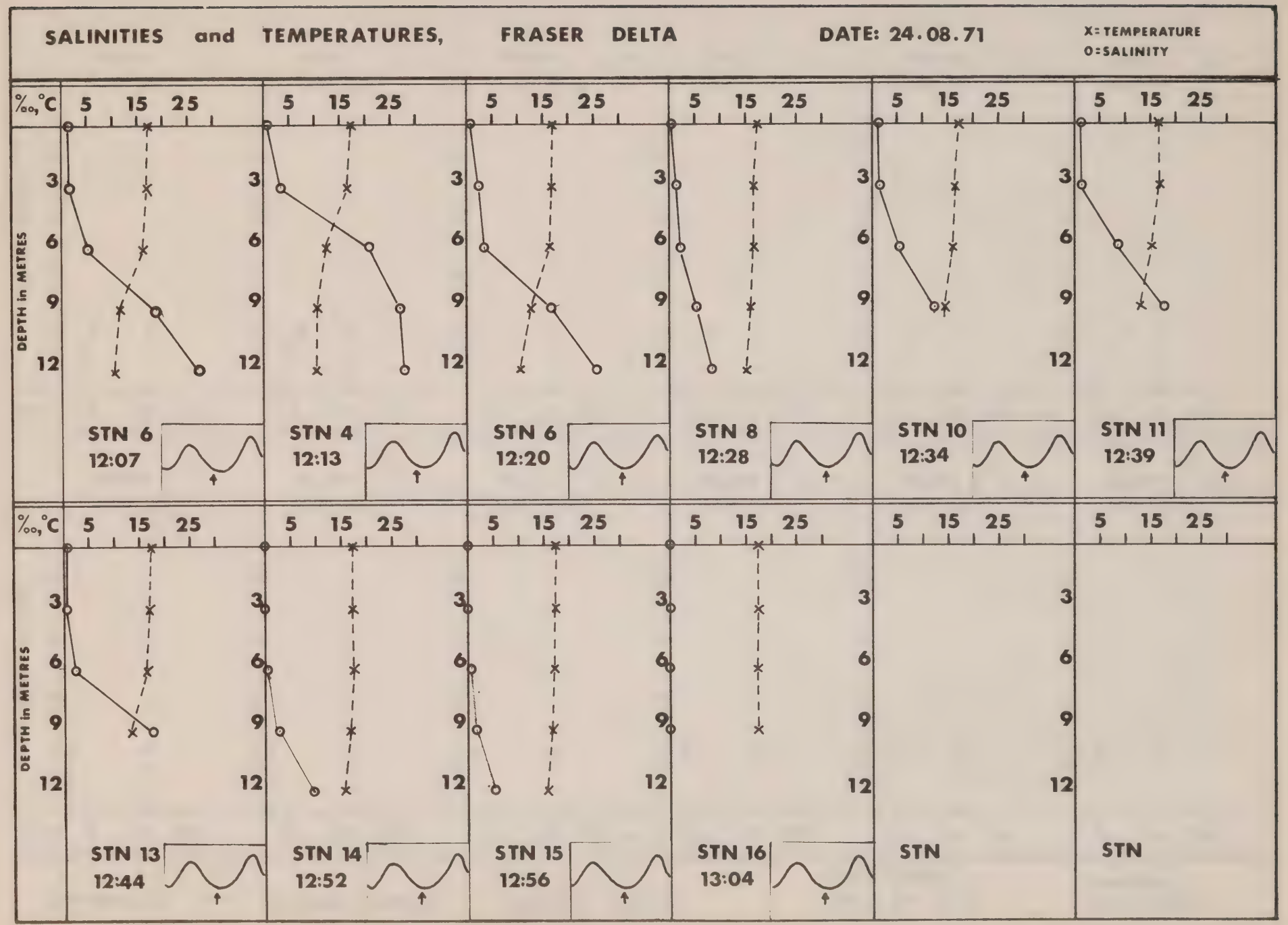

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 23.08.71
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 2
15:27
STN 4
15:40
STN 6
15:47
STN 8
15:59
STN 10
16:12
STN 2
17:12
STN 4
17:20
STN 6
17:27
STN 8
17:35
STN 10
17:42
STN 11
17:47
STN 13
17:54

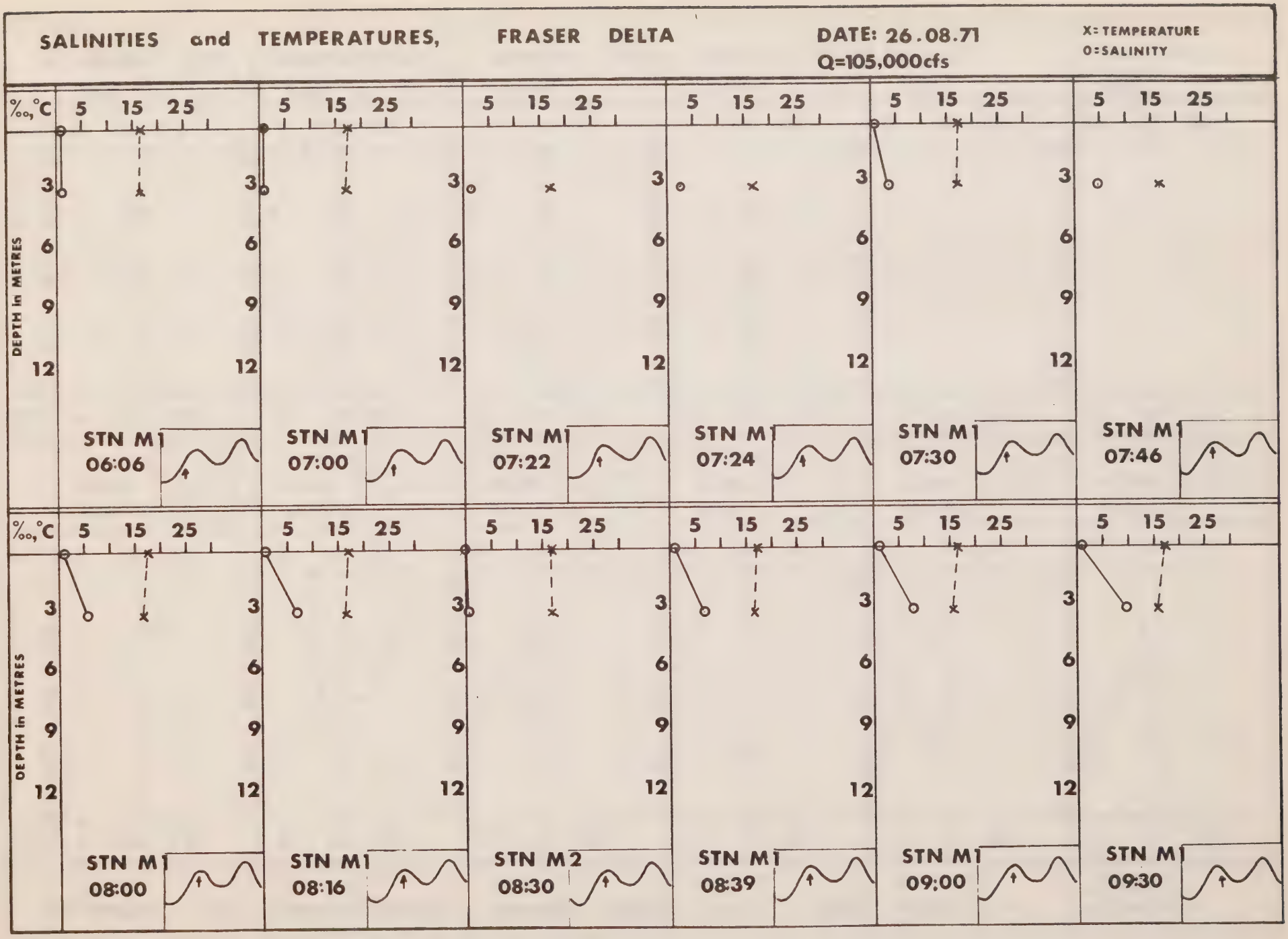

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 23.08.71
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 13
17:58
STN 13
18:00
STN 14
18:07
STN 13A
18:53
STN 14
19:02
STN 15
19:08
STN 15
19:19
STN 15
19:25
STN 14
19:29
STN 13
19:39
STN 11
19:52
STN

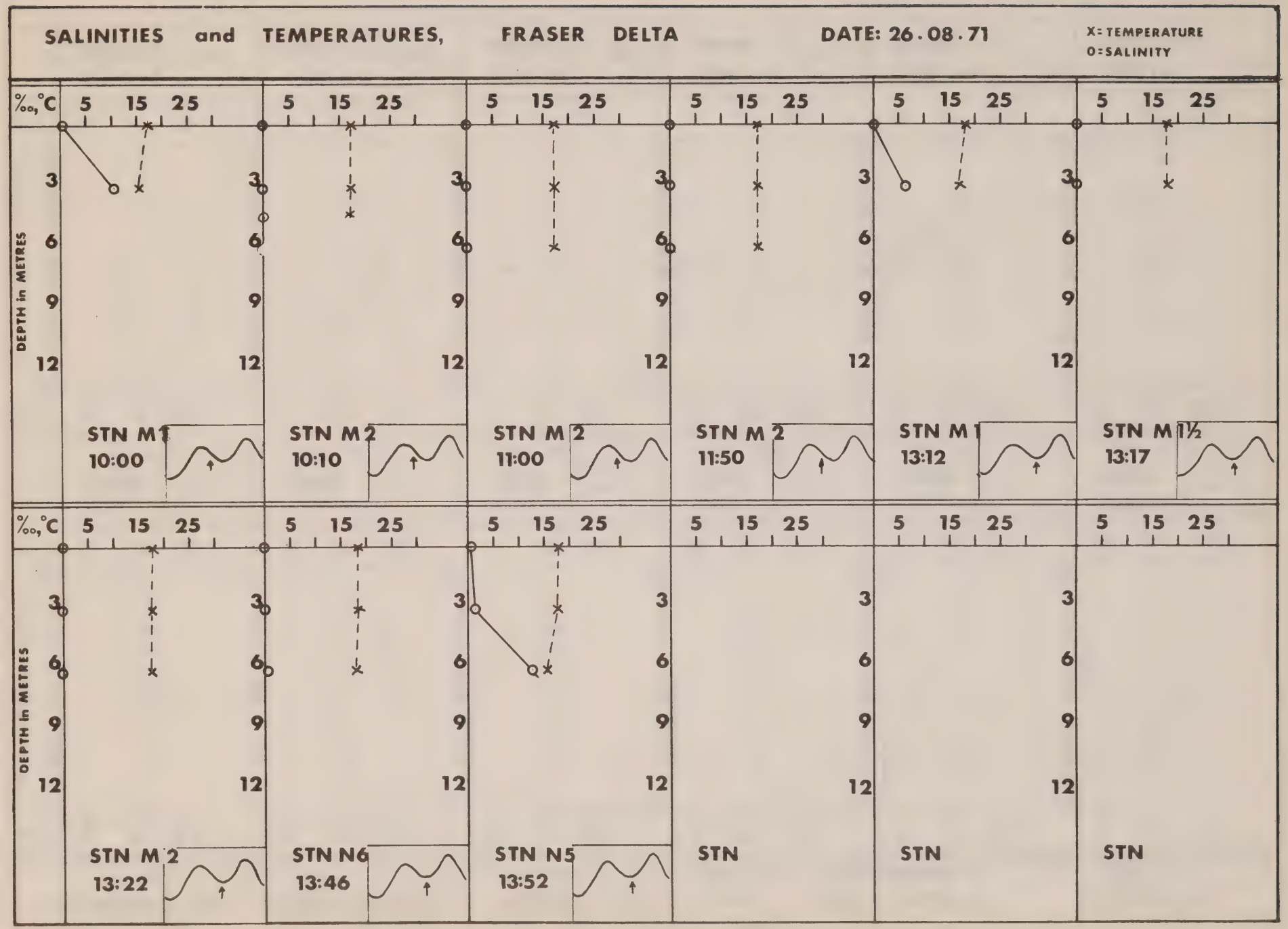

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 24.08.71
Q=102,000cfs
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN C4
05:27
STN C2
05:42
STN C1
05:52
STN C1
07:50
STN C2
07:56
STN C5
08:07
STN C6
08:13
STN 17
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STN 16
08:22
STN 15
08:29
STN 14
08:33
STN C4
08:38

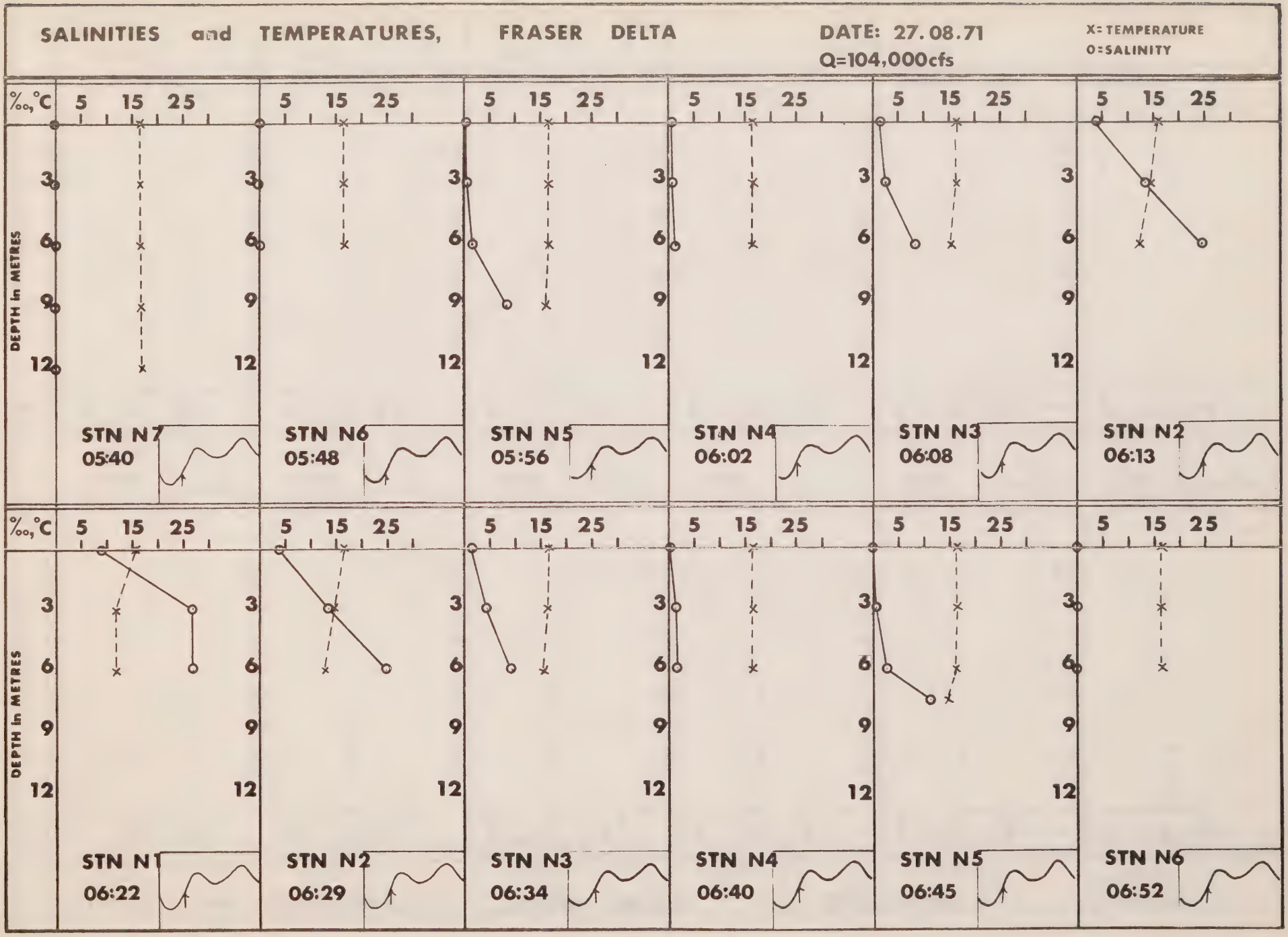

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 24.08.71
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN C7
08:43
STN 13
08:47
STN 11
08:53
STN 10
08:58
STN 8
09:03
STN 8 North
09:05
STN 8 Center
09:08
STN 8 South
09:12
STN 6
09:17
STN 8
09:24
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09:30
STN 11
09:34

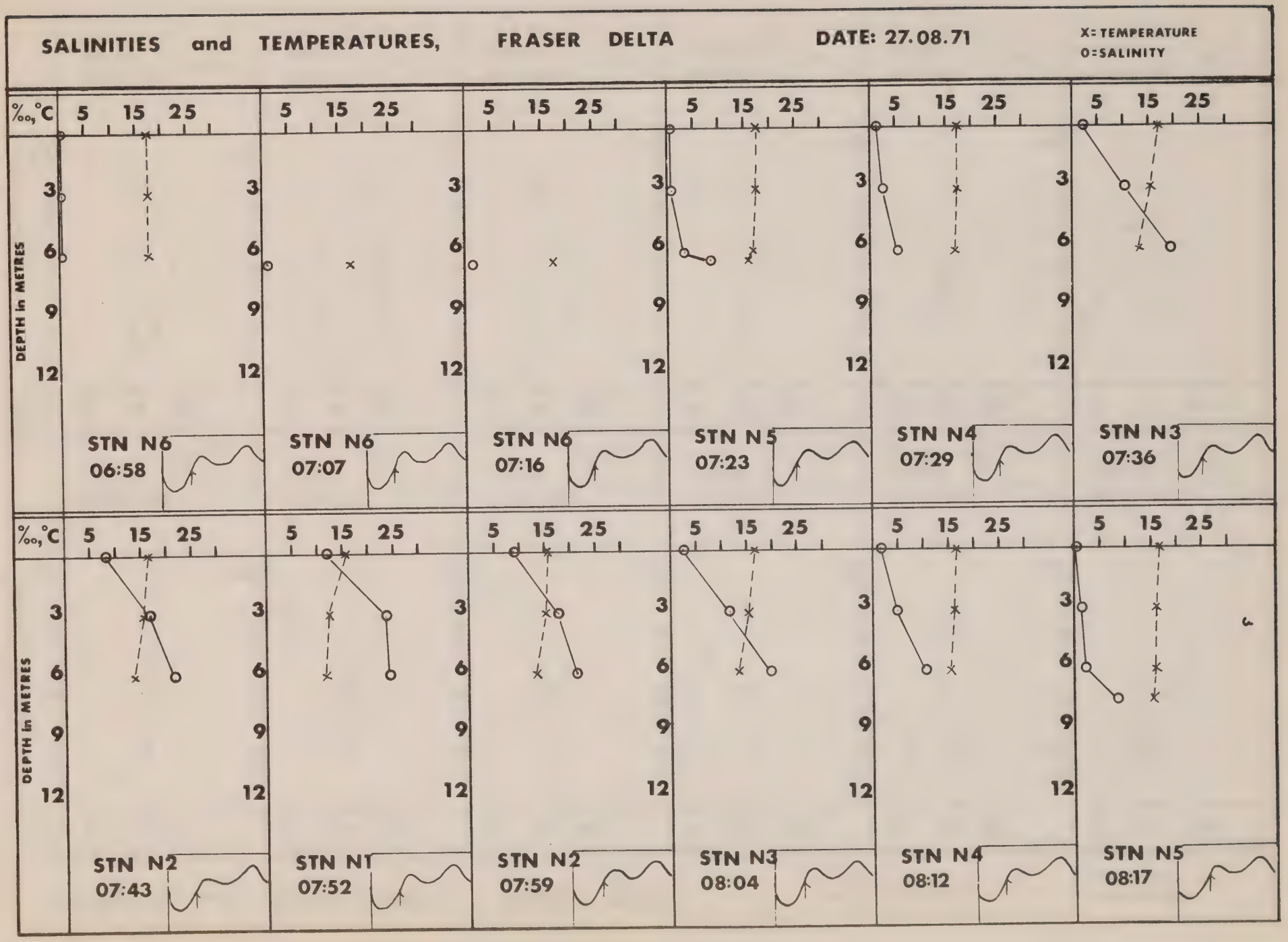

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 24.08.71
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 13
09:41
STN 14
09:47
STN 15
09:52
STN 16
10:03
STN C4
10:12
STN C7
10:15
STN C1
11:30
STN C4
11:43
STN 13
11:47
STN 11
11:52
STN 10
11:56
STN 8
12:02

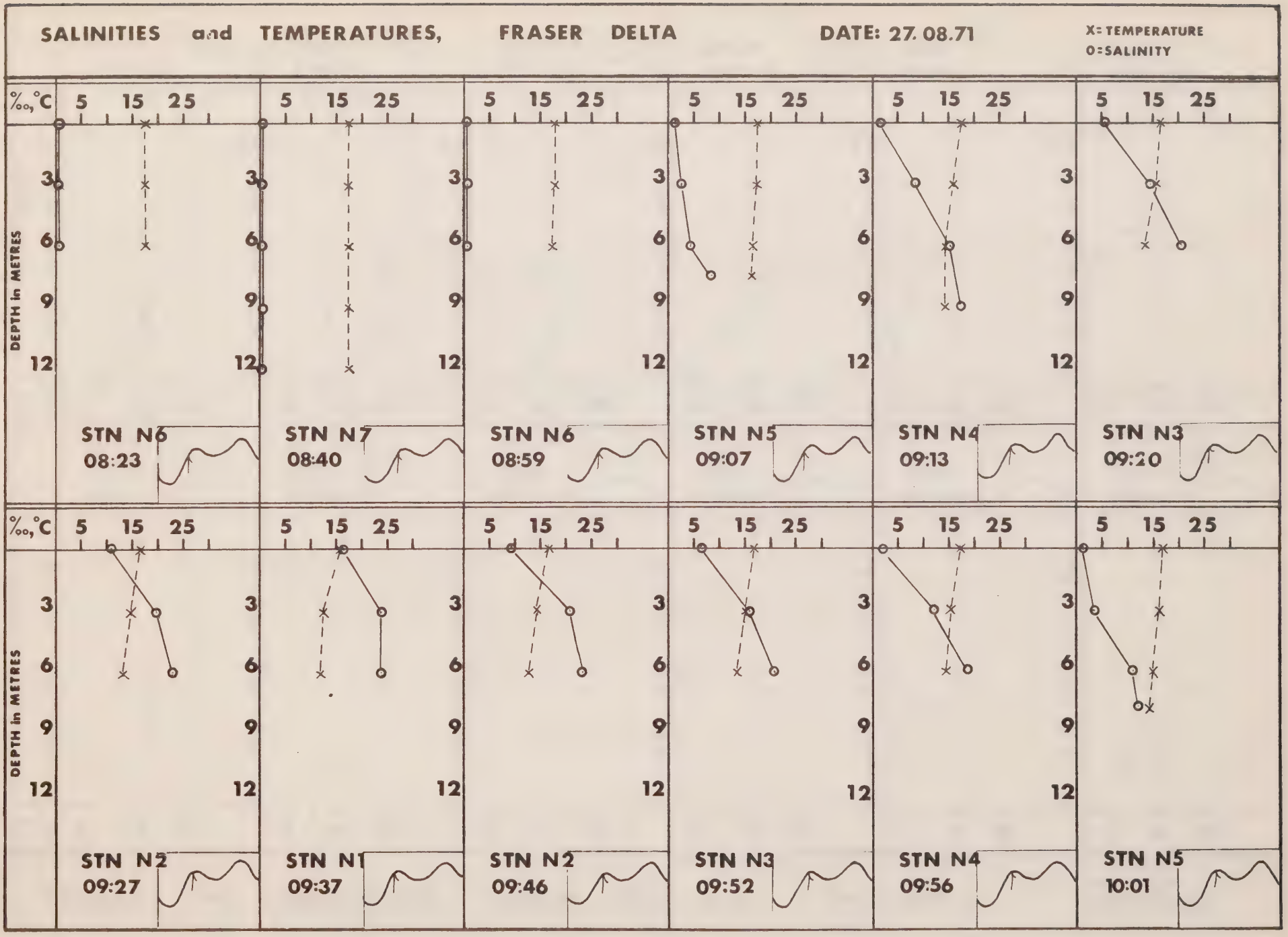

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 24.08.71
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 6
12:07
STN 4
12:13
STN 6
12:20
STN 8
12:28
STN 10
12:34
STN 11
12:39
STN 13
12:44
STN 14
12:52
STN 15
12:56
STN 16
13:04
STN
STN

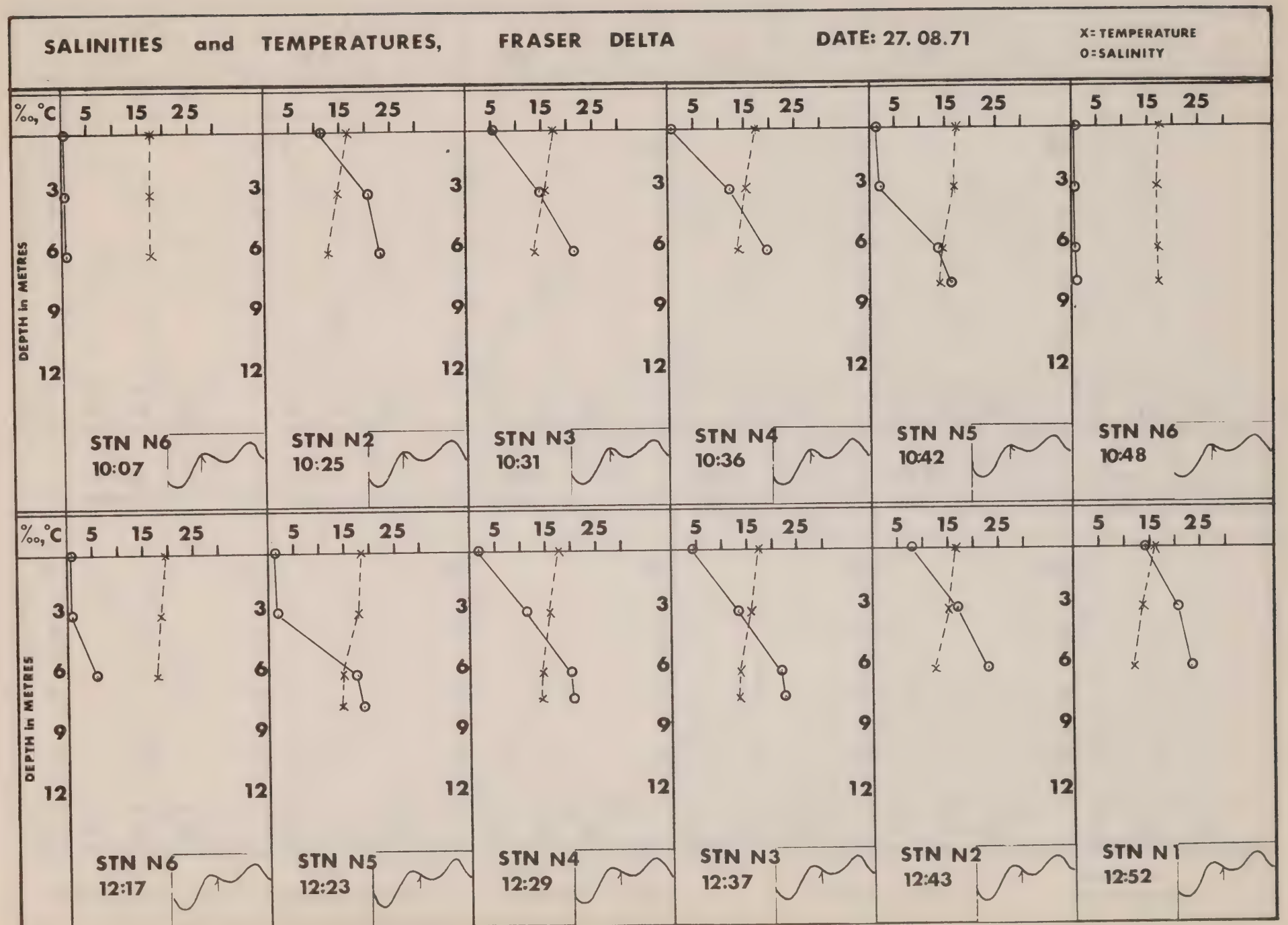

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 26.08.71
Q=105,000cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN M1
06:06
STN M1
07:00
STN M1
07:22
STN M1
07:24
STN M1
07:30
STN M1
07:46
STN M1
08:00
STN M1
08:16
STN M2
08:30
STN M1
08:39
STN M1
09:00
STN M1
09:30

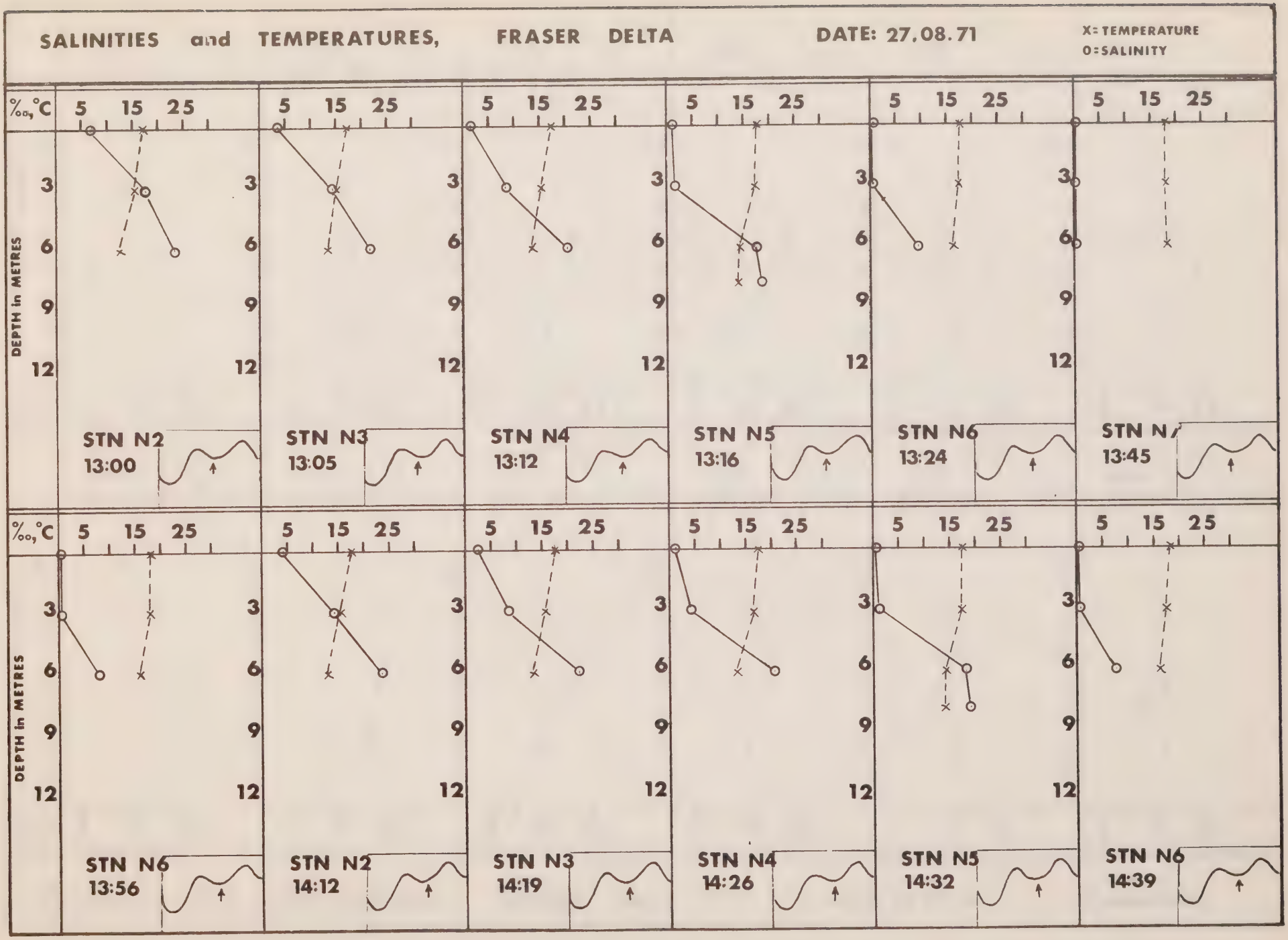

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 26.08.71
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN M1
10:00
STN M2
10:10
STN M 2
11:00
STN M 2
11:50
STN M 1
13:12
STN M 1½
13:17
STN M 2
13:22
STN N6
13:46
STN N5
13:52
STN
STN
STN

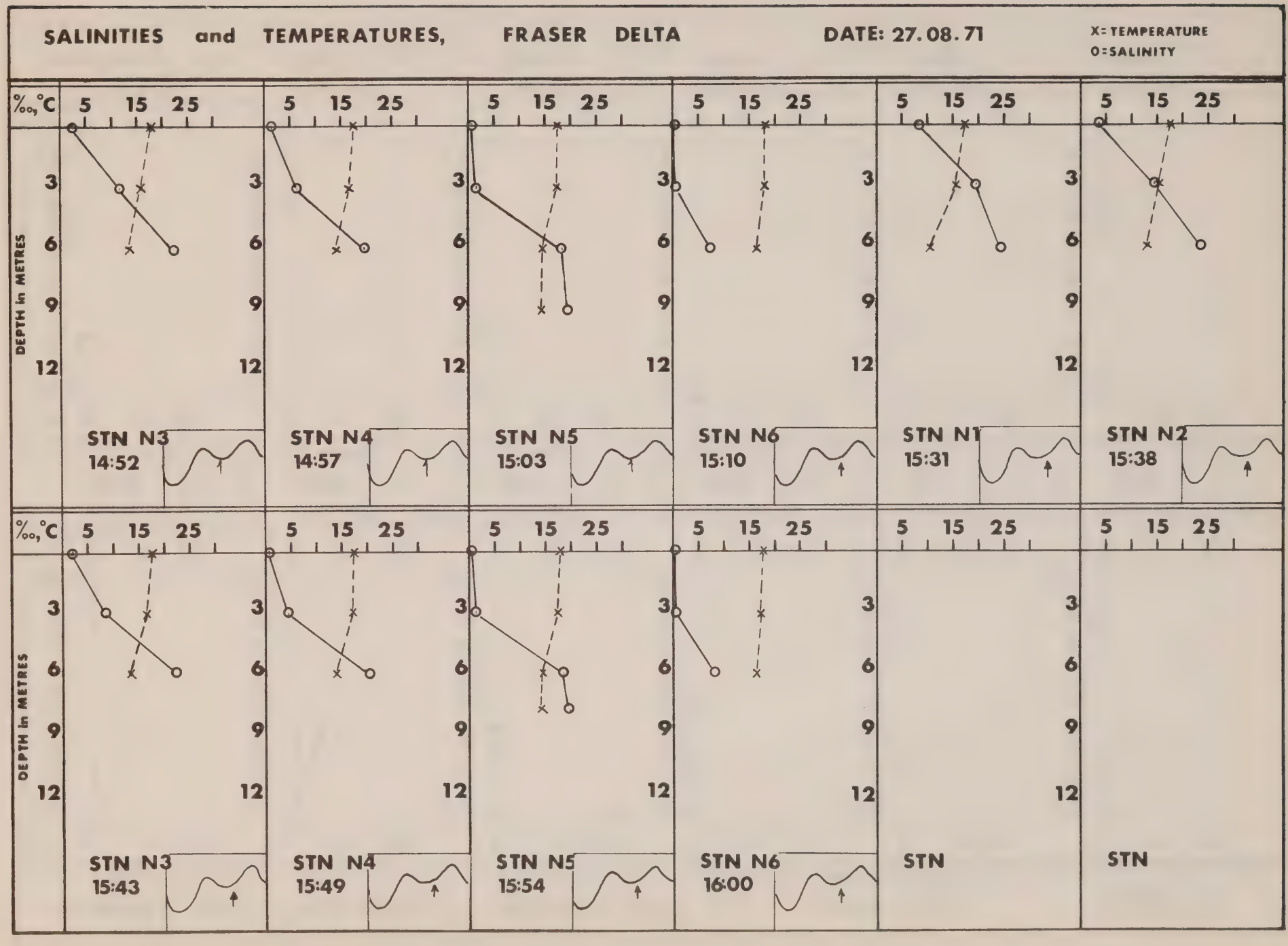

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 27.08.71
Q=104,000cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN N7
05:40
STN N6
05:48
STN N5
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STN N3
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STN N1
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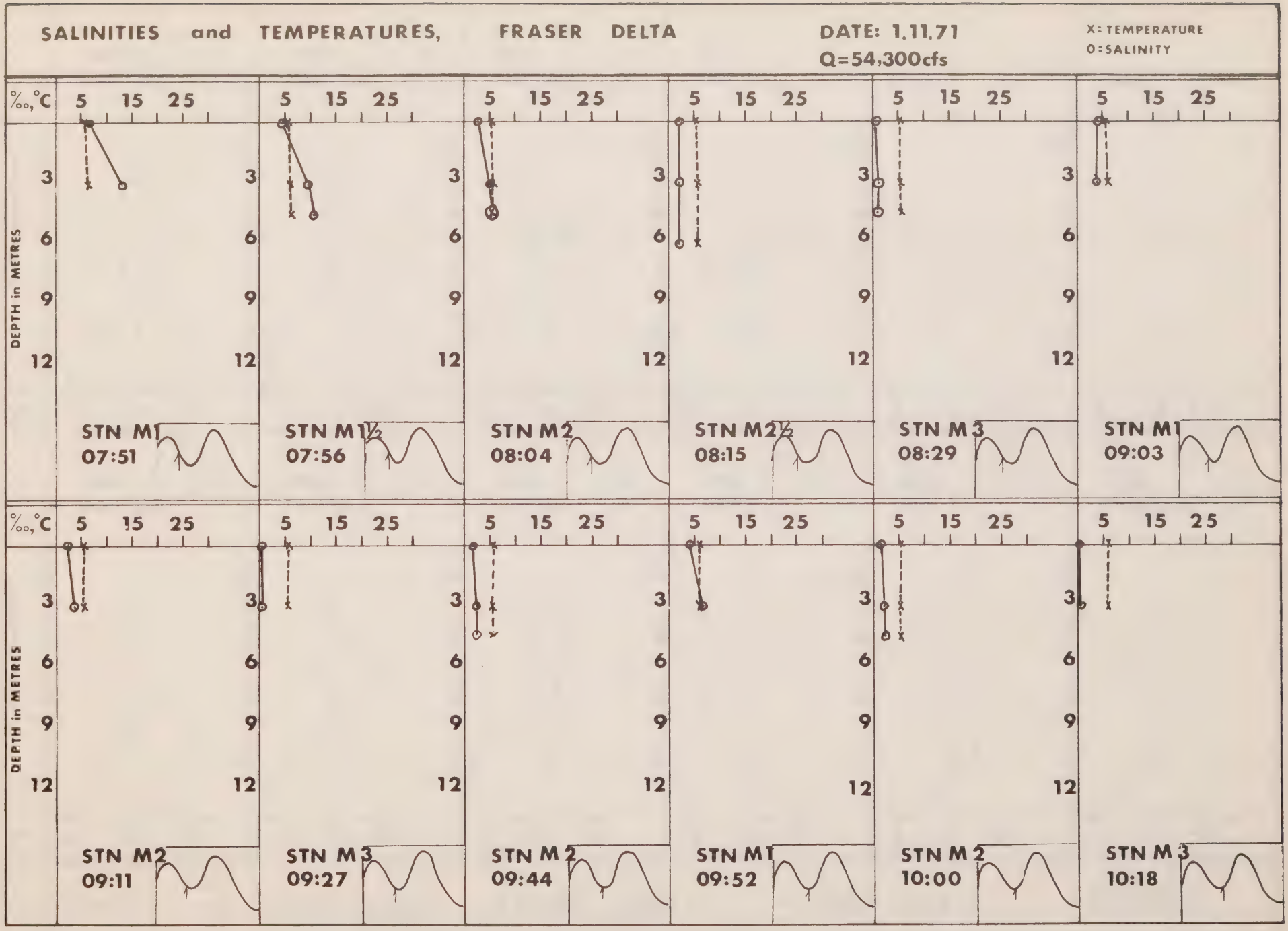

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 27.08.71
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN N6
06:58
STN N6
07:07
STN N6
07:16
STN N5
07:23
STN N4
07:29
STN N3
07:36
STN N2
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STN N2
07:59
STN N3
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STN N4
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08:17

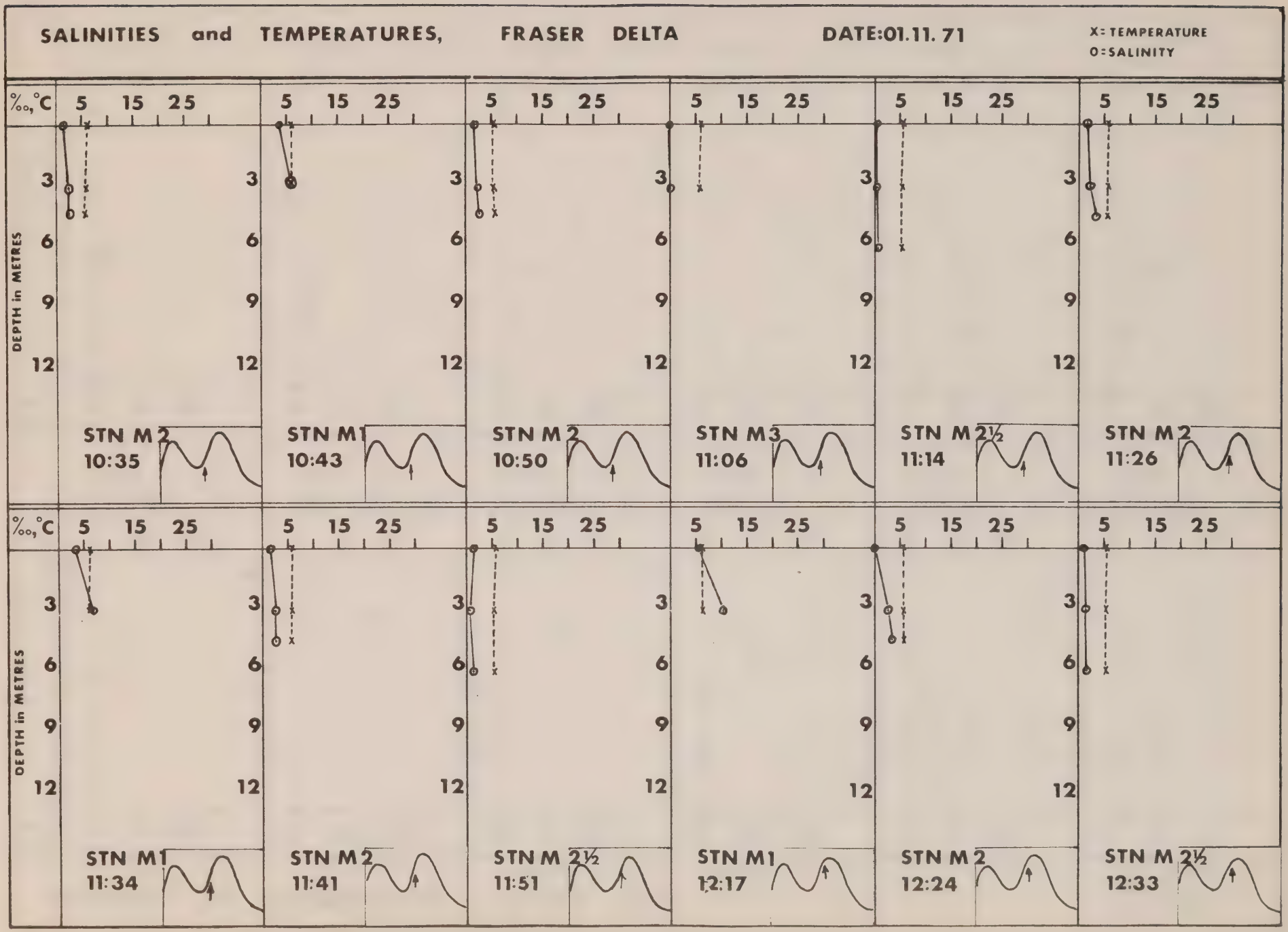

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 27.08.71
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN N6
08:23
STN N7
08:40
STN N6
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STN N5
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STN N4
09:13
STN N3
09:20
STN N2
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STN N3
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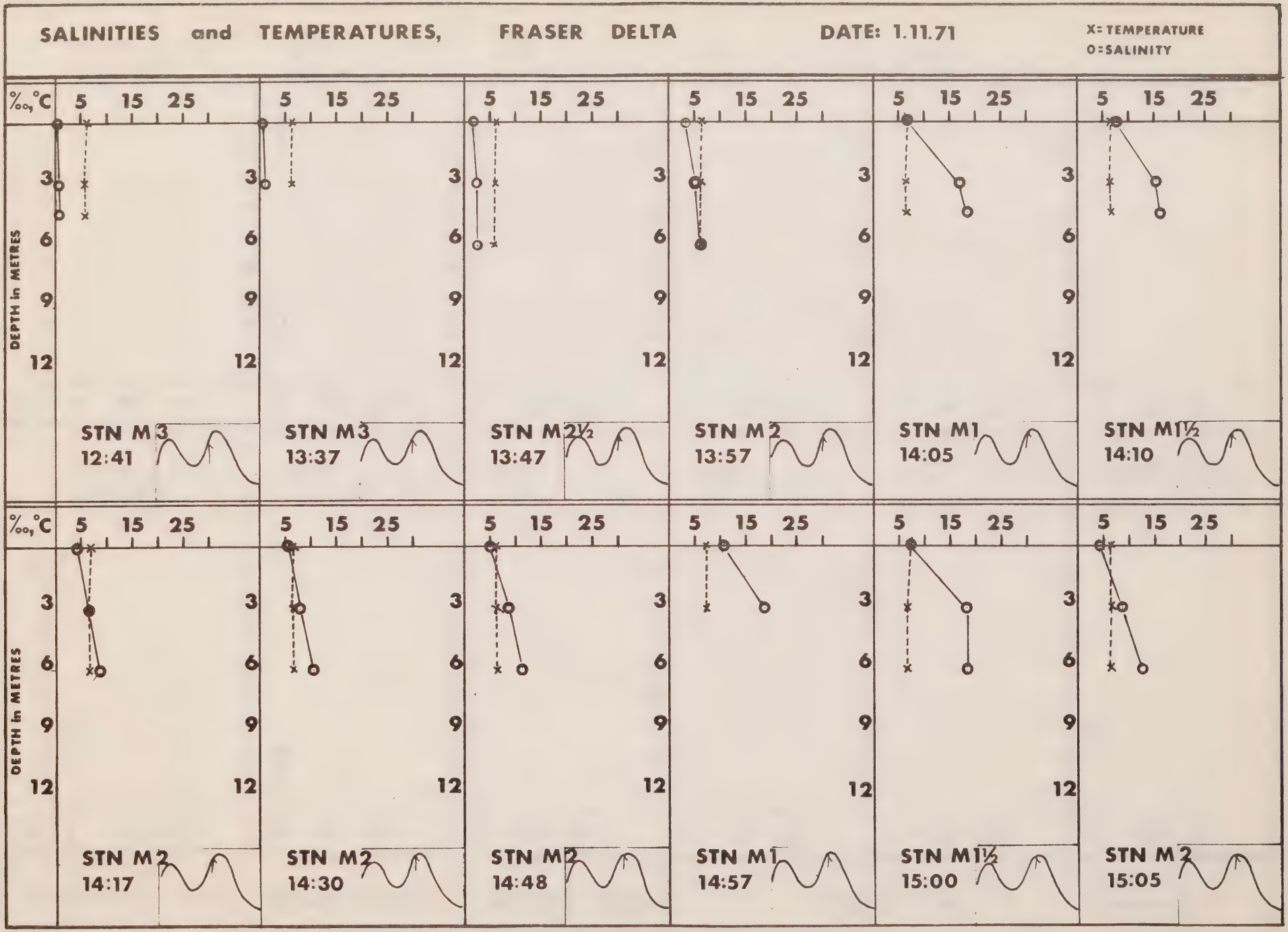

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 27. 08.71
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN N6
10:07
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10:25
STN N3
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STN N4
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STN N5
10:42
STN N6
10:48
STN N6
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STN N2
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STN N1
12:52

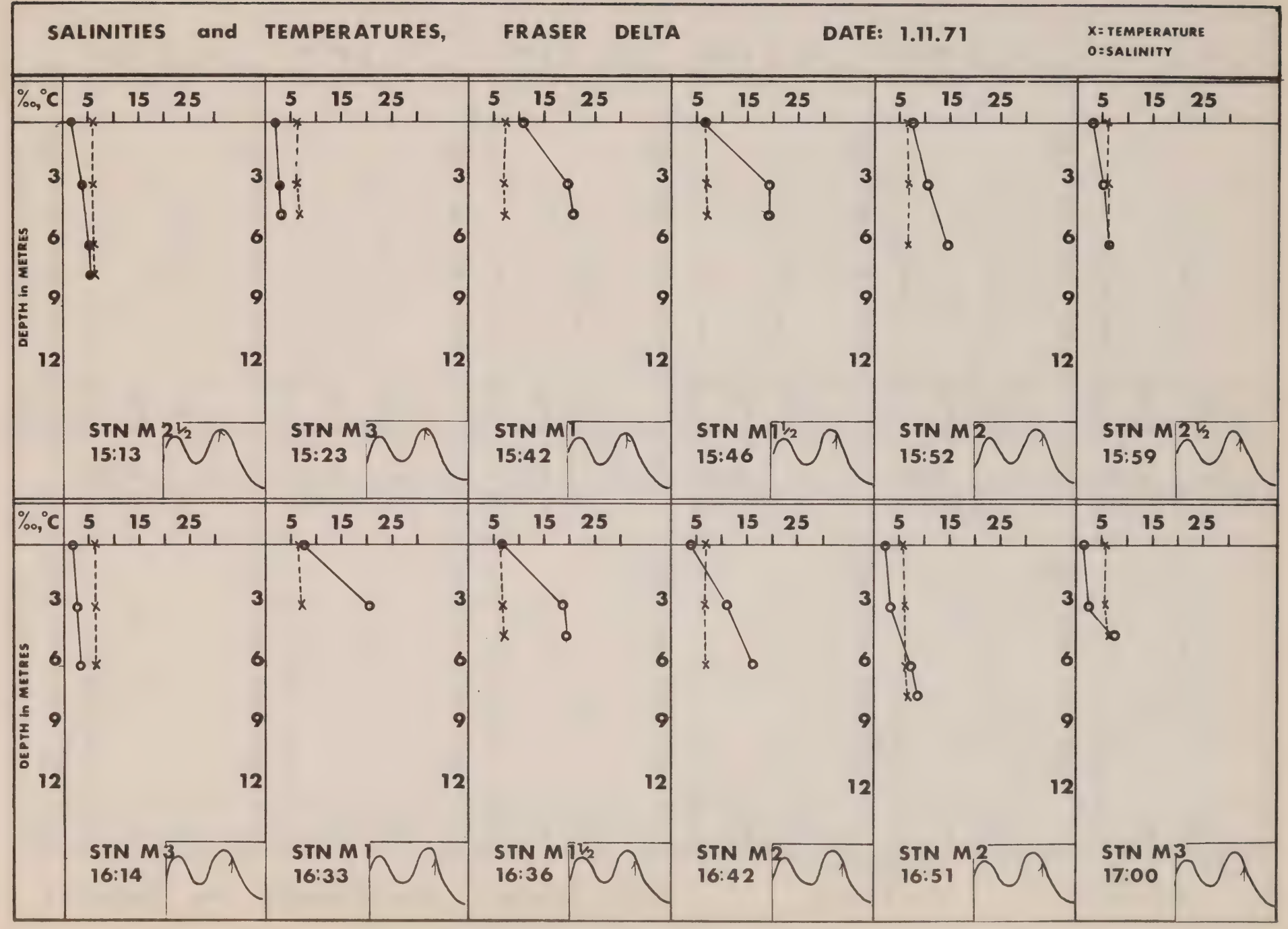

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 27,08.71
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN N2
13:00
STN N3
13:05
STN N4
13:12
STN N5
13:16
STN N6
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STN N7
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14:39

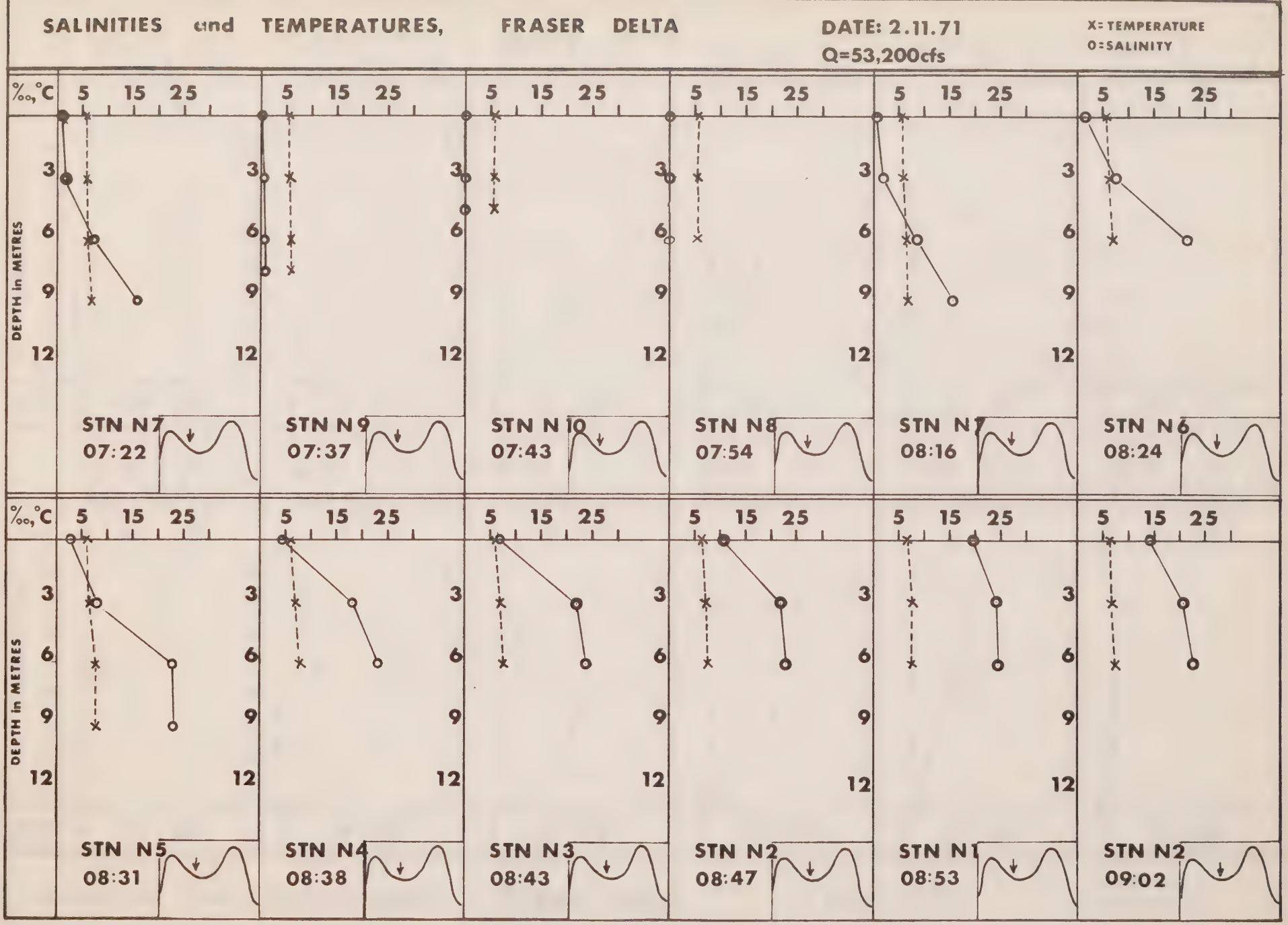

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 27.08.71
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN N3
14:52
STN N4
14:57
STN N5
15:03
STN N6
15:10
STN N1
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STN
STN

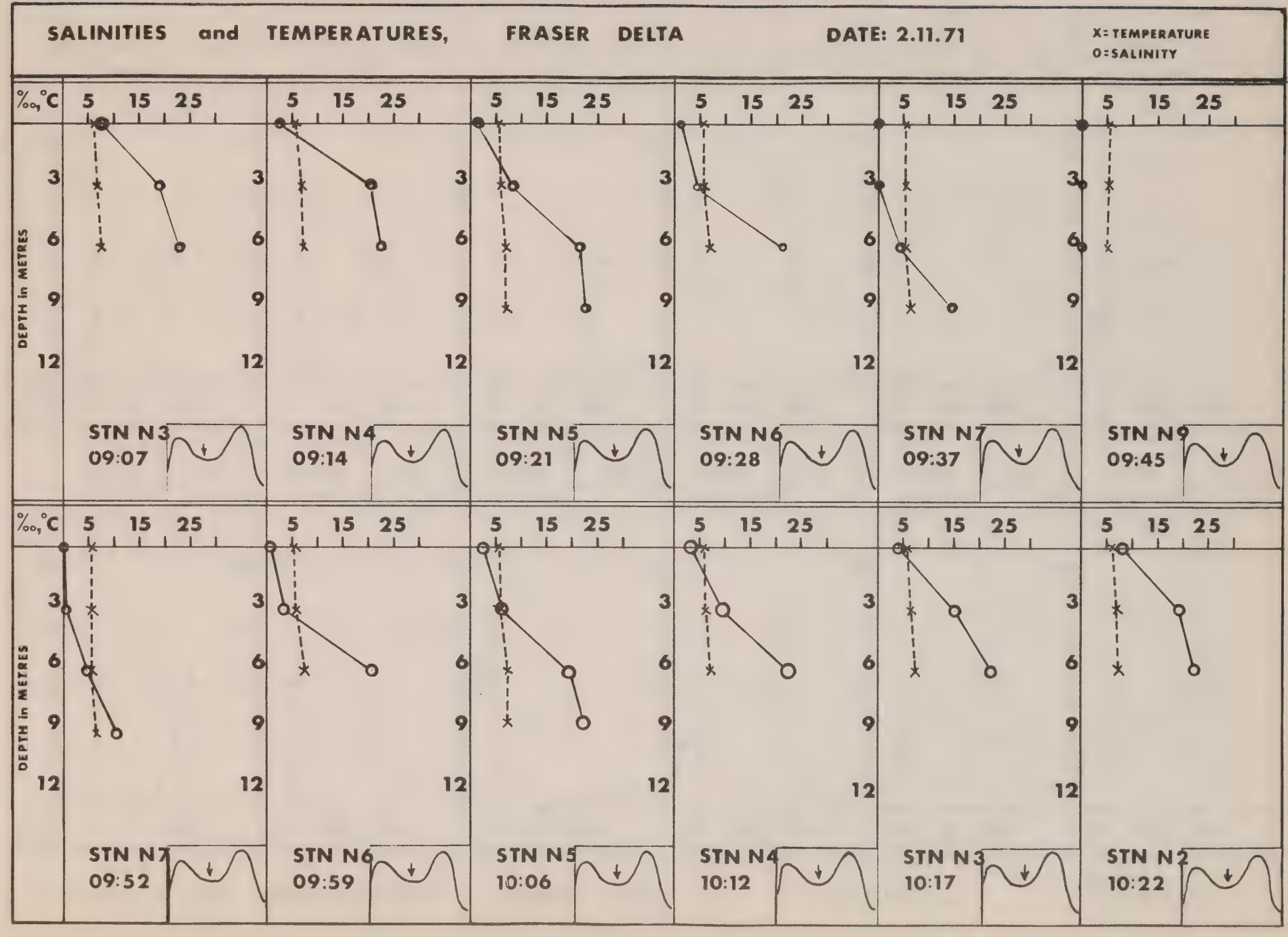

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 1.11.71
Q=54,300cfs
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN M1
07:51
STN M1½
07:56
STN M2
08:04
STN M2½
08:15
STN M3
08:29
STN M1
09:03
STN M2
09:11
STN M3
09:27
STN M2
09:44
STN M1
09:52
STN M2
10:00
STN M3
10:18

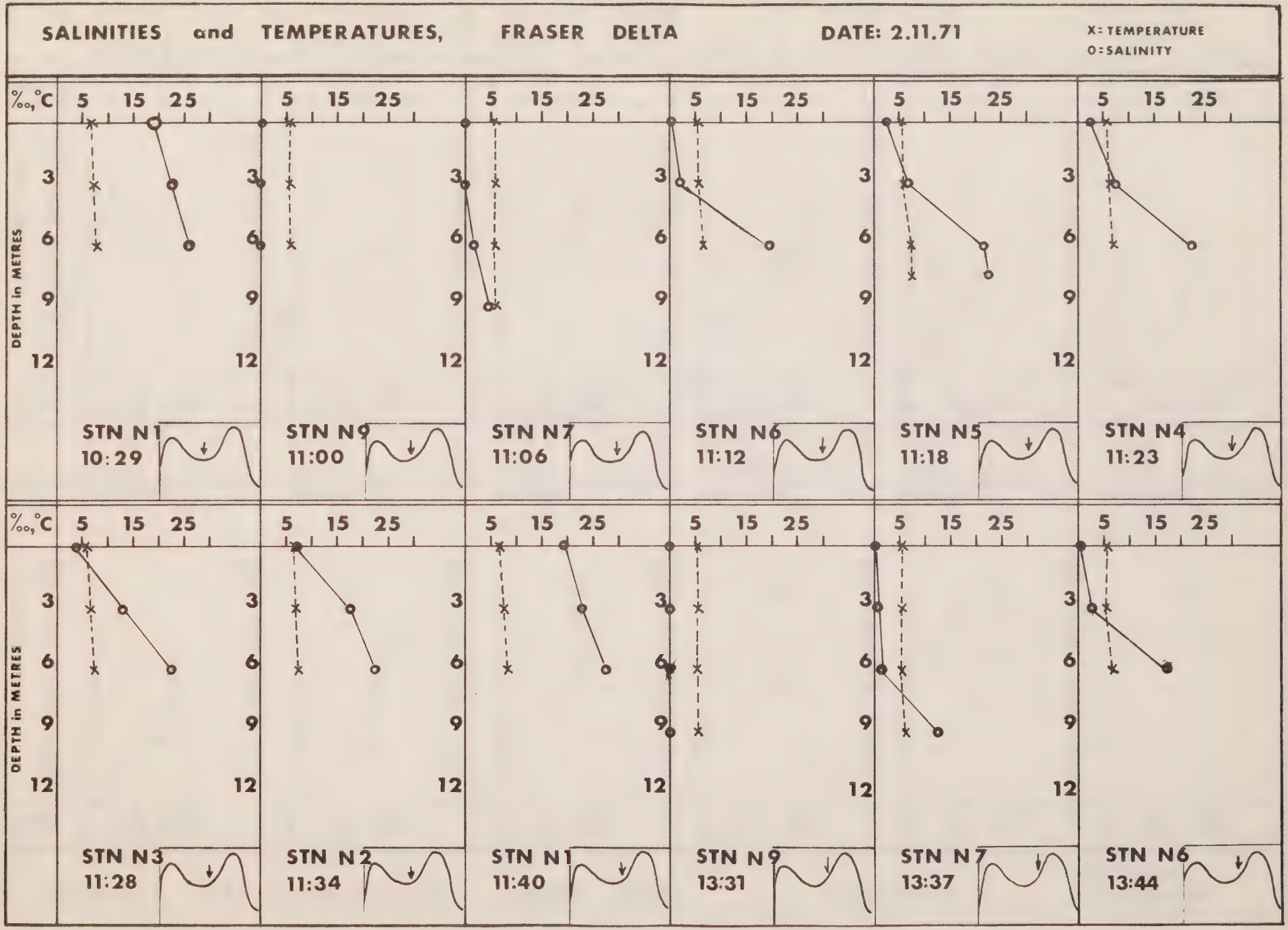

SALINITIES and TEMPERATURES, FRASER DELTA
DATE:01.11.71
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN M 2
10:35
STN M 1
10:43
STN M 2
10:50
STN M 3
11:06
STN M 2½
11:14
STN M 2
11:26
STN M 1
11:34
STN M 2
11:41
STN M 2½
11:51
STN M 1
12:17
STN M 2
12:24
STN M 2½
12:33

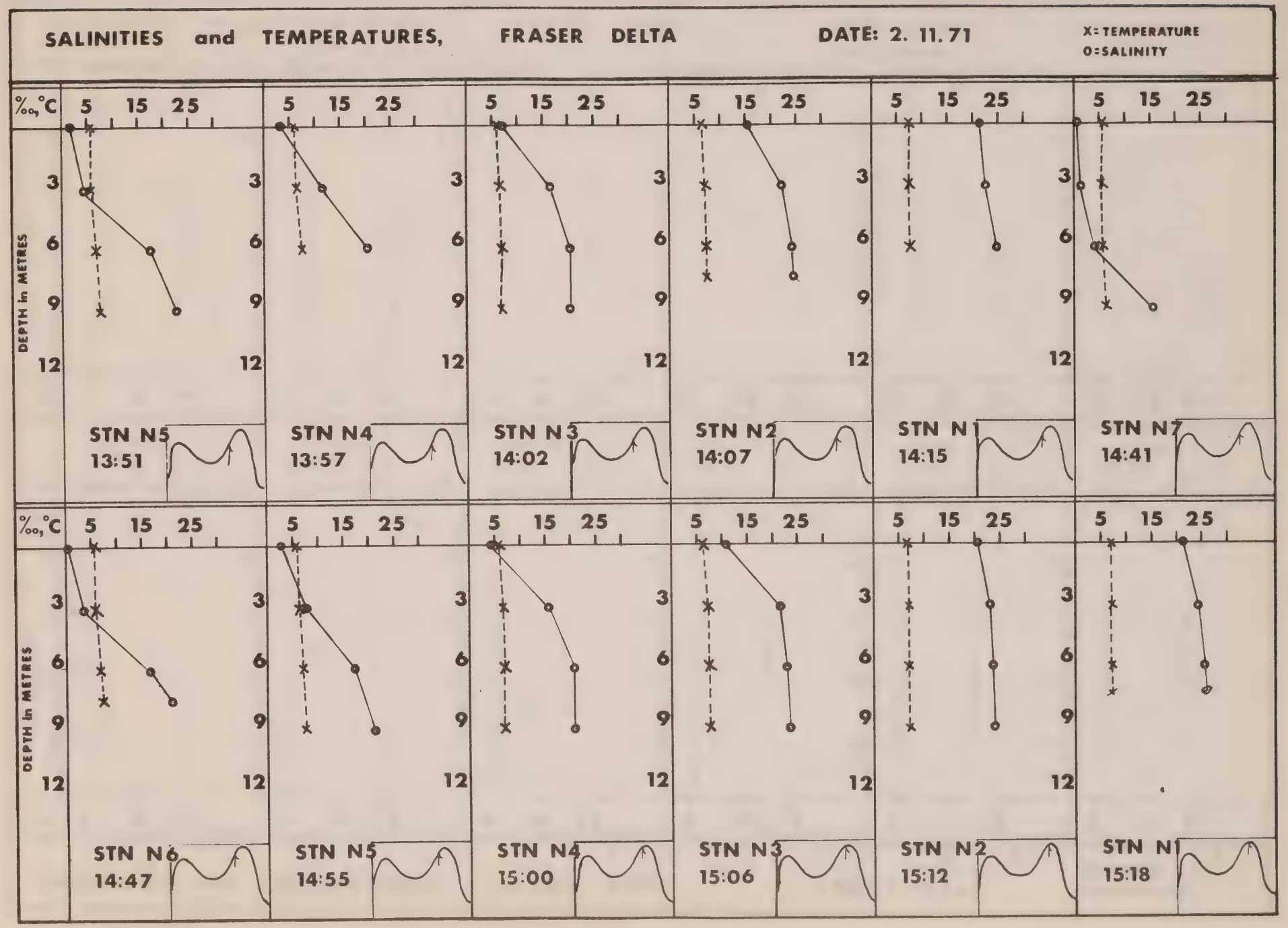

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 1.11.71
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN M3
12:41
STN M3
13:37
STN M2½
13:47
STN M2
13:57
STN M1
14:05
STN M1½
14:10
STN M2
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STN M1½
15:00
STN M2
15:05

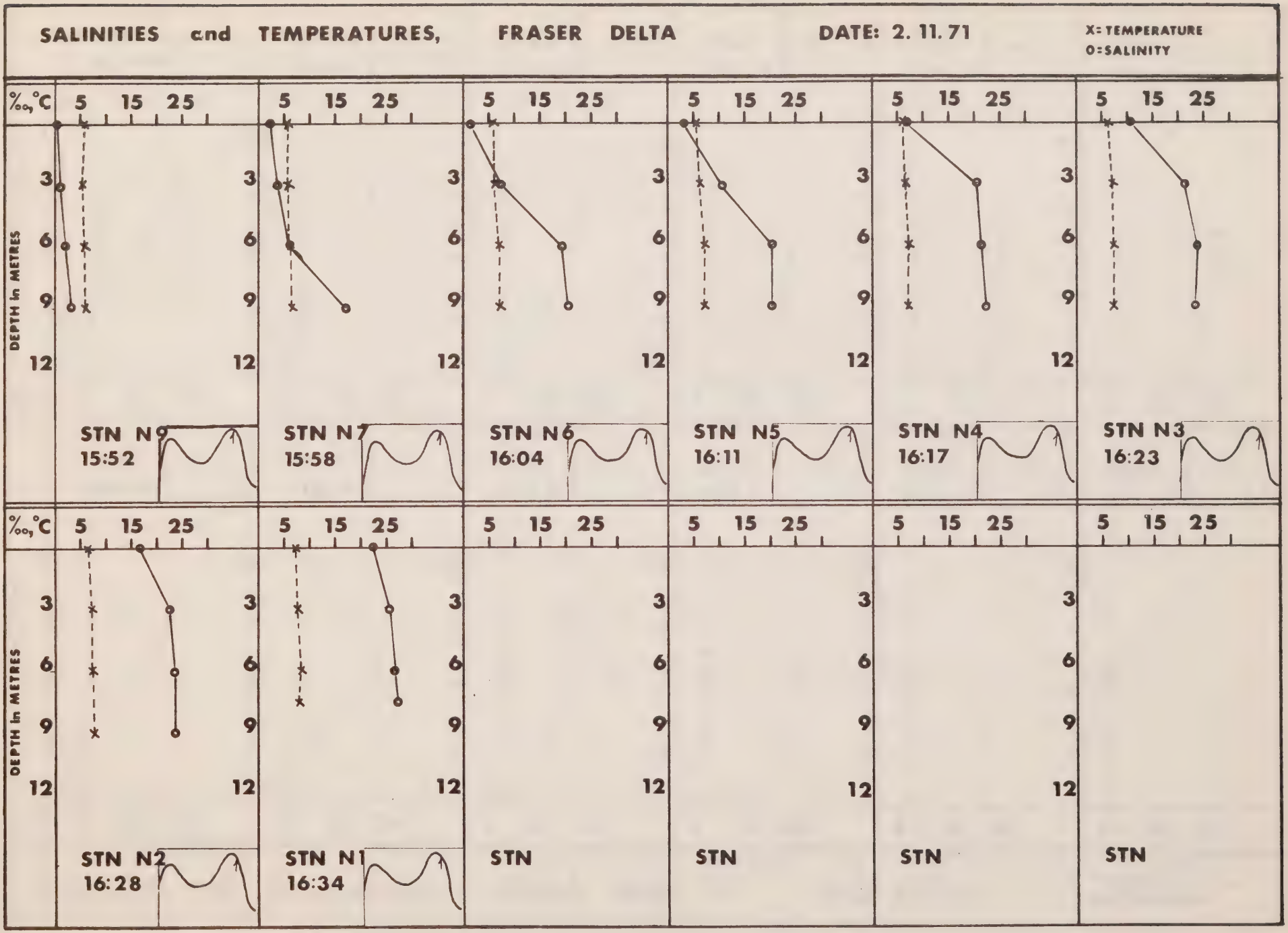

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 1.11.71
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN M 2½
15:13
STN M 3
15:23
STN M 1
15:42
STN M 1½
15:46
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STN M 3
17:00

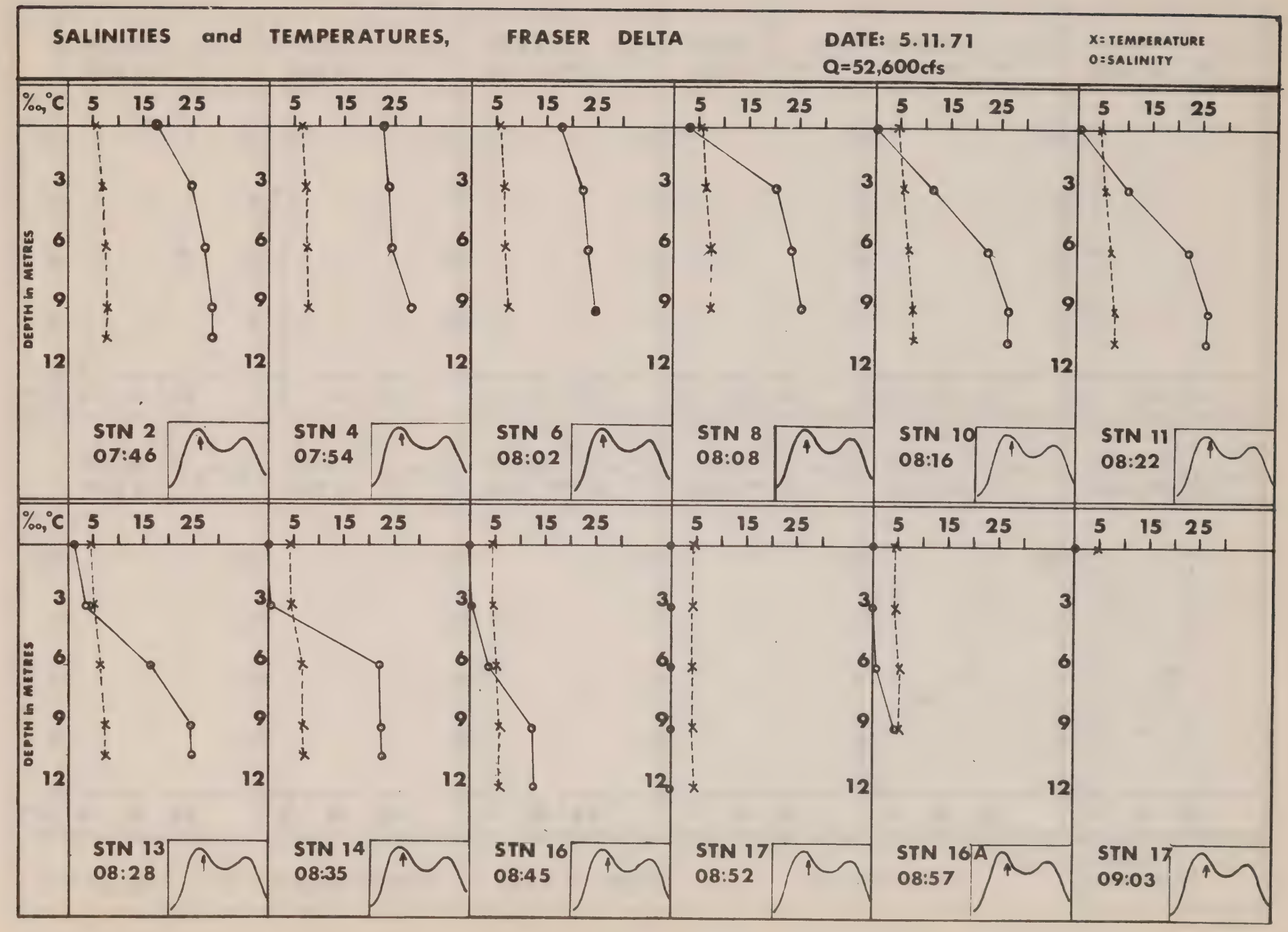

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 2.11.71
Q=53,200cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN N7
07:22
STN N9
07:37
STN N10
07:43
STN N8
07:54
STN N7
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08:24
STN N5
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STN N4
08:38
STN N3
08:43
STN N2
08:47
STN N1
08:53
STN N2
09:02

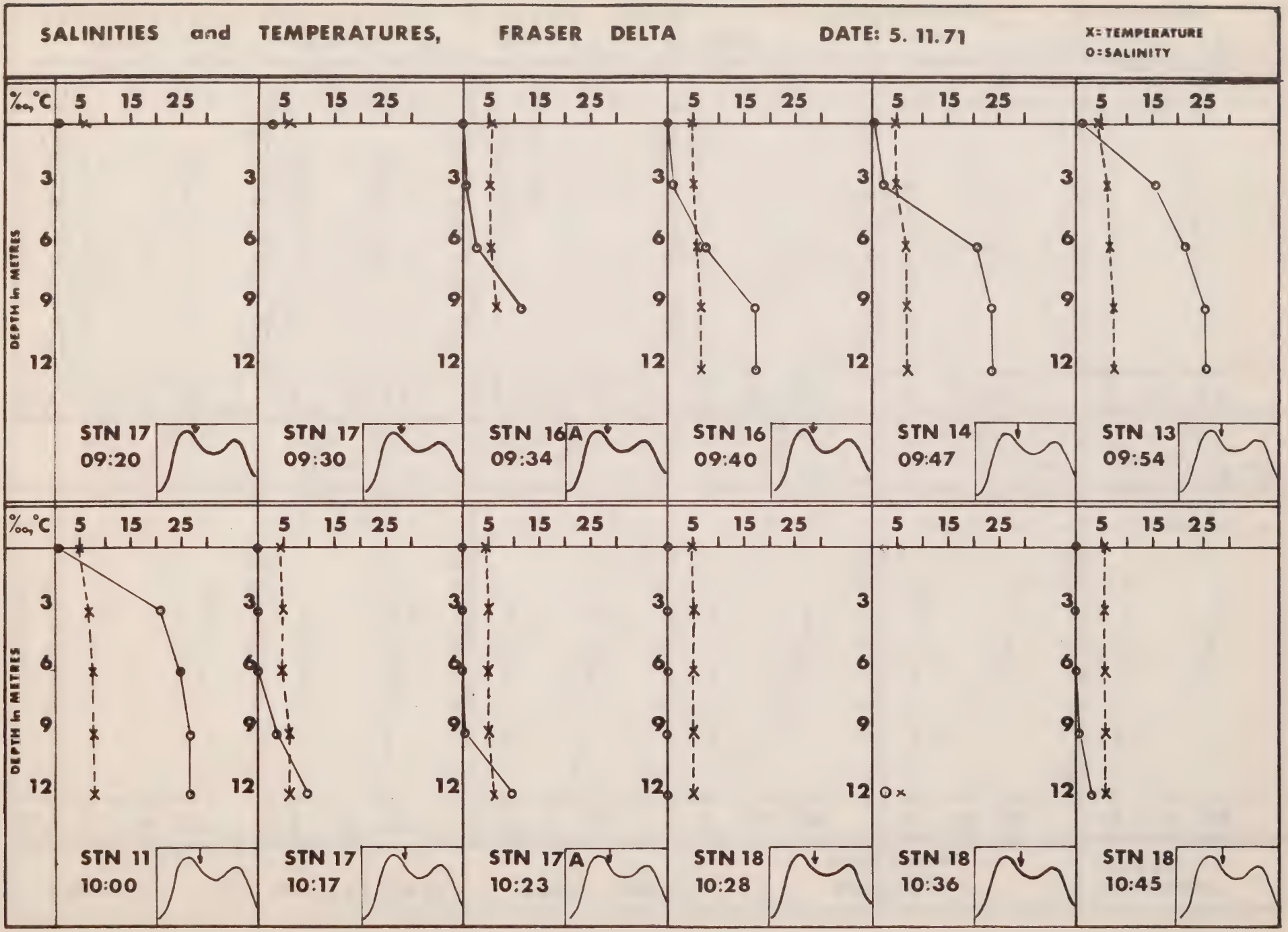

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 2.11.71
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN N3
09:07
STN N4
09:14
STN N5
09:21
STN N6
09:28
STN N7
09:37
STN N9
09:45
STN N7
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STN N5
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STN N4
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STN N3
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STN N2
10:22

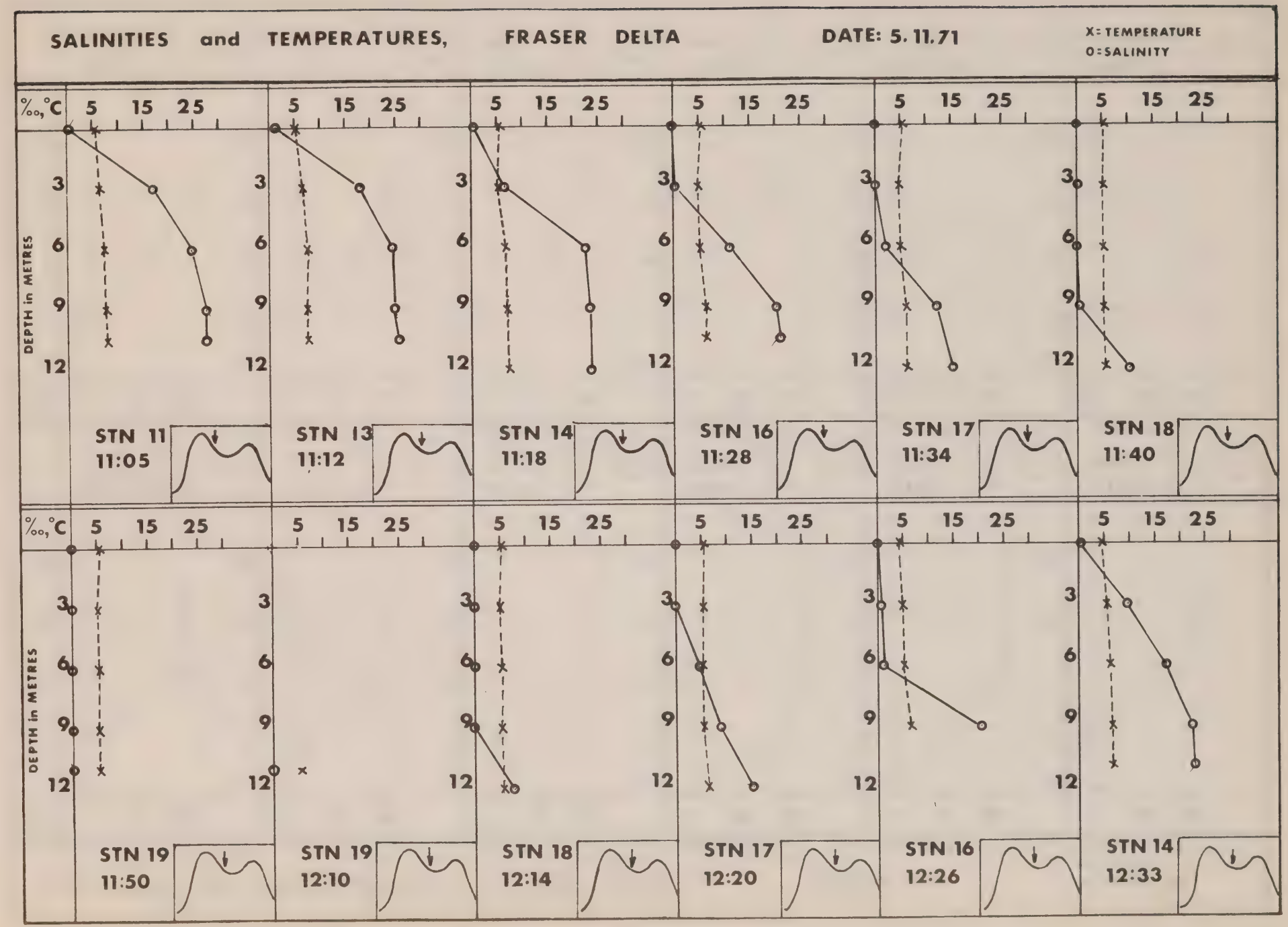

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 2.11.71
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN N1
10:29
STN N9
11:00
STN N7
11:06
STN N6
11:12
STN N5
11:18
STN N4
11:23
STN N3
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STN N7
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STN N6
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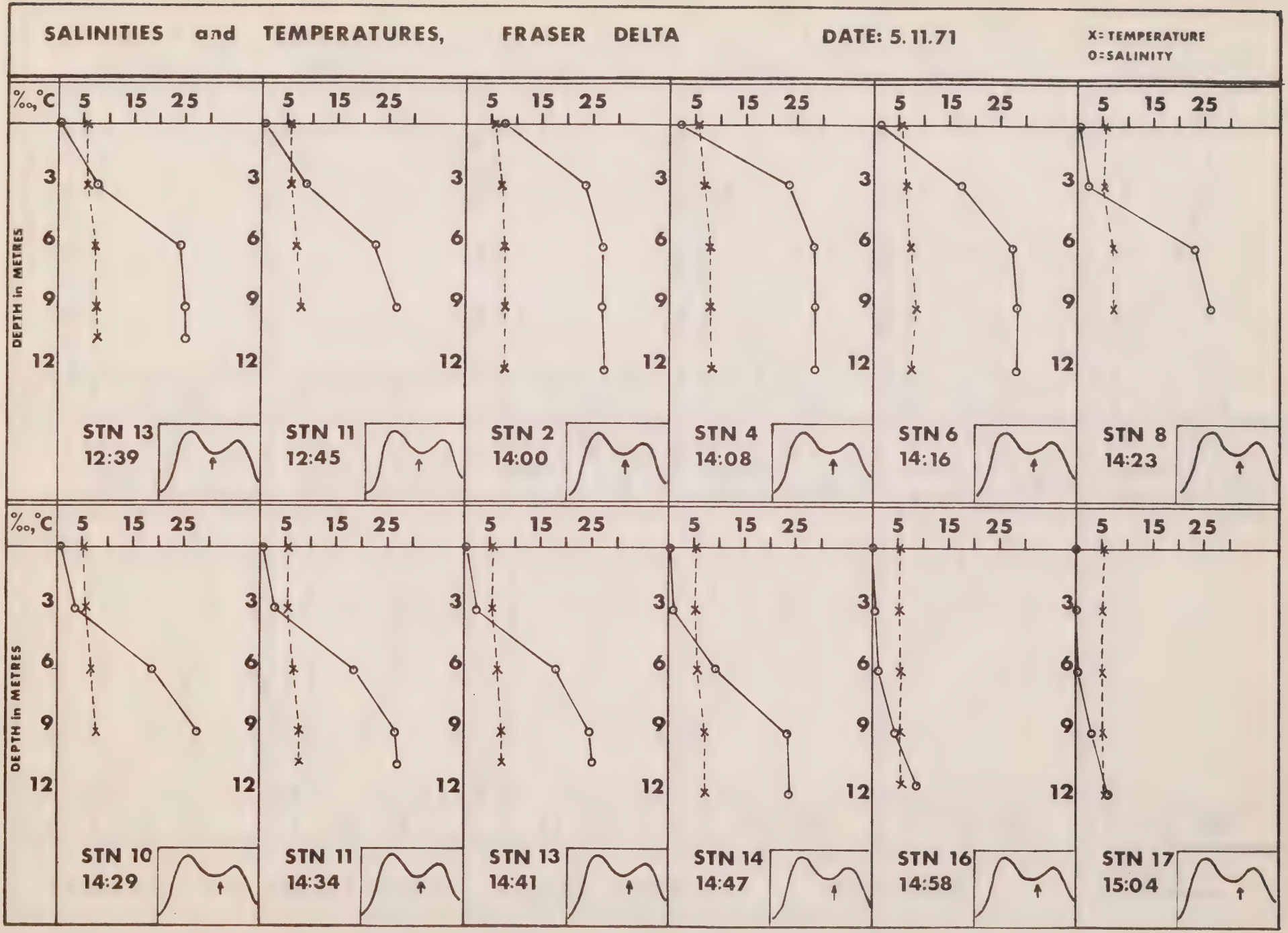

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 2. 11. 71
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN N5
13:51
STN N4
13:57
STN N3
14:02
STN N2
14:07
STN N1
14:15
STN N7
14:41
STN N6
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STN N4
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STN N3
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STN N2
15:12
STN N1
15:18

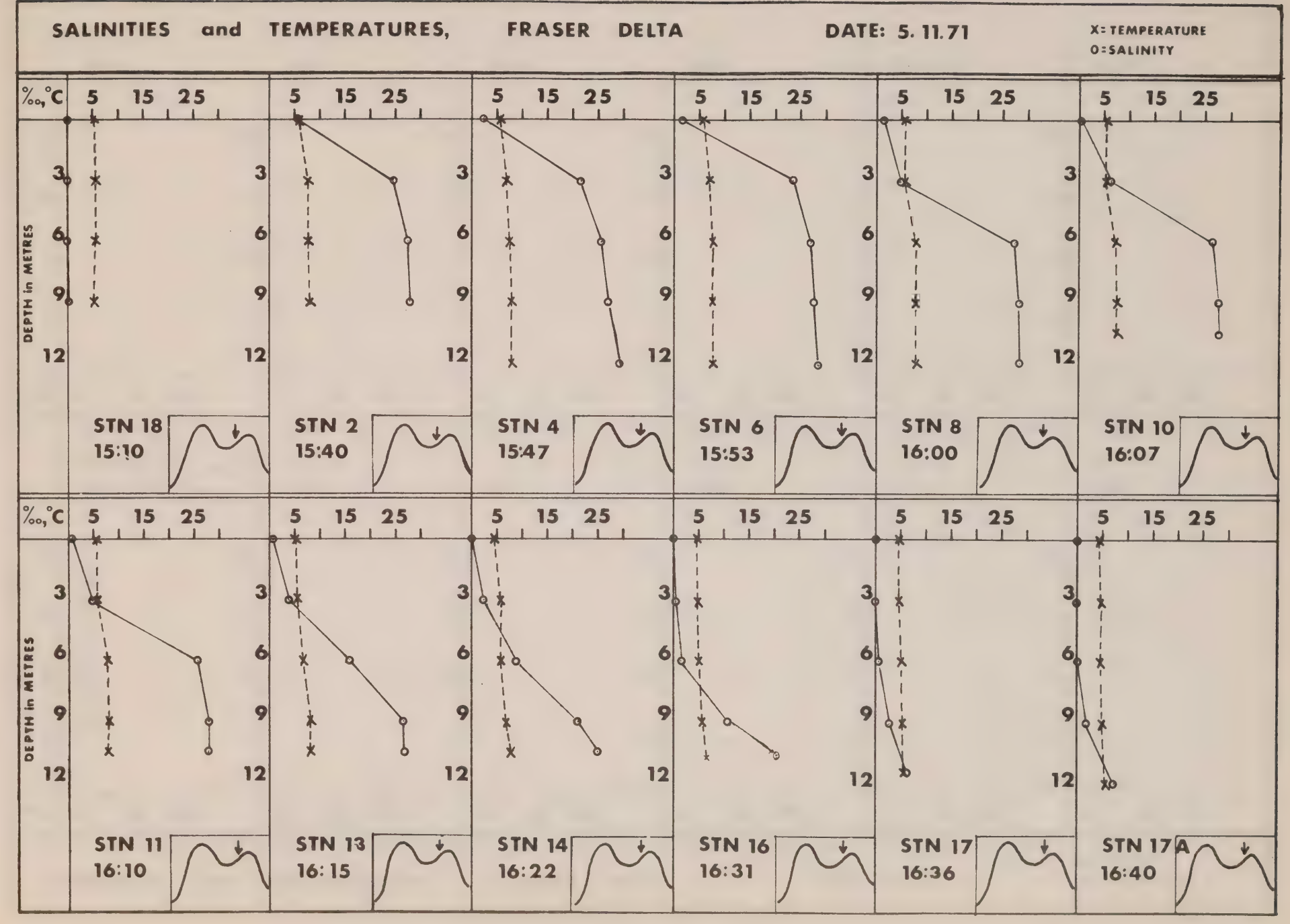

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 2. 11. 71
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN N9
15:52
STN N7
15:58
STN N6
16:04
STN N5
16:11
STN N4
16:17
STN N3
16:23
STN N2
16:28
STN N1
16:34
STN
STN
STN
STN


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 5.11.71
Q=52,600cfs
X= TEMPERATURE
O=SALINITY
‰, °C
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DEPTH in METRES
3
6
9
12
STN 2
07:46
STN 4
07:54
STN 6
08:02
STN 8
08:08
STN 10
08:16
STN 11
08:22
STN 13
08:28
STN 14
08:35
STN 16
08:45
STN 17
08:52
STN 16A
08:57
STN 17
09:03


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 5. 11.71
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 17
09:20
STN 17
09:30
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STN 16
09:40
STN 14
09:47
STN 13
09:54
STN 11
10:00
STN 17
10:17
STN 17A
10:23
STN 18
10:28
STN 18
10:36
STN 18
10:45


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 5. 11. 71
X = TEMPERATURE
O = SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 11
11:05
STN 13
11:12
STN 14
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STN 16
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STN 18
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11:50
STN 19
12:10
STN 18
12:14
STN 17
12:20
STN 16
12:26
STN 14
12:33


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 5.11.71
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 13
12:39
STN 11
12:45
STN 2
14:00
STN 4
14:08
STN 6
14:16
STN 8
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STN 10
14:29
STN 11
14:34
STN 13
14:41
STN 14
14:47
STN 16
14:58
STN 17
15:04


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 5. 11. 71
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 18
15:10
STN 2
15:40
STN 4
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STN 6
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STN 8
16:00
STN 10
16:07
STN 11
16:10
STN 13
16:15
STN 14
16:22
STN 16
16:31
STN 17
16:36
STN 17A
16:40

SALINITIES and TEMPERATURES, FRASER DELTA DATE: 5.11.71

X: TEMPERATURE
O: SALINITY

‰, °C 5 15 25

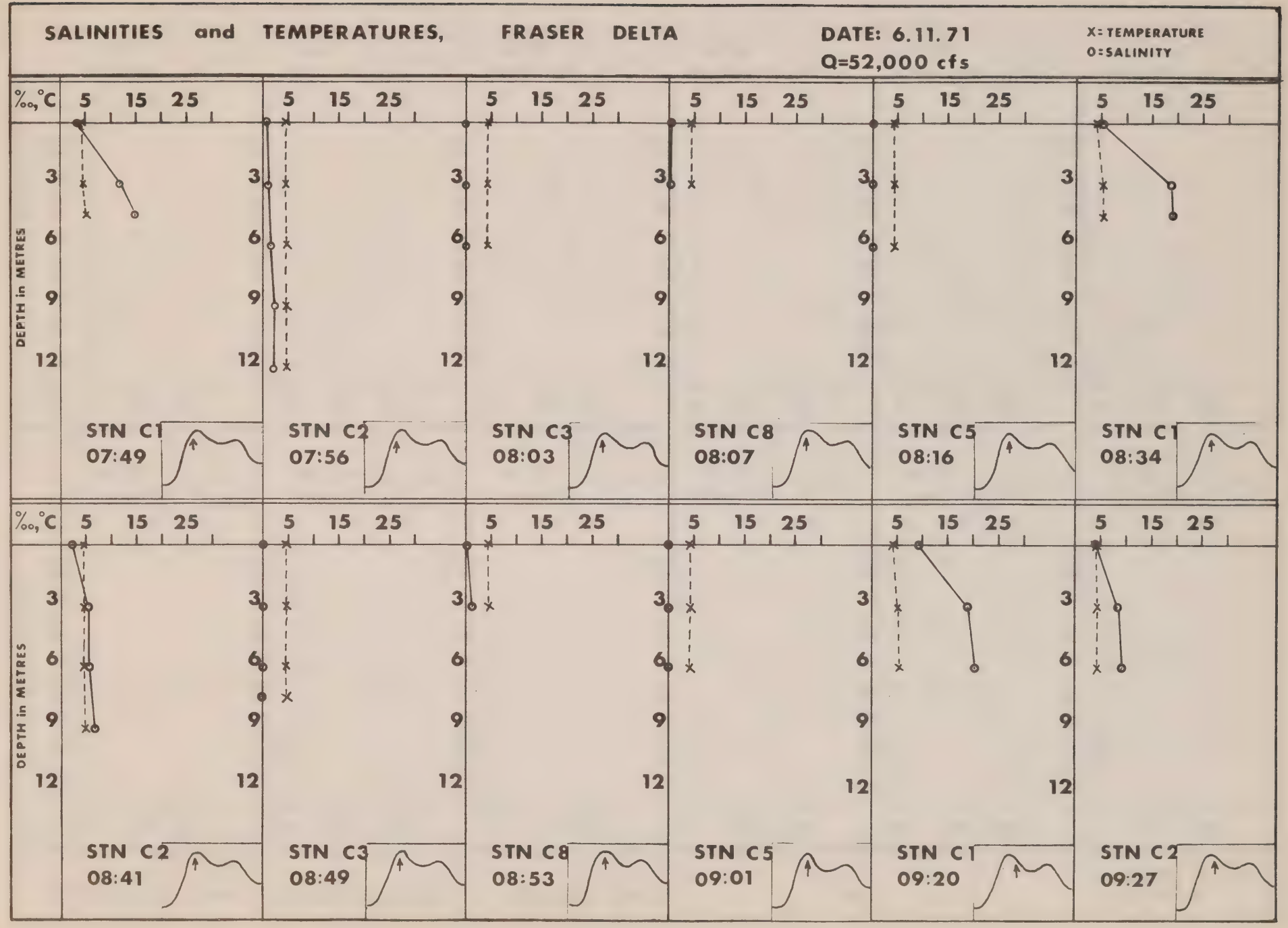
DEPTH in METRES

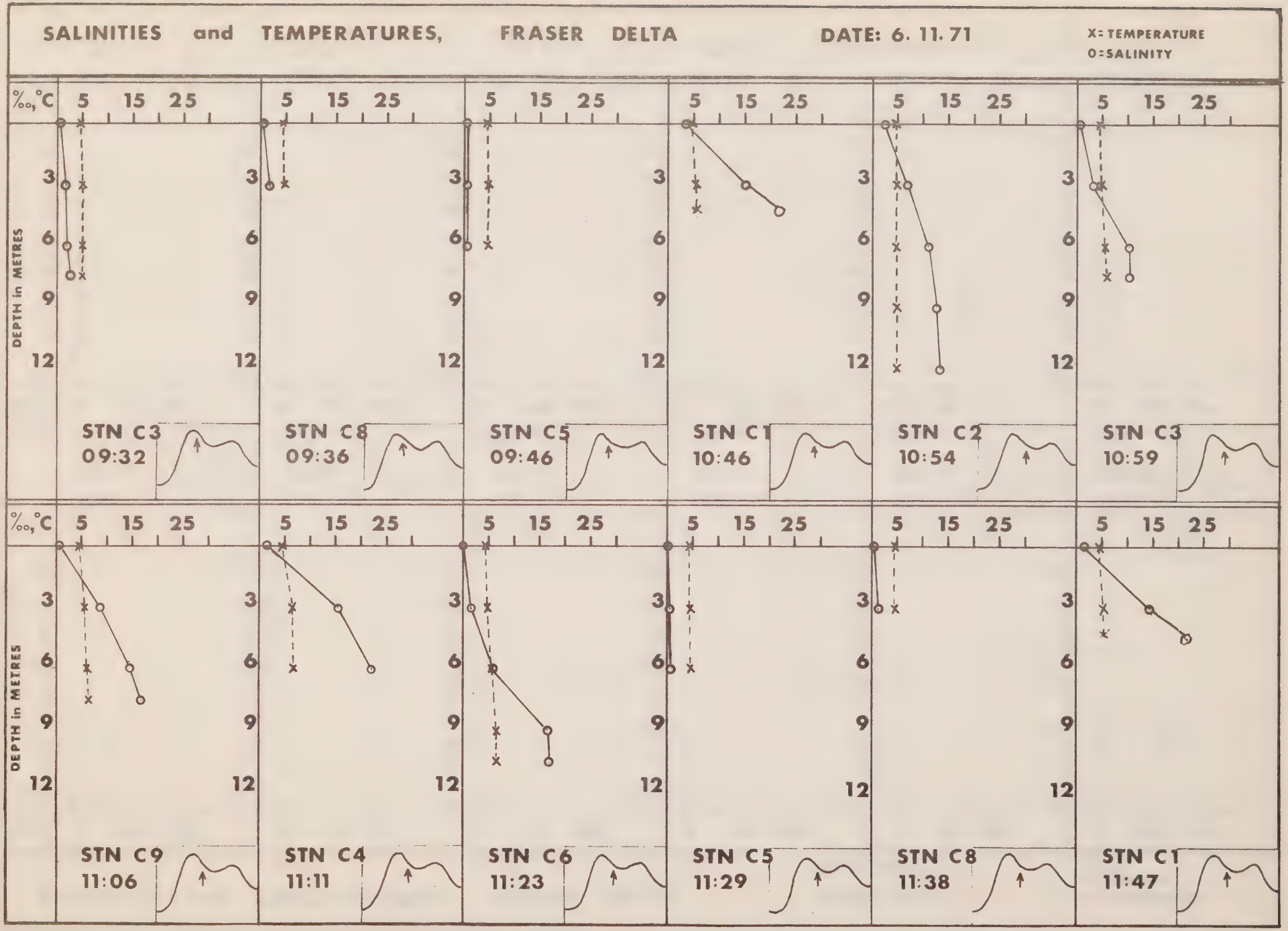
3
6
9
12

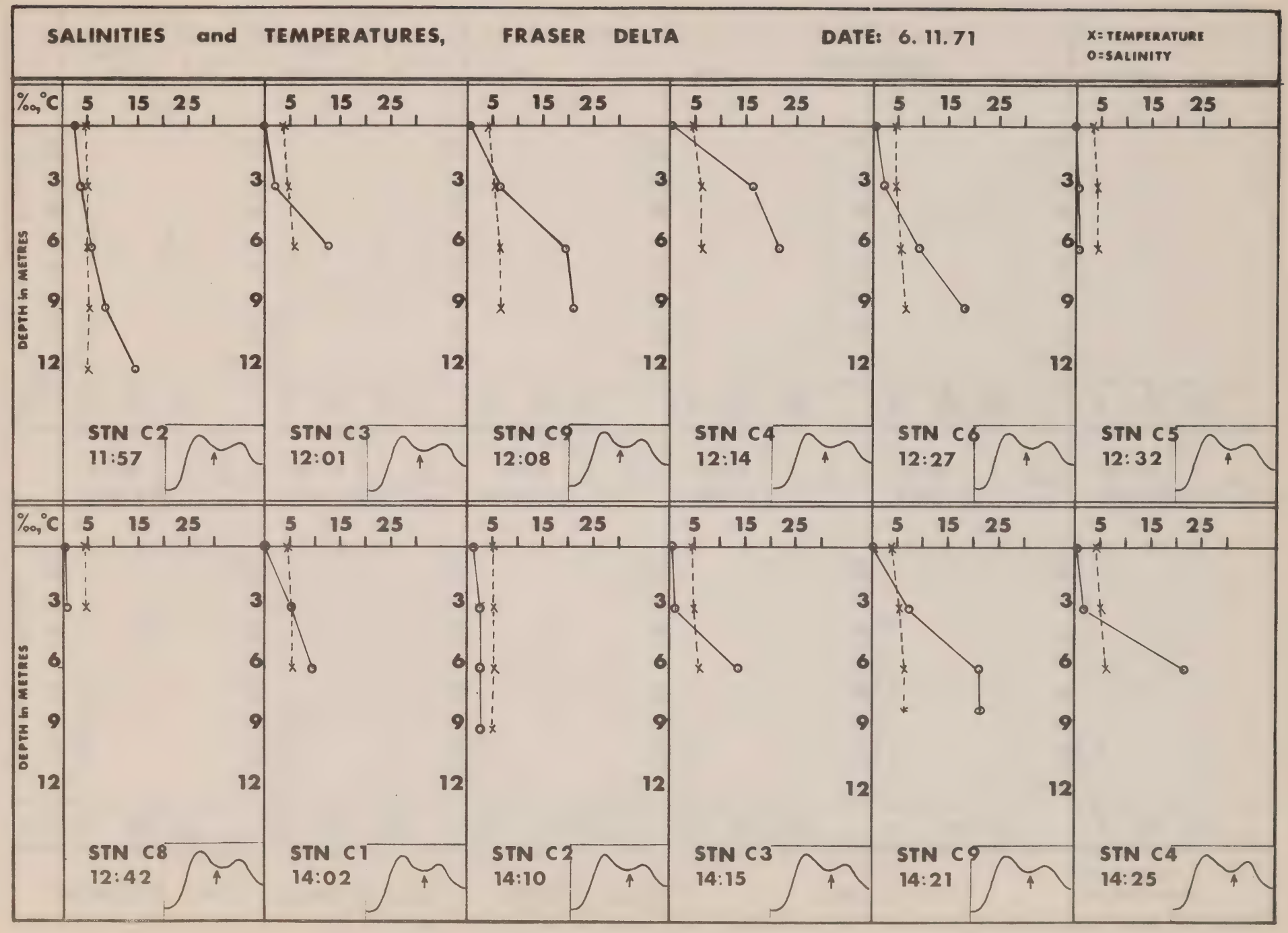
STN 18
16:44

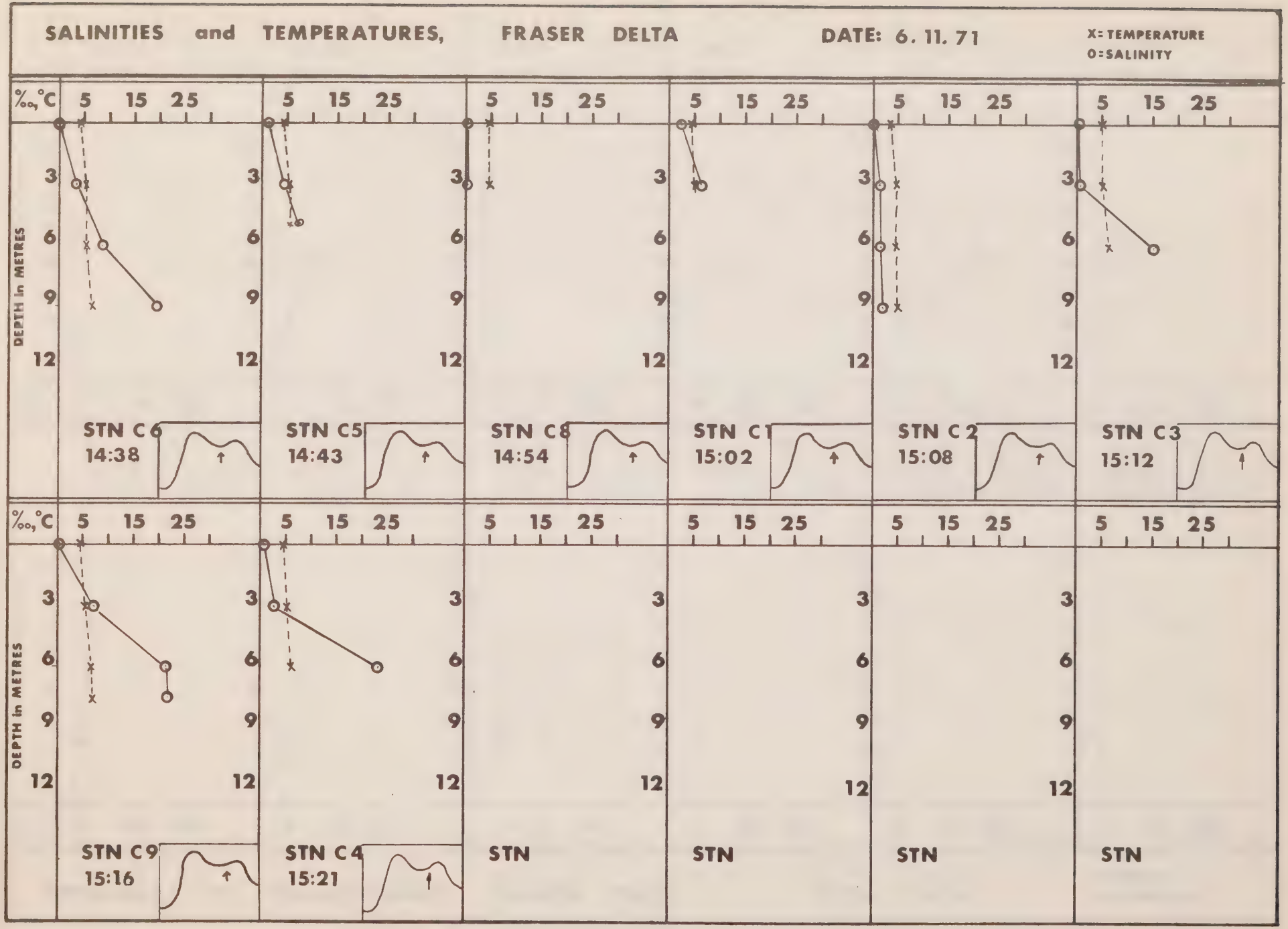


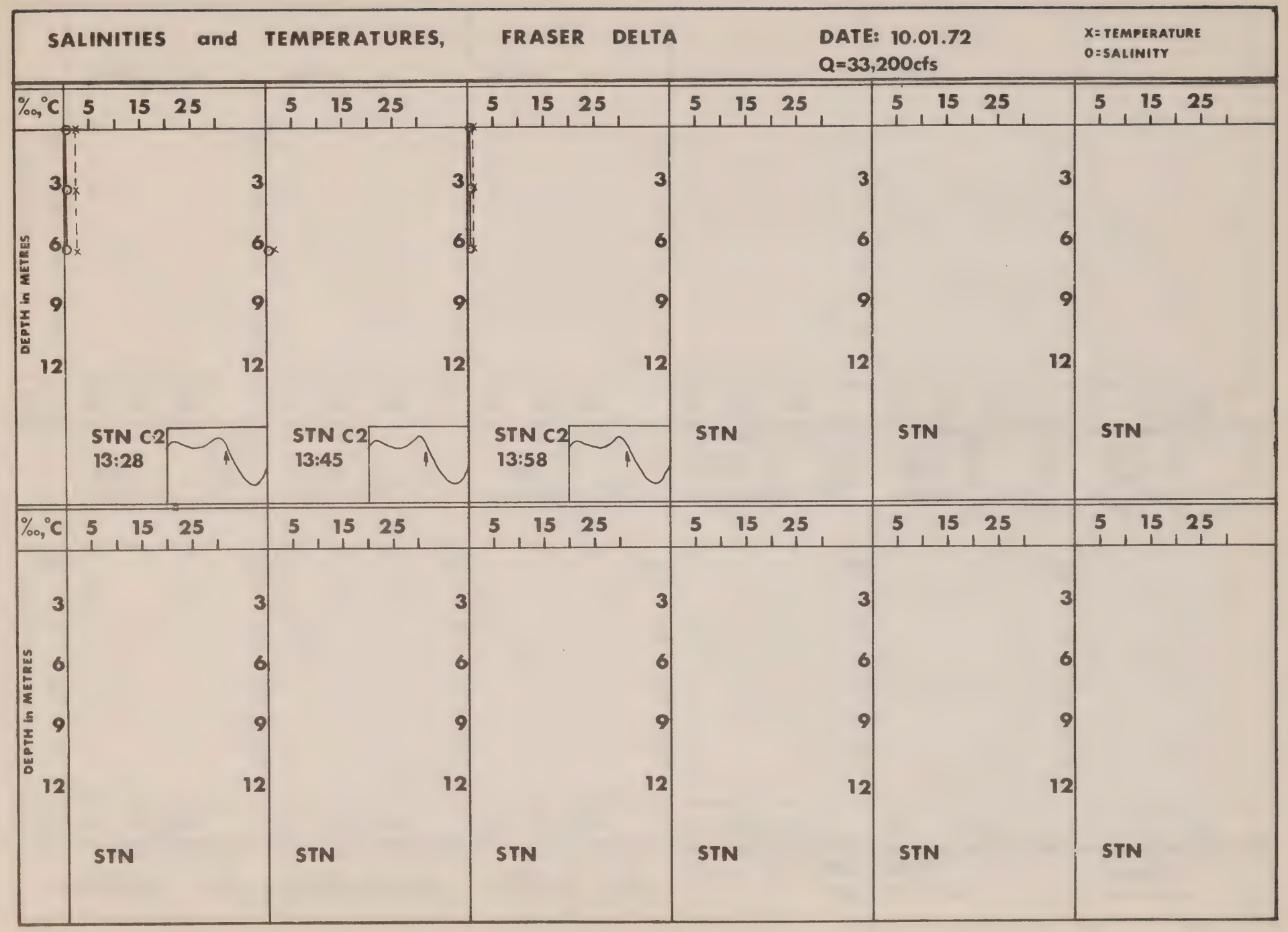
STN

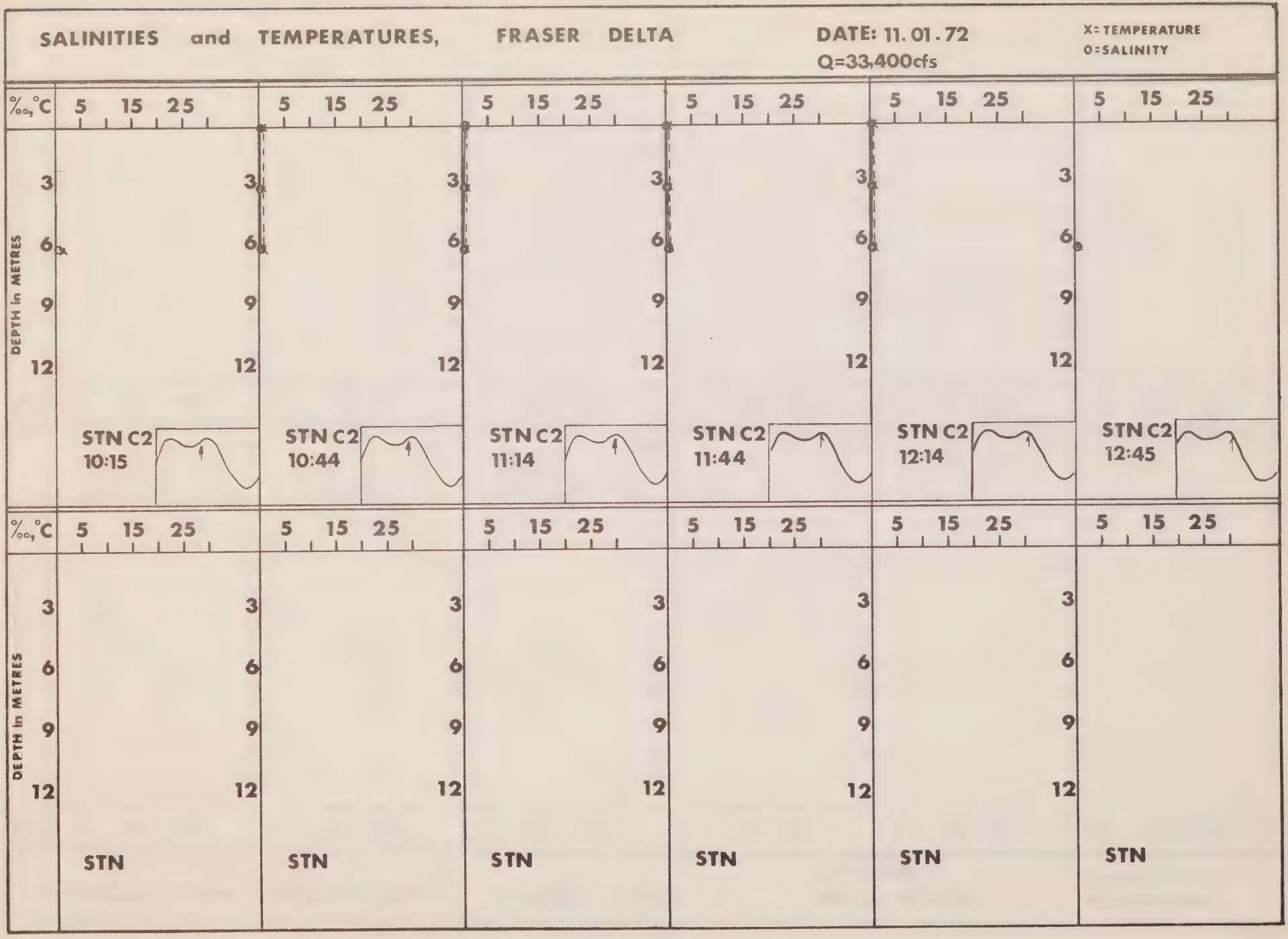

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 6.11.71
Q=52,000 cfs
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN C1 07:49
STN C2 07:56
STN C3 08:03
STN C8 08:07
STN C5 08:16
STN C1 08:34
STN C2 08:41
STN C3 08:49
STN C8 08:53
STN C5 09:01
STN C1 09:20
STN C2 09:27

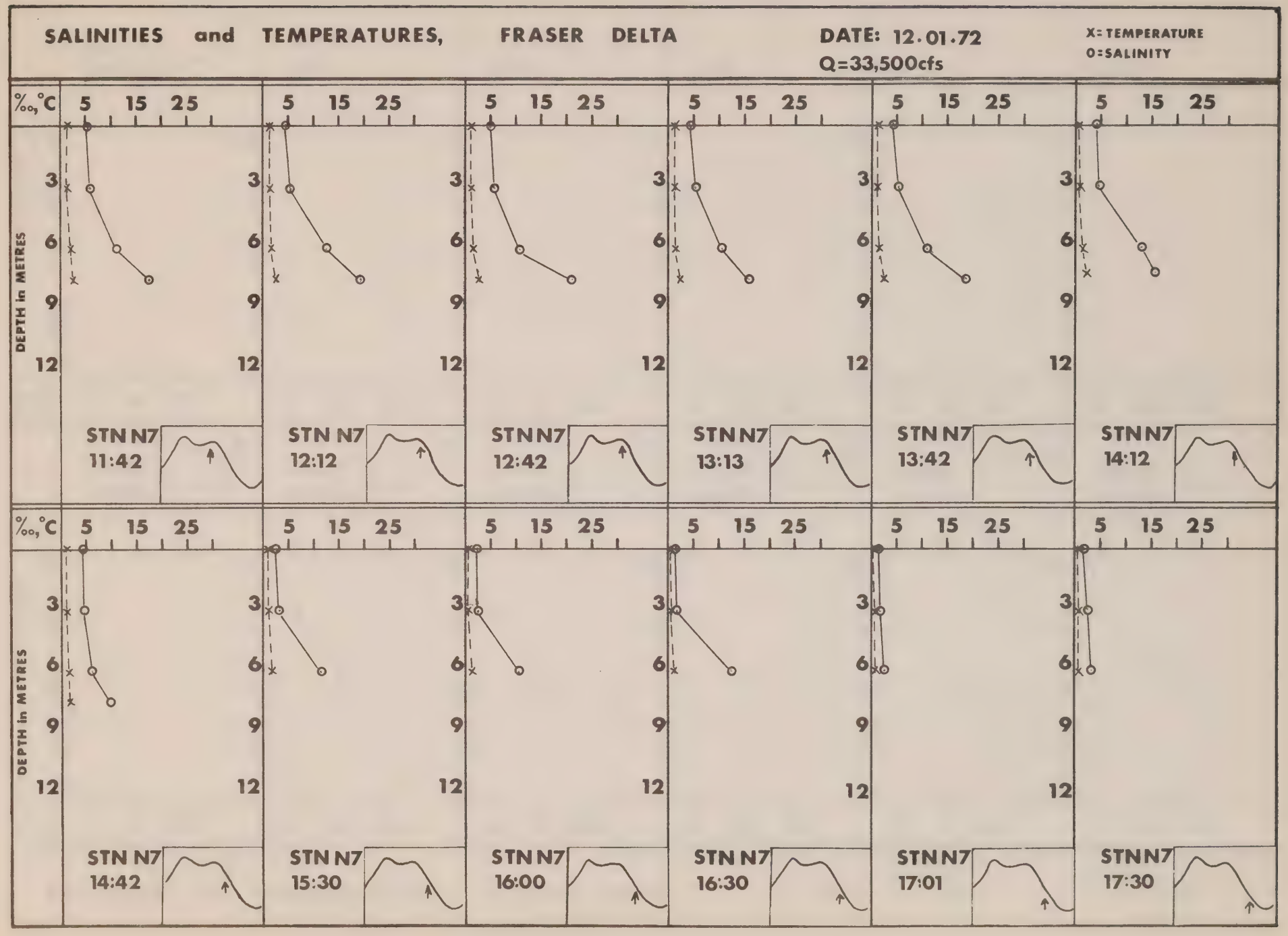

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 6. 11. 71
X = TEMPERATURE
O = SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN C3
09:32
STN C8
09:36
STN C5
09:46
STN C1
10:46
STN C2
10:54
STN C3
10:59
STN C9
11:06
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STN C6
11:23
STN C5
11:29
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STN C1
11:47

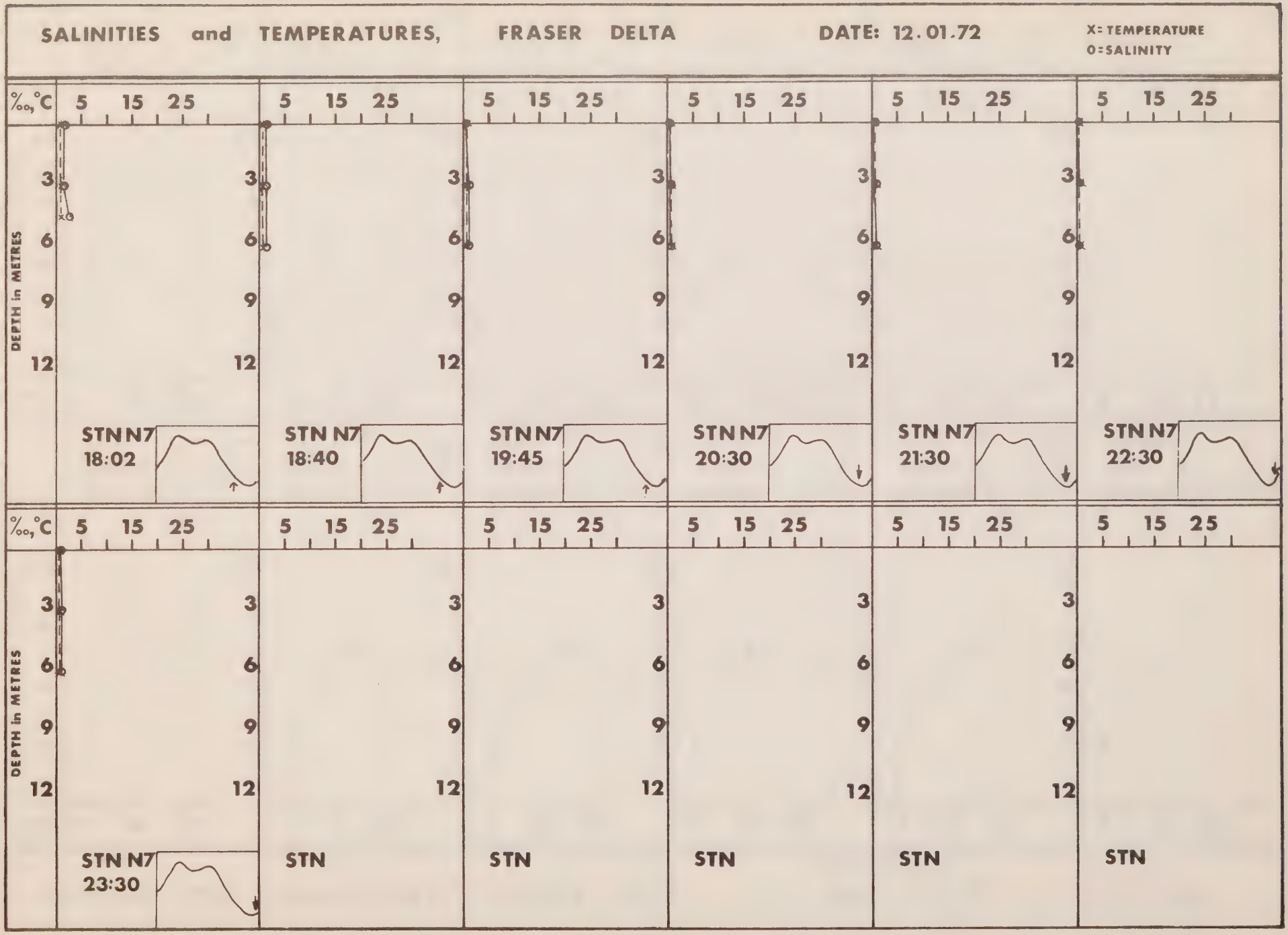

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 6. 11. 71
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN C2
11:57
STN C3
12:01
STN C9
12:08
STN C4
12:14
STN C6
12:27
STN C5
12:32
STN C8
12:42
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14:02
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STN C9
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STN C4
14:25

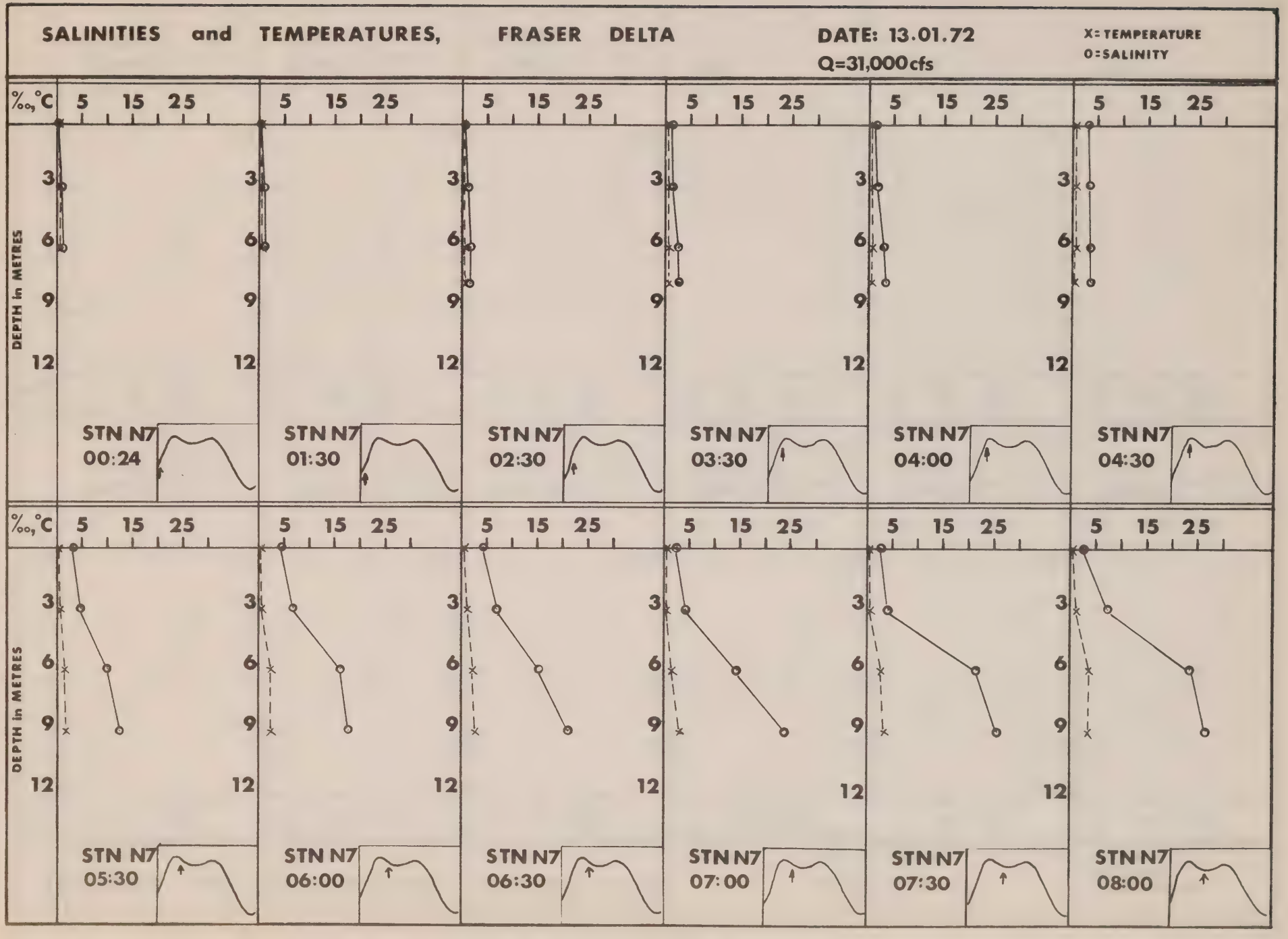

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 6. 11. 71
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN C6
14:38
STN C5
14:43
STN C8
14:54
STN C1
15:02
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STN C3
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STN C9
15:16
STN C4
15:21
STN
STN
STN
STN

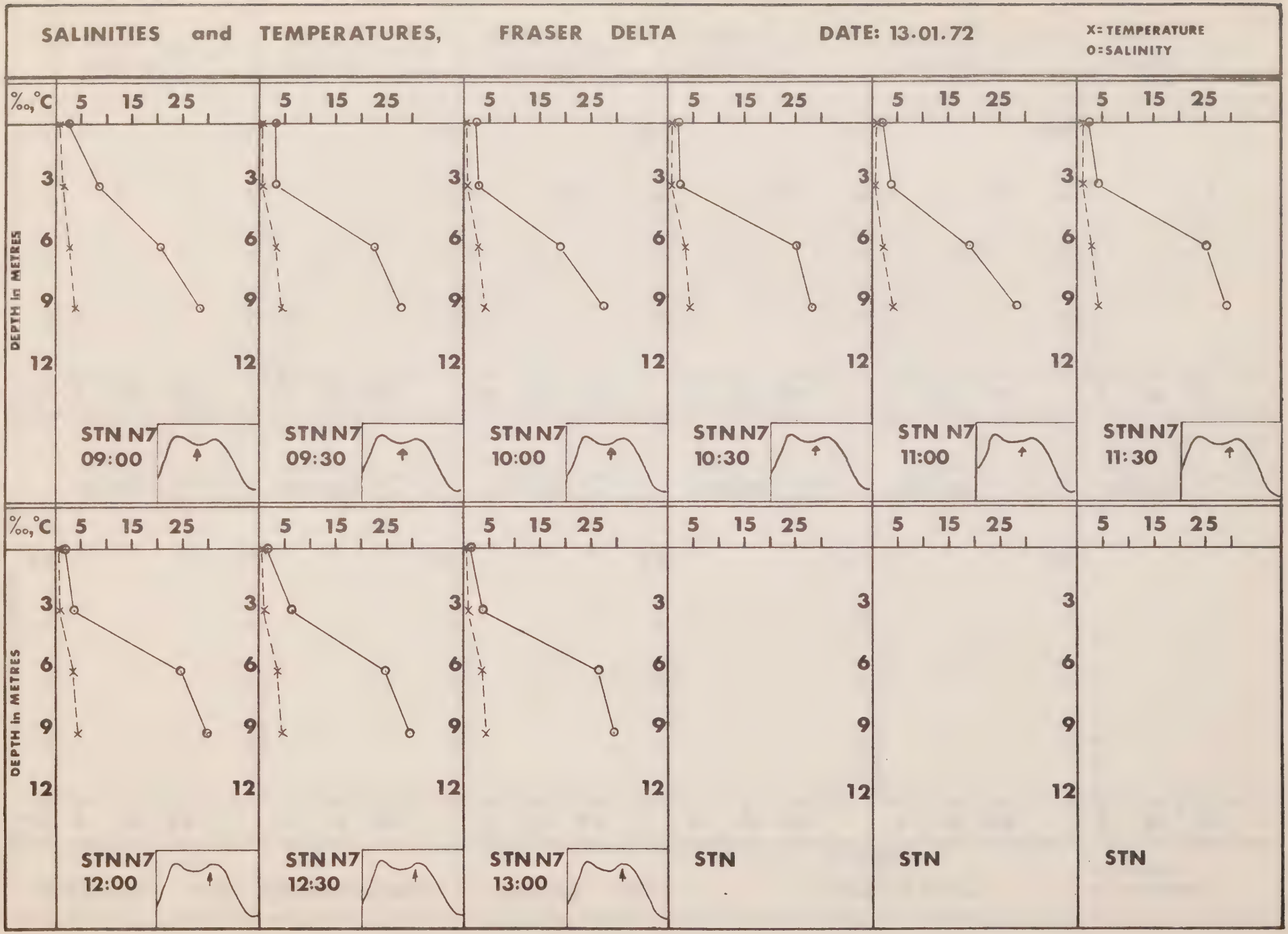

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 10.01.72
Q=33,200cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN C2
13:28
STN C2
13:45
STN C2
13:58
STN

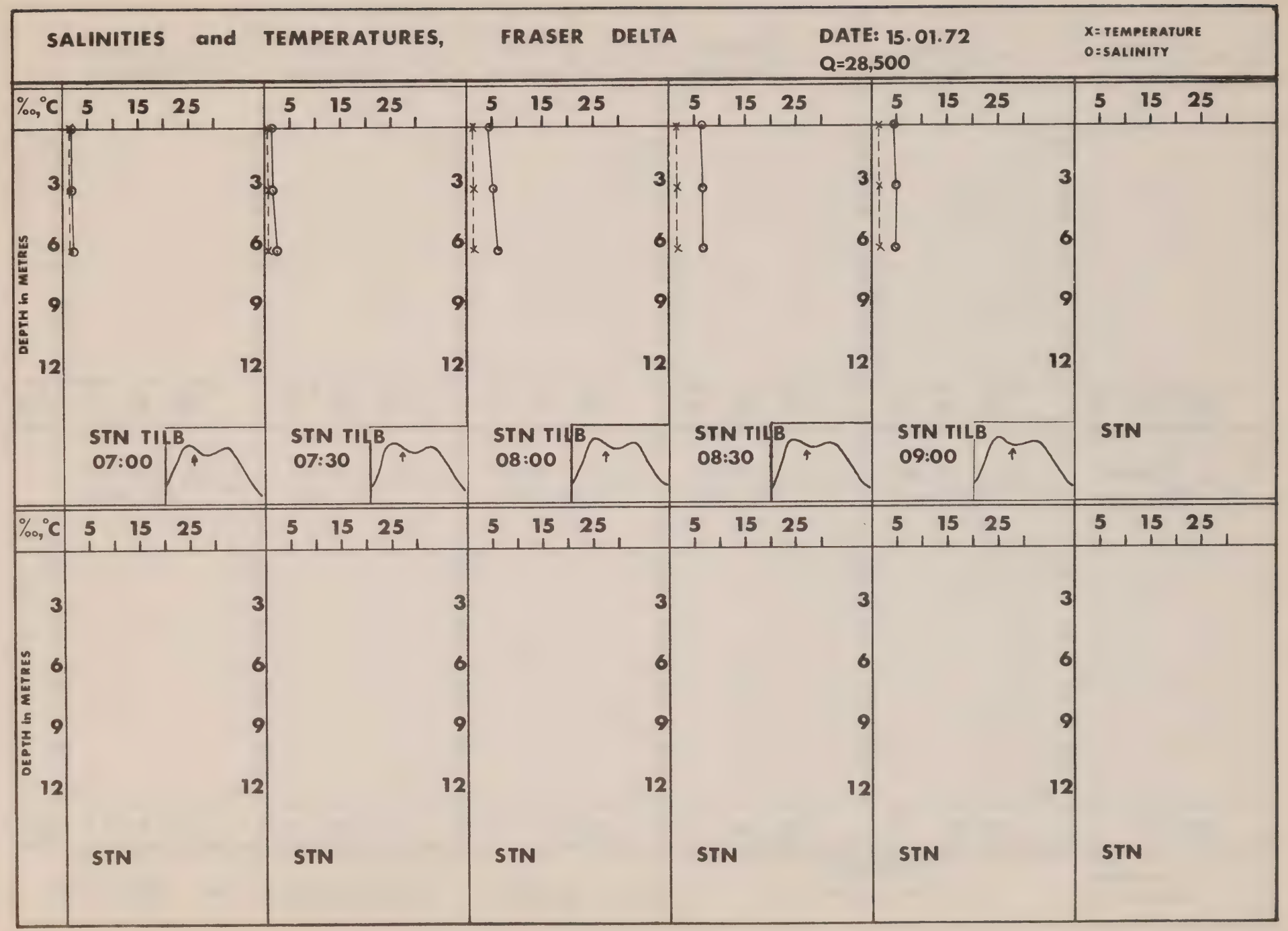

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 11.01.72
Q=33,400cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN C2
10:15
STN C2
10:44
STN C2
11:14
STN C2
11:44
STN C2
12:14
STN C2
12:45
STN

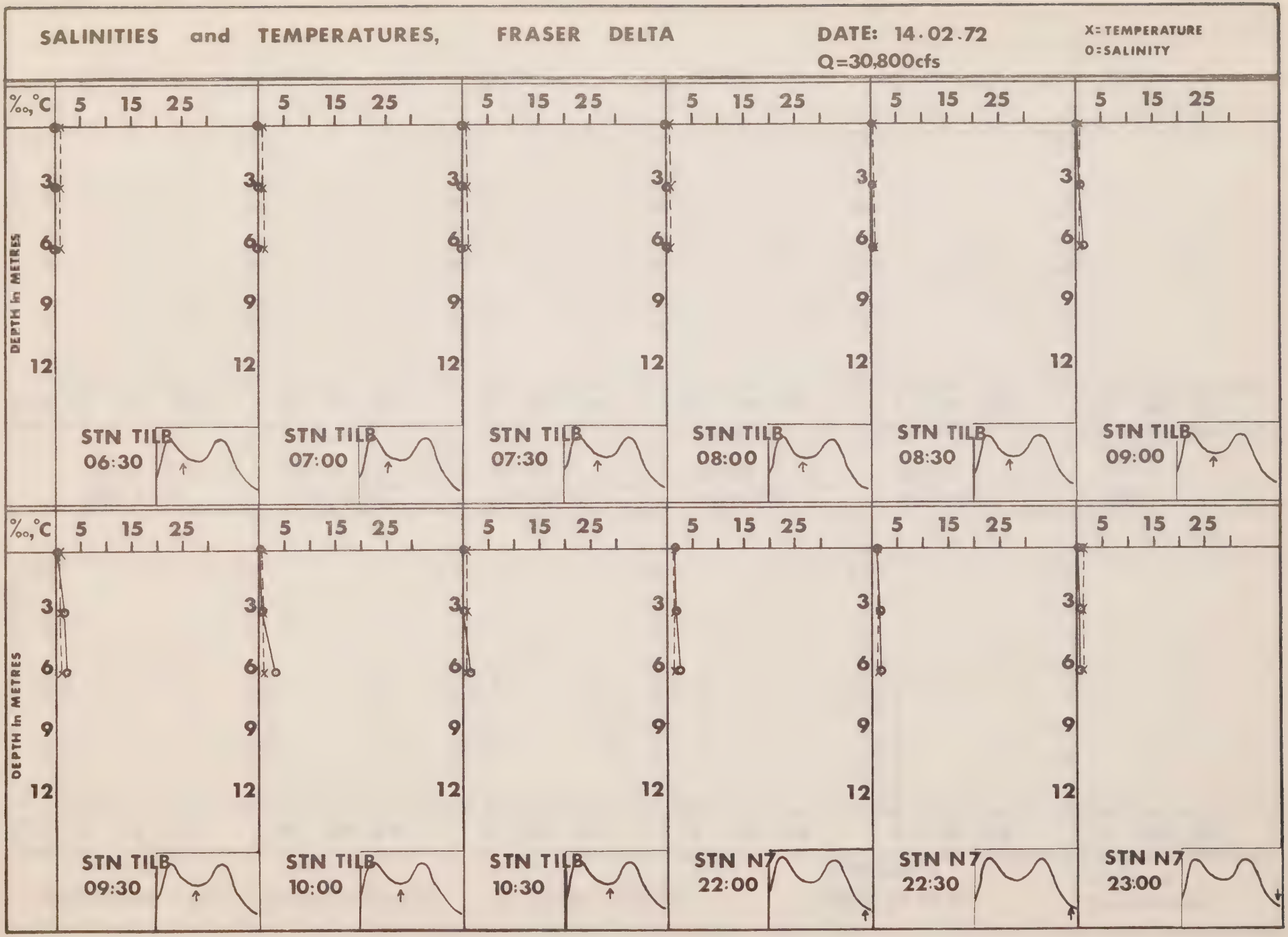

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 12.01.72
Q=33,500cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN N7
11:42
STN N7
12:12
STN N7
12:42
STN N7
13:13
STN N7
13:42
STN N7
14:12
STN N7
14:42
STN N7
15:30
STN N7
16:00
STN N7
16:30
STN N7
17:01
STN N7
17:30


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 12.01.72
X: TEMPERATURE
O: SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN N7
18:02
STN N7
18:40
STN N7
19:45
STN N7
20:30
STN N7
21:30
STN N7
22:30
STN N7
23:30
STN
STN
STN
STN
STN


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 13.01.72
Q=31,000cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN N7
00:24
STN N7
01:30
STN N7
02:30
STN N7
03:30
STN N7
04:00
STN N7
04:30
STN N7
05:30
STN N7
06:00
STN N7
06:30
STN N7
07:00
STN N7
07:30
STN N7
08:00


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 13.01.72
X= TEMPERATURE
O= SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN N7
09:00
STN N7
09:30
STN N7
10:00
STN N7
10:30
STN N7
11:00
STN N7
11:30
STN N7
12:00
STN N7
12:30
STN N7
13:00
STN
STN
STN


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 15.01.72
Q=28,500
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN TILB 07:00
STN TILB 07:30
STN TILB 08:00
STN TILB 08:30
STN TILB 09:00
STN
STN


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 14.02.72
Q=30,800cfs
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN TILB 06:30
STN TILB 07:00
STN TILB 07:30
STN TILB 08:00
STN TILB 08:30
STN TILB 09:00
STN TILB 09:30
STN TILB 10:00
STN TILB 10:30
STN N7 22:00
STN N7 22:30
STN N7 23:00

SALINITIES and TEMPERATURES, FRASER DELTA DATE: 14.02.72

X = TEMPERATURE
O = SALINITY

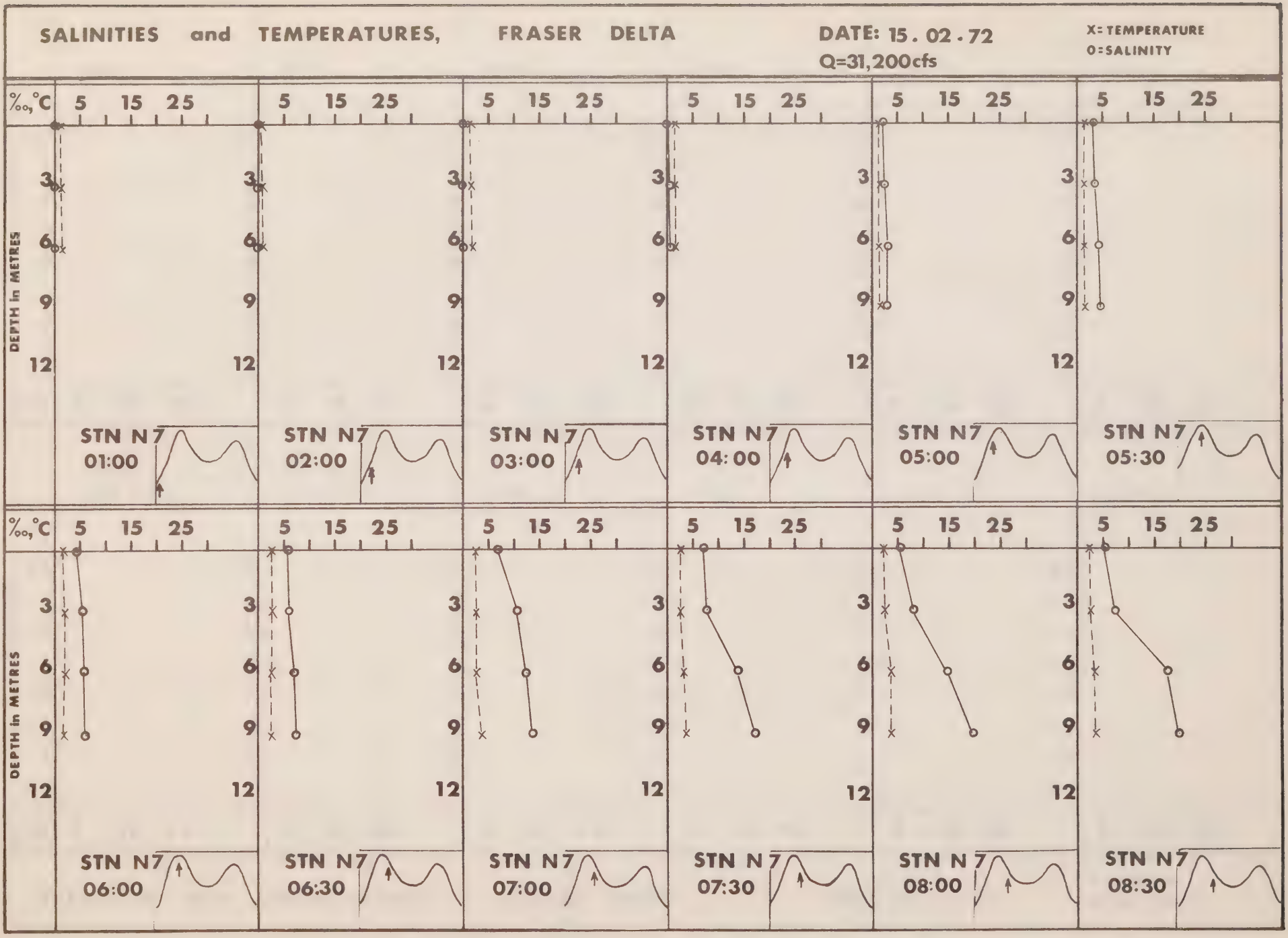
‰, °C 5 15 25

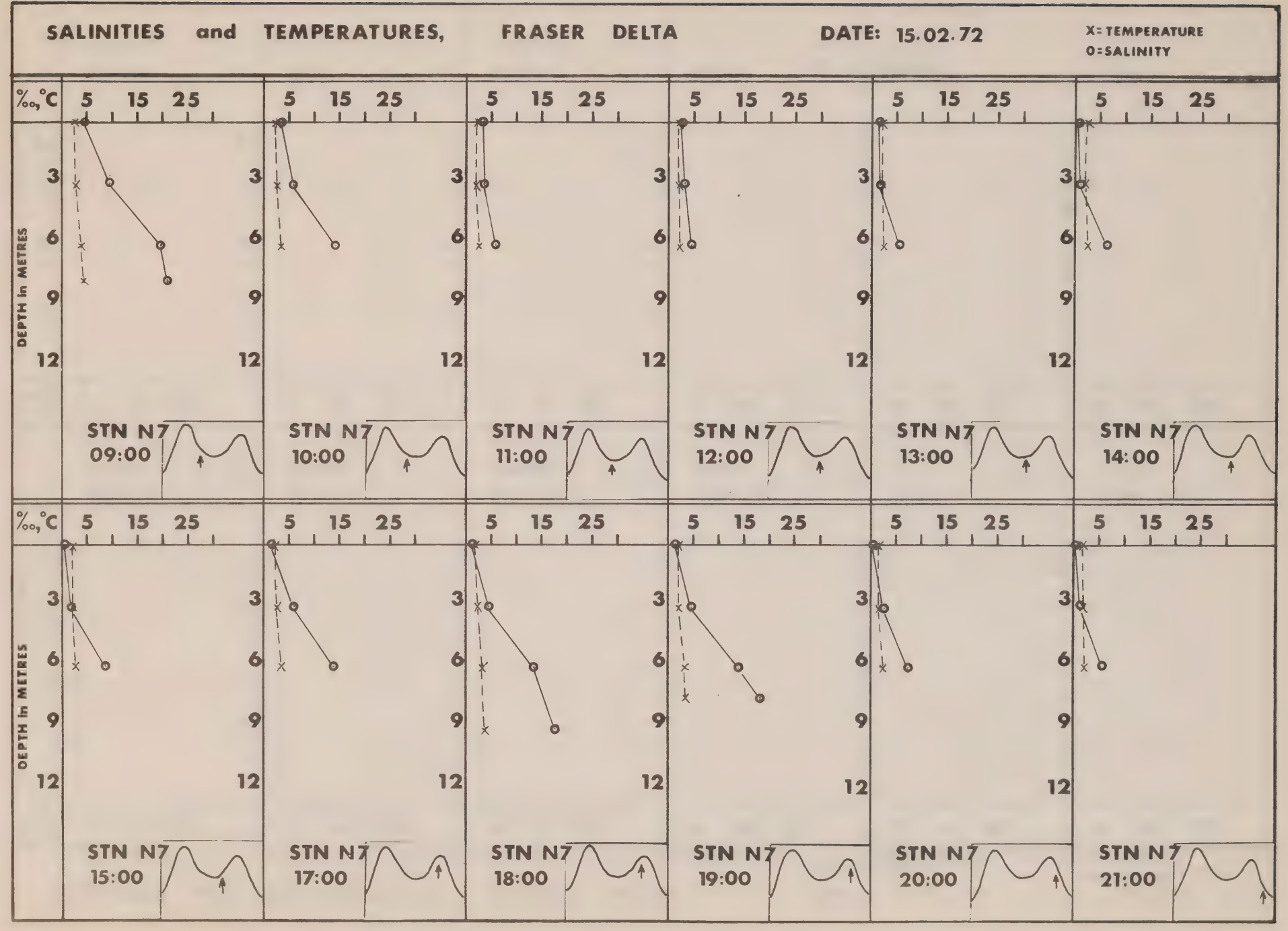
DEPTH in METRES 3 6 9 12

STN N7 23:30

STN N7 00:30

STN

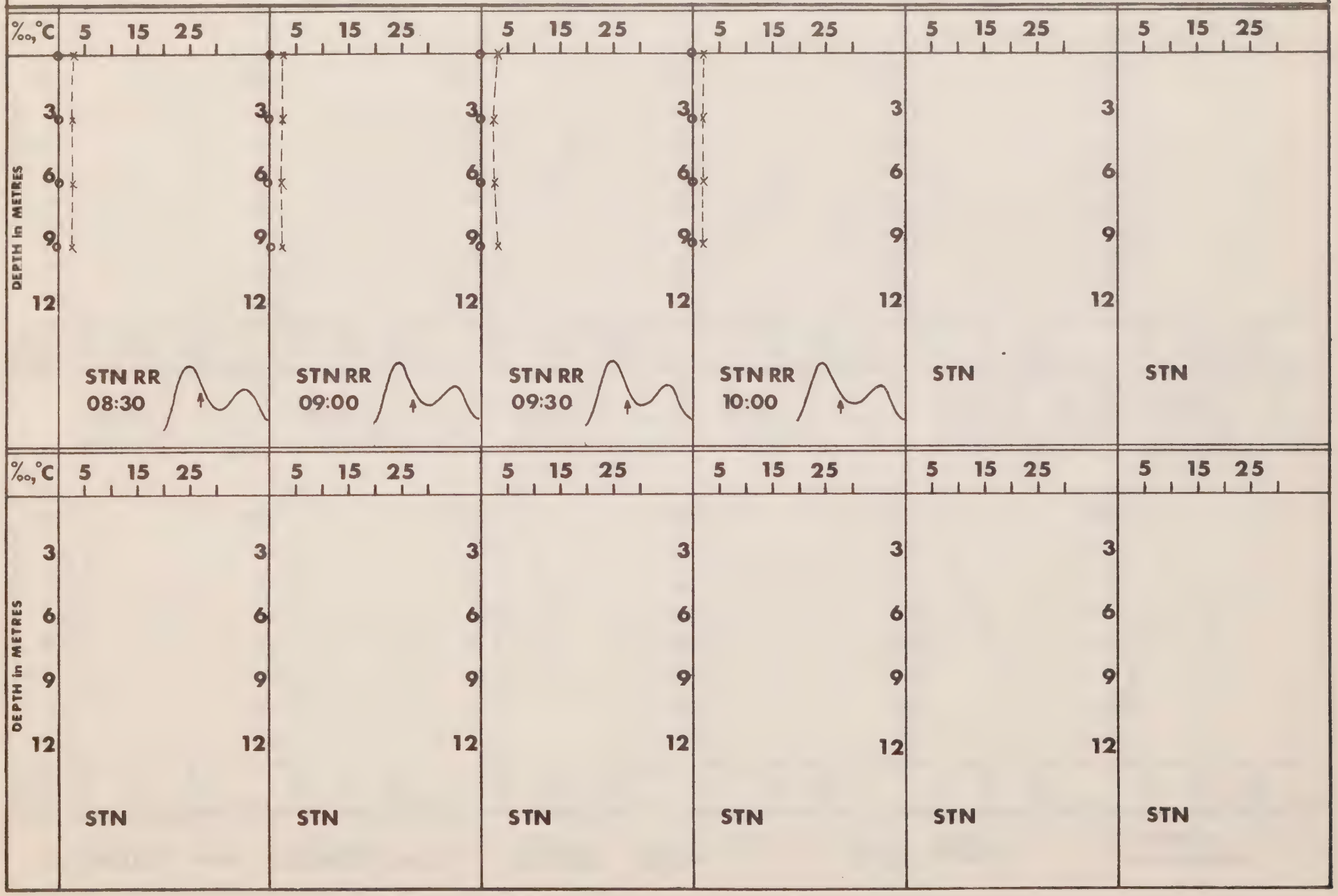

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 15 . 02 . 72
Q=31,200cfs
X= TEMPERATURE
O= SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN N7
01:00
STN N7
02:00
STN N7
03:00
STN N7
04:00
STN N7
05:00
STN N7
05:30
STN N7
06:00
STN N7
06:30
STN N7
07:00
STN N7
07:30
STN N7
08:00
STN N7
08:30

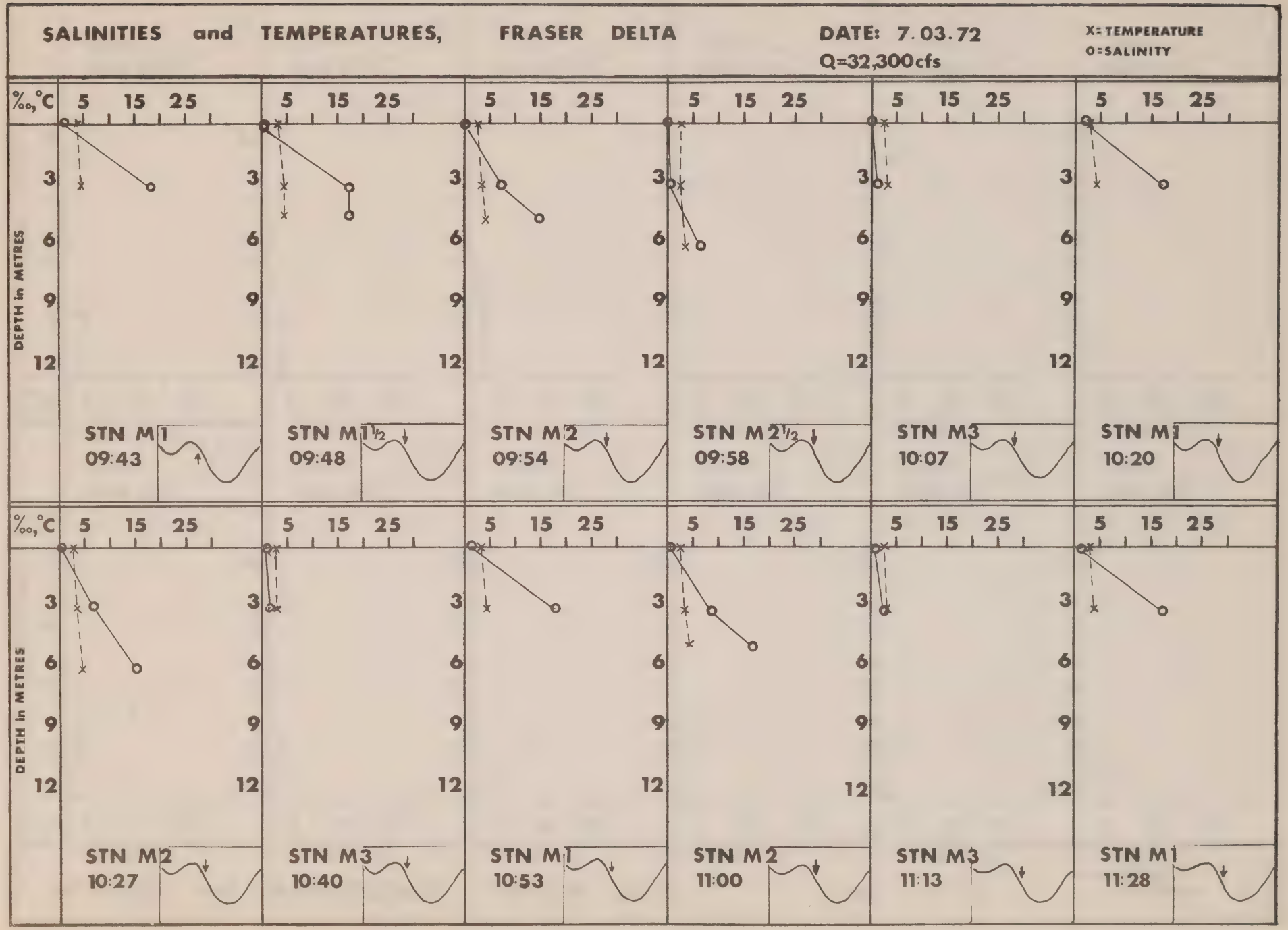

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 15.02.72
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN N7
09:00
STN N7
10:00
STN N7
11:00
STN N7
12:00
STN N7
13:00
STN N7
14:00
STN N7
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STN N7
17:00
STN N7
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STN N7
19:00
STN N7
20:00
STN N7
21:00

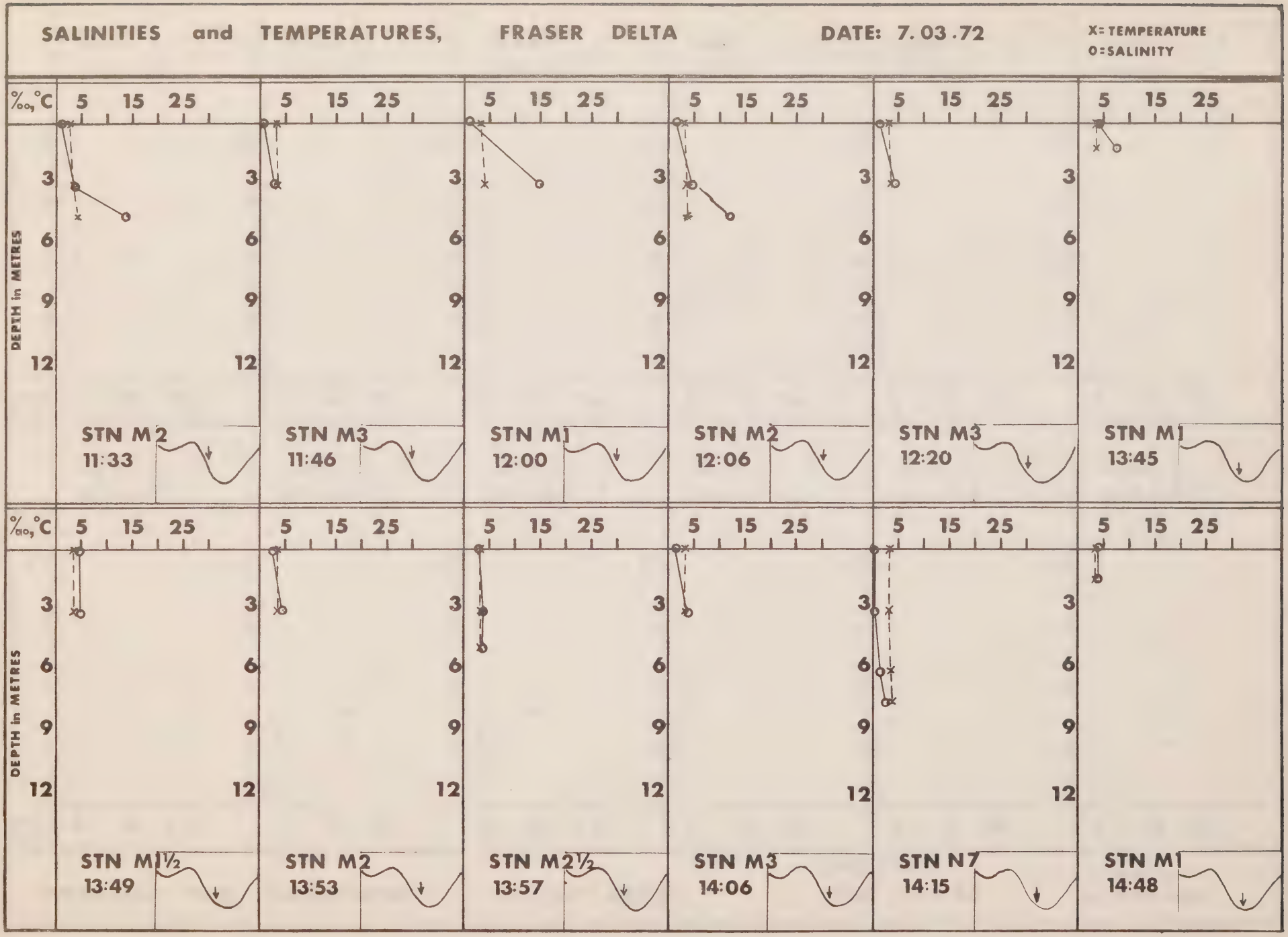
SALINITIES and TEMPERATURES, FRASER DELTA

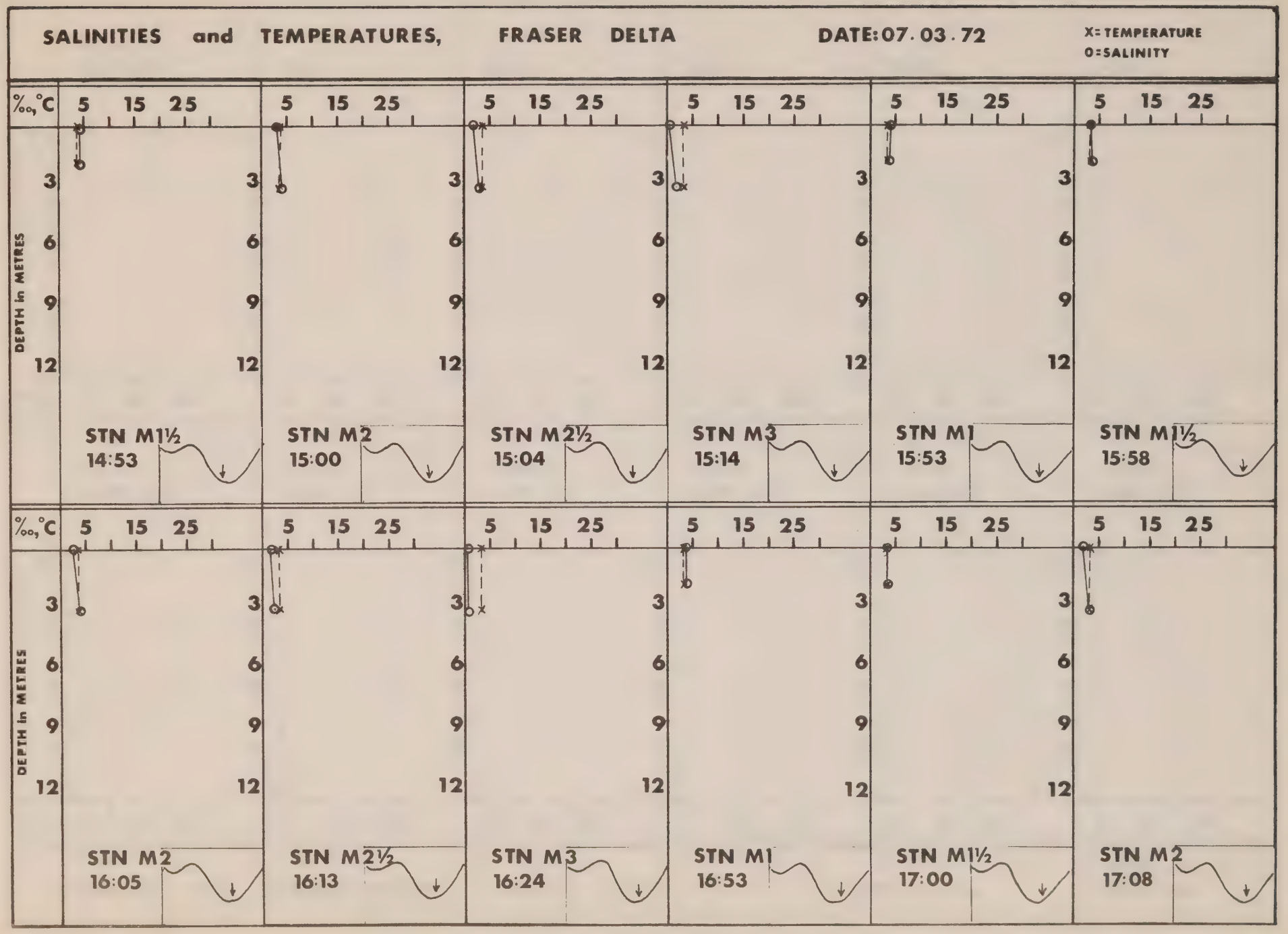
DATE: 16.02.72
Q=33,500cfs

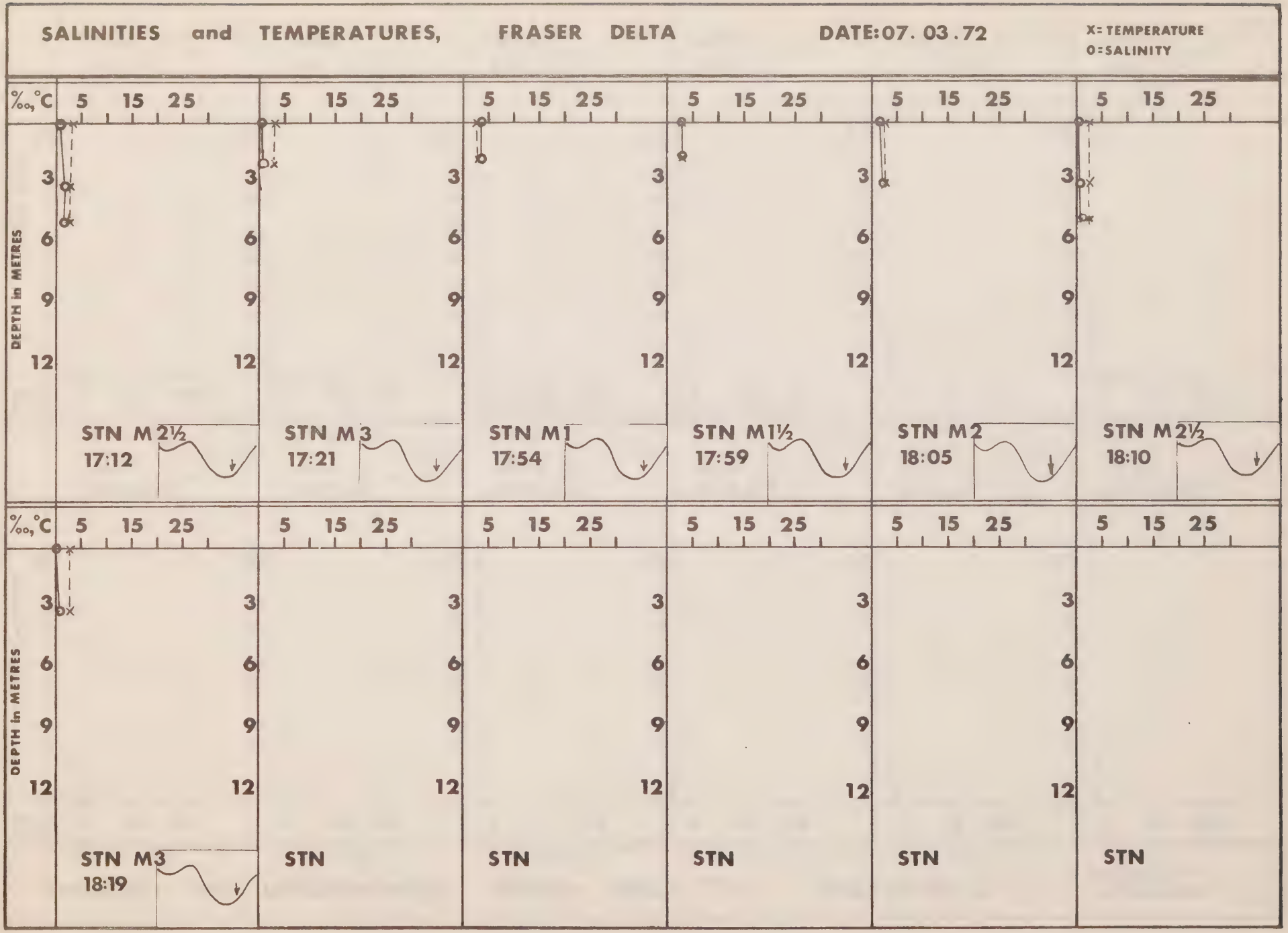
X= TEMPERATURE
O=SALINITY

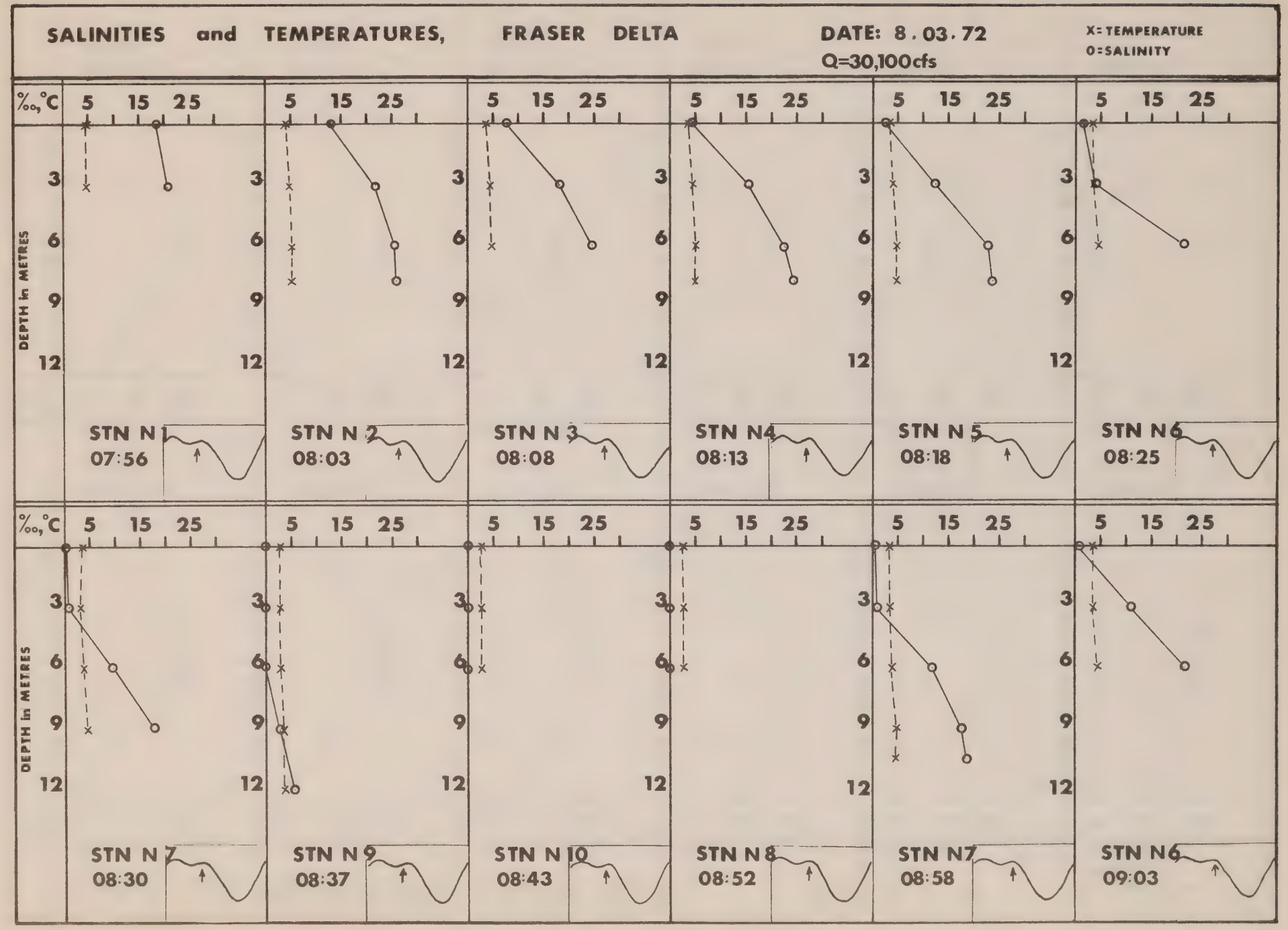


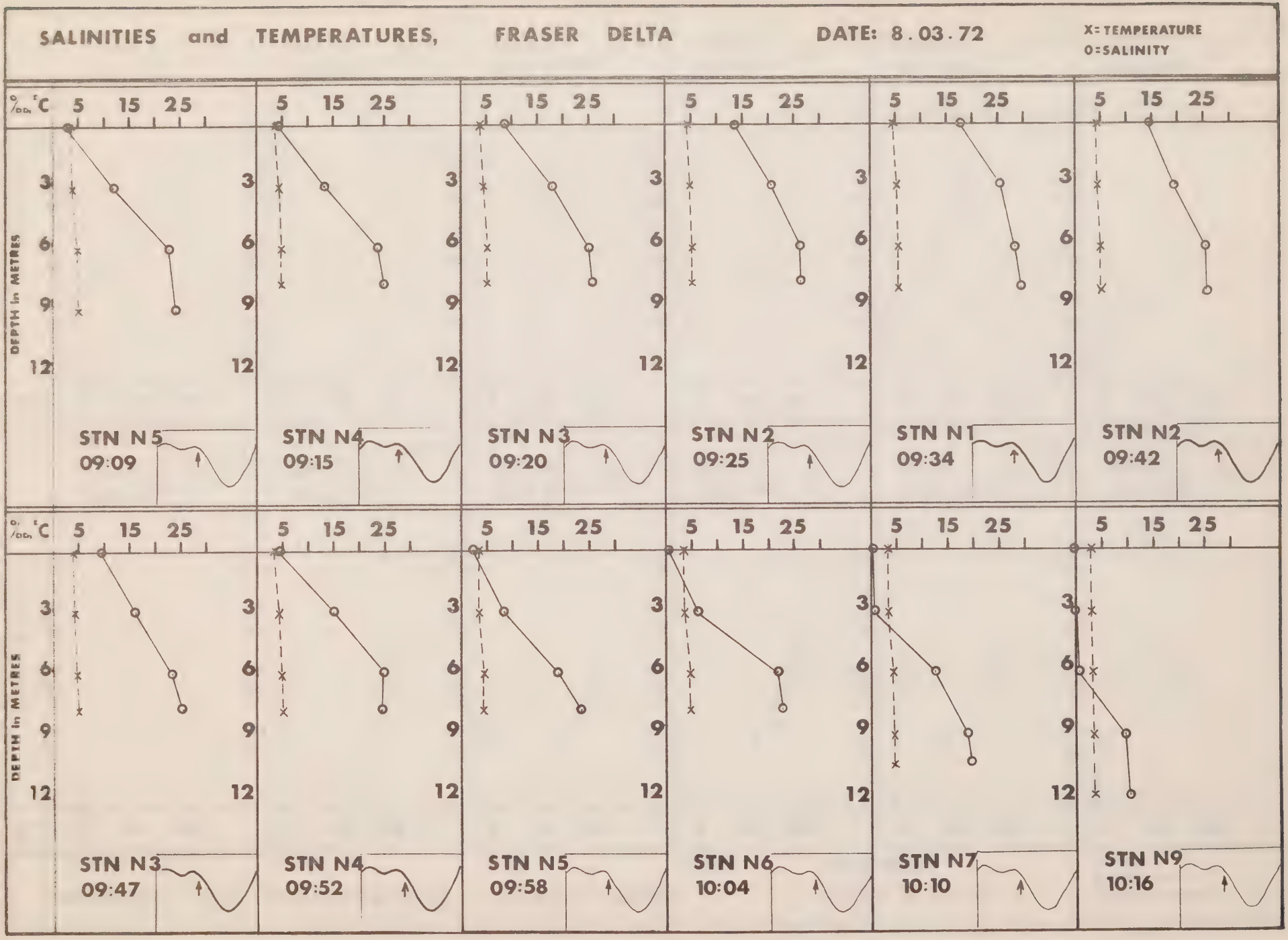

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 7.03.72
Q=32,300cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN M1
09:43
STN M1½
09:48
STN M2
09:54
STN M2½
09:58
STN M3
10:07
STN M1
10:20
STN M2
10:27
STN M3
10:40
STN M1
10:53
STN M2
11:00
STN M3
11:13
STN M1
11:28

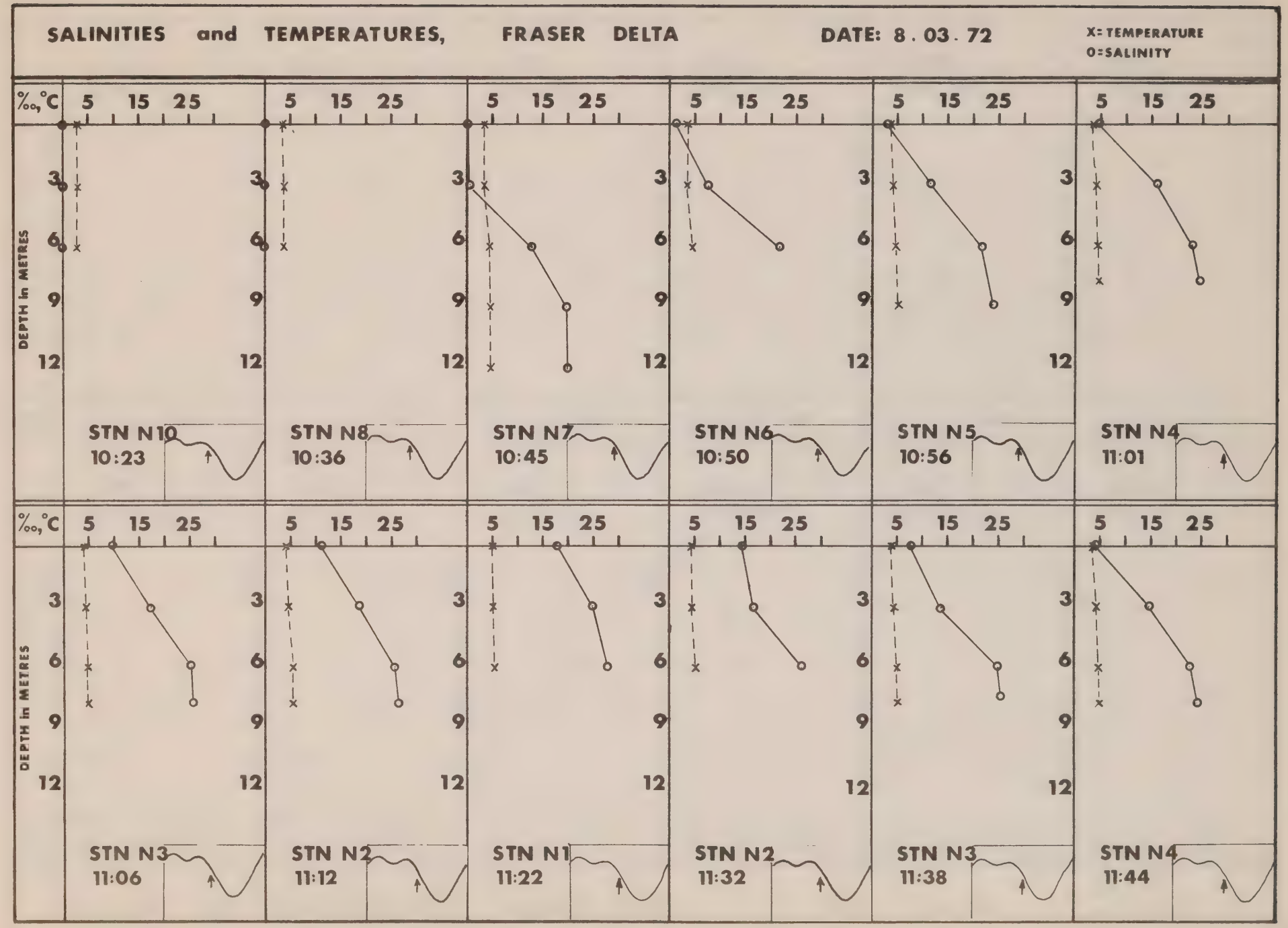

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 7.03.72
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN M2
11:33
STN M3
11:46
STN M1
12:00
STN M2
12:06
STN M3
12:20
STN M1
13:45
STN M1½
13:49
STN M2
13:53
STN M2½
13:57
STN M3
14:06
STN N7
14:15
STN M1
14:48

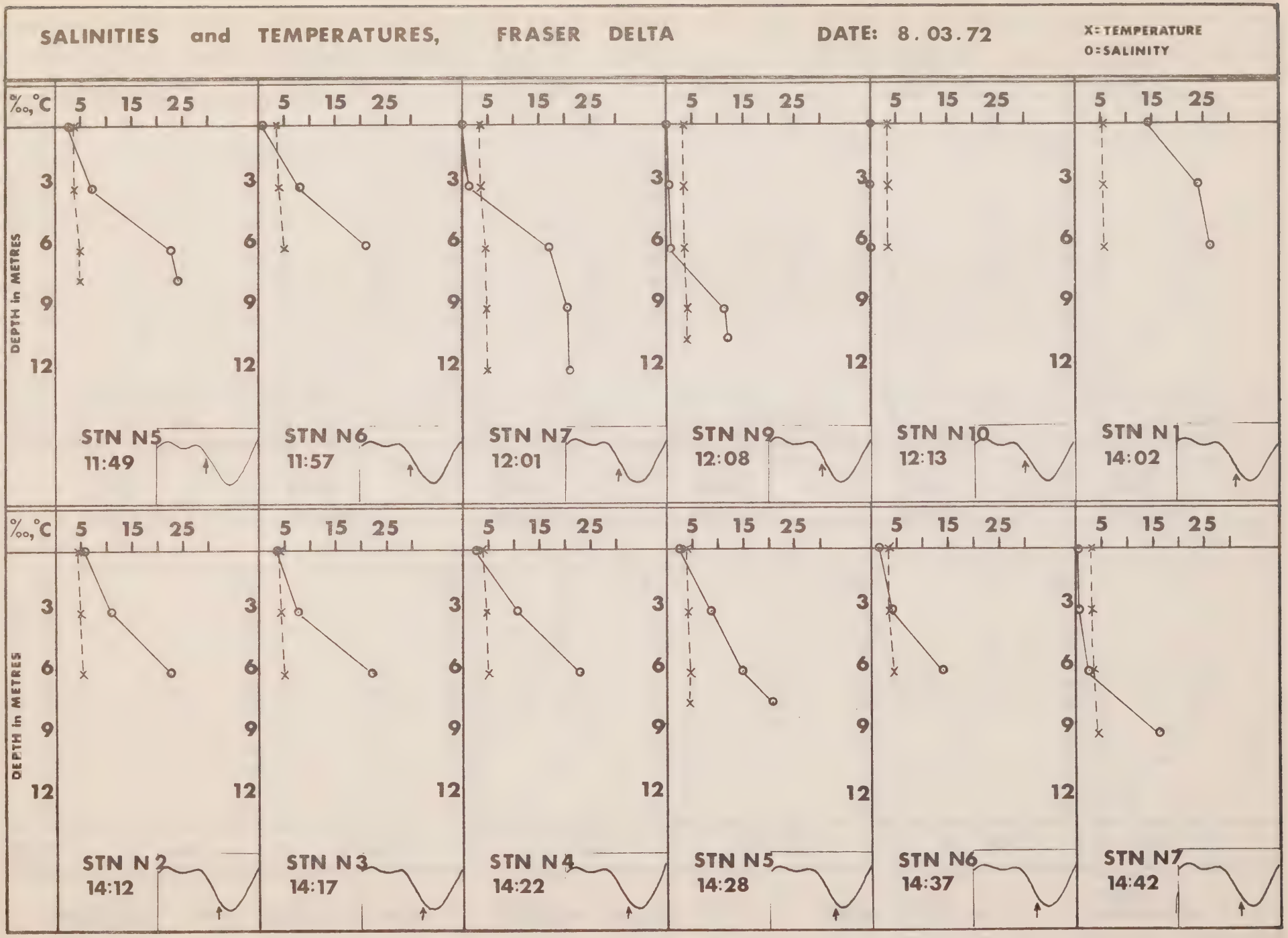

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 07.03.72
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN M1½
14:53
STN M2
15:00
STN M2½
15:04
STN M3
15:14
STN M1
15:53
STN M1½
15:58
STN M2
16:05
STN M2½
16:13
STN M3
16:24
STN M1
16:53
STN M1½
17:00
STN M2
17:08

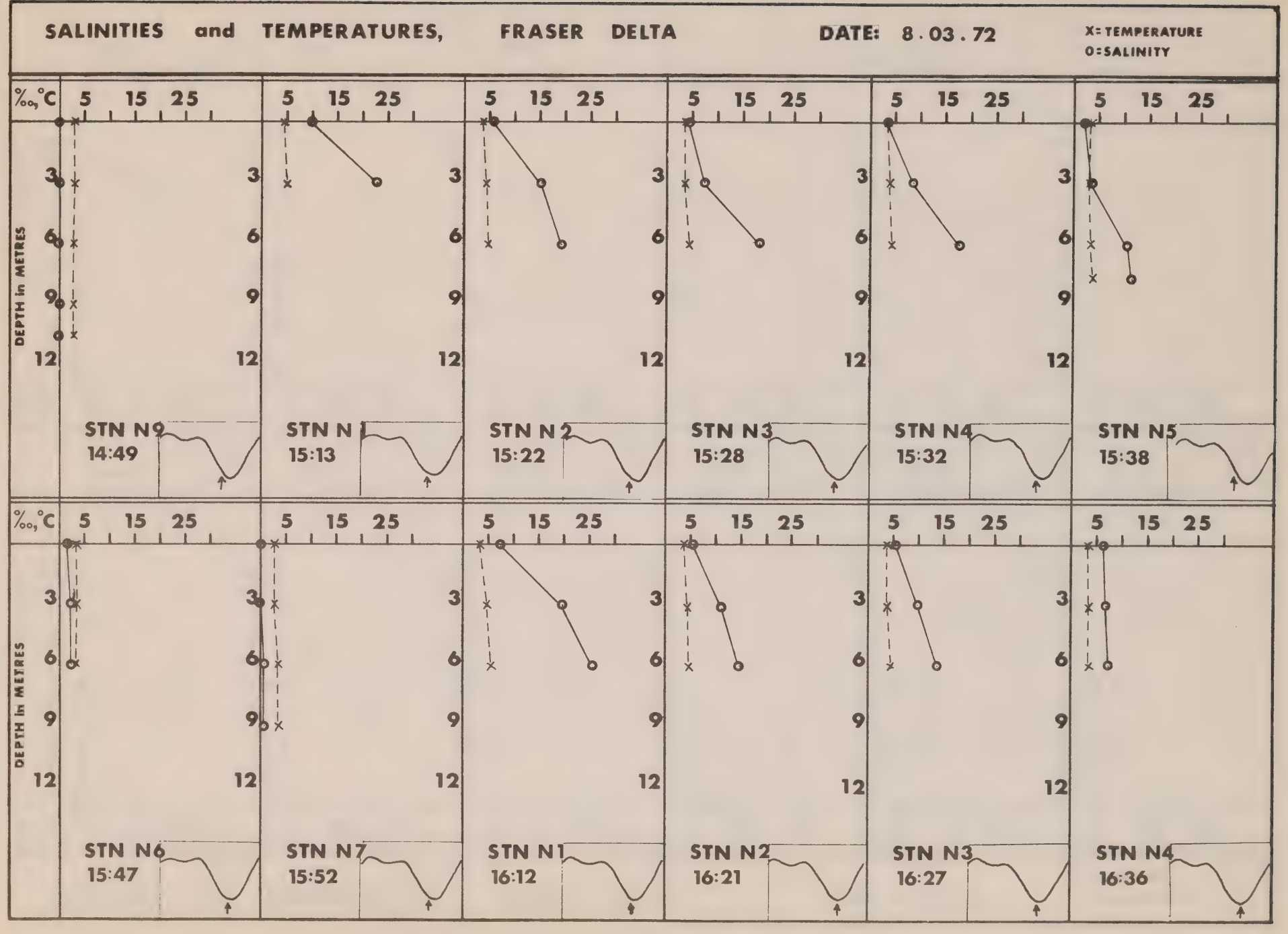

SALINITIES and TEMPERATURES, FRASER DELTA
DATE:07. 03 .72
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN M 2½
17:12
STN M 3
17:21
STN M 1
17:54
STN M 1½
17:59
STN M 2
18:05
STN M 2½
18:10
STN M 3
18:19
STN
STN
STN
STN
STN


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 8.03.72
Q=30,100cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN N 1
07:56
STN N 2
08:03
STN N 3
08:08
STN N4
08:13
STN N 5
08:18
STN N6
08:25
STN N 7
08:30
STN N 9
08:37
STN N 10
08:43
STN N 8
08:52
STN N7
08:58
STN N6
09:03


SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 8.03.72
X: TEMPERATURE
O: SALINITY
°/oo °C
5 15 25
DEPTH in METRES
3
6
9
12
STN N5
09:09
STN N4
09:15
STN N3
09:20
STN N2
09:25
STN N1
09:34
STN N2
09:42
STN N3
09:47
STN N4
09:52
STN N5
09:58
STN N6
10:04
STN N7
10:10
STN N9
10:16

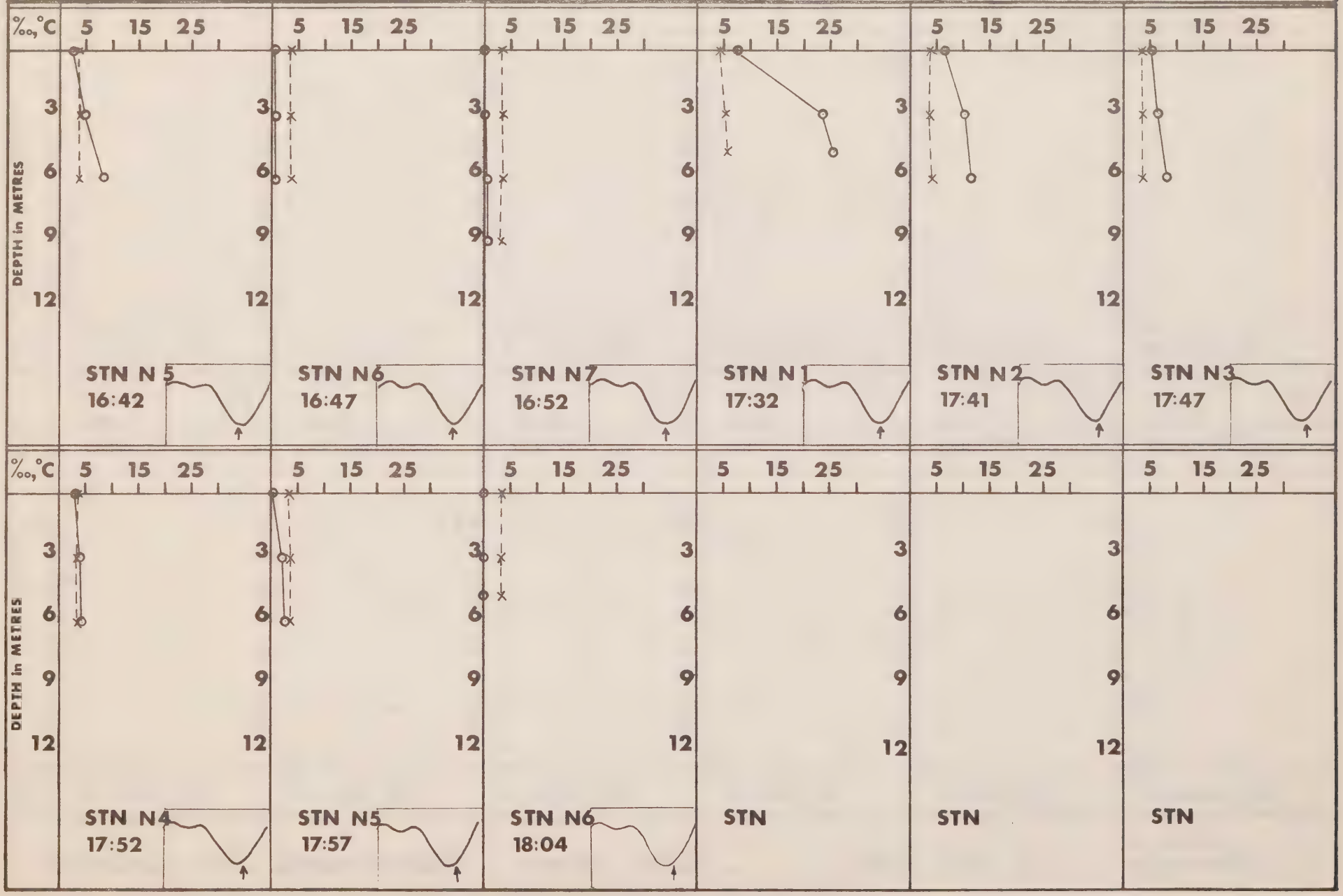

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 8.03.72
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN N10
10:23
STN N8
10:36
STN N7
10:45
STN N6
10:50
STN N5
10:56
STN N4
11:01
STN N3
11:06
STN N2
11:12
STN N1
11:22
STN N2
11:32
STN N3
11:38
STN N4
11:44

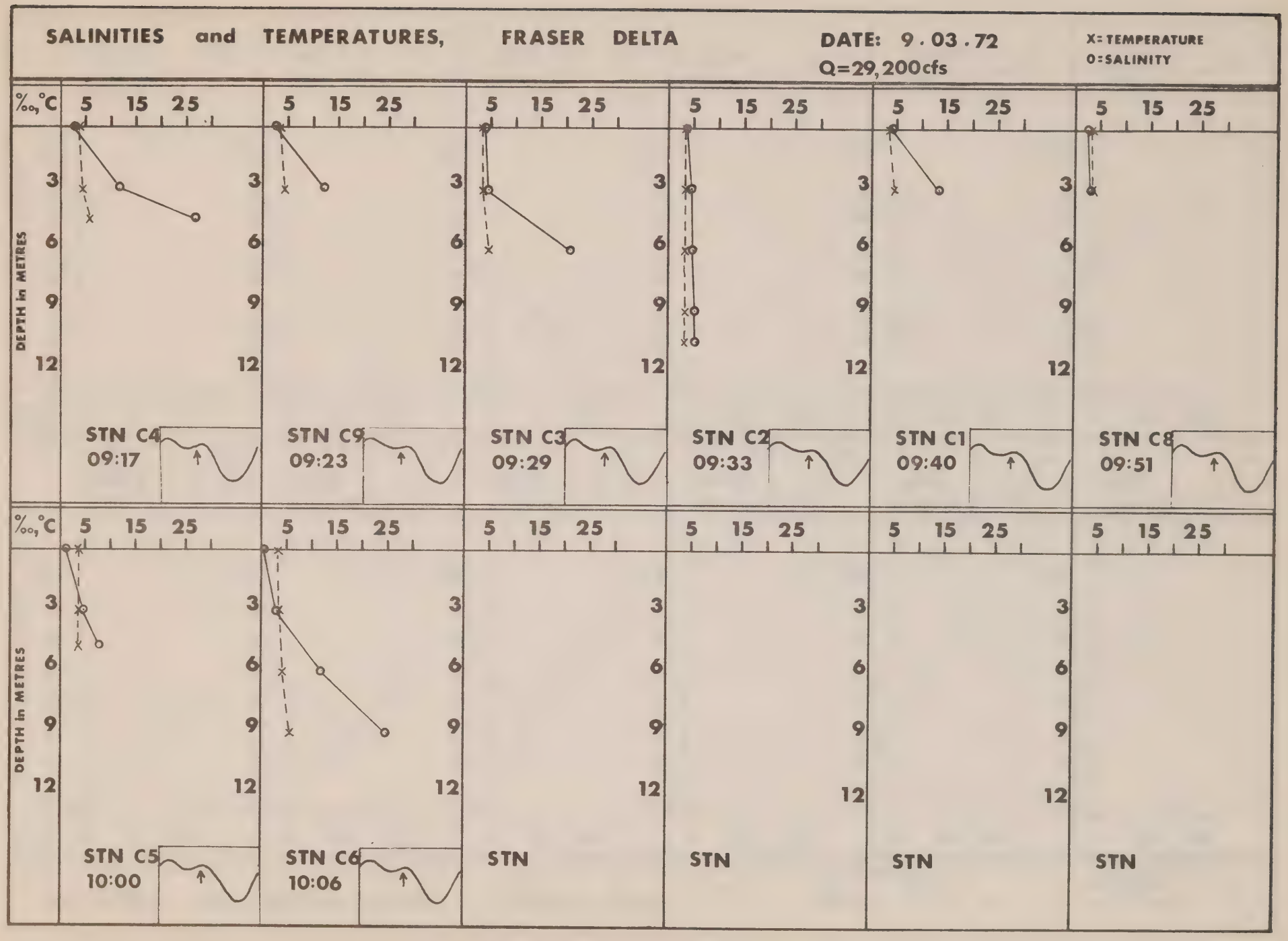

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 8.03.72
X=TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN N5
11:49
STN N6
11:57
STN N7
12:01
STN N9
12:08
STN N10
12:13
STN N1
14:02
STN N2
14:12
STN N3
14:17
STN N4
14:22
STN N5
14:28
STN N6
14:37
STN N7
14:42

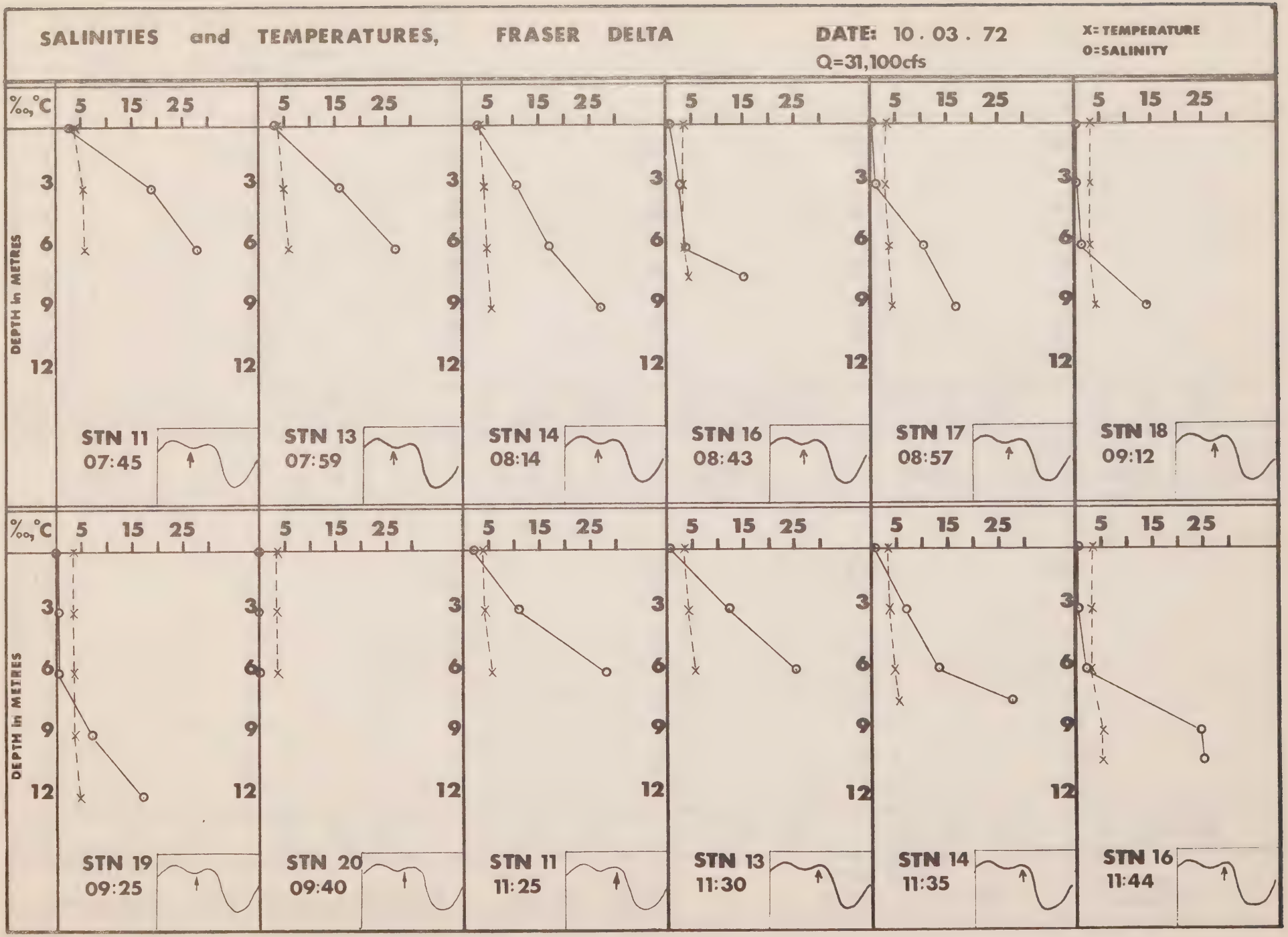

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 8.03.72
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN N9
14:49
STN N1
15:13
STN N2
15:22
STN N3
15:28
STN N4
15:32
STN N5
15:38
STN N6
15:47
STN N7
15:52
STN N1
16:12
STN N2
16:21
STN N3
16:27
STN N4
16:36

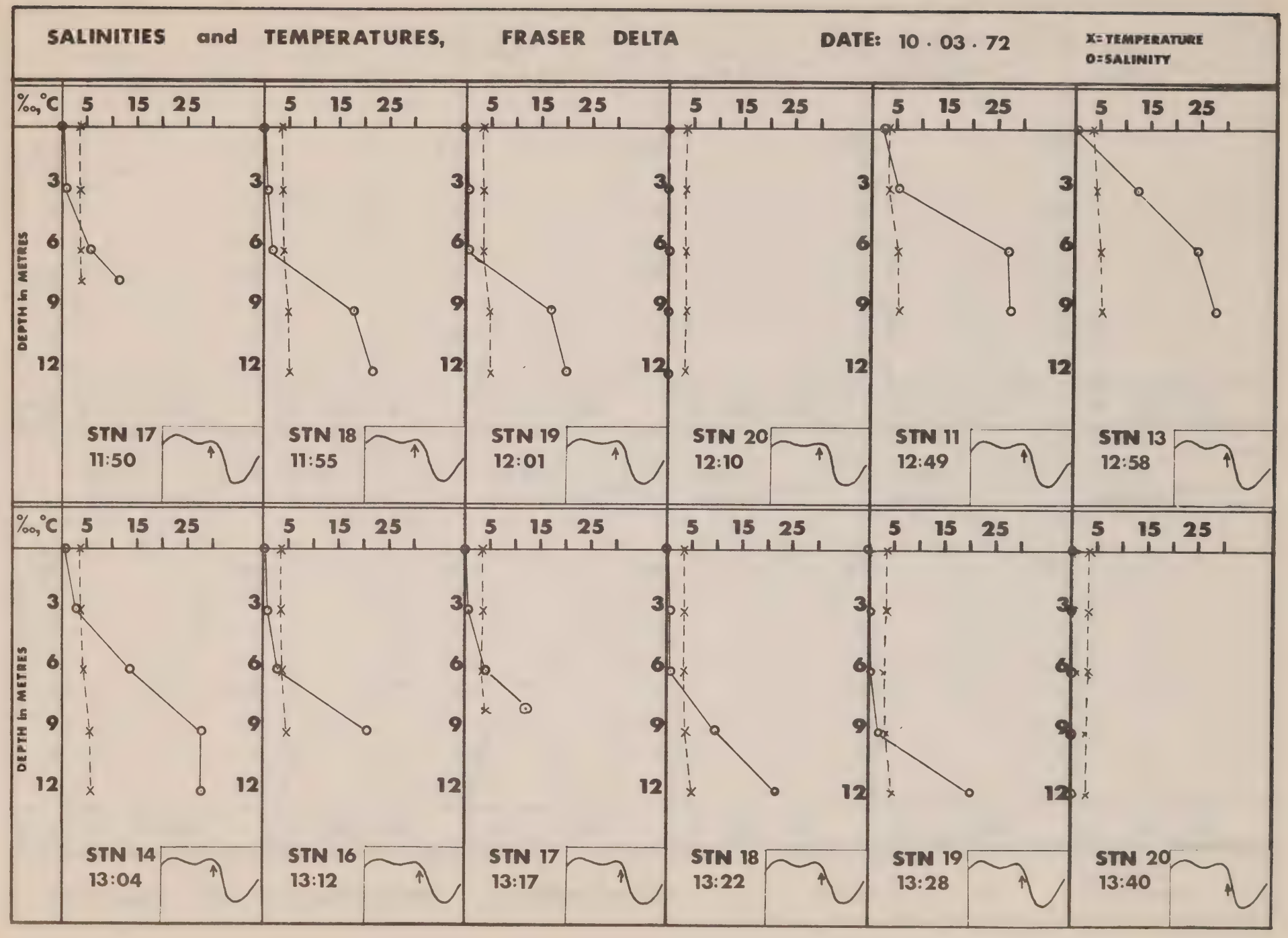
SALINITIES and TEMPERATURES, FRASER DELTA DATE: 8.03.72

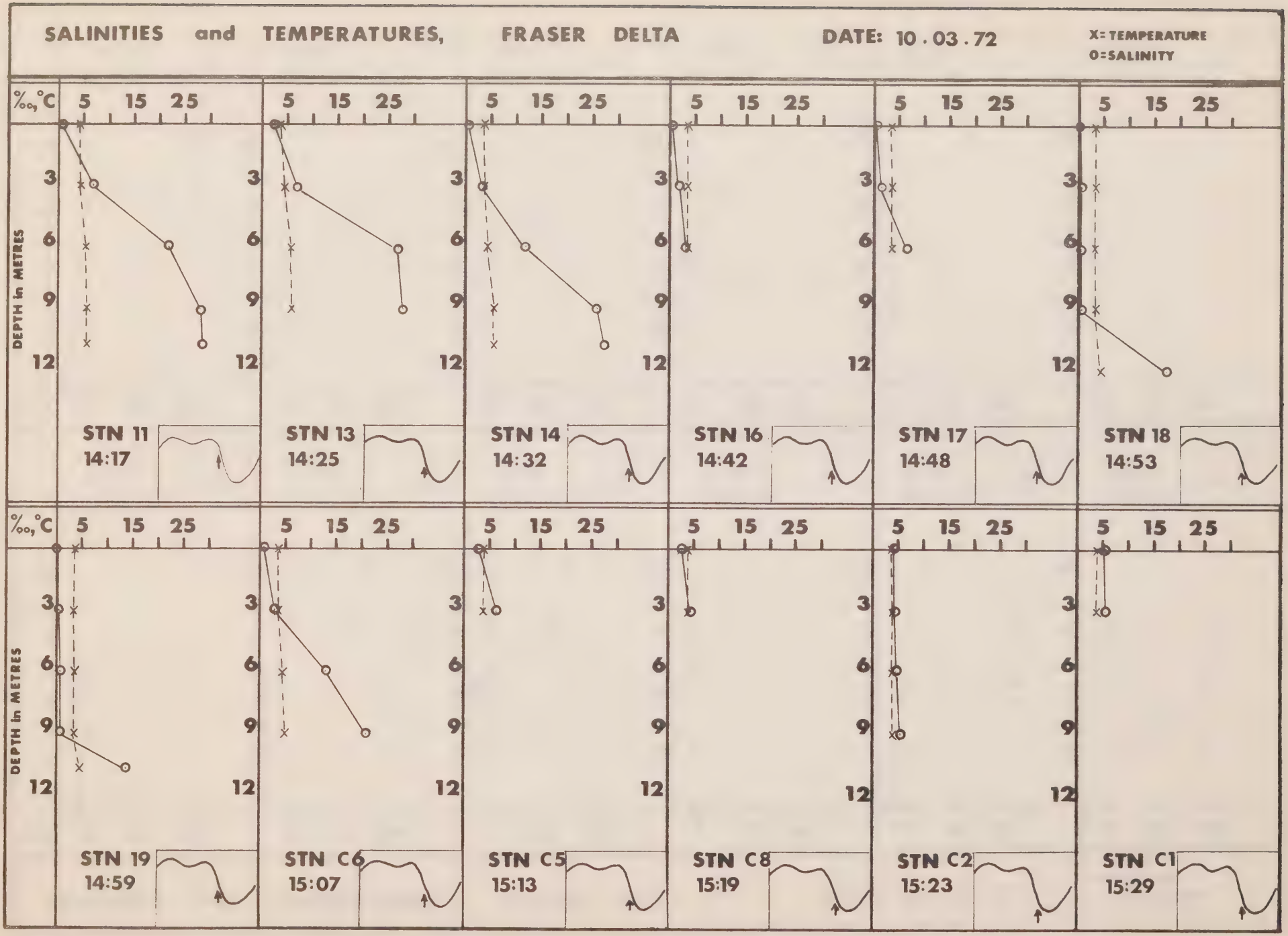
X = TEMPERATURE
O = SALINITY




SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 9.03.72
Q=29,200cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN C4
09:17
STN C9
09:23
STN C3
09:29
STN C2
09:33
STN C1
09:40
STN C8
09:51
STN C5
10:00
STN C6
10:06
STN
STN
STN
STN

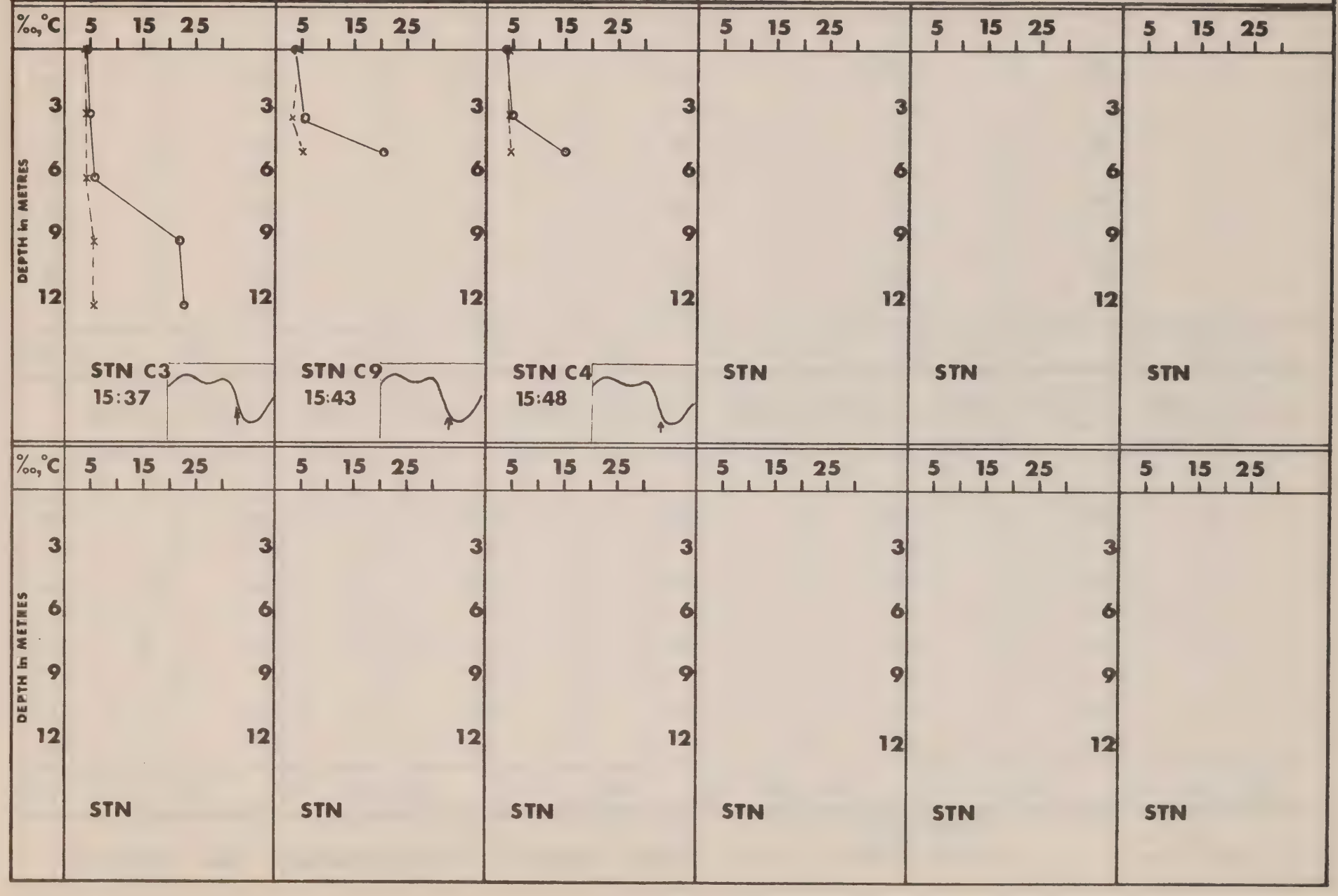

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 10 . 03 . 72
Q=31,100cfs
X= TEMPERATURE
O=SALINITY
‰,°C
5 15 25
DEPTH in METRES
3
6
9
12
STN 11
07:45
STN 13
07:59
STN 14
08:14
STN 16
08:43
STN 17
08:57
STN 18
09:12
STN 19
09:25
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09:40
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11:25
STN 13
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STN 14
11:35
STN 16
11:44

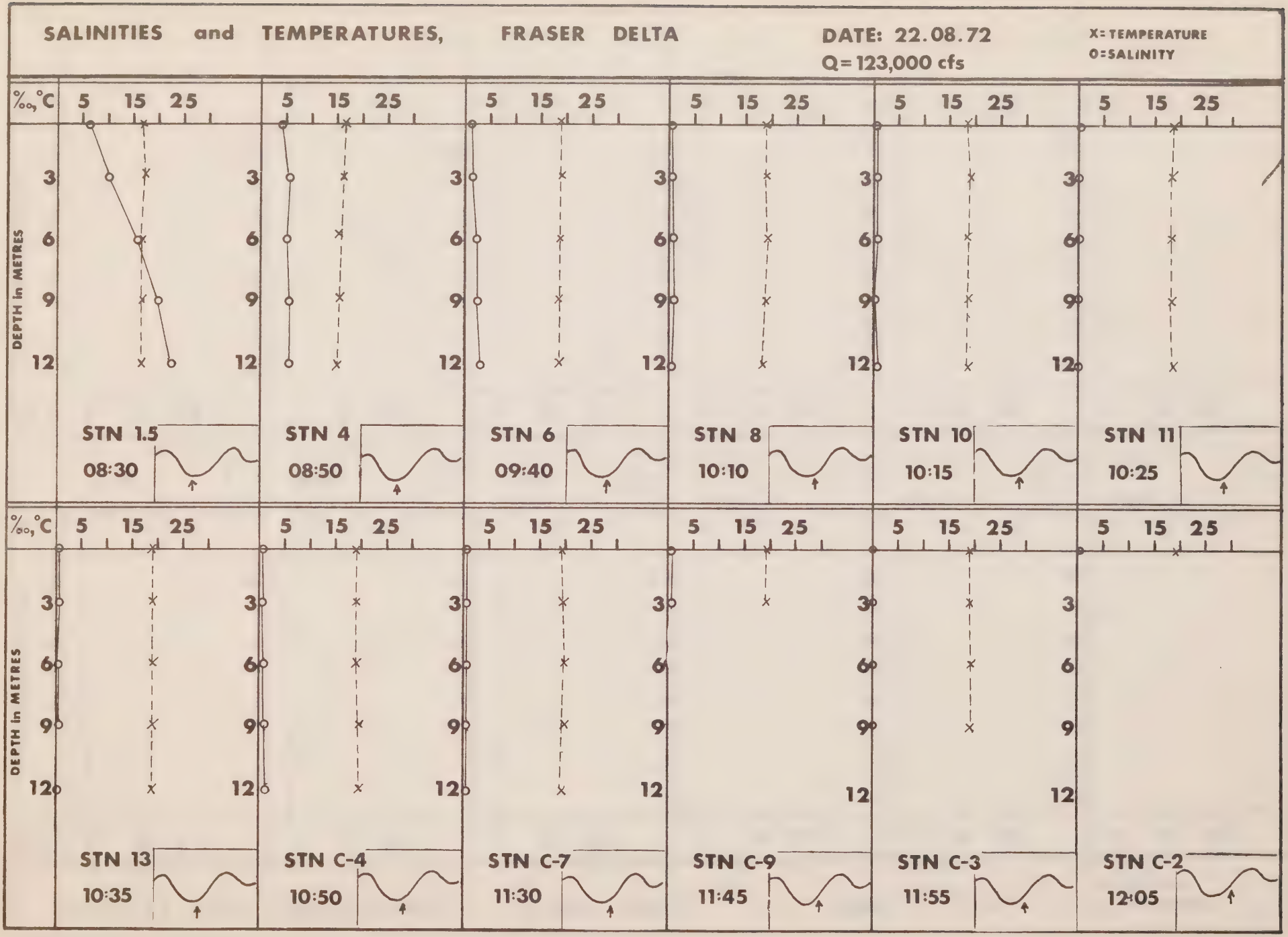

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 10 · 03 · 72
X= TEMPERATURE
O= SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 17
11:50
STN 18
11:55
STN 19
12:01
STN 20
12:10
STN 11
12:49
STN 13
12:58
STN 14
13:04
STN 16
13:12
STN 17
13:17
STN 18
13:22
STN 19
13:28
STN 20
13:40

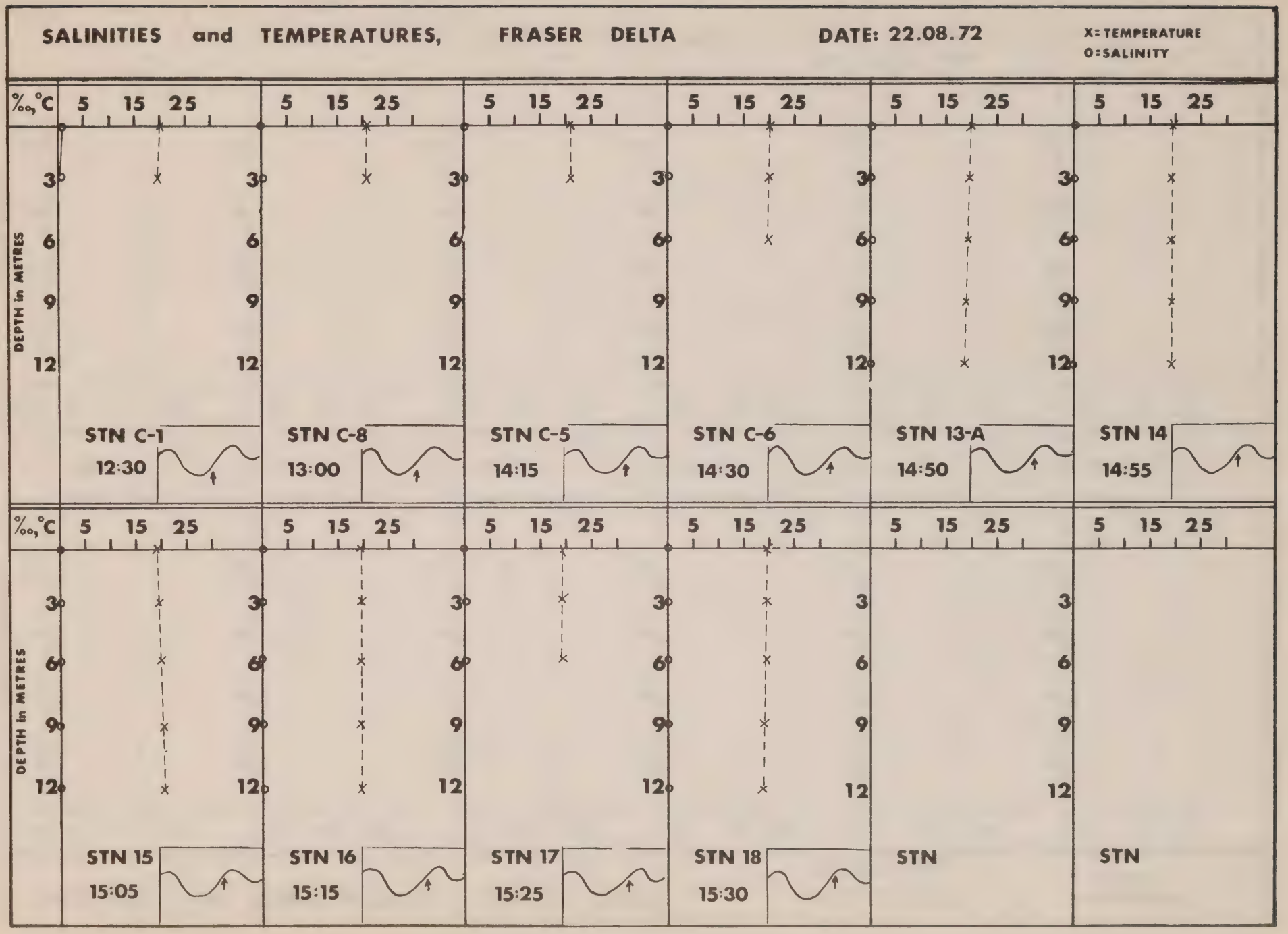

SALINITIES and TEMPERATURES, FRASER DELTA
DATE: 10 . 03 . 72
X= TEMPERATURE
O=SALINITY
‰, °C
5 15 25
DEPTH in METRES
3
6
9
12
STN 11
14:17
STN 13
14:25
STN 14
14:32
STN 16
14:42
STN 17
14:48
STN 18
14:53
STN 19
14:59
STN C6
15:07
STN C5
15:13
STN C8
15:19
STN C2
15:23
STN C1
15:29

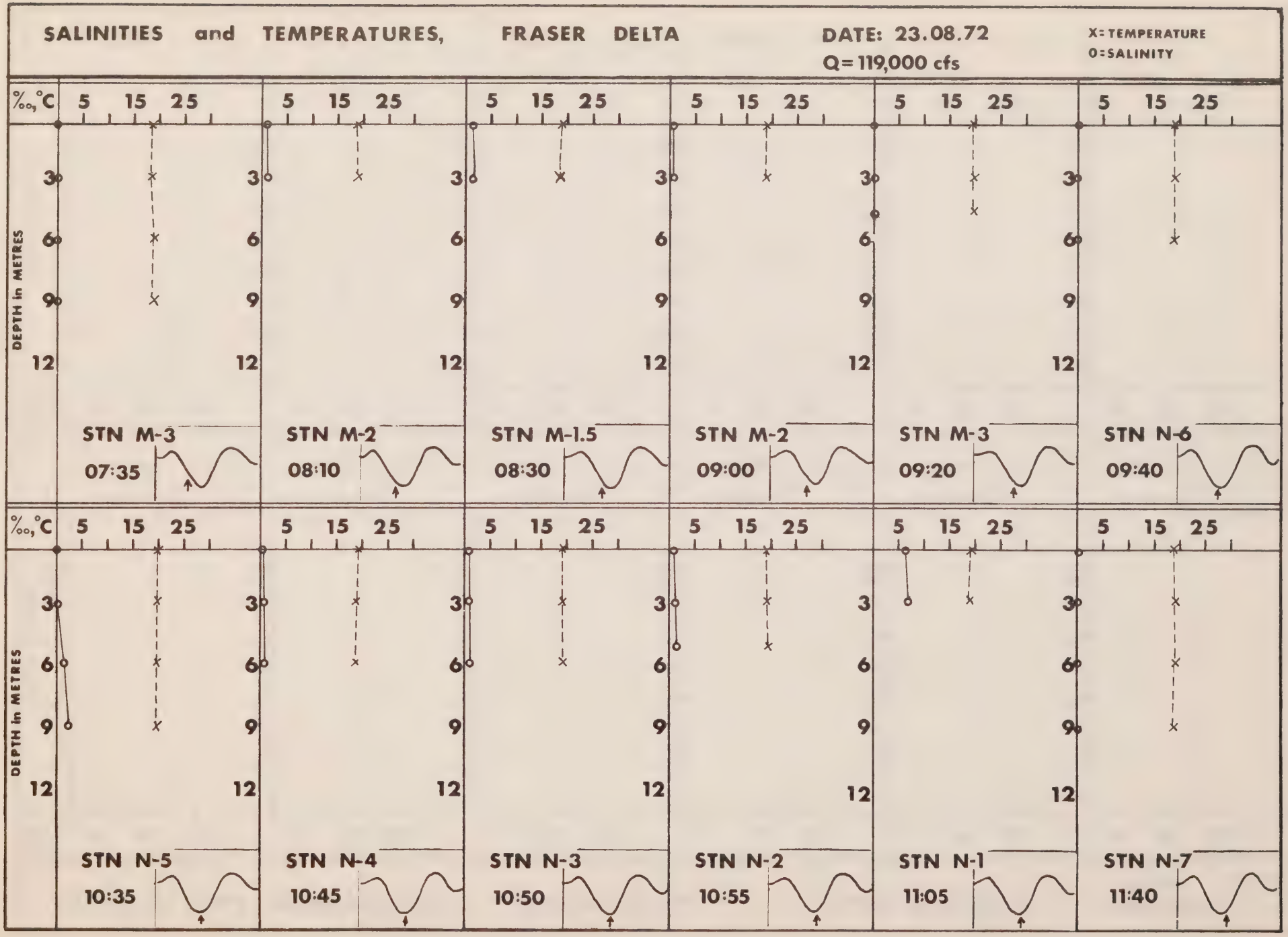
SALINITIES and TEMPERATURES, FRASER DELTA **DATE: 10 . 03 . 72**

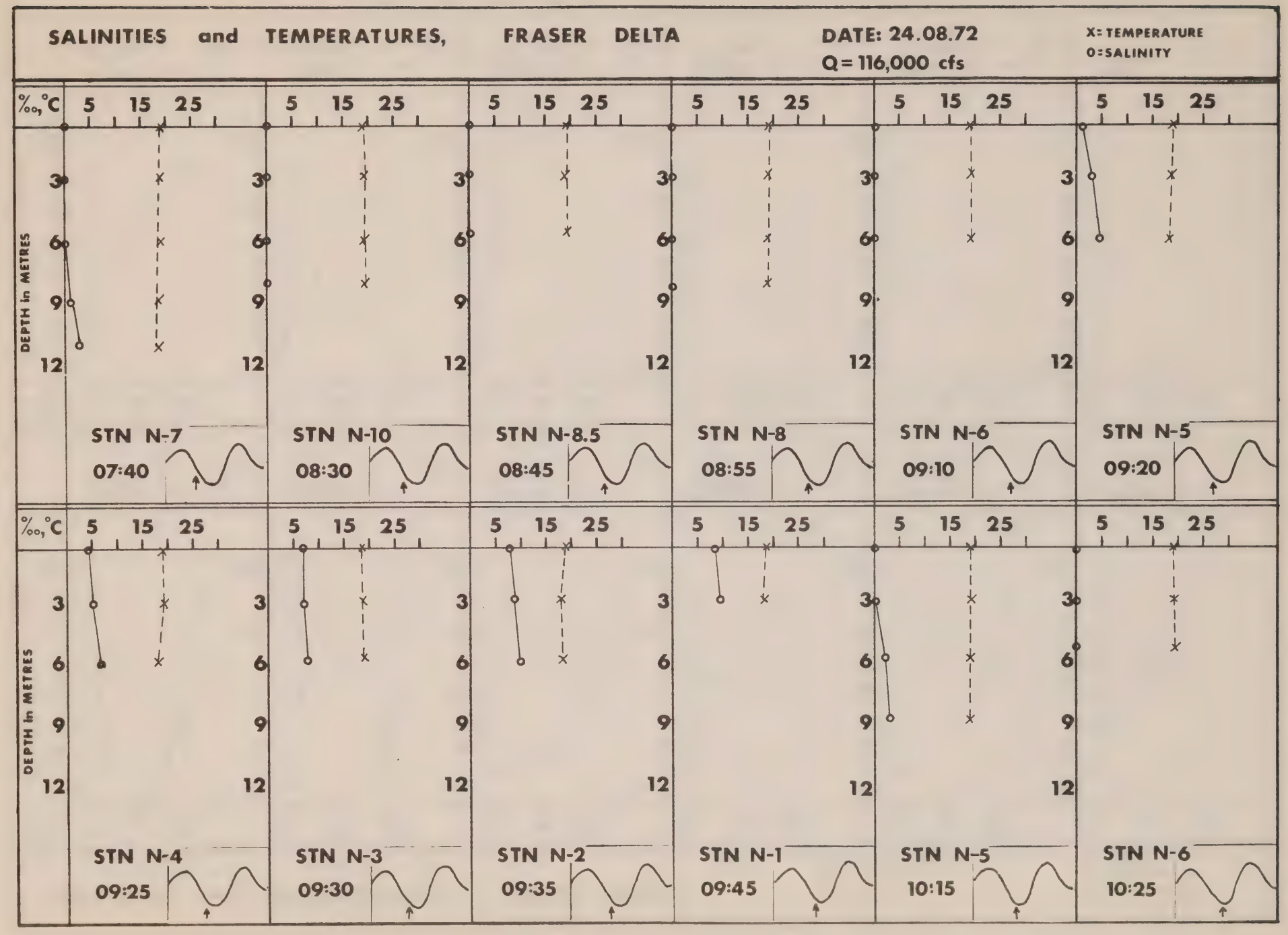
X = TEMPERATURE
O = SALINITY

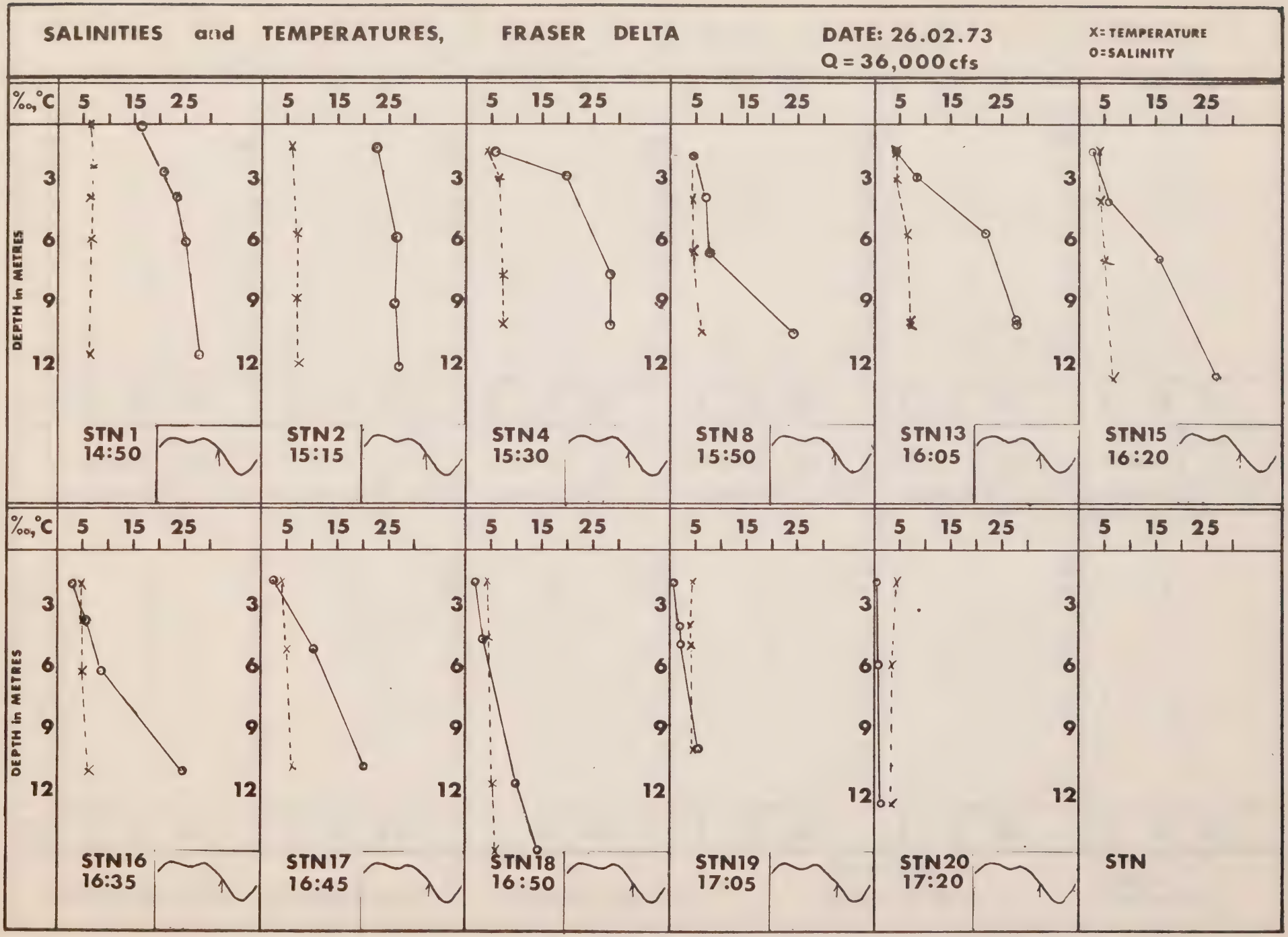


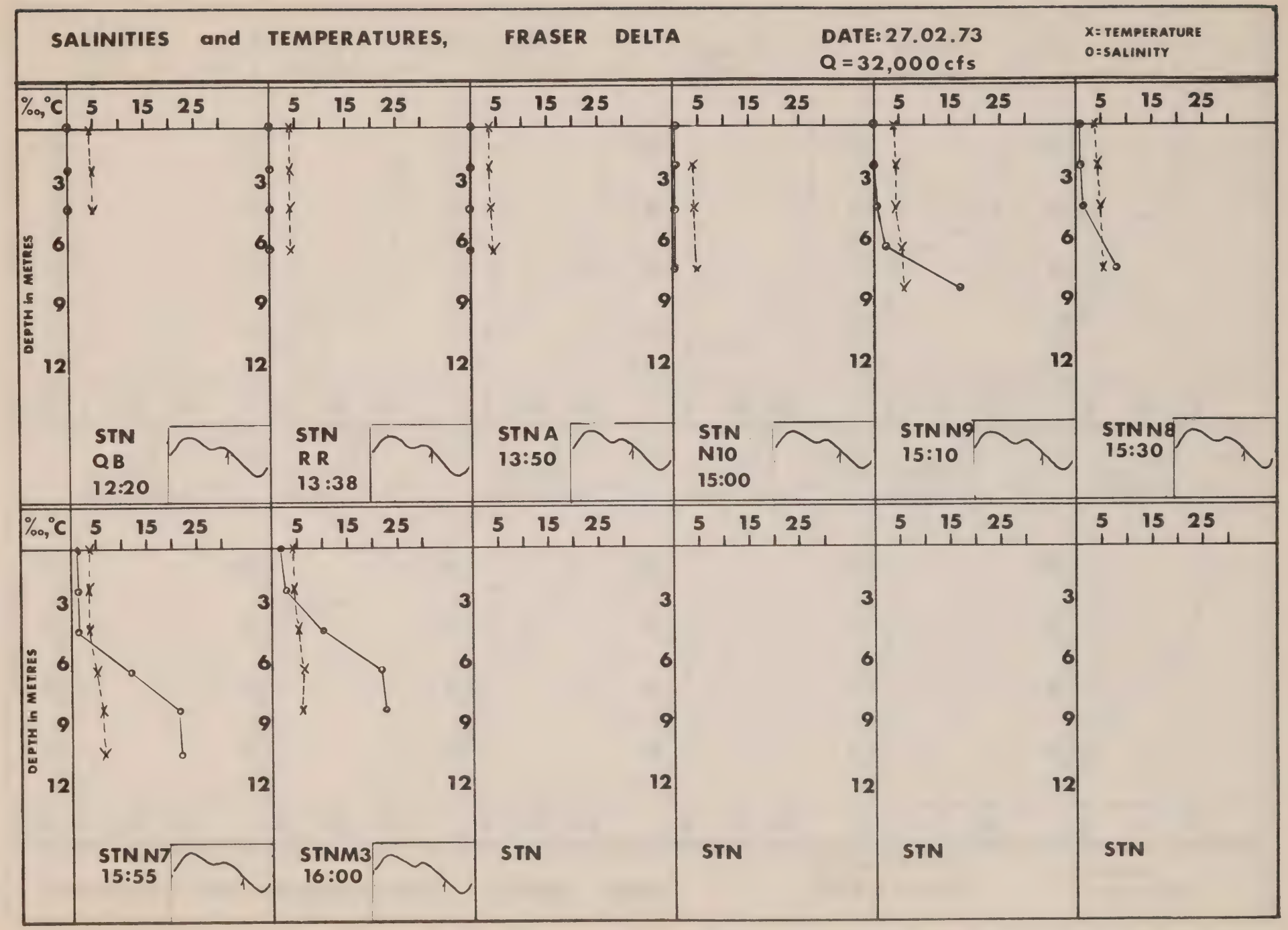

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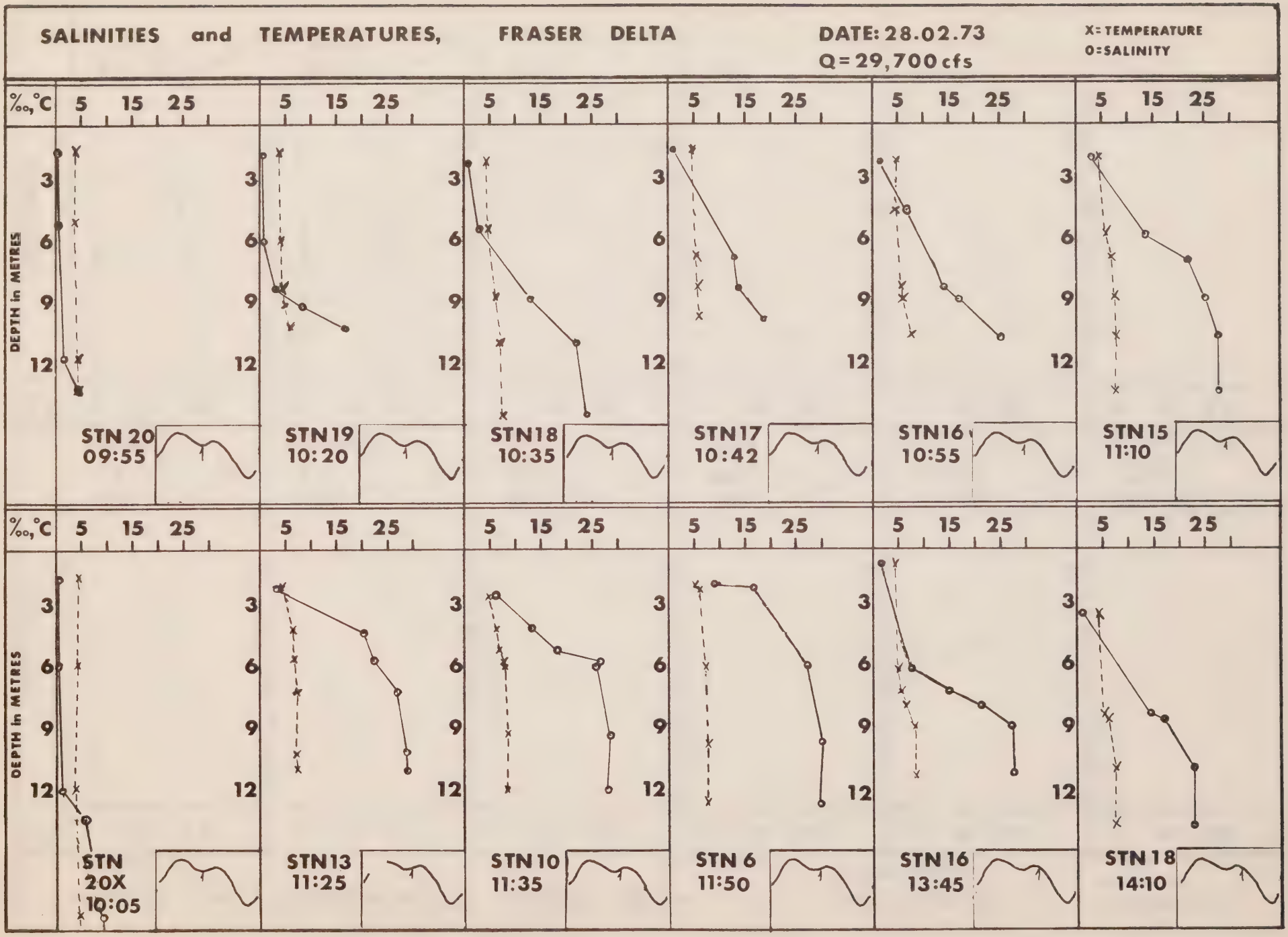

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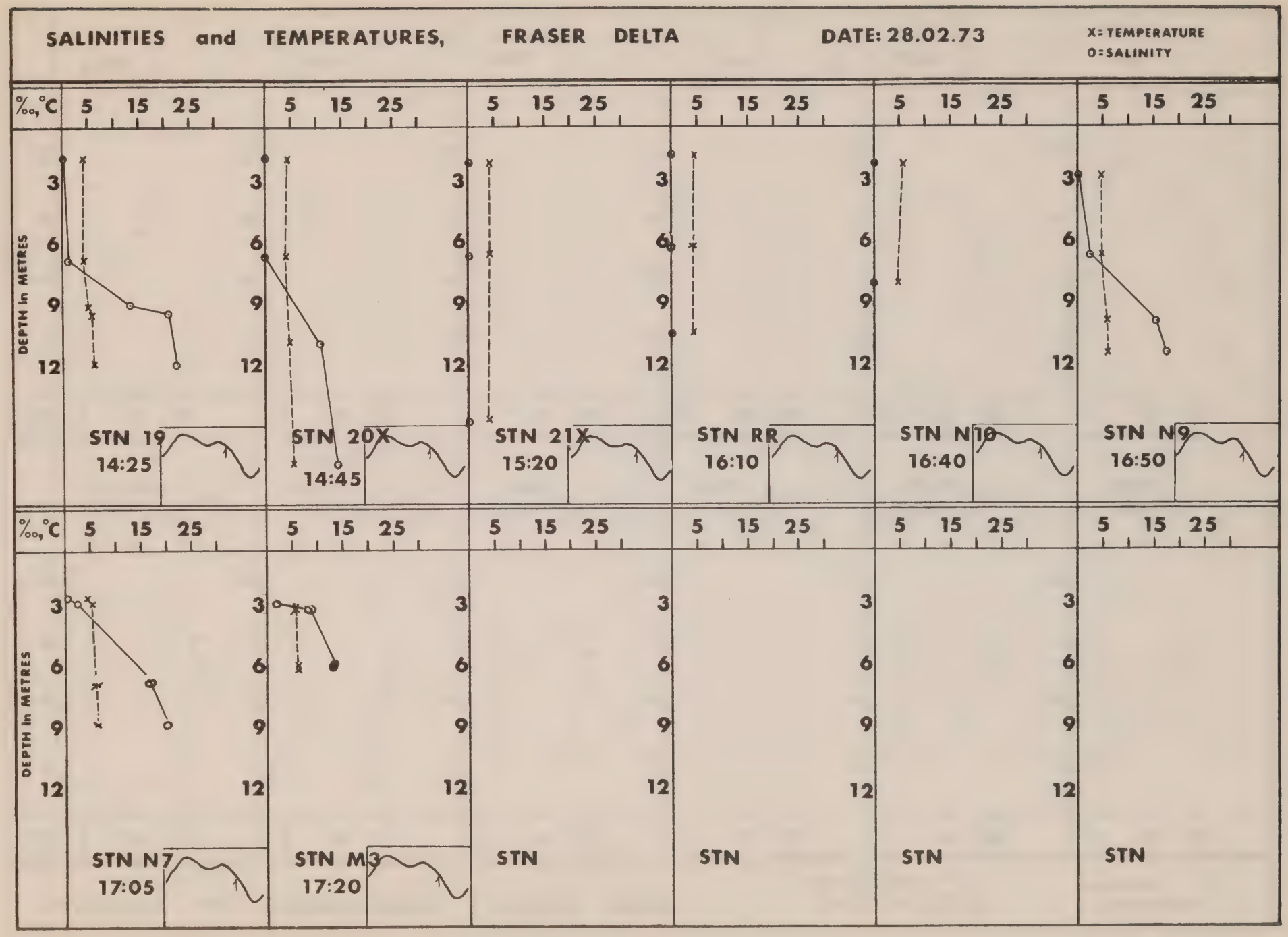

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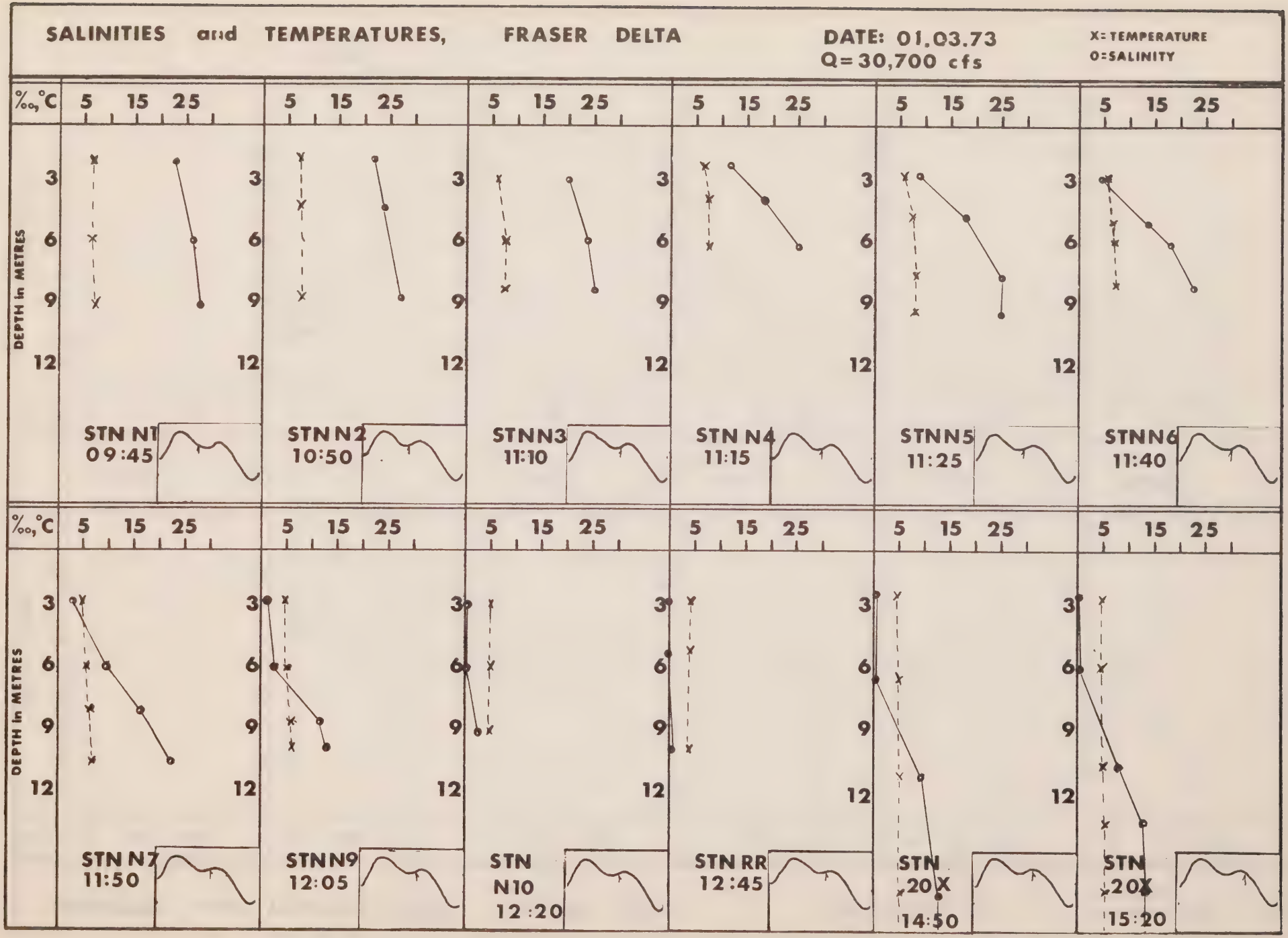

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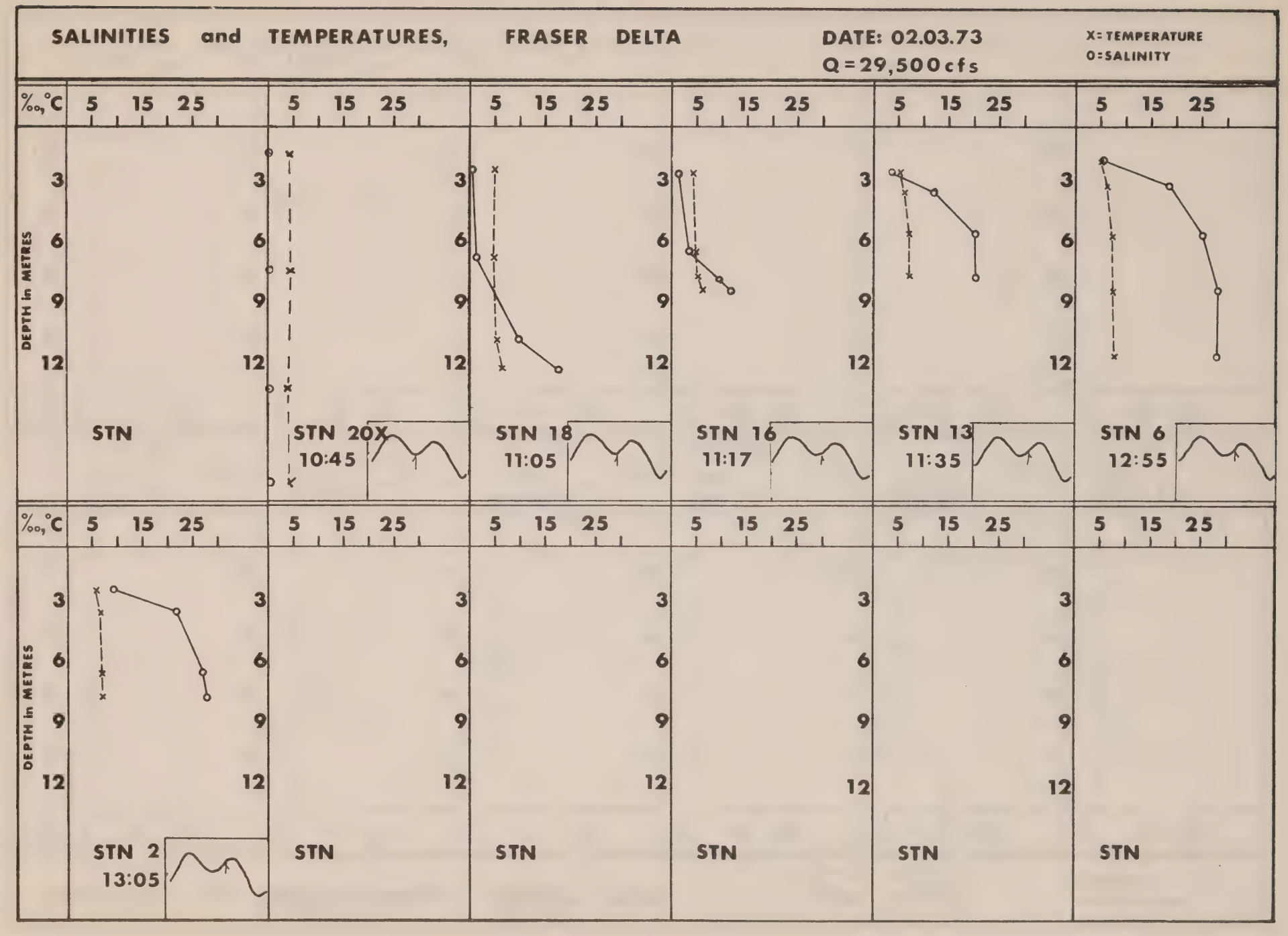

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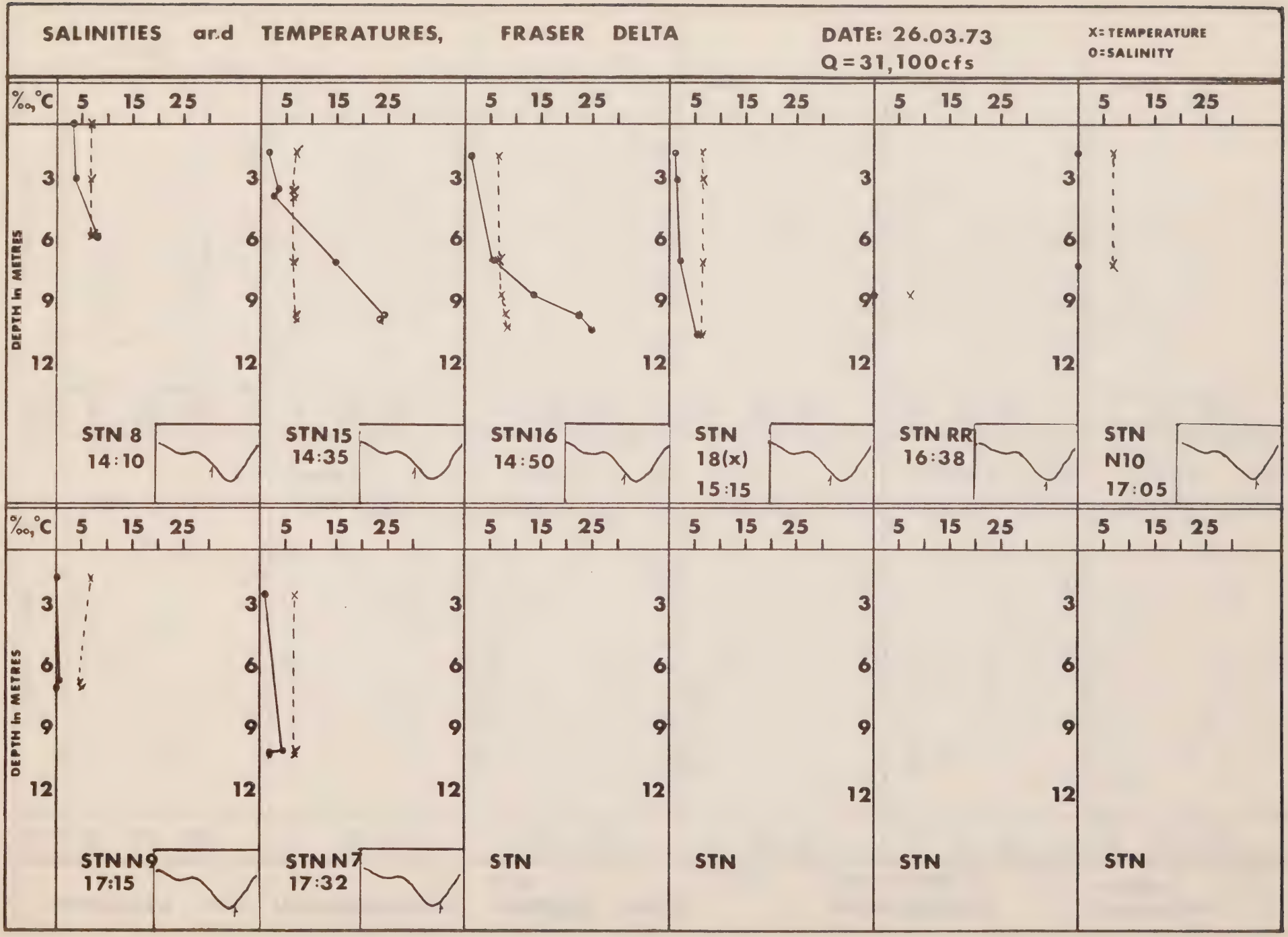

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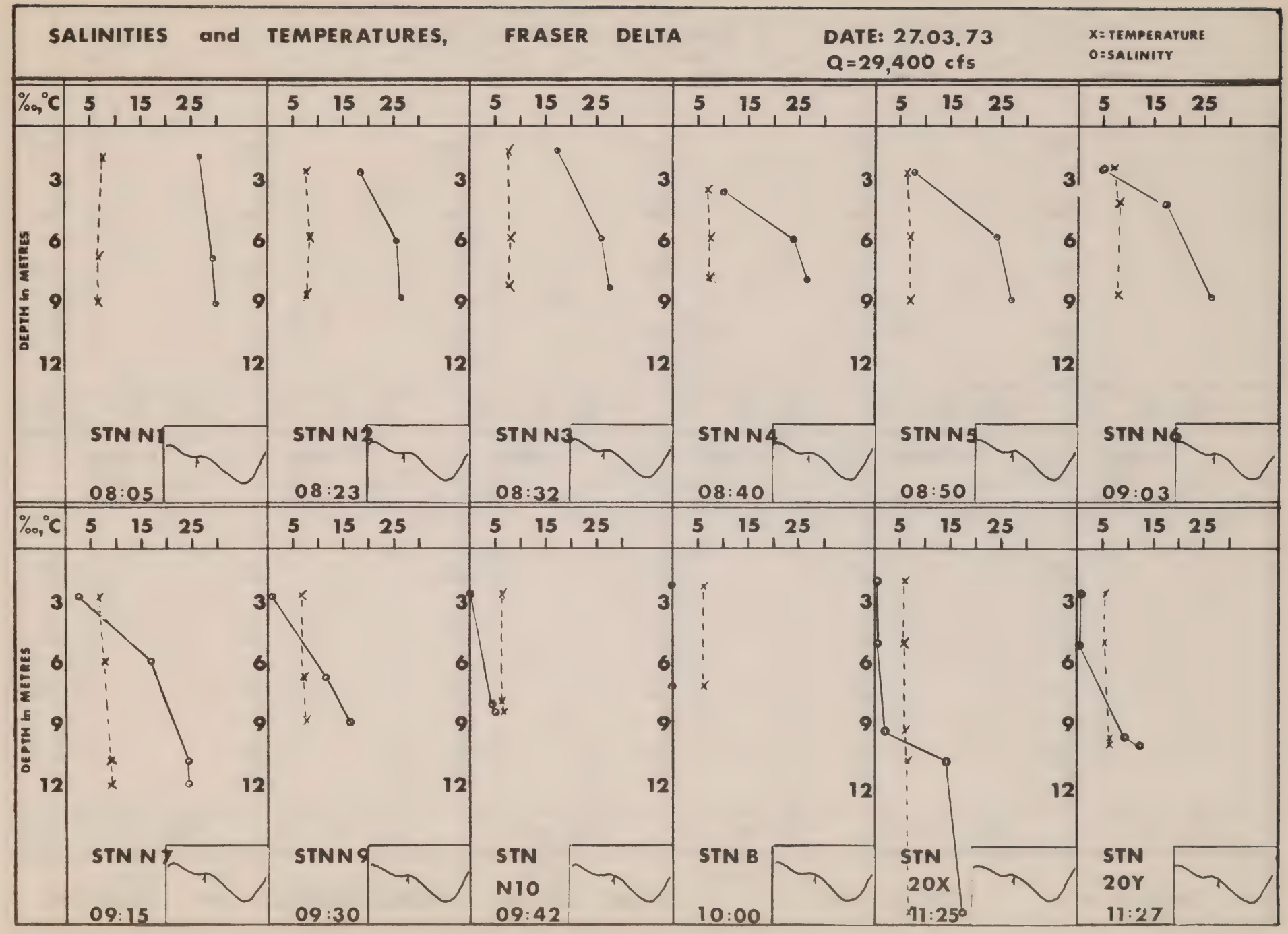

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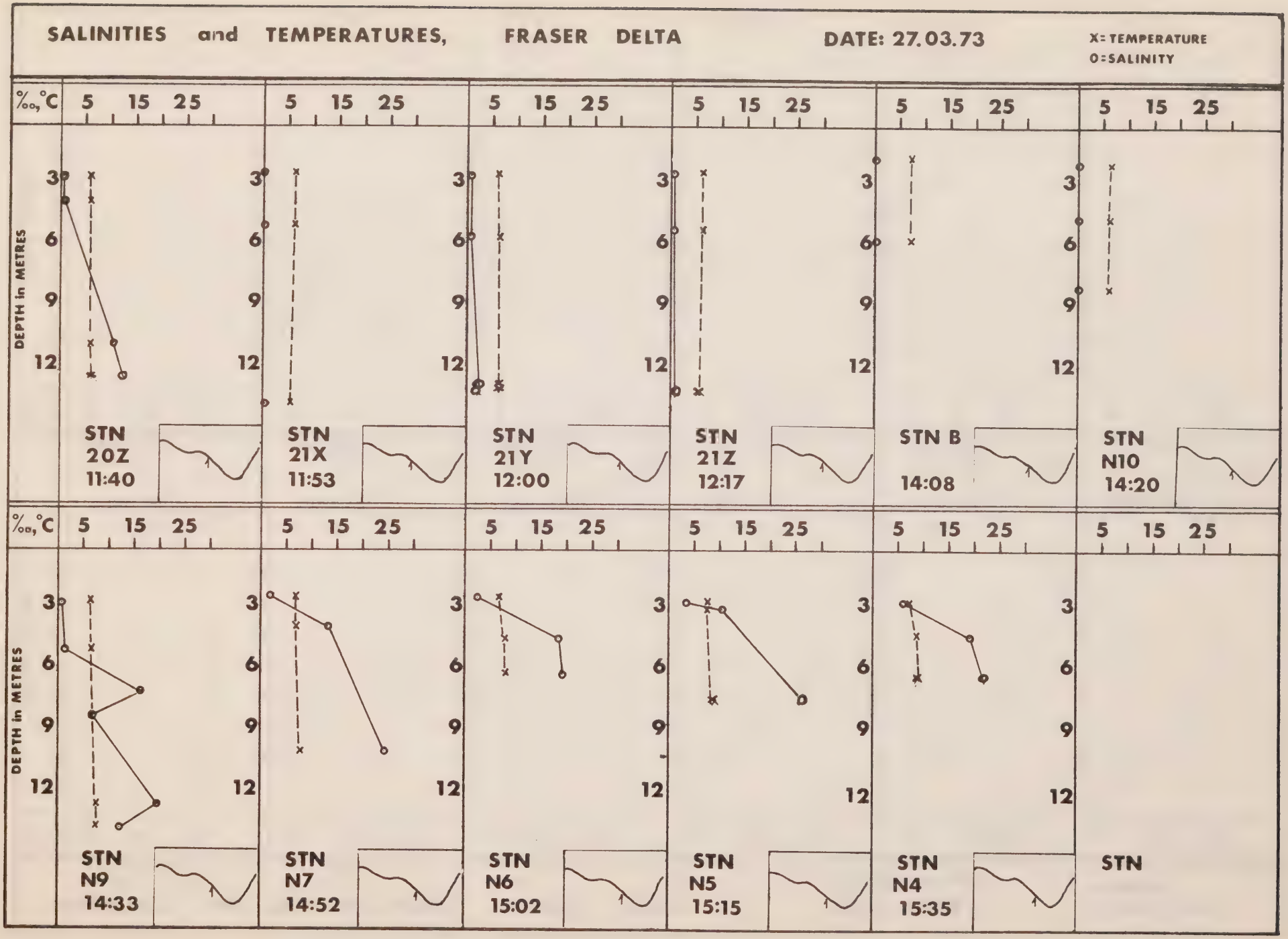

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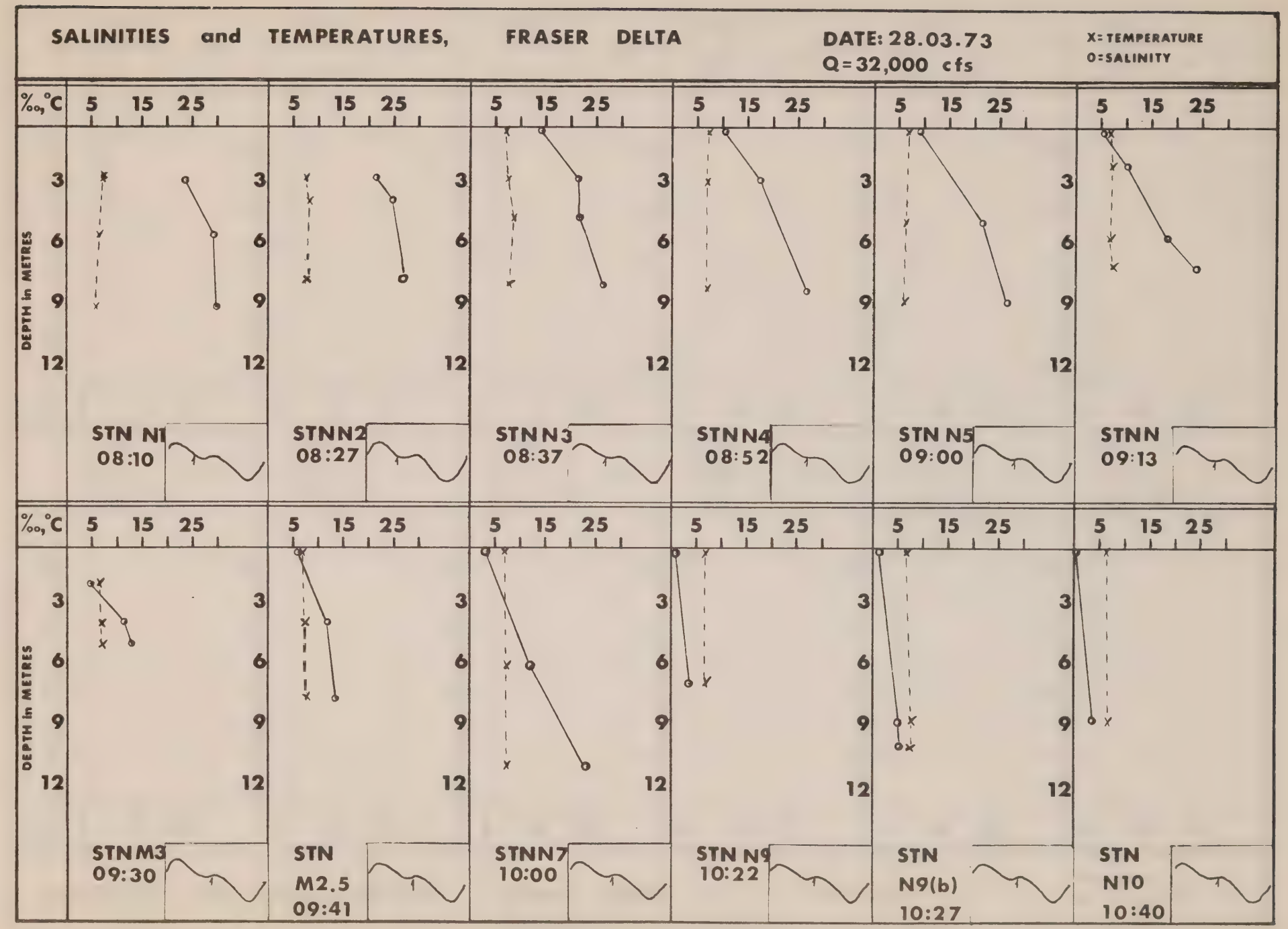

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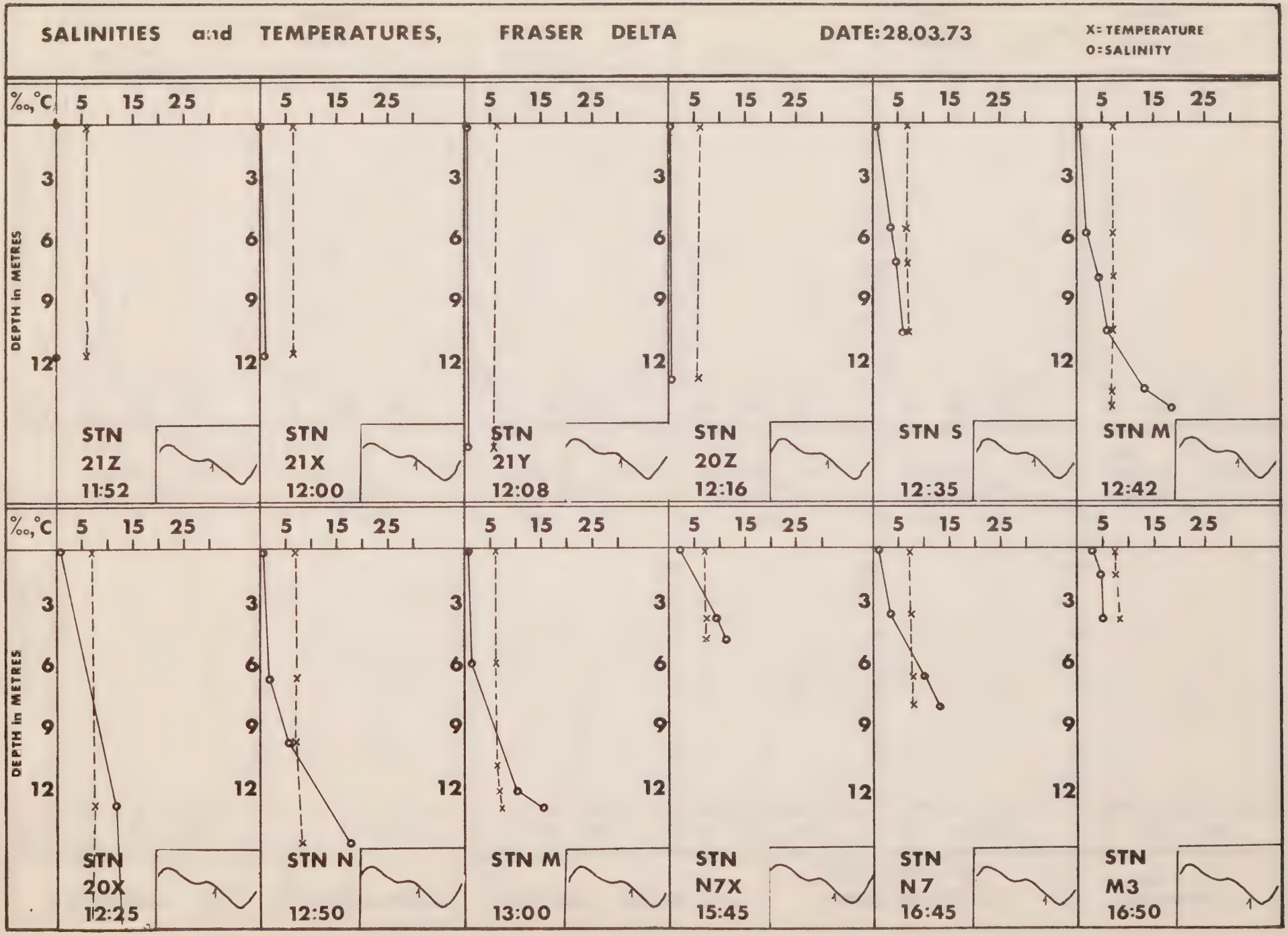

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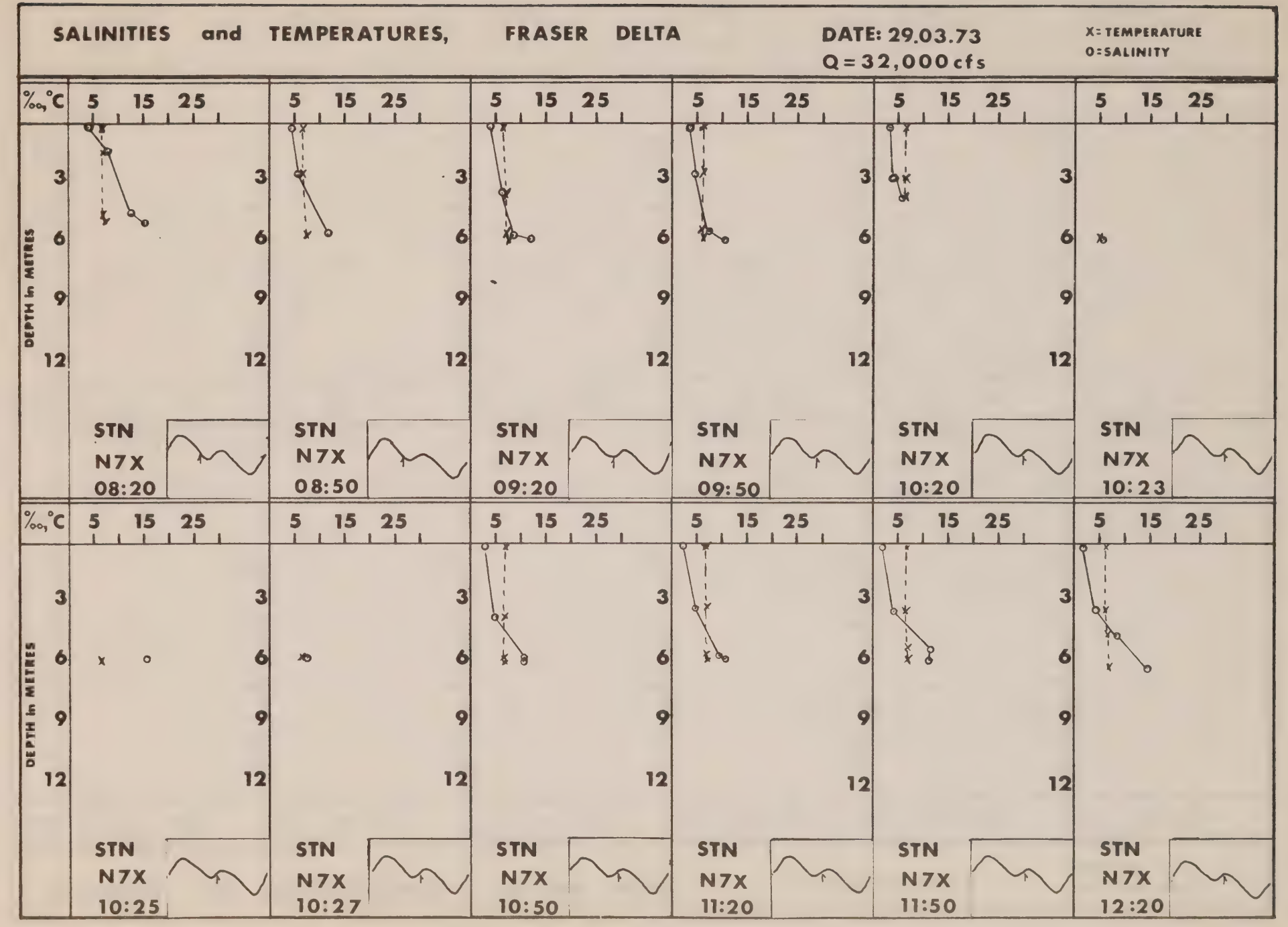

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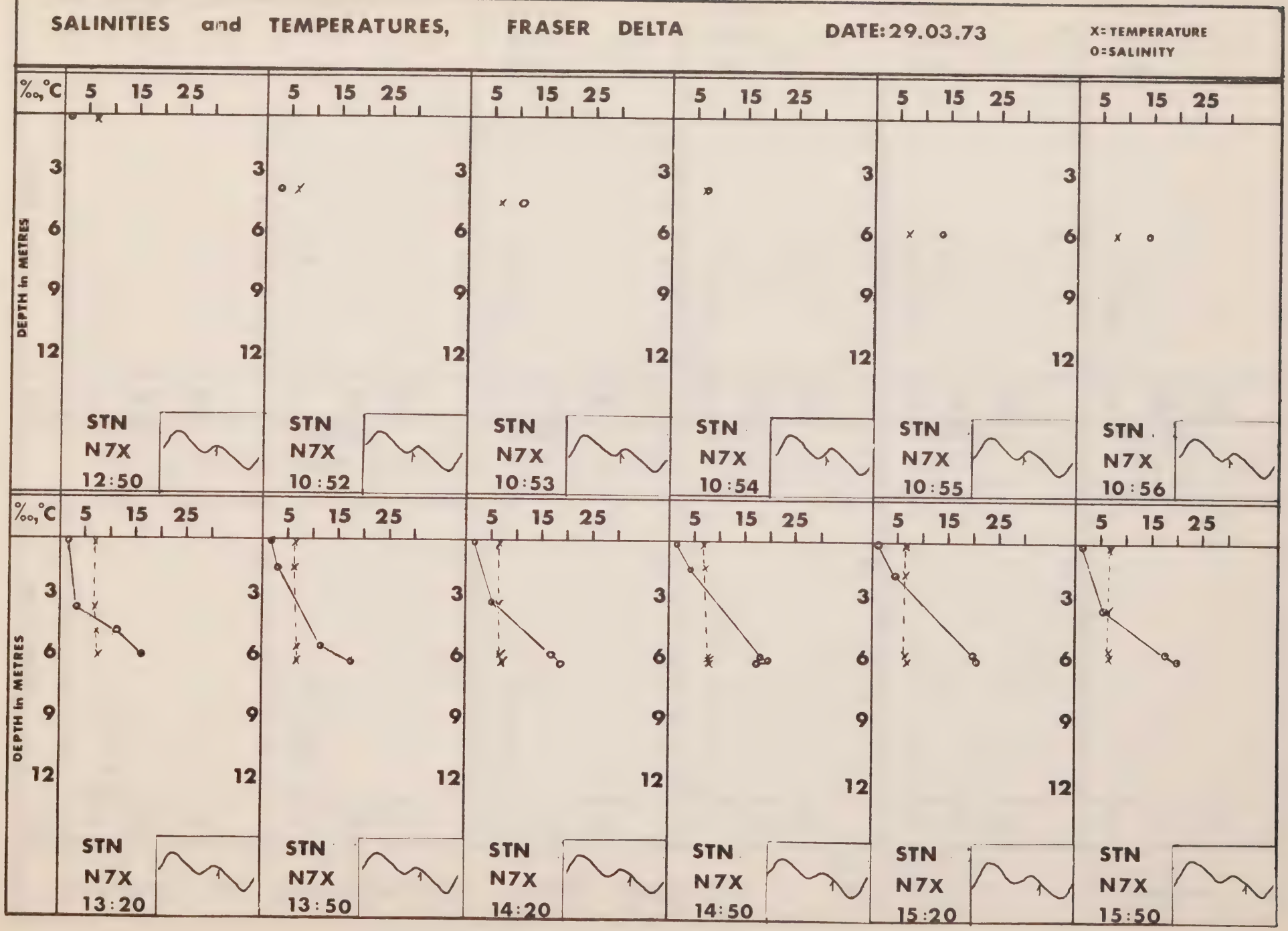

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SALINITIES and TEMPERATURES, FRASER DELTA
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DEPTH in METRES
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DEPTH in METRES
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DEPTH in METRES
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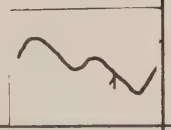
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CAI EP 321
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Pacific Marine Science Report 75-3

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DISPERSION OF DYED SEA-WATER DISCHARGED FROM MOVING VESSELS IN COASTAL WATERS

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PACIFIC MARINE SCIENCE REPORT 75-3

DISPERSION OF DYED SEA-WATER DISCHARGED FROM MOVING VESSELS IN COASTAL WATERS

by

D. FARMER & D. LEMON

INSTITUTE OF OCEAN SCIENCES, PATRICIA BAY
Victoria, B.C.

August, 1975

This is a manuscript which has received only limited circulation. On citing this report in a bibliography, the title should be followed by the words "UNPUBLISHED MANUSCRIPT" which is in accordance with accepted bibliographic custom.

NOTE

The work described in this report was conducted under contract by Dobrocky Seatech Ltd. for Coastal Zone Oceanography Section, Institute of Ocean Sciences, Patricia Bay. This report has been issued simultaneously by Dobrocky Seatech Ltd. under the title "Dispersion of dyed sea-water discharged from moving vessels in coastal waters by D. Lemon[1] and D. Farmer[2].

1 Dobrocky Seatech Ltd., Victoria

2 Coastal Zone Oceanography, Environment Canada, Victoria

1. INTRODUCTION

Dispersal of sewage effluent from ships can present a significant pollution problem in crowded coastal waters. The degree of pollution nuisance depends upon the speed with which the effluent is dispersed. In the ocean, this is accomplished by the process of turbulent diffusion, a phenomenon which is not yet fully understood. Theories that do exist do not describe all aspects of the situation satisfactorily. Moreover they depend upon one or more empirical parameters which can only be evaluated from observational evidence. A reasonably large body of measurements of oceanic diffusion have also been gathered since the advent of Rhodamine dye and fluorometric profiling techniques (Pritchard and Carpenter, 1960). These measurements, in conjunction with the various theories provide sufficient basis for some generalized predictions about oceanic diffusion.

The present study is particularly concerned with this dispersion problem in coastal waters. Special difficulties arise in such areas on account of the great diversity of oceanographic conditions that can exist. In addition to meteorological influences, tidal effects and river run-off can greatly affect the local stratification and mixing rates. Therefore it was decided to perform some experiments in order to see how well the previously existing measurements and theories could be applied to the problem of ship's effluent dispersal. The experiment was also intended to investigate the effects of vertical stratification, ambient turbulence level and vessel wake on the diffusing patch.

This report consists of a summary of necessary theoretical background, which includes the development of a wake in a stratified fluid, and the spread of a passive, conservative scalar due to turbulent diffusion. This is followed by a description of the experiment and the treatment of the data. These observations are then compared to the theories and a predictive model based on the experimental results is chosen from the available theories. Finally, we derive certain formulae which are intended to provide a predictive capability for application to problems of practical concern in coastal waters. An appendix lists a recommended sequence of steps to be followed in applying the results of this report to particular pollution situations.

2. THEORY

The initial stages of diffusion of a patch of this sort must be influenced to a certain extent by the wake turbulence from the ship itself. At some later point in time, when the wake turbulence has decayed below the ambient turbulence level of the surrounding ocean, one may expect that the normal oceanic diffusion processes will take over. The questions which need to be answered are, "To what extent does the wake influence the diffusion process, and how long does its influence last?". To answer these questions it is necessary to know something about the theory and measurements of (turbulent) wakes.

(a) Wakes

A self-propelled body moving through a fluid produces a momentumless wake. It is this sort of wake which we must consider in the case of a ship, not the sort of wake which develops downstream of an obstacle in a flow. Since the ocean commonly has a vertical density gradient, we must also consider the behaviour of wakes in stratified fluids.

Most work on self-propelled wakes in the literature deals with entirely submerged bodies. It is necessary, therefore, to take the results for submerged bodies, since nothing else is available, and apply it to surface wakes. In an unstratified fluid, the wake behind a self-propelled body is circular (in an average sense) and its mean diameter expands as (Merritt, 1972)

$$b/D = K \left(\frac{C_D x}{D}\right)^n , \qquad (2.1)$$

where b is the wake diameter, D is the body diameter, x is the downstream distance, C_D is the drag coefficient appropriate to that particular body, and K and n are the constants to be determined. If we sample at a fixed point in the wake of a self-propelled body, this becomes

$$\frac{b}{D} = K \left(\frac{C_D Vt}{D}\right)^n , \qquad (2.2)$$

where V is the velocity of the body. Several experimental investigations have been made of the growth of a wake behind a self-propelled body. Schooley and Stewart (1963) found

$$\frac{b}{D} = 1.0 \left(\frac{x}{D}\right)^{1/3} , \qquad (2.3)$$

while Naudascher's (1965) results can be fitted by

$$\frac{b}{D} \simeq 1.2 \left(\frac{x}{D}\right)^{1/4} . \qquad (2.4)$$

Experiments by Merritt (1972) give

$$\frac{b}{D} = 1.3 \left(\frac{x}{D}\right)^{1/4} , \tag{2.5}$$

with the possibility that an asymptotic size may be reached.

If one uses the relation

$$u' \simeq \frac{db}{dt} \tag{2.6}$$

for an estimate of the turbulent velocity fluctuations, then the turbulence intensity in the wake decays following the relation

$$\frac{u'}{V} = 0.325 \left(\frac{x}{D}\right)^{-3/4} , \tag{2.7}$$

which agrees with Naudascher's (1965) results.

In a stratified fluid, the wake of a submerged, self-propelled body is critically affected by the stratification. The initial vertical growth of the wake suffers a collapse at a time determined by the density gradient in the fluid (Schooley and Stewart, 1963). The collapse occurs when the turbulent energy within the wake can no longer sustain the vertical extent of the wake against the buoyancy forces seeking to return the mixed fluid to an equilibrium level. After the wake collapses, the rate of horizontal expansion is enhanced.

Merritt (1972) has performed a series of experiments on wake development in stratified fluids with the following results. The wake collapses at a time $t_c = T/3$, where T is the Brunt-Vaisala, or buoyancy period, g is the gravitational acceleration and ρ the density:

$$T = 2\Pi/(g/\rho_o \frac{\partial \rho}{\partial z})^{\frac{1}{2}} . \tag{2.8}$$

In the period before the vertical collapse the wake grows as

$$\frac{b}{D} = KF^n \left(\frac{t}{T}\right)^n \tag{2.9}$$

where F = VT/D is the Froude number. The best values of K and n are 1.3 and 0.25 respectively. The maximum vertical growth, achieved at the time of collapse is

$$\frac{hmax}{D} = 0.9F^{\frac{1}{4}} \tag{2.10}$$

and the asymptotic vertical size is given by

$$\frac{h_f}{D} = 0.5F^{\frac{1}{4}} \tag{2.11}$$

The horizontal extent of the wake during the collapsing phase is given by

$$\frac{b_h}{D} \simeq 2F^{\frac{1}{4}} \left(\frac{t}{T}\right)^{\frac{1}{2}} , \tag{2.12}$$

and after the vertical collapse by

$$\frac{b_c}{D} \simeq 2F^{\frac{1}{4}} \left(\frac{t}{T}\right)^{\frac{1}{4}} . \tag{2.13}$$

It is this vertical extent of the collapsed wake which is of particular significance in the present study since it determines the thickness of the effluent plume.

(b) Turbulent Diffusion

There is no completely satisfactory theory of turbulent diffusion, because the general turbulence problem has not been solved. Many theories exist which attempt, with varying degrees of success, to parametrize the problem.

A theory based on a diffusion equation can describe only the mean concentration field. Any single manifestation will necessarily differ from that described because diffusion is a random process. The predicted value at any given point and time would be found only if many experiments were done under identical conditions and an ensemble average were taken of the results. In view of this great irregularity, a proper, complete theory should be able to predict the variance of the concentration at a point, as well as the mean field as a function of space and time. This is necessary if predictions are to be made of pollution levels, for example, since a low mean concentration is small comfort if very large fluctuations can occur.

There are two ways of approaching diffusion: one is from a fixed frame of reference, the other from a frame attached to the diffusing cloud. Clearly, in the case of a free-floating, diffusing patch in the ocean, the best approach is the relative one, using a reference frame attached to the center of mass of the diffusing cloud. Equations which predict the concentration field at fixed points in space are of no use in describing the diffusion of a randomly moving cloud. The rate at which the cloud changes, regardless of where its position happens to be is the most important thing.

These theories will be briefly outlined. They apply to the lateral diffusion of a dye patch laid in the wake of a vessel. Experimental evidence clearly shows that in stratified waters vertical diffusion is greatly inhibited, so that the vertical extent of the patch is determined principally by

the initial wake. We shall henceforth be mainly concerned with the horizontal diffusion of the resultant effluent plume.

1. Constant eddy coefficient

This is the simplest theory of turbulent diffusion. It assumes that turbulent diffusion is analogous to molecular diffusion and can be parameterized by a single quantity K called an eddy coefficient. In this case, the concentration field C obeys the equation

$$\frac{\partial C}{\partial t} = K \frac{\partial^2 C}{\partial x^2} \tag{2.14}$$

where x is the horizontal coordinate.

For an infinitely long plume of initial width ℓ_o in a body of water of infinite horizontal extent the solution is (Grosch, 1972)

$$C(t,x) = \frac{1}{2}\left[\operatorname{erf}\left[\frac{x/\ell_o + \tfrac{1}{2}}{\sqrt{4t/t_o}}\right] - \operatorname{erf}\left[\frac{x/\ell_o - \tfrac{1}{2}}{\sqrt{4t/t_o}}\right]\right] \tag{2.15}$$

where $t_o = \ell_o^2/K$, K being evaluated from experimental data. The variance of the distribution (2.15) is

$$\sigma^2 = 1/12 + 2t/t_o \quad , \tag{2.16}$$

so that if we choose σ as the size scale for the patch,

$$\ell/\ell_o = \sqrt{1 + 24t/t_o} \quad . \tag{2.17}$$

For $t > t_o$ then, the patch size grows proportionally to $t^{\frac{1}{2}}$, and the mean concentration decays as the reciprocal of ℓ/ℓ_o, and is proportional to $t^{-\frac{1}{2}}$.

2. 4/3 Law

This is one of the class of theories which allow the eddy coefficient to vary with the scale size of the diffusing patch. Richardson (1926) studied diffusion of particles in the atmosphere and concluded from experimental evidence that it was best described by a diffusion equation in which

$$K = \varepsilon \ell^{4/3} \tag{2.18}$$

with ε a constant and ℓ being the distance between particles. To apply this to a diffusing dye patch in the ocean, it is necessary to decide what to choose for the scale size ℓ, as there are no particles between which to measure distances. Grosch (1972) considers two choices: one is to use the distance from the center of the patch, x; the other is to use the entire size of the patch, ℓ. This latter choice requires some criterion for determining just what the patch "size" is, as the theoretical mean distribution only approaches zero asymptotically. The most reasonable choice seems to be that used already: the standard deviation of the patch distribution. Grosch argues that, since turbulent eddies significantly smaller than the size of the entire patch provide internal mixing, but are not very efficient at diffusing the patch into surrounding waters, the best choice is the integral scale model, where ℓ is taken as the standard deviation of the patch. This model predicts that the patch size (taken as being σ) should follow

$$\ell/\ell_o = (1 + 8t/t_o)^{3/2} \quad , \tag{2.19}$$

and that the mean concentration

$$\overline{C} = (1 + 8t/t_o)^{-3/2} \tag{2.20}$$

For $t > t_o$, ℓ will increase as $t^{3/2}$ and $\overline{C}$ should decrease as $t^{-3/2}$. This of course assumes 2-dimensional mixing only.

The similarity theory of turbulence offers some justification for the 4/3 law. Because the spectrum of energy in turbulence is not constant, the energy contained in eddies at different scale sizes is different. Therefore, the rate at which mixing occurs varies with the scale of diffusion. The constant eddy coefficient model is not equipped to handle this, and therefore does not apply very well to oceanic diffusion. In the ocean, the energy spectrum increases with increasing scale size, up to some limit which is much larger than the size (1 Km) of patches considered in this study. Therefore as the patch grows in size, progressively larger, and hence more energetic, eddies begin to play a role in the diffusion of the patch, instead of simply advecting it bodily. If this region of the turbulent energy spectrum happens to be an inertial subrange, then (Csanady, 1971) the eddy coefficient K should be proportional to $\ell^{4/3}$. If it is not an inertial subrange, then K will have some other dependence. The turbulent spectrum at larger scales in the ocean is not sufficiently well known to state whether or not this is true. The validity of the 4/3 law therefore must remain in doubt.

Csanady (1971) discusses some of the fundamental aspects of turbulent diffusion theory. In dye patch diffusion studies it is important to know what the diffusion parameters are relative to the patch itself; one must, in Batchelor's (1952) words "follow the cloud", since we are not interested, in this case, in effects at a fixed point. The theory of relative diffusion has not progressed much since Batchelor's work, and it is appropriate only to describe the behaviour of the mean concentration field, not the field of concentration fluctuations.

The quantity of prime interest is the dispersion tensor which defines the spatial spread of the concentration field (Csanady, 1971)

$$\sigma_{ij}^2 = \frac{1}{C_I} \int x_i x_j \, C(\underset{\sim}{x},t) \, d\underset{\sim}{x} \quad , \tag{2.21}$$

where C_I is the integrated concentration

$$C_I = \int C(\underset{\sim}{x},t) \, d\underset{\sim}{x} \quad . \tag{2.22}$$

The characteristic dimensions of the patch are given by σ_{ij}; in the experiment done here, σ_{22} corresponds to σ_x, the patch width. It is possible if one assumes that the mean concentration profiles tend to a Guassian shape, to define a so-called "diffusivity tensor" Kij with

$$\frac{\partial C}{\partial t} = \frac{\partial}{\partial x_i} (Kij \frac{\partial C}{\partial x_j}) \tag{2.23}$$

(Csanady, 1971). In the isotropic case, Kij = Kδij, where δij is the "Kronecker δ", and

$$K = \frac{1}{2} \frac{d\sigma^2}{dt} \quad . \tag{2.24}$$

Arguments from the similarity theory of turbulence may be used to define three distinct diffusion regimes, each with a different form for K (Csanady, 1971). The first regime is found at diffusion times shorter than the characteristic time scale of the turbulence; in this initial phase, relative velocities are still correlated and it may be shown that

$$K = Bt \tag{2.25}$$

where B is a constant related to the average product of the turbulent velocity fluctuations. If the patch is of a size corresponding to an inertial subrange in the turbulence, then

$$K = C_1 \varepsilon^{1/3} \sigma^{4/3} \tag{2.26}$$

where ε is the energy dissipation rate and C_1 is a constant. This is the 4/3 law referred to before. In this case K may also be written in the form

$$K = C_1 \varepsilon^{1/3} (\sigma_o^{2/3} + 2/3\ C_1 \varepsilon^{1/3} t)^2 \qquad (2.27)$$

where σ_o is the initial patch size. In this case K is asymptotically proportional to t^2. At very long times, if the cloud becomes large compared to the turbulent length scale, then there is no longer a distinction between absolute and relative diffusion, and K reduces to a constant

$$K = K_L \quad . \qquad (2.28)$$

3. EXPERIMENT

The experiment was performed twice; once in Saanich Inlet, and once in the Strait of Juan de Fuca, at Royal Roads, (Fig. 15). These two areas were chosen to provide as great a contrast in environment as possible. Saanich Inlet is highly stratified, semi-enclosed and fairly quiet as far as turbulence is concerned. The Juan de Fuca site has a well-mixed surface layer and has a high degree of turbulence from both wind and tidal action.

We shall describe the experiment in Saanich fully, and cover only points where the Juan de Fuca experiment differed.

(a) Saanich Inlet Experiment

The experiment was performed on April 10, 1975 in Saanich Inlet near Patricia Bay. Five hundred grams of Rhodamine B fluorescent dye were placed in CSS RICHARDSON's sewage tank, which was then filled with sea water. The initial dye concentration in the tank was 3.59×10^{-2} g/L. The tank was discharged while the ship was steaming in a straight line at ten knots. The initial patch was about 1 Km long and a few (<10) metres in width. A series of drift drogues were placed in the patch as it was laid, in order to aid the profiling boats in finding the patch. Both horizontal and vertical measurements were taken to define the patch.

Horizontal profiling was done using a 22 foot launch towing a Variosens autoranging fluorometer at 1 metre depth; output was recorded on chart paper. The launch speed was held as nearly constant as possible at 2.6 m/sec. Vertical profiling was done using a Turner Model III fluorometer with the intake hose lowered from the 40 foot launch SEATECH II. To counteract the effects of lag and smearing in the hoses, the intake was lowered in 1 metre intervals, and the reading was allowed to stabilize at each depth before the intake was lowered again. The profiling vessels were tracked by radar from the 130 foot vessel SEA LION securely moored at three points to the naval buoys at Patricia Bay. The positions of the profiling vessels were plotted using a transparent plotting table overlay on the radar set. Time marks were given to SEATECH I by CB radio and these were then marked on the chart paper. The average speed of the boat was evaluated from the radar plots, and used to convert distance on the chart paper to real distance. The positions of the horizontal transects and the vertical stations were also plotted from the radar, thus enabling a picture of the diffusing patch to be constructed. Thirty-five horizontal transects and fifteen vertical profiles were taken over a period of seven hours, before measurements ceased.

Oceanographic conditions were measured by bottle casts at the beginning and end of the experiment, and by BT casts at alternate vertical profiling stations.

(b) Juan de Fuca Experiment

The Juan de Fuca experiment was performed in Royal Roads on May 2, 1975. More dye was used this time: 2 Kg. giving an initial concentration

of 1.89 g/L. The concentration used in Saanich Inlet was too low, and made finding the dye difficult after two or three hours. SEA LION was used to lay the dye as RICHARDSON was not available. The first ten transects had to to be made without radar tracking, by visual navigation on board SEATECH I. Radar tracking started after SEA LION tied up at a set of naval buoys.

The initial patch was 2 Km long. A total of twenty-six horizontal transects and ten vertical profiles were taken. The last eight horizontal transects were done by SEATECH II as the sea had become too rough for the smaller SEATECH I to operate. This increased the interval between transects considerably, as one boat had to perform both the vertical and horizontal profiling. The dye patch was followed for eight hours before it was finally lost.

Oceanographic conditions were measured by bottle stations before and after the experiment, and a total of five BT casts taken during the experiment.

4. DATA AND DATA ANALYSIS

Turbulent diffusion is a random process. No two dye patches behave in the same manner, even under apparently identical environmental conditions. As it diffuses, the patch may assume highly irregular shapes and concentration profiles. It is therefore necessary to select some parameters from the measurements which can be used to characterize the diffusion and may be compared to theory and previous results.

The horizontal extent of the patch is best characterized by the spatial variance of the concentration field, defined by the quantity

$$\sigma_{ij}^2 = \frac{\int x_i x_j \, C(\underset{\sim}{x},t) \, d\underset{\sim}{x}}{\int C(\underset{\sim}{x},t) \, d\underset{\sim}{x}}$$

where σ_{ij}^2 are elements of the dispersion tensor (Csanady, 1971).

The variance thus described is one of the more stable parameters associated with the patch; more so than the maximum concentration since it is relatively unaffected by decay or absorption of the dye while the diffusion process is going on. If x_1 is the coordinate along the long axis of the patch, and x_2 is the coordinate (locally) perpendicular to this (referred to the center of mass), then σ_{22} gives an estimate of the patch width for any given transect. The other quantities of interest are C_{max}, the maximum concentration observed on each transect, and $\overline{C}$, which is a mean concentration defined by

$$\overline{C} = \frac{1}{L} \int C \, dx_2$$

where L is the width of the patch at that transect, defined by the limits of observable dye concentrations.

The patch was initially long and narrow, as it had been laid in the wake of the ship. It was therefore apparent that lateral diffusion would be more important than that parallel to the long axis of the patch (slender plume assumption), (Csanady, 1971). We decided to concentrate on the lateral expansion of the patch, since the radar plots showed that this was indeed the direction in which most of the growth took place.

The horizontal profiles were treated as follows: using the radar plots to convert the horizontal axis on the chart output to distance, and the fluorometer calibration curves to convert the vertical axis to concentration, the profiles were digitized on a Hewlett-Packard 9821 digitizer and calculator. Each profile then being stored as a series of points, the required parameters were calculated.

The center of mass, integrated and average concentrations were found for each transect. If $\bar{x}$ is the center of mass, C_I the integrated

concentration and $\bar{C}$ the average concentration, then

$$C_I = \int_{x_1}^{x_2} C \, dx \quad , \tag{4.3}$$

$$\bar{C} = C_I / (|x_1 - x_2|) \quad , \tag{4.4}$$

$$\bar{x} = \frac{1}{C_I} \int_{x_1}^{x_2} xC \, dx \quad . \tag{4.5}$$

x_1 and x_2 are the edges of the transect, defined as the point where the dye concentration drops below the background level. The standard deviation was computed on a second pass through the data, using

$$\sigma_x = \left[\frac{1}{C_I} \int_{x_1}^{x_2} (x-\bar{x})^2 \, C \, dx \right]^{\frac{1}{2}} \quad . \tag{4.6}$$

The integrations were performed using the trapezoidal rule; between two consecutive points a and b the contribution to the integral was estimated as

$$\Delta I = \frac{1}{2} (b-a)[\, f(a) + f(b)] \tag{4.7}$$

These contributions were then summed across the transect to give the entire integral. The function f(x) took on the forms C, xC or $(x - \bar{x})^2 C$ depending on whether integrated concentration, center of mass or variance was being computed. The results of these computations are shown in Figures 1 to 6, giving C_{max}, $\bar{C}$ and σ_x as a function of time for both the Saanich and Juan de Fuca experiments.

Okubo (1971) uses an alternate method proposed by Joseph and Sendner (1958) to parametize the patch size. This method involves first contouring the dye patch, measuring the area enclosed by an iso-concentration curve and then defining an equivalent radius r_e of a circle of equal area. One then calculates the variance on the basis of this equivalent circular distribution, defining the variance σ_r^2 by

$$\sigma_r^2 \equiv \int_0^\infty r_e^2 C\, 2\pi r_e\, dr_e \Big/ \int_0^\infty C\, 2\pi r_e\, dr_e \qquad (4.8)$$

This method was not used for two reasons. The first was that the number of transects made was not sufficient to contour the dye patch without a great deal of guesswork, especially in the later stages. The second was that this method is really designed for patches which, however irregular they may be, are not significantly larger in one dimension than the other. It did not seem appropriate to use this type of data reduction on a patch which was, at least initially, long and narrow. It seemed better to measure the effective patch width, as the length did not grow very fast.

The vertical measurements were treated in a similar fashion. The depth of the center of mass of the vertical dye distribution was taken as a convenient scale depth. This is shown in Figure 7 and Figure 8 for both days. The maximum depth of penetration of dye was plotted for each station as well as the depth at which the peak concentration of dye was found. These results, plotted against time, are shown in Figures 9 and 10.

Visual examination of these plots results in a first impression of a great deal of scatter, especially in the Saanich results. However, it is possible to fit the points with some empirical relationships which will later be compared with some theoretical predictions.

Fitting a straight line by eye leads to the following results:

Juan de Fuca:

$$\sigma_x = 1.07 t^{0.913} \text{ cm} \qquad (4.9)$$

$$\bar{C} = 4.07 \times 10^4 t^{-3.15} \text{ g/L} \qquad (4.10)$$

$$C_{max} = 3.7 \times 10^3 t^{-2.78} \text{ g/L} \qquad (4.11)$$

Saanich

$$\sigma_x = 30.2 t^{0.498} \text{ cm} \qquad (4.12)$$

$$\bar{C} = 1.44 \times 10^{-2} t^{-1.8} \text{ g/L} \qquad (4.13)$$

$$C_{max} = 3.6 \times 10^{-4} t^{-1.03} \text{ g/L} \qquad (4.14)$$

where t is in seconds. These formulae apply only if $t > 600$ sec, since only after this point is the data appropriate for such calculations.

The average initial dilution provided by the wake mixing was calculated using the average concentration from the first transect and the initial concentration measured using the tank sample to define a dilution factor

$$D = C_{initial}/\overline{C} \qquad (4.15)$$

For Saanich, D was 7.8×10^4 and for Juan de Fuca, D was 1.89×10^5. There is some unreliability in these, as the value of $\overline{C}$ depends upon where the transect was taken. An estimate for an average D could be useful, however, and a good value is 10^5. Note that this is not the dilution in the wake, but that which has occurred after about 10 minutes of mixing. The initial dilution into the wake is more likely to be of order 10^2.

The most important feature of the oceanographic environment was the stability of the water column near the surface where the diffusion took place. The density structure was determined by standard oceanographic bottle casts before and after the diffusion experiment on both days. In order to check for variations in the vertical structure, BT casts were performed on alternate vertical stations. Density profiles are shown for Saanich Inlet in Figure 11 and for Juan de Fuca in Figure 12. (Note that the scales of these two figures are quite different.) BT casts (samples shown in Figure 13) showed no great variation over the period of the experiment in either case. Saanich Inlet, as expected, is much more highly stratified than Juan de Fuca.

Buoyancy periods (Equation 2.8) were estimated using a finite difference approximation to the density derivative for both cases. In the Saanich profile there is an essentially uniform gradient over the top five metres, which gives a value for T of 4.61 min. Juan de Fuca exhibits weaker stratification, the value over the top fifteen metres being about 18.5 min. Note that the buoyancy period is proportional to $(\partial\rho/\partial z)^{-\frac{1}{2}}$. Thus in spite of the very large difference in density gradient between the two locations, the buoyancy periods differ by only a factor of four. This has important implications for the depth to which the turbulent wake initially mixes the effluent.

5. RESULTS

Values for K may be computed from Figure 3 for the Saanich experiment and Figure 6 for the Juan de Fuca measurement. The lines shown in the graphs which are fitted by eye are

$$\sigma_x = 30.2t^{\frac{1}{2}} \text{ cm} \tag{5.1}$$

for Saanich, and

$$\sigma_x = 1.07t^{0.913} \text{ cm} \tag{5.2}$$

for Juan de Fuca, where t is in seconds. Using (2.24) these expressions for σ_x can be used to compute a value of K for each case:

Saanich: $K = 4.56 \times 10^2 \text{ cm}^2 \text{ sec}^{-1}$.

Juan de Fuca $K = 1.05t^{0.83} \text{ cm}^2 \text{ sec}^{-1}$.

Figure 1 and Figure 4 show the maximum concentration as a function of time for Saanich and Juan de Fuca respectively. The best straight line fits by eye to the log-log plots are:

Saanich: $C_{max} = 3.6 \times 10^{-4}t^{-1.03}$ (5.3)

Juan de Fuca: $C_{max} = 3.7 \times 10^{3}t^{-2.78}$ (5.4)

with concentrations in g/L and t in seconds. Figure 2 and Figure 5 show the average concentration per transect for Saanich and Juan de Fuca respectively. The best fitting lines (using the same units as above) are:

Saanich: $\overline{C} = 1.44 \times 10^{-2}t^{-1.8}$ (5.5)

Juan de Fuca $\overline{C} = 4.07 \times 10^{4}t^{-3.15}$ (5.6)

These results allow some comparison with the various theoretical predictions. The first question to be considered is that of wake effects.

During the Saanich experiment the value of the buoyancy period T in the upper five metres was 2.53 min., which gives a wake collapse time of about 45 seconds. In Juan de Fuca T was eighteen minutes, with a corresponding collapse time of six minutes. In both experiments, the wake must have collapsed before the first transect of the dye plume could be made. No effects from the period before or during the wake collapse should be visible. The vertical extent of the dye would therefore have been essentially constant at the asymptotic values for the vertical wake extent, under the assumption that the dye is confined to the wake. In Saanich Inlet this asymptotic depth based on Equation 2.11 was 7.5 metres; in Juan de Fuca it was 11.64 metres. These calculations are based on a completely submerged vessel. Be-

cause of the proximity of the surface it is reasonable to expect that these are upper limits for the asymptotic vertical thickness of the wake, and that the actual vertical extent may have been significantly less.

According to Equation 2.7, with a vessel speed of ten knots (5.15 m/sec) and with an initial wake diameter D of four metres, the velocity fluctuations in the wake, u', will drop to a mean level of 1 cm/sec in twelve minutes, and 0.5 cm/sec in thirty minutes. Although it is very difficult to guess what the ambient level of turbulent velocities might have been in the water during the experiment, it is probable that the wake turbulence would have decayed below the ambient level in fifteen to thirty minutes.

Figure 9 and Figure 10 show the maximum depth of dye penetration as a function of time for Saanich and Juan de Fuca, respectively. Inspection of the graphs shows that this depth averaged about 6 metres ±1.15 m in Saanich, and 7 metres ±1.5 m in Juan de Fuca. There is a good deal of scatter in these points, but the depth seems to be essentially constant. Part of the scatter is probably due to the profiling boat drifting relative to the dye patch while making its soundings. It thus appears that for the two experiments described in this paper, the asymptotic vertical thickness of the wake for a surface vessel is about 0.7 times the value derived in Equation (2.11). This should be kept in mind when making practical calculations employing Merritt's (1972) result.

Equation 2.13 predicts, after vertical collapse, that the wake should expand horizontally in proportion to $t^{\frac{1}{4}}$, until the wake turbulence intensity declines below the ambient oceanic level. The results 5.1 and 5.2 show that the patch width (defined as σ_x) expands, in both cases, much more quickly than $t^{\frac{1}{4}}$; moreover, in Juan de Fuca at least, inspection of Figure 6 will show no area where a $t^{\frac{1}{4}}$ curve could reasonably be fitted. The amount of scatter in the Saanich points makes it more difficult to state definitely whether this is possible or not, but inspection of Figure 3 showed that it is unlikely to be true.

It is also unlikely that the wake turbulence persisted above the ambient level for more than thirty minutes. It should be kept in mind that these formulae for the rate of wake expansion were derived for wakes produced in non-turbulent fluid. The existence of the ambient oceanic turbulence, especially at the scales on the order of the size of the wake may significantly accelerate the wake expansion.

The effects of the ship's wake seem on the basis of these experiments to be confined to the early history of the diffusing patch. The wake provides initial mixing and dilution, and gives the patch its initial shape and vertical extent, but does not later affect the diffusion to any significant extent. Almost all vertical mixing is done by the ship during discharge, the dye being mixed throughout the wake and not penetrating beyond to any discernable extent throughout the time of measurement. The stability of the water column determines the depth to which the wake will mix initially, but appears to have little other effect. The degree of vertical mixing by the oceanic turbulence was not appreciable.

In Saanich Inlet, the horizontal diffusion appears to be best described by the long diffusion time case described by Csanady (1971). In this case, we have a constant eddy coefficient of 4.6×10^2 cm^2 sec^{-1}, significantly lower than usual ocean values of 10^3 to 5×10^3 (Grosch, 1972). The Juan de Fuca experiment comes close to Csanady's (1971) short diffusion time case, which predicts apparent diffusivity varying linearly with time:

$$K = 1.05\ t^{0.83}\ \text{cm}^2\ \text{sec}^{-1}\ .$$

Although the exponent here is somewhat less than 1, it is close, and considering the degree of scatter in the data, can probably be taken as representative of the short time case. There does not appear to be any evidence of a region where inertial-subrange diffusion might hold.

Okubo (1971) has written a review paper in which he has collected data from recent diffusion experiments and used them to derive some empirical relations which may be used to predict the behaviour of diffusing dye patches.

The size of the dye patches in those experiments using Okubo's variance calculation as given in Equation 4.8 is best fitted by the function

$$\sigma^2 = 0.0108\ t^{2.34} \qquad (5.8)$$

with σ in cm and t in seconds. However, these were all performed in the open ocean, not in semi-enclosed coastal waters; this may account for the slightly higher growth rate than the one observed here in Juan de Fuca Strait. There is sufficient scatter in these plots however, that the Saanich and Juan de Fuca points do lie within the cluster of Okubo's points.

Turbulence is not the only factor which plays a role in oceanic diffusion. Current shear, both horizontal and vertical may also have a significant effect. Pritchard, Okubo and Carpenter (1966) found evidence that vertical current shear produced a significant elongation and skewing of the patch with depth, and a somewhat increased rate of decay of peak concentrations. Okubo and Karweit (1969) constructed a model on the basis of the classical diffusion equation superimposed upon a uniform shear flow. This model showed that the concentration profile should be skewed toward the region of lower current velocity. Experiments in Lake Huron by Murthy and Csanady (1970) found profiles similar to those predicted by the model of Okubo and Karweit.

Shear was not measured in the experiments described here and might reasonably be expected to be relatively unimportant. However, there will be many coastal situations, e.g. estuaries, where current shear will dominate and the resultant skewing of the dye patch must certainly be considered.

The other main factors which may affect the rate of diffusion are wind and water column stability. Foxworthy, Tibby and Barsom (1966) found that high wind speeds and low water column stability led to enhanced and significant vertical diffusion. They state that there may be some

increase in horizontal diffusion with decreasing stability, but there is not sufficient data to be sure.

The experiments done here showed no large effect on vertical mixing arising from water column stability; vertical diffusion is controlled by the ship's wake. There was a much higher rate of horizontal diffusion in Juan de Fuca than in Saanich Inlet. In the Juan de Fuca experiment, there was wind (5-10 knots) and a less stratified water column. It seems more likely, however, that the increased rate of horizontal mixing was due to the higher ambient turbulence level in Juan de Fuca Strait. The calculations of the vertical extent of the wake (Equation 2.11) are based on a buoyancy period that is independent of depth. This is equivalent to a linear density profile. Although the Saanich profile (Fig. 11) is reasonably linear over the top 8 metres, the structure in Juan de Fuca (Fig. 12) is more complicated. The theory gives us little help in interpreting the influence of such a profile, although it is perhaps reasonable to assume that dye penetrating below the surface stratification would be distributed throughout the well-mixed layer between 3 and 7 metres.

It is interesting to note that the Juan de Fuca values of σ_x (Fig. 6) fit a straight line quite well, whereas the Saanich Inlet data (Fig. 3) as mentioned above, are extremely variable. Although we have approximated the Saanich data by a line that represents a constant value of K there is not a strong justification for this. To some extent this scatter can be attributed to low dye concentrations, which made the patch hard to follow. Nevertheless, we shall keep to our chosen $\sigma_x(t)$ relationship in what follows since it provides a useful contrast to the Juan de Fuca case. There is no doubt that further work is warranted in quiet and enclosed waters such as Saanich Inlet before any serious calculations are made.

6. SUMMARY AND CONCLUSIONS

Vertical mixing is provided chiefly by the action of the ship's wake. It is only weakly dependent on water column stability. Equation (2.11) defines the asymptotic vertical extent of the wake which is the same as the vertical thickness of the final diffusing patch. We may rewrite the expression so that, allowing for a 0.7 reduction due to surface effects,

$$h_f = 0.23 V^{\frac{1}{4}} D^{3/4} \left(-\frac{\partial \rho}{\partial z}\right)^{-1/8} \text{ cm.} \qquad (6.1)$$

V is the ship velocity (cm/sec) and D may be taken as the ship draught (cm). Note the very weak dependence of h_f on the density stratification, which is consistent with the results observed in these experiments. It will be recalled that the dye patch thickness in Saanich was only 0.86 of the thickness in Juan de Fuca, whereas the density gradient was 16 times greater in Saanich.

In Saanich Inlet, which represents a quiet and enclosed region, the diffusion process may be described after discharge by the classical diffusion equation, using a constant eddy coefficient of 5×10^2 cm^2 sec^{-1}. The expansion of the dye patch is described by (2.17) and the decay of the concentration by (2.15). This process corresponds to Csanady's (1971) long diffusion time, where the patch size is of the order of the larger turbulence scales.

In the more active waters of Juan de Fuca Strait, the diffusion may be described after discharge (allowing for an initial finite patch size) by an eddy coefficient which varies with time:

$$K = 1.05\ t^{0.83} \text{ cm}^2 \text{ sec}^{-1} \ .$$

This is very close to Csanady's (1971) short diffusion time case, where the patch is small compared to the main energy-containing eddies, and thus velocity fluctuations are still correlated.

Although this time dependence of K makes the equation nonlinear we may transform back to the familiar diffusion equation. Let the diffusion coefficient be

$$K = \gamma t^z \qquad (6.2)$$

where z is not necessarily an integer but γ is a constant; then the substitution $\tau = t^{z+1}$ transforms the equation (2.23) into

$$\frac{\partial C}{\partial \tau} = (z+1)\gamma \frac{\partial^2 C}{\partial x^2} = K' \frac{\partial^2 C}{\partial x^2} \qquad (6.3)$$

Having solved the diffusion equation (6.4), the required result may be obtained by substituting t^{z+1} for τ. The correct solution to the equation is given by (2.15), which describes diffusion from a line source of finite width. For practical purposes, one may use the result for a true line source of infinitesimal width; the formulae are easier to handle, and the error is negligible if the initial plume width is very much less than the length. The solution for such a source is given by Carslaw and Jaeger (1959):

$$C = .5Q(\pi K'\tau)^{-\frac{1}{2}} \exp(-x^2/4K'\tau). \qquad (6.4)$$

The corresponding result for a point source is

$$C = Q(4\pi K'\tau)^{-1}\exp[-(x^2+ y^2)/4K'\tau]. \qquad (6.5)$$

These theoretical results can be combined with the results from the experiments done here to make predictions about the behaviour of a dye patch.

Before predictions can be made about the patch behaviour, the quantity Q must be defined. Q is clearly not the original concentration of effluent in the ship's tanks, which we shall call Q_T. The relations (6.4) and (6.5) apply only after the effluent has undergone initial mixing into the wake. If the initial distribution is assumed to be mixed down to the depth h_f (from Equation 6.1) and we consider a plume of unit width (1 cm) then the quantity Q is defined

$$Q = \frac{RQ_T}{Vh_f} \qquad (6.6)$$

where V is the ship speed in cm. sec^{-1} and R is the volume rate of effluent discharge in cm^3 sec^{-1}. Of course this is a somewhat arbitrary way of defining the initial plume but it serves the necessary purpose of correctly relating the parameters Q_T, V, h_f and R in the results that follow.

For practical applications we need to determine appropriate positions and times for specific concentration levels. Assuming a line source, we define the contour of some given concentration C. Then, using (6.4)

$$\ell n\ (C/Q) = -\frac{1}{2}\ \ell n\ 4\pi K'\tau - x^2/4K'\tau$$

which may be solved for x to obtain

$$x = 4K't(z+1)/2\ [\ \ell n(Q/C) - \tfrac{1}{2}\ell n\ 4\pi K' - (z+1)/2\ \ell nt]^{\frac{1}{2}} \qquad (6.7)$$

where τ has been replaced by t^{z+1}. This equation may be used to compute the distance from the plume axis reached by a given concentration contour C. Note that initially x will increase as the patch grows but will subsequently decrease. The decrease in average concentration will mean that the contour corresponding to C will move back toward the axis and finally disappear when the axis concentration decreases below C. There is therefore a maximum distance to which any concentration level C will travel, which is given by the solution of $dx/dt = 0$, with x described by (6.7). This equation is transcendental, and has to be solved either numerically or graphically. Consider the following simple example which corresponds to the Saanich Inlet results. Let $K' = 5 \times 10^2$ cm^2 sec^{-1}, and assume[1] that C/Q is 10^{-4}. Then one may plot x as a function of t and find three important quantities: x_{max}, t_{max}, and the time t_s at which the concentration C disappears from the patch entirely. This may also be found by setting $x = 0$ in (6.4) and solving for t, so that

$$t_s = \left[\frac{Q^2}{4\pi\gamma' C^2}\right]^{1/(z+1)} . \qquad (6.8)$$

In this example, t_s is 4.42 hours. The values of x_{max} and t_{max} may be found from Fig. 14 and are 1.08 Km and 6,000 seconds (1.7 hr.) These values t_s and x_{max} may be used as a scale time and a scale distance for practical application in determining required dilutions.

Some caution is necessary here. The results in (6.7) and (6.8) are valid only for line sources; if x_{max} is of order L_o or greater, where L_o is the length of the patch, then the problem is best treated as one of a point source. The time of transition is found by substituting L_o for x in (6.7) and solving for t.

For the point source case (6.5) is applicable:

$$x = 4K't^{\frac{z+1}{2}}\left[\ell n(Q/C) - \ell n 4\pi K' - (z+1)\ell nt\right]^{\frac{1}{2}} \qquad (6.9)$$

and

$$t_s = \left[\frac{Q}{4\pi\gamma C}\right]^{1/(z+1)} . \qquad (6.10)$$

It will be necessary to adjust the time after the transition as follows. If t_1 is the time taken for the original line patch to reach a size L_o, and if t_2 is the time required for a point source of strength Q to diffuse to a patch of radius L_o, then a time t' resulting from (6.9) or (6.10) must be corrected to

$$t = t' + (t_1 - t_2) . \qquad (6.11)$$

1. The assumed dilution rate from the tank concentration Q_t would then be about 10^6. This would be the order of dilution required for recreational purposes in the case of the Saanich experiment.

There may be cases where x_{max} never reaches the value L_o. In these cases, the line source equation may be used throughout.

These equations allow one to calculate how long concentrations greater than or equal to a given level C will persist, and how great an area they cover at any given time.

These results must be used with care and a full understanding of their limitations; several effects have not been included. These results deal only with the mean field. Random fluctuations have not been accounted for. If one is concerned, for example, with the accumulation of a toxin in a shellfish colony, then the mean concentration field contains sufficient information. But in the case of recreational waters, the magnitude of the fluctuations about the mean is just as important. Unfortunately, the theory of relative diffusion is not sufficiently developed to predict the magnitudes of these fluctuations. Csanady (1971) suggests that fluctuations of greater than 50% of the mean value can occur for over 10% of the time, even near the centre of the patch. Values may be much higher at the edges. The experiments described here do not contain sufficient data to analyze the level of fluctuations. Csanady (1971) discusses this aspect in more detail.

It has been assumed that the diffusing quantity is conservative. This may not be the case for many effluents. If the effluent is subject to decay or chemical reaction in seawater, the quantity Q must be modified by an appropriate factor, the form of which will depend on the individual situation. Current opinions on the decay of coliform bacteria in seawater range from very fast decay to virtually none at all. The best course under these circumstances is probably to assume no decay.

The effect of shorelines has not been taken into account. Both theory and experiment have assumed that no boundaries were close to the patch. The results given above should be applicable to small islands and perhaps the ends of exposed points. The effects of coastal boundaries are uncertain; this may prove a fruitful area for further experiments.

The scale times and distances found here are strongly dependent upon Q. For a line source, the time t_s depends on $Q^2/(z+1)$, which results in a quadratic dependence for the case where K is constant (i.e. Saanich Inlet). Small changes in Q may therefore produce significant effects. Equation (6.6) shows that the determining factor is the ratio R/Vh_f. h_f is only weakly dependent on the ship's velocity V, so that it may be regarded as nearly fixed. It is important therefore to maintain a low discharge rate and a high ship speed in order to get the lowest value of Q.

Finally, advection has not been included. All results are in the frame of reference of the patch itself. The effects of advection should not be overlooked as they may, even with tidal effects, be associated with net circulation. Thus a concentrated patch some distance from shore may be advected close to shore, whereas a "weak" patch involving the same volume of discharge but spread over a greater distance, even close to shore may never be a problem.

The results derived here were for single discharges only. In areas of heavy traffic, where many boats may be discharging sewage close to each

other in time and space (for example, near a marina), it will be necessary to use these results additively.

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APPENDIX

Recommended procedure to follow when tackling practical problems of coastal pollution due to discharged ship effluent.

This report has brought together some of the theory, laboratory work and two practical field experiments connected with this general pollution problem. We have attempted to simplify the practical aspects by deriving formulae of fairly general application which are nevertheless quite simple to use. However, these formulae involve several parameters, a complication that is unavoidable if the theory and practical measurements are to be properly represented. In any real pollution situation these constants will have to be determined and the formulae correctly applied. Below we tabulate the recommended sequence of steps to be taken.

1. For the specific geographical area collect and carefully consider all available oceanographic data. Consider typical density stratification, winds, tidal currents, estuarine circulation and other forms of advection. These results are needed to properly interpret and apply the dispersion results.

2. Collect all available data and/or estimates of vessels discharging wastes. The special considerations include number and distribution of vessels at any time, draught, number of persons aboard, typical discharge rates, ship speeds, size of holding tanks, etc.

3. Run a dye diffusion experiment along the lines described in this report in order to obtain information on the type of dispersion process that occurs (in particular, to find K' (Equation (6.4)). This experiment will also provide important information on advection and could be used to learn more about the influence of coastal boundaries. It may well be advisable to conduct more than one dye diffusion experiment.

4. Take the statistical data and/or predictions on effluent discharge to provide an appropriate source condition for the diffusing effluent. If advection is relevant, the source will of course be moving relative to the coast. Using the appropriate transformations and equations given in this report, calculate the relevant values of x_{max} (Equations 6.7 or 6.9) for the required dilution contour. It may be appropriate to consider just the steady-state situation in which diffusion (and advection) just balances the discharge; however, if the mean value changes on a time scale long compared to t_s (Equation 6.8) then time dependence should also be taken into account. In many cases, it may be possible to obtain appropriate solutions from the standard text (Carslaw and Jaeger, 1959). A series of point sources enclosed by a circle may be approximated by a circular contour of steady diffusion, a case that has been discussed by Whitehead (1927). A number of situations involving advection may also be treated analytically. A particular example is a point source such as an anchored vessel or outfall in a uniform current. The relevant solution is given in Carslaw and Jaeger, § 10.7, Equation 3. For more complicated situations it may be necessary to use numerical methods.

The application of the results in this report should also be of use in considering ways of minimizing pollution nuisance from moving or anchored vessels. For this purpose reference should be made to Equation (6.6) which relates the initial discharge concentration to the velocity and discharge rate etc. For an anchored vessel V refers to the advection velocity. It is immediately apparent that the concentration varies linearly with the discharge rate, allowing practical formulation of regulations governing pump size, etc., for the discharge of effluent. Equation (6.6) should also be used with (6.1) which gives the dependence of the vertical extent of the discharged patch as a function of ship speed and draught.

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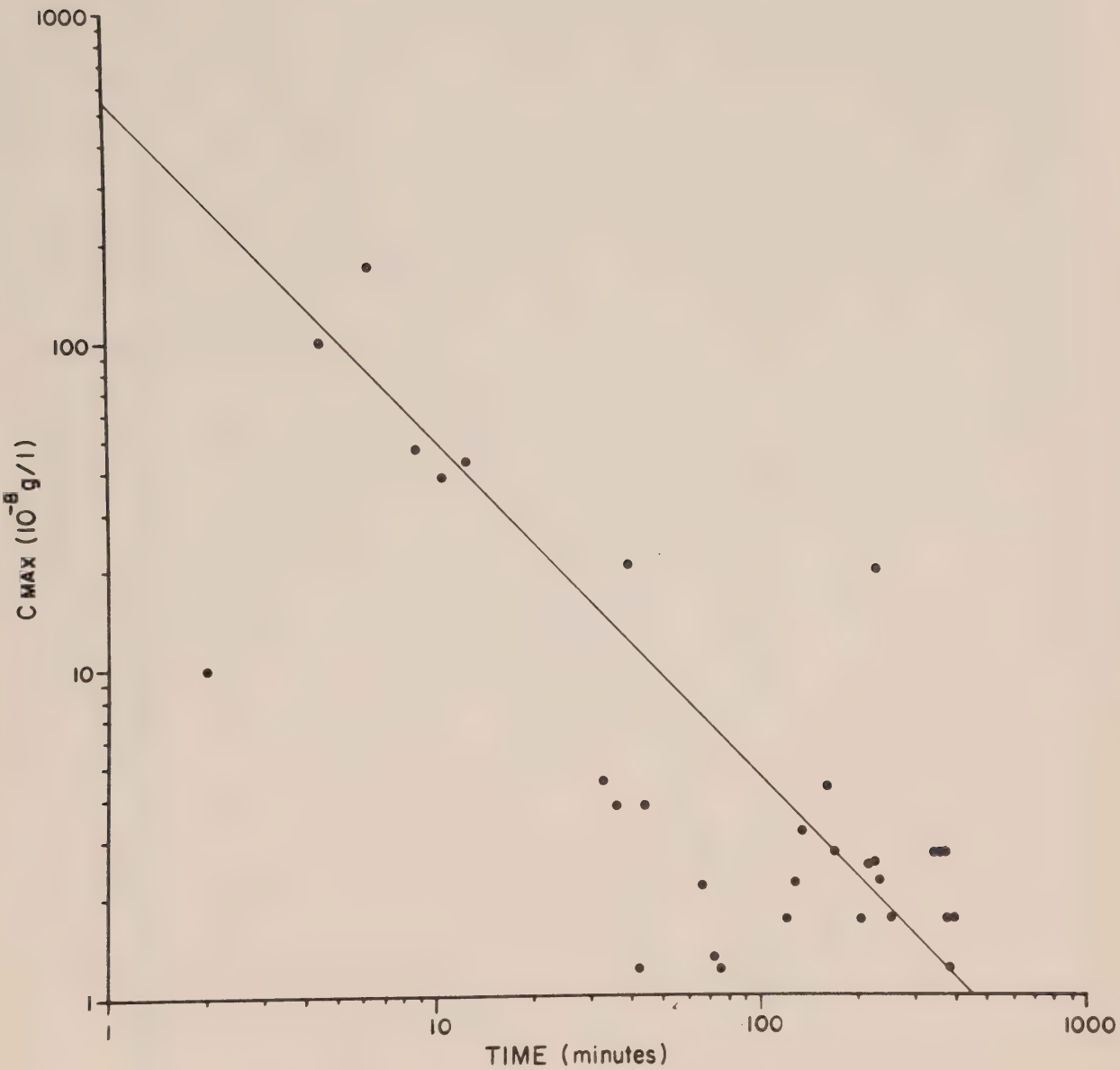


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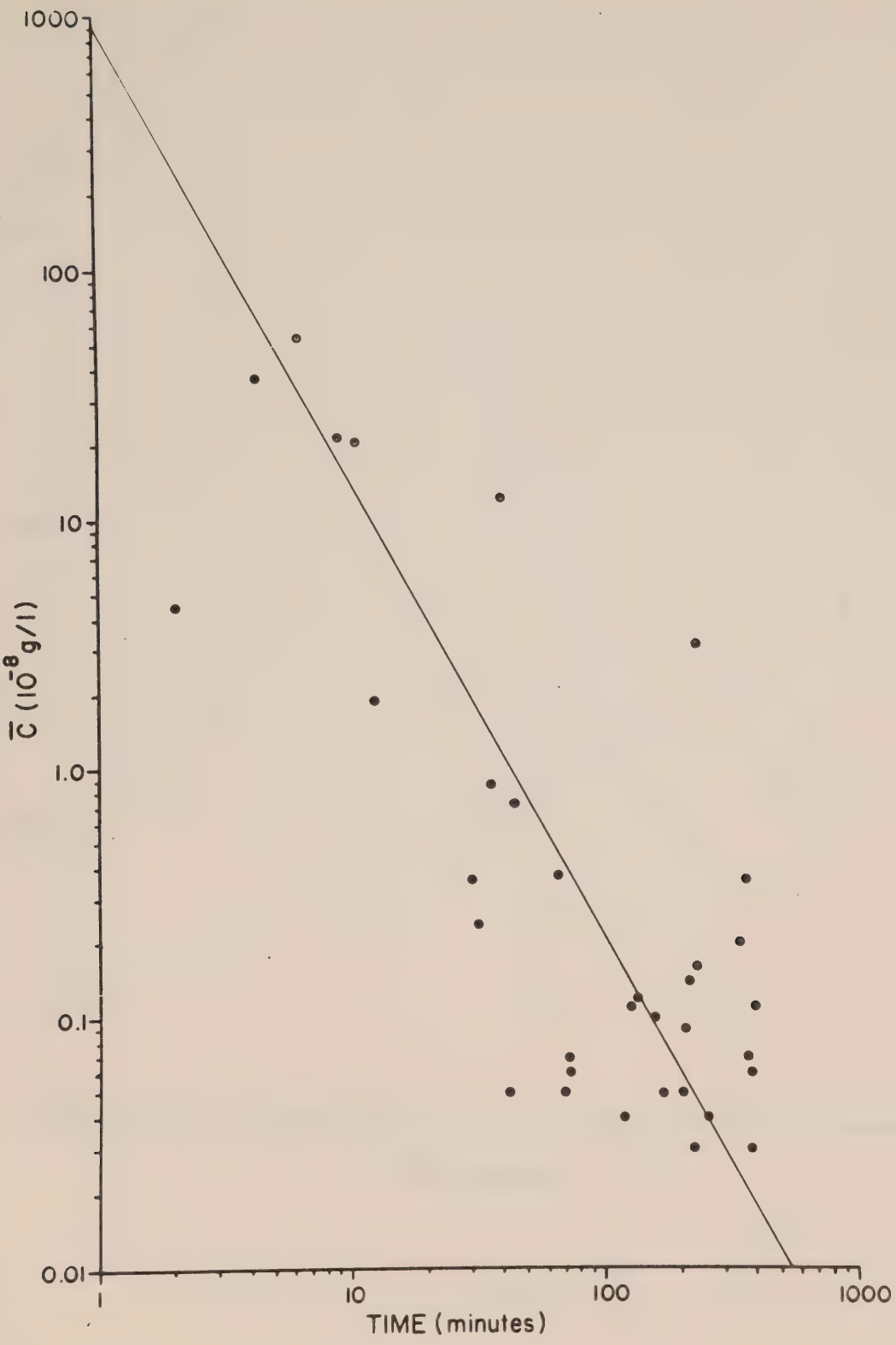


Figure 2. The average horizontal concentration as a function of time for the Saanich Inlet experiment.

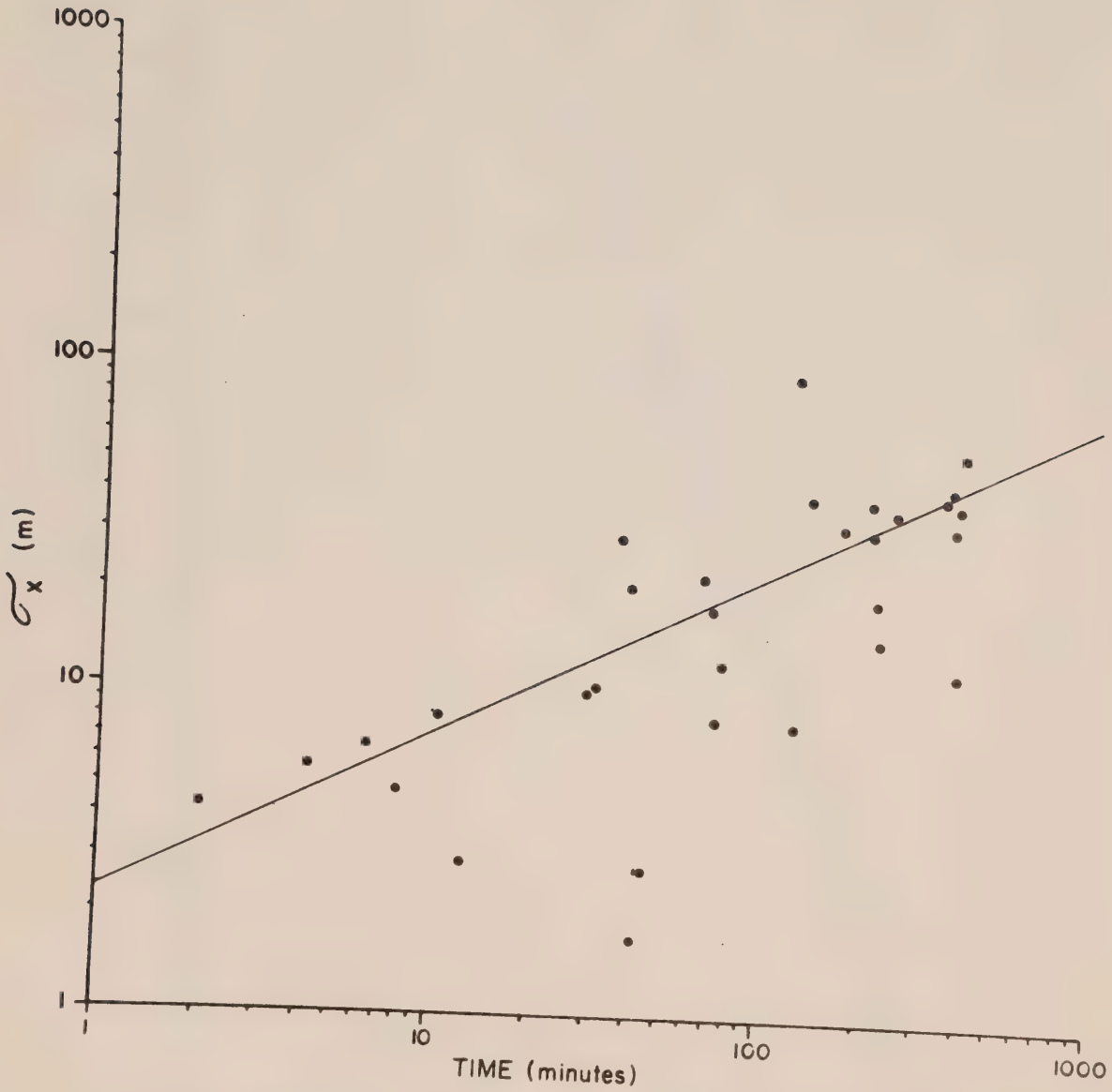


Figure 3. The transverse standard deviation of the patch vs. time for the Saanich Inlet experiment.

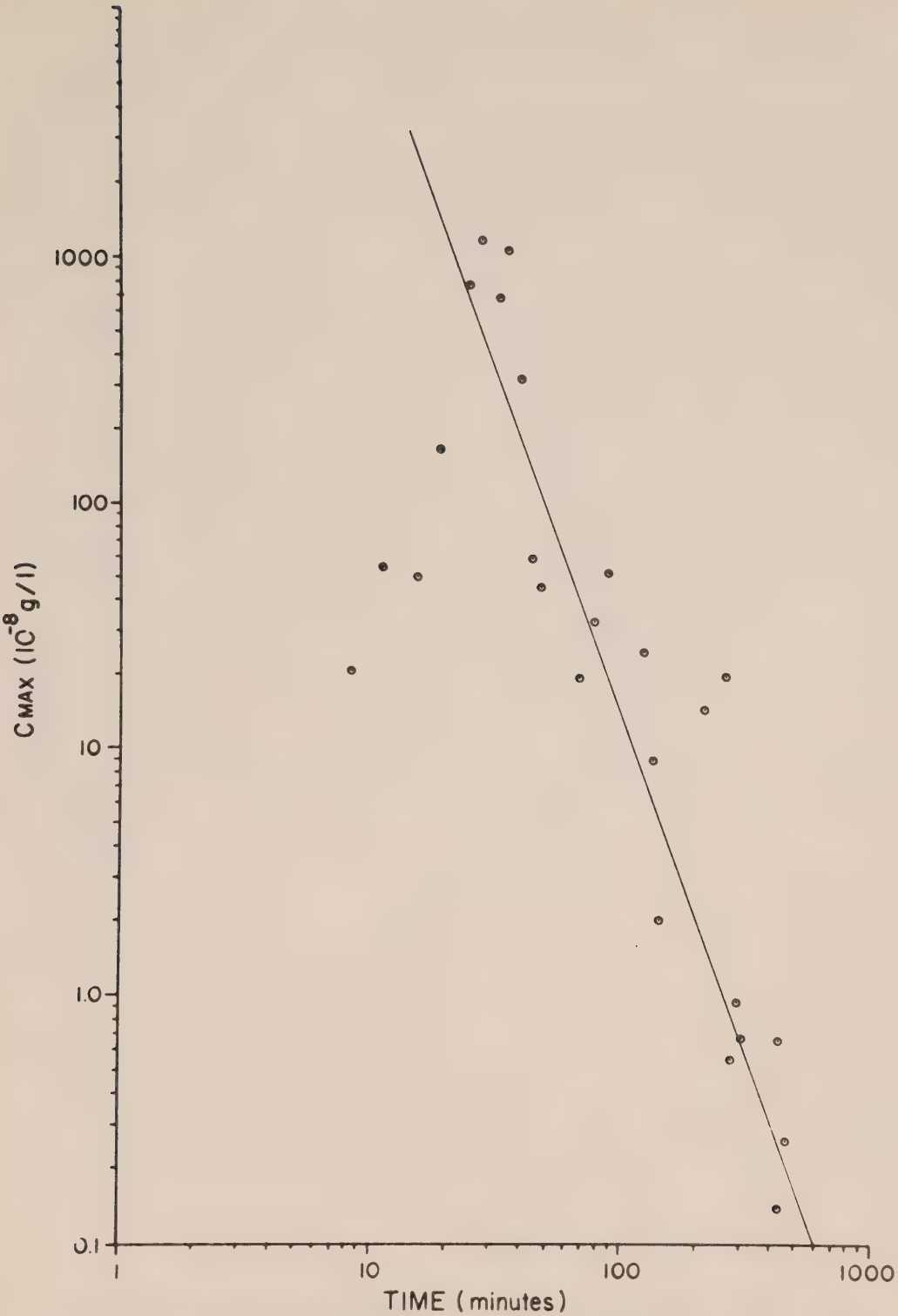


Figure 4. The maximum horizontal concentration as a function of time for th Juan de Fuca Strait experiment.

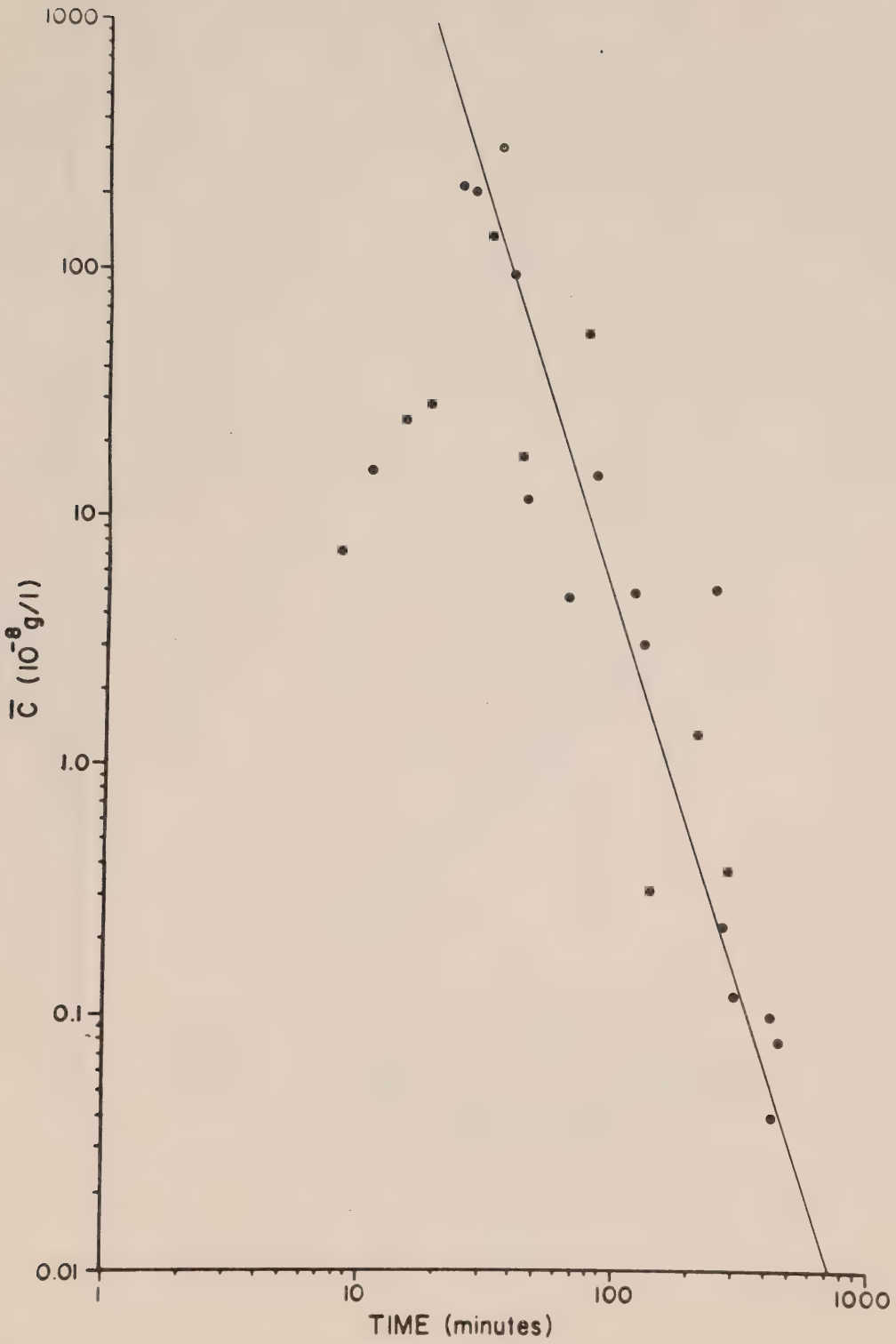


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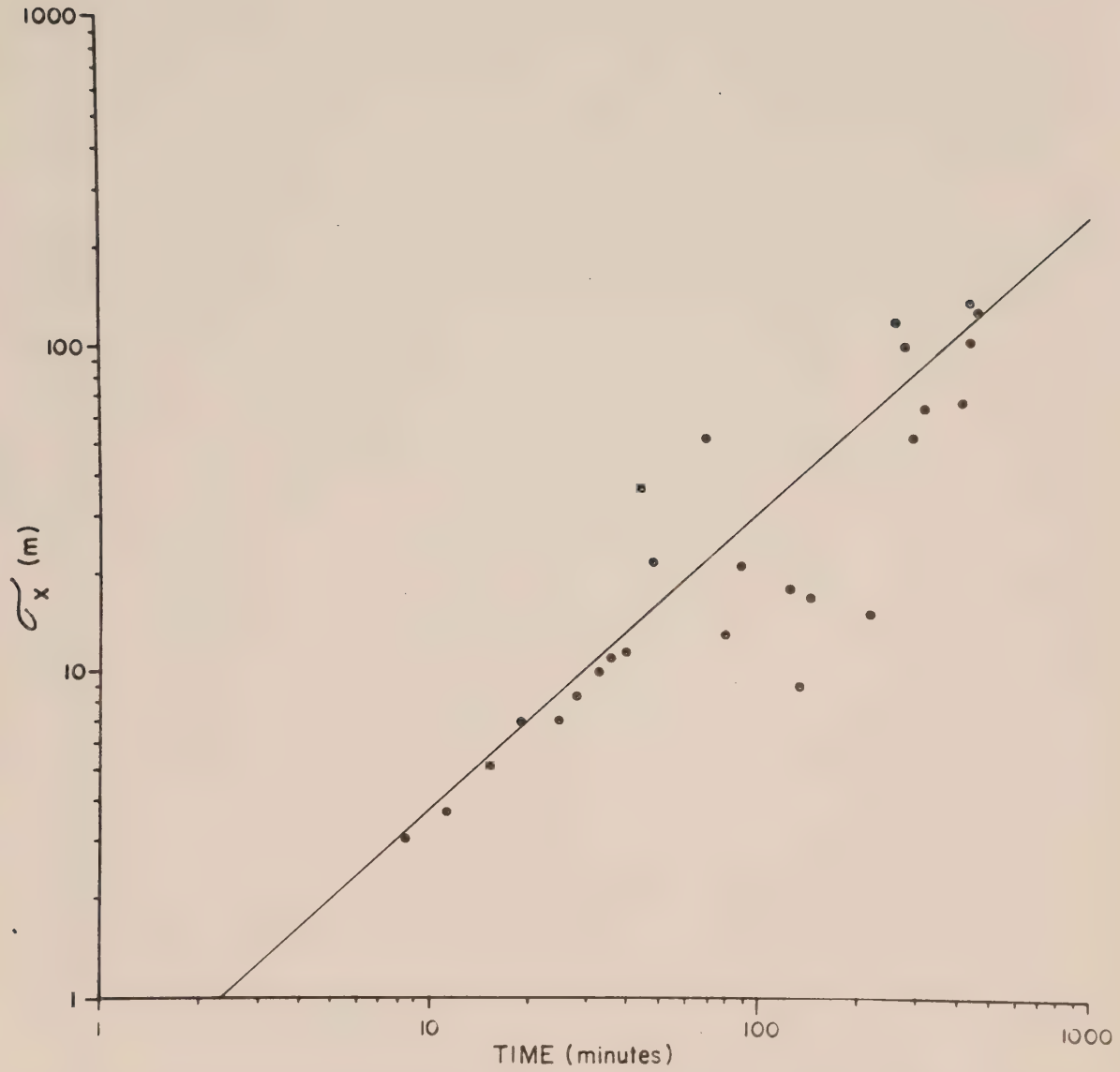


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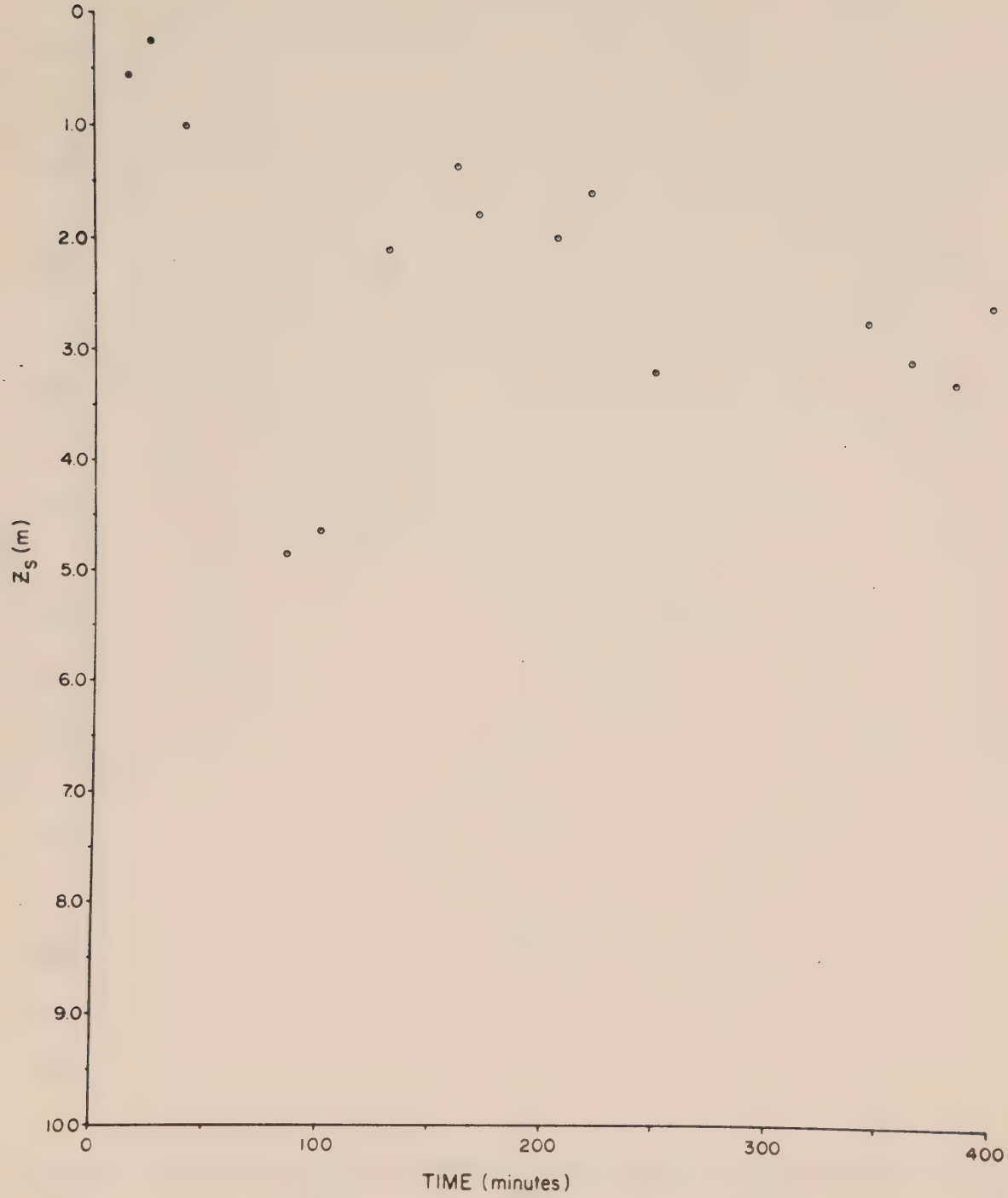


Figure 7. The scale depth of dye penetration vs. time for the Saanich Inlet experiment.

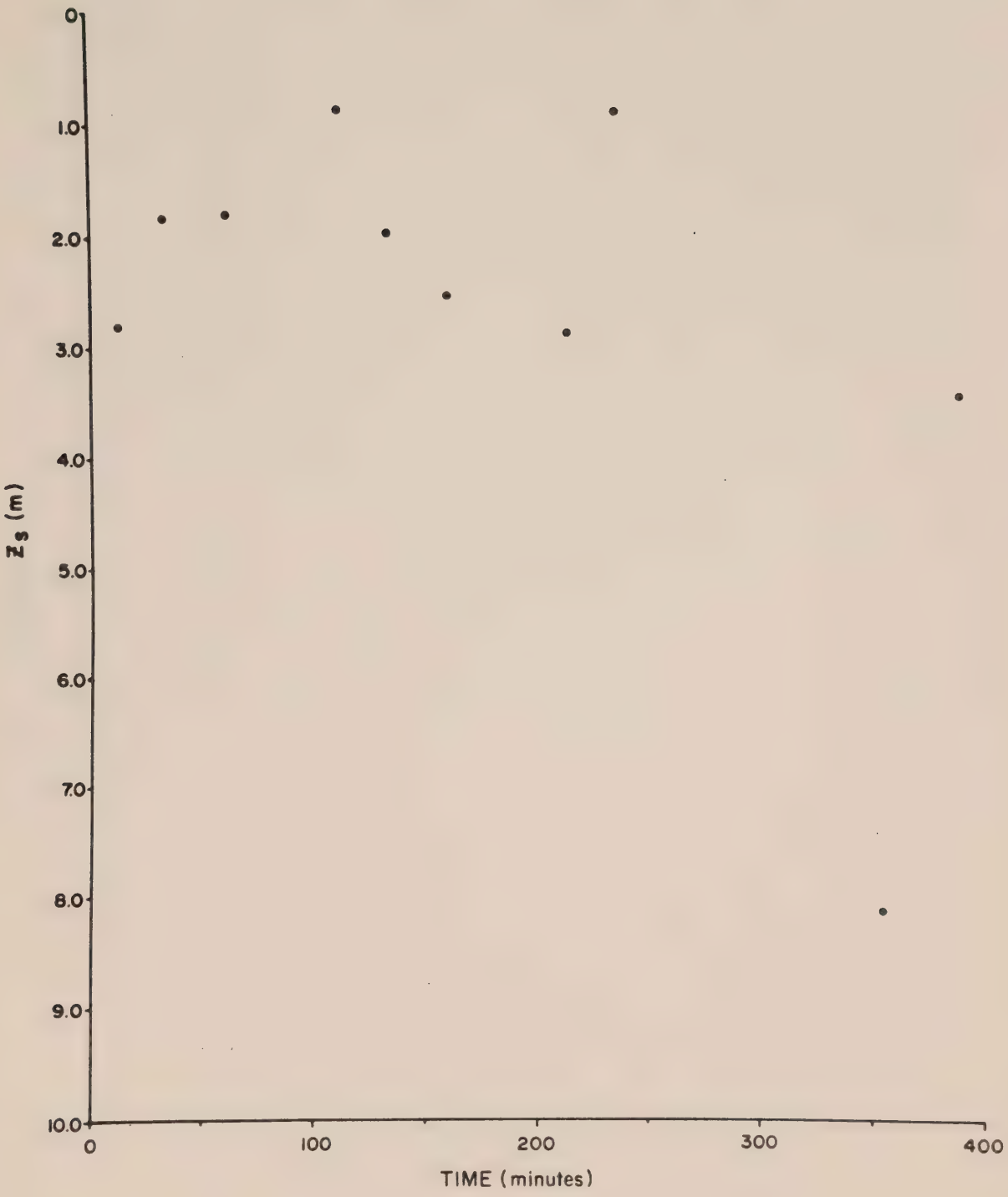


Figure 8. The scale depth of dye penetration vs. time for the Juan de Fuca Strait experiment.

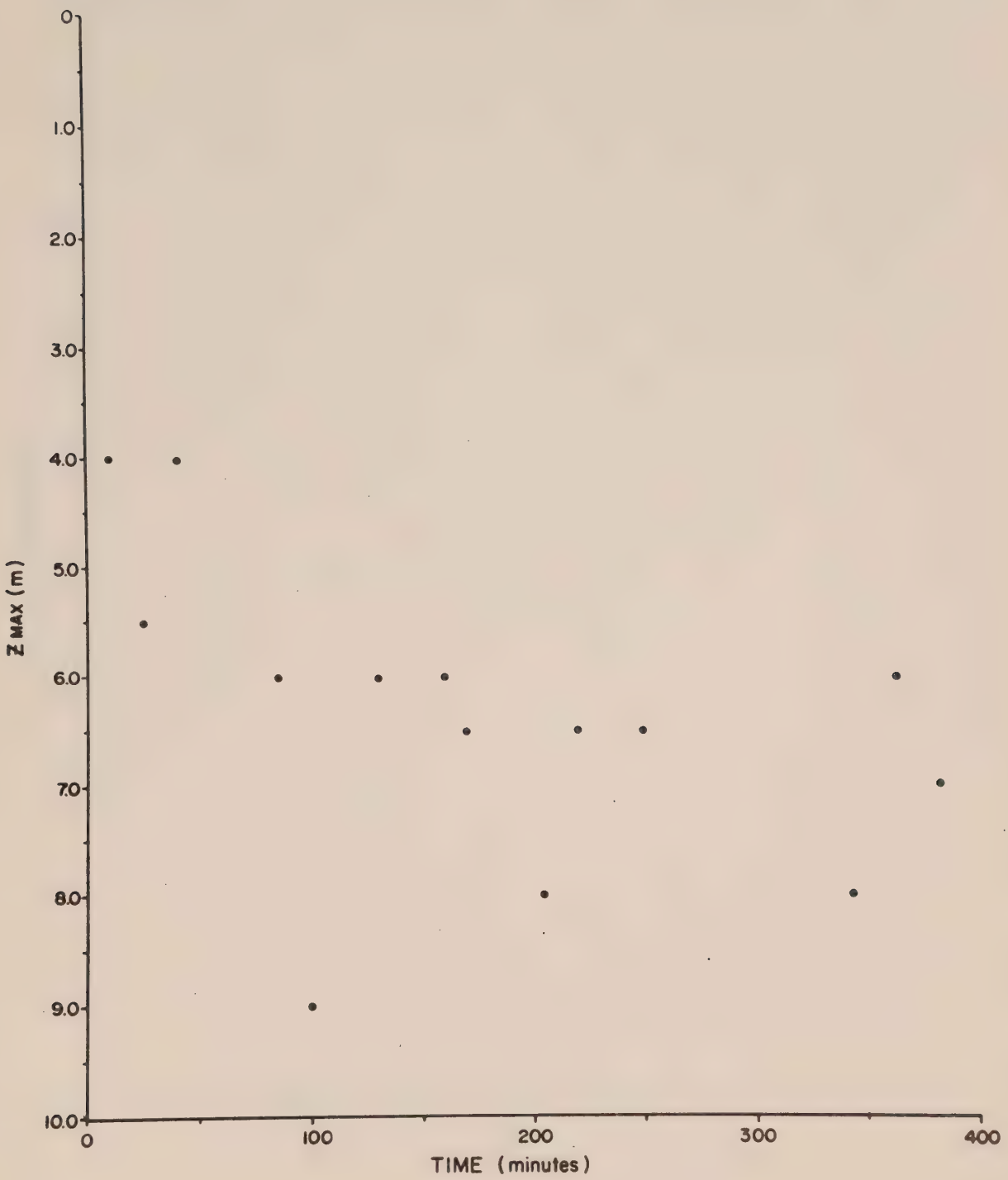


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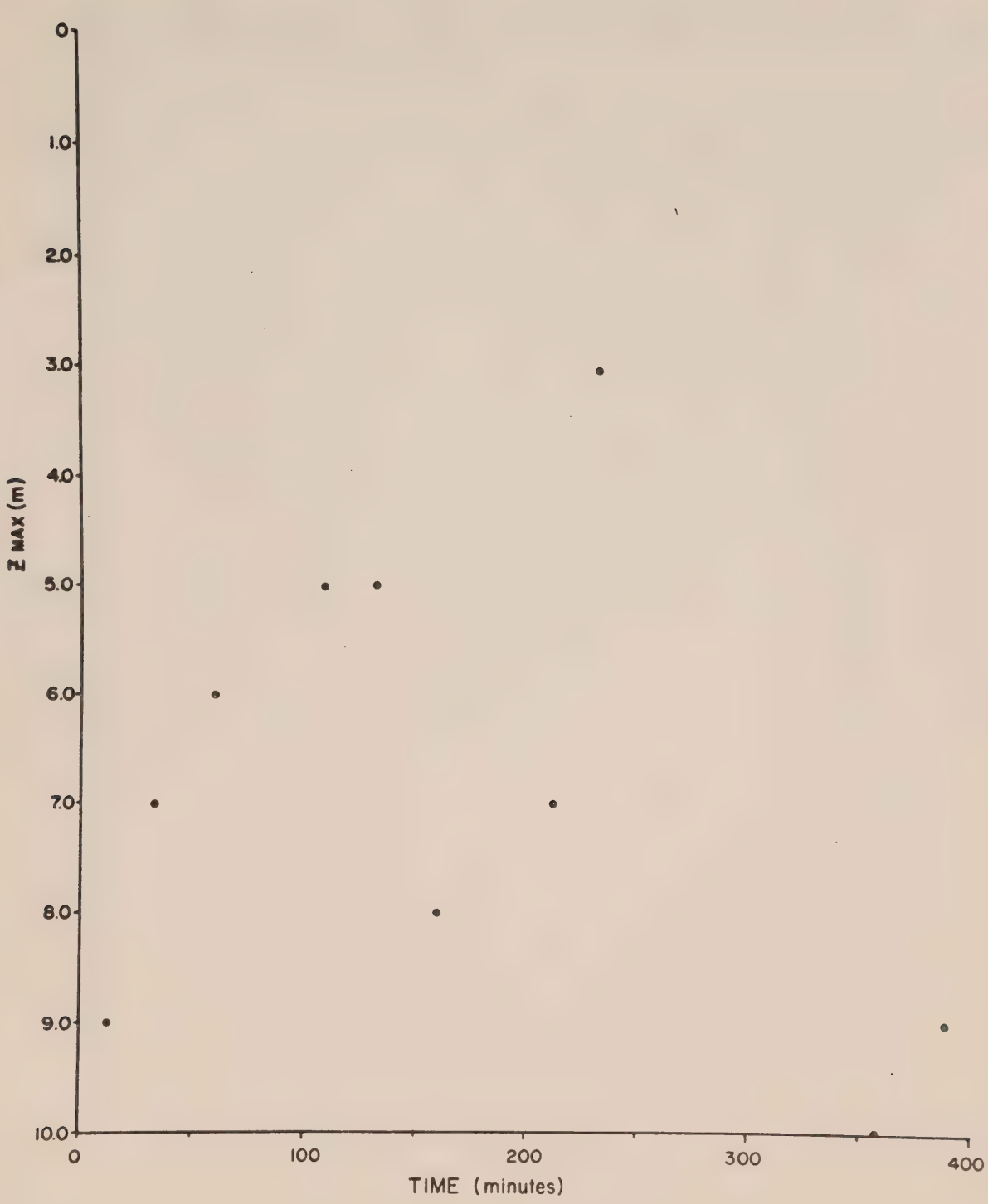


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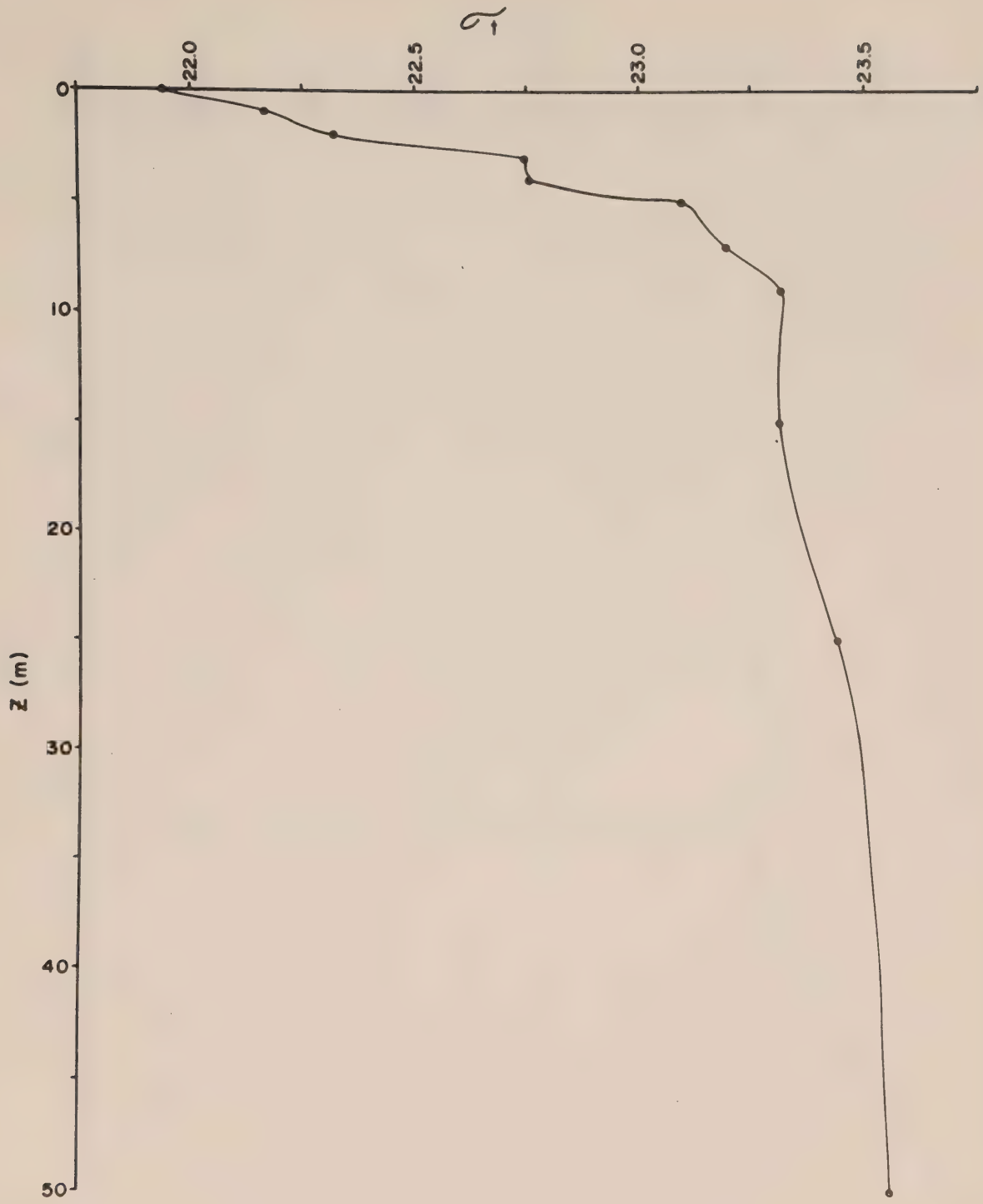


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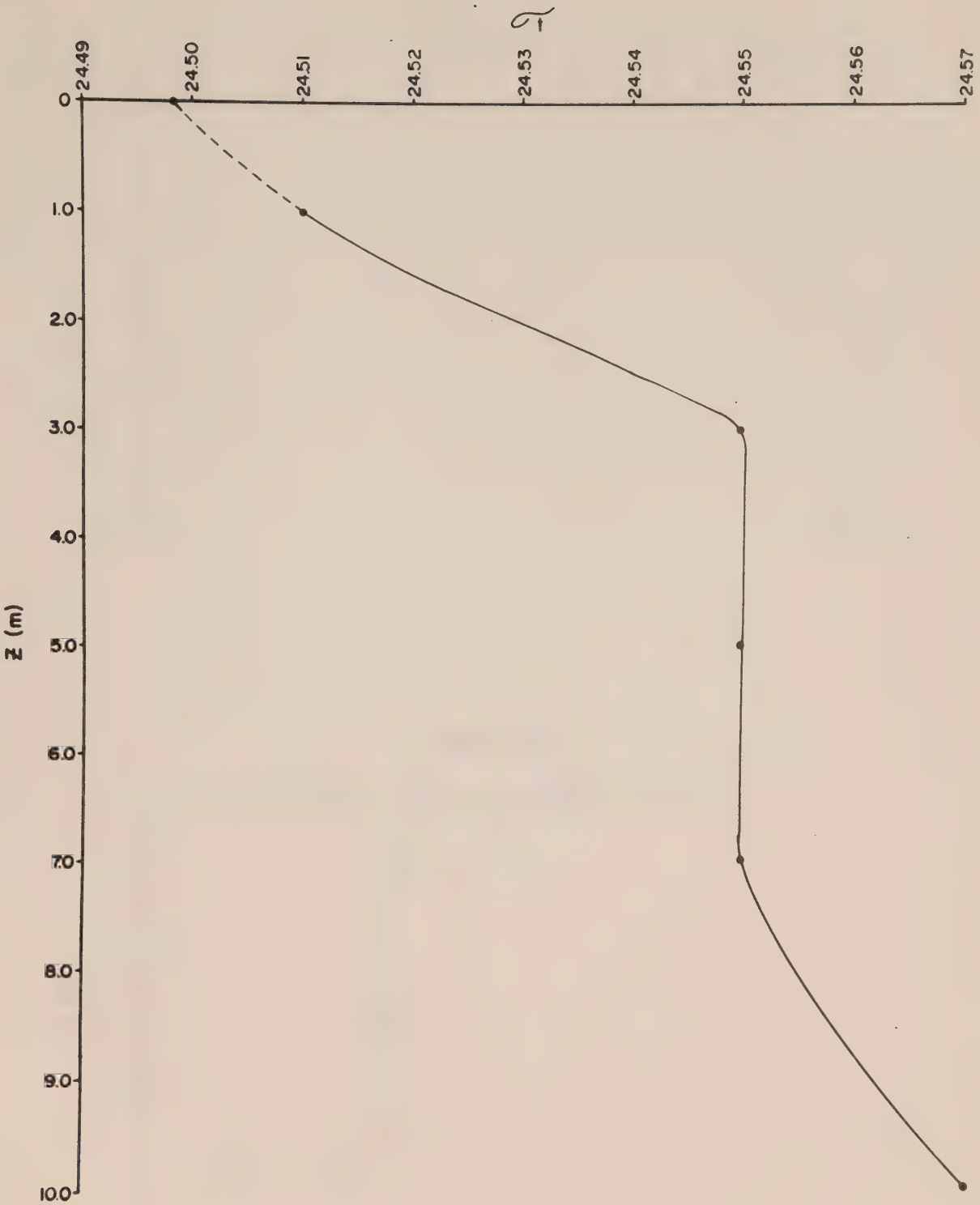


Figure 12. The density profile in Juan de Fuca Strait on 2 May 1975 eight hours twenty minutes after the dye release.

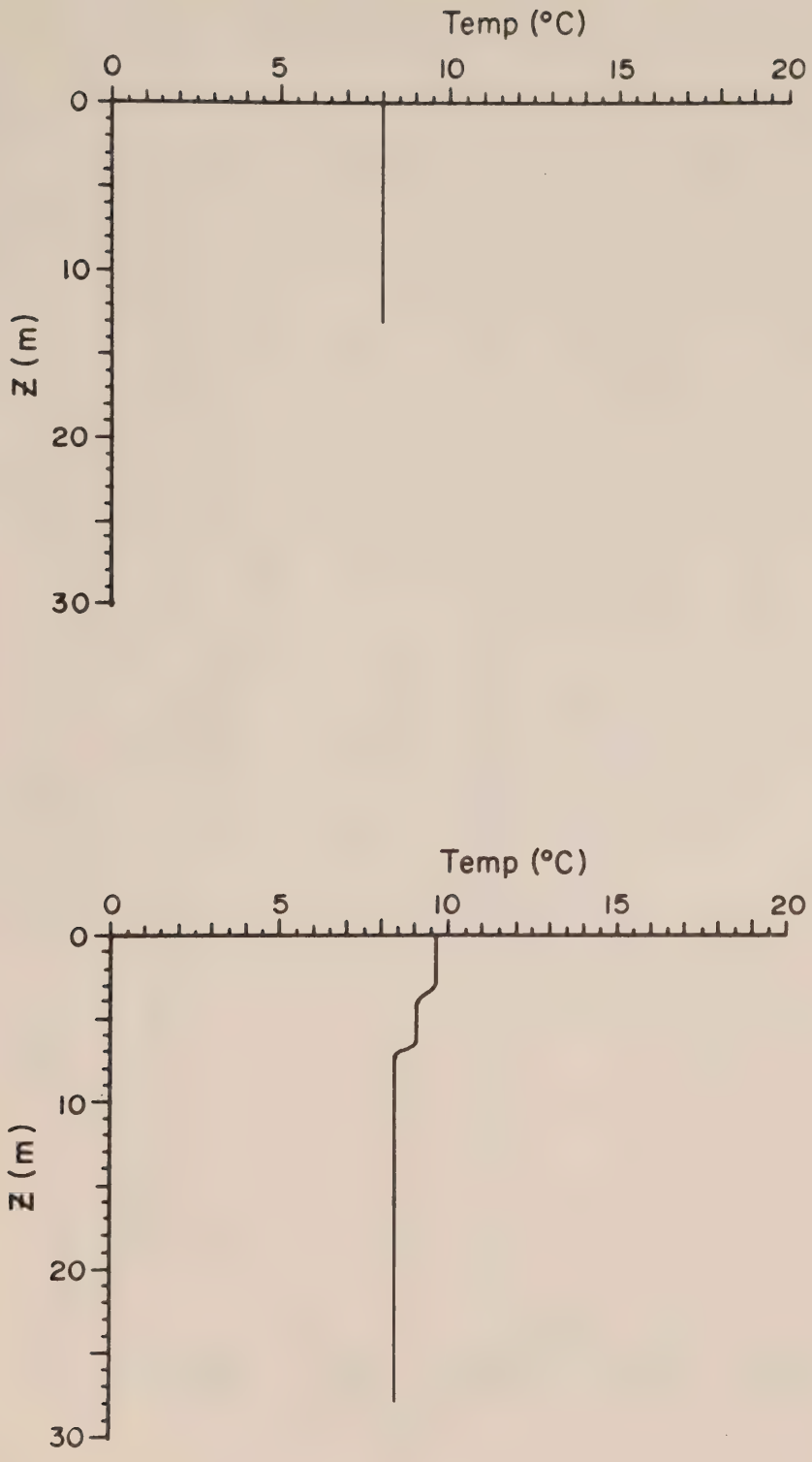


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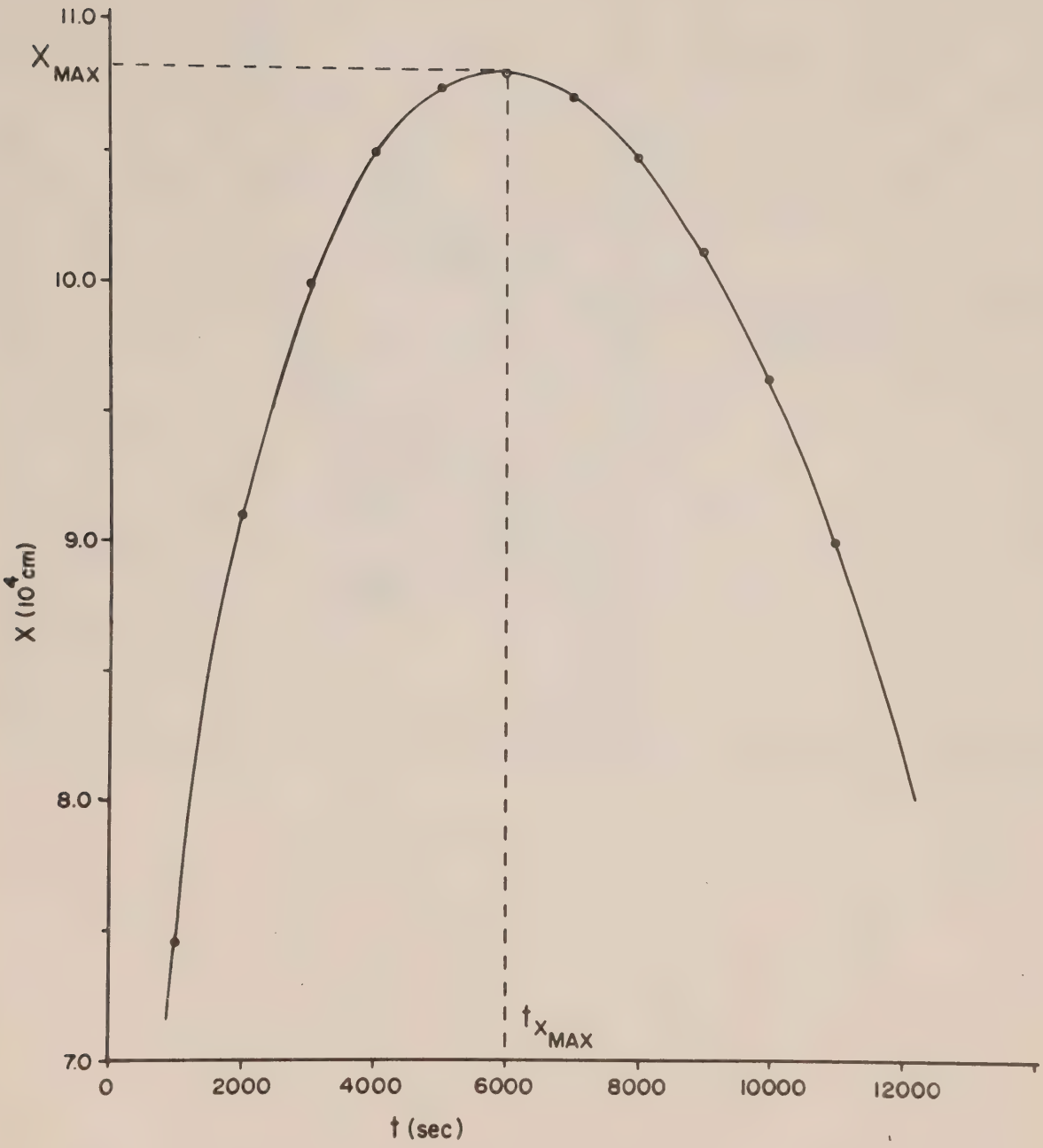


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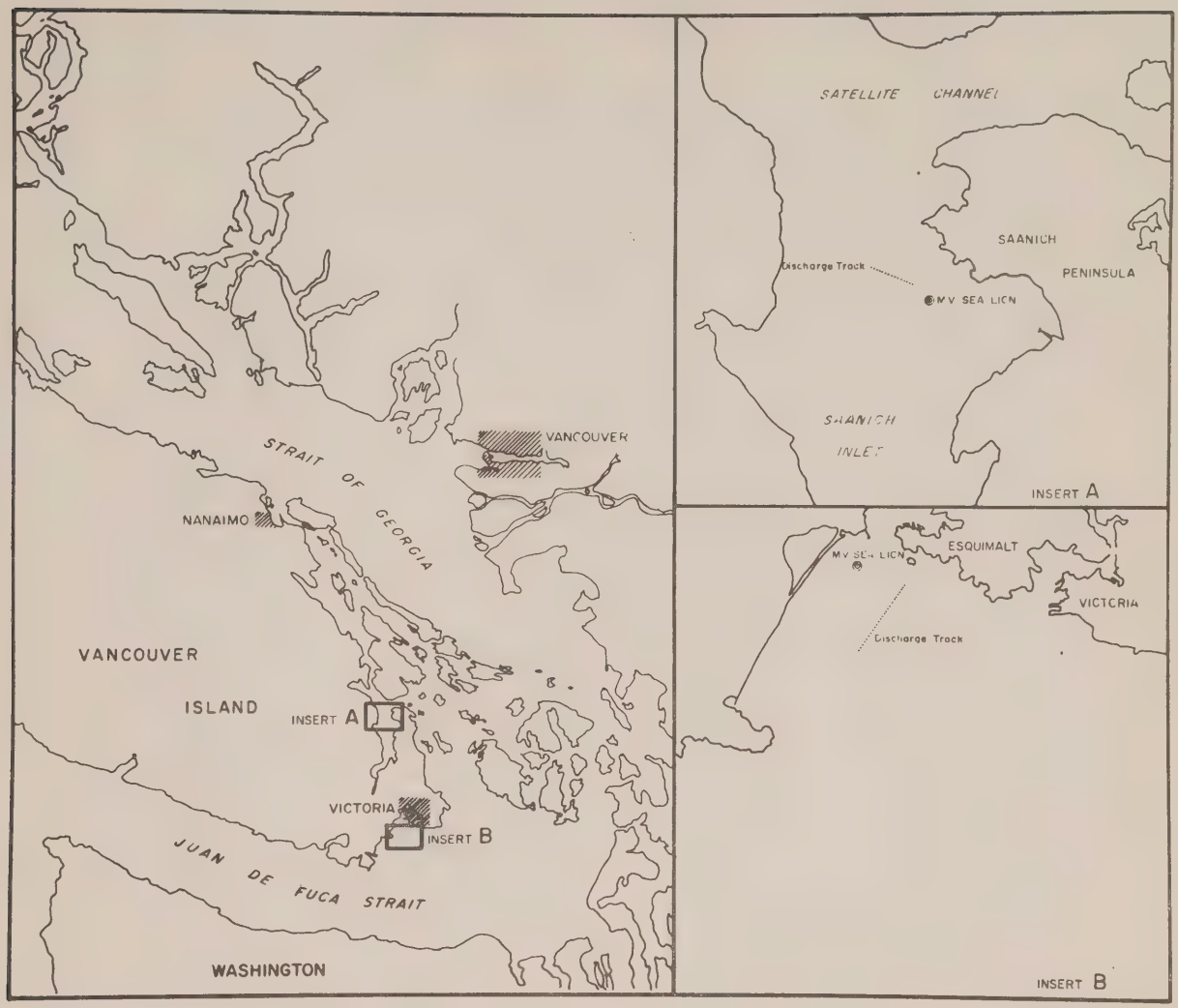


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